

APPENDIX 1
ARCHAEOLOGICAL ASSESSMENT

**Stage 1 Archaeological Assessment
Kincardine Business Park Servicing Master Plan
Lots 1, 2, 3, and 4, Concession 1 SDR
Geographic Township of Kincardine
Now the Municipality of Kincardine
County of Bruce**

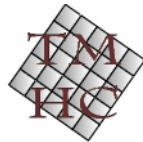
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Executive Summary

The Municipality of Kincardine is undertaking a Servicing Master Plan for the Kincardine Business Park, a 77.3 ha property located immediately east of the Town of Kincardine. The Servicing Master Plan study area encompasses a rectangular-shaped parcel of land situated in the southeast corner of the intersection of Highway 21 and Highway 9 (Durham Road; Broadway Street), comprising Lots 1, 2, 3 and 4 of Concession 1 South of the Durham Road in the Geographic Township of Kincardine, Bruce County, Ontario. The study area includes agricultural lands, residential and farm lots and natural areas, in addition to a developed commercial block along Highway 21. Timmins Martelle Heritage Consultants Inc. was contracted to carry out a Stage 1 archaeological assessment for the Servicing Plan Study Area by B.M Ross & Associates who are coordinating the study on behalf of the Municipality of Kincardine. The intent of the Master Plan is to identify infrastructure requirements (roads, water, sanitary sewage and stormwater) for the continued development of the business park. The Stage 1 assessment was undertaken as part of the larger planning study but also as a precursor to more specific Environmental Assessment requirements. All work was done in accordance with the *Standards and Guidelines for Consultant Archaeologists* (MTC 2011).

The Stage 1 background study included a review of soils, physiography and drainage for the area, former and current land use, as well as registered archaeological sites and past archaeological activity within the immediate vicinity. According to the map-based review, the study area contains or is in proximity to features signalling archaeological potential, namely: 1) watercourses (active and seasonal); 2) 19th century thoroughfares and colonization roads (Hwy. 21 - Goderich Road and Hwy. 9 - Durham Road); 3) the 19th century settled town core of Kincardine; and 4) registered and known archaeological sites. Therefore, based on a mapping review, some portions of the study area have potential for either First Peoples or EuroCanadian sites (63.9% have been unassessed; 21.47% previously assessed; of the unassessed lands - 13.84% treed, 50.06% agricultural land). Nonetheless, some lands within the study area have also witnessed significant prior disturbance (11.38%) and do not retain archaeological potential. Most notable in this regard are the commercial complexes and rights-of-way. More isolated disturbances are present within the residential/farm lots (where buildings and laneways are present). However, due to restrictions on property access, a formal property inspection could not be undertaken to visually confirm extent of disturbance. Other areas within the property are also of low potential, namely the watercourse (2.85%) and its sloped valley lands (0.39%).

Two parcels within the study area have been previously assessed: 1) a Millennium Way northern extension (TMHC 2006; constructed); and 2) a portion of a proposed residential development off Highway 9 (AMICK 2005; further work necessary). One 19th century archaeological site found during the latter study (BbHj-37) requires Stage 3 assessment. Based on the information compiled in the background study, the following recommendations are made:

- 1) The previously assessed lands in the 2006 TMHC survey of the Millennium Way road extension are of no further archaeological concern and no additional assessment is recommended.
- 2) Registered site BbHj-37, recorded by AMICK during a 2005 partial survey of a proposed development property within the study area, requires Stage 3 testing to current MTCS standards. Based on the information provided in the consultant report for this project, the



site would be classified as a post-contact site of cultural heritage value or interest. The proposed excavation strategy should follow that defined for small post-contact sites of established cultural heritage value or interest (MTCS 2011; Table 3.1. Standards 3 and 4), with initial test units placed at 10 metre intervals across the surface scatter and an additional 40% of units placed in areas of interest. As the Stage 2 reporting indicated a maximum site size of roughly 60 by 60 metres, methodological provisions for Stage 3 testing of large sites (MTCS 2011; Section 3.31, Subsection 3.3.1 Standard 1) might also be applicable. Until Stage 3 testing is undertaken, all lands within 70 metres of the Stage 2 site limits have further archaeological concern and are protected from land alterations (other than typical agricultural cultivation) by the provisions of the *Ontario Heritage Act* which prohibit any ground disturbance within a registered archaeological site.

- 3) The remaining lands surveyed by AMICK in 2005 require no further archaeological assessment.
- 4) All former and active agricultural lands within the study area that were not previously surveyed demonstrate potential for the discovery of archaeological resources. Based on provincial standards these require ploughing and a pedestrian or “walk-over” survey at a five metre interval. Ploughed surfaces must be well-weathered by heavy rainfall and the ploughed surface must be clean of vegetation resulting in at least 80% surface visibility.
- 5) The low-lying, wet and steeply sloped lands associated with the tributary of the Penetangore River are considered to have low archaeological potential and do not require further assessment. However, given that a formal field inspection could not be undertaken, the precise limits of these could not be mapped and therefore a detailed field inspection will minimally be required prior to any future servicing work taking place in these areas.
- 6) The previously disturbed lands within the commercial zones and residential/farm lots do not retain potential to house intact archaeological resources and therefore no further work is recommended in these areas. However, given that a formal field inspection could not be undertaken, the precise limits of these could not be mapped and therefore a detailed field inspection will minimally be required prior to any future servicing work taking place in these areas.
- 7) The treed lands associated with the Penetangore River tributary and the grassed areas within the residential/farm lots and commercial zone have potential for the discovery of archaeological resources. Based on provincial standards, these lands must be subject to a test pit survey at a five metre interval. Where test pitting is conducted each test pit should measure approximately 30 cm (shovel-width) in diameter and be excavated into the first five centimetres of subsoil. The soil from each test pit should be passed through 6 mm hardware cloth in an effort to retain any artifacts that might be present. When the screening process is completed, the soil strata should be examined and the pits filled in as best as possible and re-capped with sod.

These recommendations are subject to report review and acceptance by the Ministry of Tourism, Culture and Sport.



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Ministry of Tourism, Culture and Sport, Toronto



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1.0 PROJECT CONTEXT

1.1 Development Context

1.1.1 Introduction

The Municipality of Kincardine is undertaking a Servicing Master Plan for the Kincardine Business Park, a 77.3 ha property located immediately east of the Town of Kincardine. The Servicing Master Plan study area encompasses a rectangular-shaped parcel of land situated in the southeast corner of the intersection of Highway 21 and Highway 9 (Durham Road; Broadway Street), comprising Lots 1, 2, 3 and 4 of Concession 1 South of the Durham Road, in the Geographic Township of Kincardine, Bruce County, Ontario. The study area includes agricultural lands, residential and farm lots and natural areas, in addition to a developed commercial block along Highway 21. Timmins Martelle Heritage Consultants Inc. was contracted to carry out a Stage 1 archaeological assessment for the Servicing Plan Study Area by B.M Ross & Associates who are coordinating the study on behalf of the Municipality of Kincardine. The intent of the Master Plan is to identify infrastructure requirements (roads, water, sanitary sewage and stormwater) for the continued development of the business park. The Stage 1 assessment was undertaken as part of the larger planning study but also as a precursor to more specific Environmental Assessment requirements. All work was done in accordance with the *Standards and Guidelines for Consultant Archaeologists* (MTC 2011).

All archaeological assessment activities were performed under the professional archaeological license of Tara Jenkins, M.A. (P357) and in accordance with the 2011 *Standards and Guidelines for Consultant Archaeologists* (MTC 2011). Permission to commence the study was given by Lisa J. Courtney, of B.M. Ross & Associates Ltd., agent for the Municipality of Kincardine. No property access was given and no formal property inspection was undertaken as this study is being carried out for planning purposes only.

1.1.2 Purpose and Legislative Context

The *Ontario Heritage Act* makes provisions for the protection and conservation of heritage resources in the Province of Ontario. Heritage concerns are recognized as a

matter of provincial interest in Section 2.6.2 of the *Provincial Policy Statement* which stipulates that municipalities shall have regard for the conservation of features of significant architectural, cultural, historical, archaeological or scientific interest. The purpose of a Stage 1 background study is to determine if there is potential for cultural resources to be found on a property for which a change in land use is pending. It is used to determine the need for a Stage 2 field assessment involving the search for archaeological sites. In accordance with *Provincial Policy Statement* 2.6, if significant sites are found, a strategy (usually avoidance, preservation or excavation) must be put forth for their mitigation.

The Servicing Master Plan is being undertaken as a planning precursor to future environmental assessment work for specific servicing elements within the Kincardine Business Park. As such, it is intended to act as an environmental screening tool and help satisfy future requirements under the *Environmental Assessment Act*. The latter provides for the protection and conservation of the “environment,” widely defined to cover “cultural heritage” resources. Section 5(3)(c) of the *Act* stipulates that heritage resources to be affected by a proposed undertaking be identified during the environmental screening process. Within the context of an environmental assessment, the purpose of a Stage 1 background study is to determine if identify any negative impacts to known or potential archaeological resources.

2.0 STAGE 1 BACKGROUND REVIEW

2.1 Research Methods and Sources

A Stage 1 background study and property inspection was conducted to gather information about known and potential archaeological resources within the study area. According to the Province of Ontario’s 2011 *Standards and Guidelines for Consultant Archaeologists*, a Stage 1 background study must include a review of:

- an up-to-date listing of sites from the Ontario Archaeological Sites Database (OASD) of archaeological sites with 1 km of the property;
- reports of previous archaeological fieldwork within a radius of 50 metres;
- topographic maps at 1:10,000 (recent and historical) or the most detailed scale available;
- historic settlement maps (e.g., historical atlas, surveys)
- archaeological management plans or other archaeological potential mapping (when available); and
- commemorative plaques or monuments on or near the property.



For this project, the following activities were carried out to satisfy or exceed the above requirements:

- a database search was filed with Robert von Bitter of the Ministry of Tourism, Culture and Sport requesting a listing of registered archaeological sites within 1 km of the study area (received Sept. 6, 2013);
- a review of known prior archaeological reports for the property and adjacent lands was undertaken (note: the Ministry of Tourism, Culture and Sport currently does not keep a publicly accessible record of archaeological assessments carried out in the Province of Ontario, so a complete inventory of prior assessment work nearby is not available);
- Ontario Base Mapping (1:10,000) was considered through ArcGIS and mapping layers provided by geographynetwork.ca; detailed mapping provided by the client was also examined, and;
- a review of public consultation documents was undertaken.

Additional sources of information were also consulted, including modern aerial photographs, local history accounts, soils and physiography data provided by the Ontario Ministry of Agriculture, Food and Rural Affairs (OMAFRA), and both 1:50,000 (Natural Resources Canada) and finer scale topographic mapping.

As access to privately-owned lands within the study area could not be provided, a formal property inspection could not be undertaken. The report recommendations reflect this fact.

When compiled, background information was used to create a summary of the characteristics of the study area, in an effort to evaluate its archaeological potential. The Province of Ontario (MTC 2011 – Section 1.3.1) has defined the criteria that identify archaeological potential as:

- previously identified archaeological sites
- water sources
 - primary water sources (lakes, rivers, streams, creeks)
 - secondary water courses (intermittent streams and creeks, springs, marshes, swamps)
 - features indicating past water sources (e.g., glacial lake shorelines indicated by the presence of raised sand or gravel beach ridges, relic river or stream channels indicated by clear dip or swale in topography, shorelines of drained lakes or marshes, cobble beaches)
 - accessible or inaccessible shoreline (e.g., high bluffs, swamp or marsh fields by the edge of a lake, sandbars stretching into marsh)
- elevated topography (e.g., eskers, drumlins, large knolls, plateaux)
- pockets of well-drained sandy soil, especially near areas of heavy soil or rocky ground



- distinctive land formations that might have been special or spiritual places, such as waterfalls, rock outcrops, caverns, mounds, and promontories and their bases; there may be physical indicators of their use, such as burials, structures, offerings, rock paintings or carvings
- resource areas, including:
 - food or medicinal plants (e.g., migratory routes, spawning areas, prairie)
 - scarce raw materials (e.g., quartz, copper, ochre or outcrops of chert)
 - early Euro-Canadian industry (e.g., fur trade, logging, prospecting, mining)
- areas of early Euro-Canadian settlement. These include places of early military or pioneer settlement (e.g., pioneer homesteads, isolated cabins, farmstead complexes), early wharf or dock complexes, pioneer churches and early cemeteries. There may be commemorative markers of their history, such as local, provincial, or federal monuments or heritage parks.
- early historical transportation routes (e.g., trails, passes, roads, railways, portage routes)
- property listed on a municipal register or designated under the *Ontario Heritage Act* or that is a federal, provincial, or municipal historic landmark or site; and
- property that local histories or informants have identified with possible archaeological sites, historical events, activities or occupations.

In Southern Ontario (south of the Canadian Shield), any lands within 300 metres of any of the features listed above are considered to have potential for the discovery of archaeological resources.

Typically, a Stage 1 assessment will determine potential for precontact First Peoples' and historic era sites independently. This is due to the fact that lifeways varied considerably during these eras so that criteria used to evaluate potential for each type of site also varies.

It should be noted that some factors can also negate the potential for discovery of intact archaeological deposits. Subsection 1.3.2 of the 2011 *Standards and Guidelines for Consultant Archaeologists* indicates that archaeological potential can be removed in instances where land has been subject to extensive and deep land alterations that have severely damaged the integrity of any archaeological resources. Major disturbances indicating removal of archaeological potential include, but are not limited to:

- quarrying
- major landscaping involving grading below topsoil
- building footprints; and
- sewage and infrastructure development.

Some activities (agricultural cultivation, surface landscaping, installation of gravel trails, etc.) may result in minor alterations to the surface topsoil but do not



necessarily affect or remove archaeological potential. It is not uncommon for archaeological sites, including structural foundations, subsurface features and burials, to be found intact beneath major surface features like roadways and parking lots. Archaeological potential is, therefore, not removed in cases where there is a chance of deeply buried deposits, as in a developed or urban context or floodplain where modern features or alluvial soils can effectively cap and preserve archaeological resources.

2.2 Project Context: Archaeological Context

2.2.1 Study Area: Overview and Physical Setting

The Kincardine Business Park Servicing Master Plan study area occupies the southeast corner of the intersection of Highway 9 (Durham Road) and Highway 21 near the east edge of the Town of Kincardine (Maps 1 to 3). The study area is a roughly 77.3 hectare rectangular parcel that comprises Lots 1, 2, 3, and 4, Concession 1 South of the Durham Road, in the Geographic Township of Kincardine, Bruce County, Ontario, now in the Municipality of Kincardine. The majority of the study area is undeveloped vacant and agricultural lands. However, it also includes developed commercial parcels along Highway 21 and three residential/farm lots along Highway 9. Finally, the southernmost portion of the study area also contains the treed valley lands of a tributary of the Penetangore River.

The study area falls within the Huron Slope physiographic region (Chapman and Putnam 1966:263) (Map 4). The Huron Slope covers an area of 1000 square miles of gently sloping land from Algonquin shore cliff to the Wyoming moraine along the eastern shore of Lake Huron. The upper till sheet is formed from brown calcareous clay and lies 1m-3m deep over stratified clay of the same colour (Chapman and Putnam 1966:264). The clay found within the upper till sheet is reworked lacustrine material from the underlying clay beds. These features stand in contrast to the sandy beach, plains and dune topography of the Huron Fringe that rests to the west, between Hwy 21 and Lake Huron. The underlying bedrock of the Norfolk formation and consists of fine grained limestone, magnesium limestone and dolomite bedrock (Hoffman and Richards 1954:14). The overall topography of the Huron Slope is smooth and gently rolling. The study area rests within bevelled till plains (Map 4). A shoreline of glacial Lake Algonquin is present within the sand plain east of Highway 21, at a distance of roughly 1.5 km from the study area.

The predominant soil type within the study area is Perth Clay Loam (Map 5), an imperfectly draining soil developed on calcareous fine textured till and associated with soft maple and elm tree cover (Hoffman and Richards 1954:49). Perth clay loam covers a significant portion of Bruce County. Within the study area, Brookston Clay Loam is present within the pathways of active and intermittent tributaries of the Penetangore River. The latter soil is poorly draining, associated with elm, ash and cedar tree cover



and derived from clay till intermixed with lacustrine materials (Hoffman and Richards 1954:49).

The Penetangore River drains the Kincardine area and lands to the east. The study area rests between two main branches of the river (which merge at a point roughly 1.3 km to the west), the more northerly being the North Penetangore River. Kincardine Creek feeds into the North Penetangore River roughly 500 metres north of the study area. A lesser but active tributary of the river crosses through the southern portion of the study area, with other feeding branches present within 300 metres of it (Map 6). Swales and ditches associated with seasonal and intermittent tributaries of the river cross the central portion of the study area, which also includes at least one drainage ditch.

2.2.2 Summary of Registered or Known Archaeological Sites

An inquiry to the Ontario Archaeological Sites Database (OASD) (received September 5, 2013) indicated that there is one archaeological site within one kilometre of the study area and, in fact, falls within it. This is the Clements Site (BbHj-37), an historic-era homestead reported by AMICK consultants in 2005 (see discussion in Section 2.2.3 below).

2.2.3 Summary of Past Archaeological Investigations Within 50 Metres

During our background review it was established that at least two previous archaeological projects had taken place within 50 metres of the study area. Both of these studies were undertaken on lands within the Servicing Master Plan Study Area. As the Province does not currently maintain an accessible database of archaeological assessment areas *per se*, it is not known whether this is a complete inventory of archaeological assessment activities undertaken within 50 metres of the study area.

AMICK Consultants – Proposed Residential Subdivision – Stewart Property (41T-2005-02.22) (PIF: P038-143; Licensee Marilyn Cornies, P038)(AMICK 2005)

In 2005, a partial Stage 1 and 2 archaeological assessment was conducted by AMICK Consultants Limited for a proposed residential property comprising part of Lots 2 and 3, Concession 1 SDR. The proposed development area occupies the majority of the easterly two thirds of the current study area but excludes the residential/farm lots along Highway 9. Only a portion of the 2005 subject property could be surveyed at that time due to crop conditions, that being a field in the central-east portion of the current study area, encompassing lands extending south of Durham Road to the valley lands of the Penetangore River tributary. The Stage 1 background study indicated the property had potential for the discovery of archaeological resources. A Stage 2 pedestrian survey of a portion of the property resulted in the discovery of one historic-era site (1840-1860) and one isolated find spot (a waste flake). Two reports were prepared for this project: a) an interim report written in 2005; and b) a revised report submitted in 2010. The initial



report is entitled *Interim Report on the 2005 Stage 1-2 Archaeological Assessment of the Proposed Stewart Property (41T-2005-02.22), Part of Lots 2 & 3, Concession 17[sic], Town of Kincardine, County of Bruce* (PIF P038-143). The revised report is entitled: *Revised Report on the 2005 Stage 1-2 Archaeological Assessment of the Proposed Stewart Property (41T-2005-02.22) Part of Lots 2 & 3, Concession 1 SDR, Town of Kincardine, County of Bruce* (PIF P038-143). A copy of the first report was obtained by B.M. Ross from the landowner/municipality, whereas the Ministry of Tourism, Culture and Sport provided a copy of the revised report of 2010.

In interpreting the results of this study and the assessment map provided in the 2010 report, the following archaeological activities are required to clear the entire 2005 project area of archaeological concern:

- a) Stage 3 assessment of the ca. 1840-1860 historic site found on the property, namely the Clements Site (BbHj-37); Stage 4 mitigation may also be required pending the results of the Stage 3 assessment;
- b) The assessment (through test pitting or visual inspection and photo-documentation) of the valley lands associated with the tributary of the Penetangore River; if additional archaeological sites are identified during this assessment follow up assessment work may be required; and
- c) The assessment (through pedestrian survey) of those agricultural lands not available for study in 2005 and comprising the western portion of the 2005 subject property and central portion of the current study area; if additional archaeological sites are identified during this assessment follow up assessment work may be required.

The isolated waste flake also recorded during the 2005 Stage 2 survey was not recommended for further assessment. The Clements Site is described as a scatter of 61 points representing 108 artifacts covering roughly 60 by 60 metres.

Due to copyright restrictions, the survey map from the 2005 assessment is not included in this report. However, Map 8 does show the area subject to previous survey and SD-1 in the Supplementary Documentation portion of this report also shows the location of the archaeological find spots.

Timmins Martelle Heritage Consultants Inc. – Millennium Way Extension (PIF: P064-114-2006; Licensee Holly Martelle, P064) (TMHC 2006)

The following year, Timmins Martelle Heritage Consultants Inc. (TMHC) undertook a Stage 1 and 2 archaeological assessment for a 250 long by 30 metre wide extension of Millennium Way, a road that services the Kincardine Business Park. The Stage 1 assessment established that the project area had potential for the discovery of archaeological resources and the Stage 2 test pit survey (5 m interval) did not result in the



discovery of artifacts. The 2006 survey segment falls within Lot 1, Concession 1 SDR, in the northwest portion of the current study area. The results of this assessment were present in a report entitled *Stage 1 & 2 Archaeological Assessment, Class EA, Millennium Way Extension, Municipality of Kincardine, Bruce County, Ontario* (PIF P064-114-2006; Holly Martelle licensee, P064). Map 9 shows the location of the 2006 survey area.

2.3 Project Context: Historical Context

2.3.1 Pre- and Early Post-Contact First Peoples Settlement in Southern Ontario

Through the integration of region-specific archaeological information and data from province-wide models, a baseline cultural chronology for pre-contact First Peoples settlement can be proposed as generalized below and in Table 1.

There is archaeological evidence in Southern Ontario of past native settlement from at least as early as 12,000 years to pre-Confederation times. The wildlife, physical and natural resources of the area are still of great concern to local native groups who continue to hunt, trap and fish.

Paleoindian

The first human populations to inhabit the area came to the region between 12,000 and 10,000 years ago, coincident with the end of the last period of glaciation. Climate and environmental conditions were significantly different then they are today; local environs would not have been welcoming to anything but short-term settlement. Termed Paleoindians by archaeologists, Ontario's first peoples would have crossed the landscape in small groups (i.e., bands or family units) searching for food, particularly migratory game species. In this area, caribou may have provided the staple of Paleoindian diet, supplemented by wild plants, small game and fish.

Given the low density of populations on the landscape at this time and their mobile nature, Paleoindian sites are small and ephemeral. They are usually identified by the presence of fluted projectile points often manufactured on a highly distinctive whitish-grey chert named "Fossil Hill" (after the formation) or "Collingwood," from the Niagara Escarpment west of Collingwood. In Ontario, Paleoindian sites are often found in association with former glacial shorelines, beaches and embayments. Although there are no documented Paleoindian sites in the immediate vicinity of the study area, Paleoindian occupations and find spots have been recorded elsewhere in Bruce and Huron counties, some as a result of ongoing cultural resource management projects being carried out under the *Green Energy Act*. These finds have typically been associated with former glacial shorelines.



Table 1: Generalized Cultural Chronology of First Peoples Settlement in Bruce County

Period			Time Range (circa)	Diagnostic Features	Complexes
Paleoindian	Early		9000 - 8400 B.C.	fluted projectile points	Gainey, Barnes, Crowfield
	Late		8400 - 8000 B.C.	non-fluted and lanceolate points	Holcombe, Hi-Lo, Lanceolate
Archaic	Early		8000 - 6000 B.C.	serrated, notched, bifurcate base points	Nettling, Bifurcate Base Horizon
	Middle		6000 - 2500 B.C.	stemmed, side & corner notched points	Brewerton, Otter Creek, Stanly/Neville
	Late		2000 - 1800 B.C.	narrow points	Lamoka
			1800 - 1500 B.C.	broad points	Genesee, Adder Orchard, Perkiomen
			1500 - 1100 B.C.	small points	Crawford Knoll
	Terminal		1100 - 950 B.C.	first true cemeteries	Hind
Woodland	Early		950 - 400 B.C.	expanding stemmed points, Vinette pottery	Meadowood
	Middle		400 B.C. - A.D. 500	dentate, pseudo-scallop pottery	Saugeen
	Transitional		A.D. 500 - 900	first corn, cord-wrapped stick pottery	Princess Point
	Late	Early Iroquoian	A.D. 900 - 1300	first villages, corn horticulture, longhouses	Glen Meyer
		Middle Iroquoian	A.D. 1300 - 1400	large villages and houses	Uren, Middleport
		Late Iroquoian	A.D. 1400 - 1650	tribal emergence, territoriality	Odawa
Contact		Aboriginal	A.D. 1700 - 1875	treaties, mixture of Native & European items	Ojibway, Odawa populations
		Euro-Canadian	A.D. 1796 - present	English goods, homesteads	European settlement, pioneer life

Archaic

Settlement and subsistence patterns change significantly during the Archaic period as both the landscape and ecosystem adjusted to the retreat of the glaciers. Building on earlier patterns, early Archaic populations continued the mobile lifestyle of their predecessors. Through time and with the development of more resource rich local environments, these groups gradually reduced the size of the territories they exploited on a regular basis. A seasonal pattern of warm season riverine or lakeshore settlements and interior cold weather occupations has been documented in the archaeological record. Since the large cold weather mammal species that formed the basis of the Paleoindian subsistence pattern became extinct or moved northward with the onset of warmer climate conditions Archaic populations had a more varied diet, exploiting a range of plant, bird, mammal and fish species. Reliance on specific food resources like fish, deer and nuts becomes more pronounced through time and the presence of more hospitable environments and resource abundance led to the expansion of band and family sizes. In the archaeological record, this is evident in the presence of larger sites and aggregation camps, where several families or bands would come together in times of plenty. The change to more preferable environmental circumstances led to a rise in population density. As a result, Archaic sites are more abundant than those from the earlier period.



Artifacts typical of these occupations include a variety of stemmed and notched projectile points, chipped stone scrapers, ground stone tools (e.g., celts, adzes) and ornaments (e.g., bannerstones, gorgets), bifaces or tool blanks, animal bone (where and when preserved) and waste flakes, a byproduct of the tool making process.

Early, Middle and Transitional Woodland Periods

Significant changes in cultural and environmental patterns are witnessed in the Early, Middle and Transitional Woodland periods (ca. 950 B.C. to 1000 A.D.). Occupations became increasingly more permanent in this period, culminating in major semi-permanent villages by roughly 1,000 years ago. Archaeologically, the most significant changes by Woodland peoples are the appearance of artifacts manufactured from modeled clay and the emergence of more sedentary villages. The earliest pottery was crudely made by the coiling method and early house structures were simple oval enclosures. The Early and Middle Woodland periods are also characterized by extensive trade in raw materials, objects and finished tools, with sites in Ontario containing trade items with origins in the Mississippi and Ohio River valleys. A rise in mortuary ceremonialism is also evident, culminating in the construction of large burial mounds.

Late Woodland Period

Beginning circa 1000 A.D. the archaeological record in Southern Ontario documents the emergence of more substantial, semi-permanent settlements and the adoption of corn horticulture. These developments are most often associated with Iroquoian-speaking populations, the ancestors of the Wendat (Huron), Petun (Tobacco Nation) and Attawandaron (Neutral) nations who were known to have resided in the province upon the arrival of the first European explorers and missionaries. Iroquoian villages incorporated a number of longhouses, multi-family dwellings that contained several families related through the female line. Pre-contact Iroquoian sites may be identified by a predominance of well-made pottery decorated with various simple and geometric motifs, triangular projectile points, clay pipes and ground stone artifacts. Sites post-dating European contact are recognized through the appearance of various items of European manufacture. The latter include materials acquired by trade (e.g. glass beads, copper/brass kettles, iron axes, knives and other metal implements) in addition to the personal items of European visitors and Jesuit missionaries (e.g. finger rings, stoneware, rosaries, and glassware).

Algonquian Populations

At the time of European contact in the early 17th century the Bruce peninsula was occupied by Algonkian speaking groups (Odawa, Potawatomi, Ojibwa) who maintained a close relationship with the Iroquoian speaking Petun peoples living along the southern end of Georgian Bay (Fox 1990:461). Like other First Peoples in the area, these groups were dispersed in the mid-17th century as a result of the conflict between the Five Nations



Iroquois and the Huron-Petun. Many moved along the Lake Huron shoreline into Huron County, with others settling in the peninsula proper.

2.3.2 *Historic Era of First Peoples Settlement*

At the time of European contact in the early 17th century, the Bruce Peninsula was occupied by Algonquin speaking Odawa groups who maintained a close relationship with the Iroquoian speaking Petun peoples living along the southern shore of Nottawasaga Bay (Fox 1990:461). The Ojibwa (a.k.a. the “Chippewa”, who called themselves “Anishnabe”), who are also Algonquian speakers, lived in the region extending from the Georgian Bay area to the north shore of Lake Superior prior to European contact (Schmalz 1977). Both the Odawa and Ojibwa were disrupted and displaced by Iroquois hostilities in the 1650s (Schmalz 1977), but regrouped by the last quarter of the 17th century (Ferris 1989) and returned to their homeland. The 1690s witnessed significant battles between the Iroquois and Anishnabe Three Fires Confederacy (Ottawa, Ojibway, Pottawatomi), with the result being that Ojibway groups took control over Bruce County lands (Wilson McArthur 2005:49) and held them until the negotiation of Crown transfers a century later. S

The (Saugeen) Ojibwa surrendered portions of Grey and Wellington Counties in 1818 (McMullen 1997:28). This was done with the understanding that they would have continued use of Bruce County and that they would receive annuities for the lands surrendered. Further land was surrendered in the area with the establishment of the Huron Tract in 1825, later to be followed by the surrender of Bruce County in 1836 (Lee 2004:21). The surrender of Bruce County did not include the Bruce Peninsula, known as the Saugeen Peninsula by the resident Ojibwa. The Neyaashiinigiing Indian Reserve Number 27 on the southeast side of the Bruce Peninsula (Nawash Ojibwa) and the Saugeen Indian Reserve Number 29 above Southampton (Saugeen Ojibwa) were established in 1854 (Chippewas of Nawash 2010).

Furthermore, Schmalz (1977:1) indicates that a group of Ojibwa (including Mississauga, Potawatomi, Ottawa and Caughnawaga) settled in the Saugeen Township. The Chippewas of Saugeen First Nation and the Chippewas of Nawash First Nation share the same traditional territories in southwestern Ontario. They were a part of the ancient Three Fires Confederacy of Ojibwa, Odawa, and Pottawatomi. Throughout the eighteenth century the Saugeen Territory was inhabited by several generations of Ojibwa whose immediate territory was threatened neither by war nor by European settlers.

What was to become Kincardine Township formed part of a parcel of land that was subject to a surrender by the Ojibwa to the Crown in 1836 called the Treaty of Manitowaning (Lee 2004:21). The land surrendered accounted for 607,000ha (Schmalz 1977:233). The Treaty formalized the surrender of the County of Bruce which included the townships of Saugeen, Arran, Bruce, Elderslie, Kincardine, Greenock, Brant, Huron, Kinloss, Culross, and Carrick (Robertson 1906). The Treaty was concluded by Sir



Francis Bond Head at Manitowaning on August 9, 1836. Shortly thereafter, the townships were surveyed for municipal settlement.

Historic native occupation of the region is poorly documented archaeologically. Many historic native sites were short-term occupied resource exploitation camps that left behind few archaeological remains, making them difficult to find. Later native sites of the 18th and 19th centuries may be difficult to recognize because their material culture assemblages are very similar to the more prevalent and better documented Euro-Canadian sites of the same time. Further, typical Euro-Canadian histories generally included little information on First Peoples groups, their land use or site locations during the 19th century municipal settlement period. Thus, information regarding the locales of historic-era native settlements is limited and difficult to collect through traditional historical sources. Additionally, the information bias is particularly strong for the northern reaches of southern Ontario, within the traditional territory of the Saugeen-Nawash Ojibwa Nation and the Saugeen Métis Nation. In an effort to overcome some of this bias, more detailed historical background research was carried out in an effort to consult information sources that might better highlight historic-era native land use. In the past, land surveyor's field notes have proved useful in highlighting the location of 19th century land use sites. The following is a brief summary of the early surveys conducted in Kincardine townships and the details provided in the surveyors' notes.

The Township of Kincardine was surveyed by James W. Bridgland in 1850 whose notes make no reference to aboriginal presence in the area. Bridgland did, however, provide a thorough account of his survey which is accompanied by detailed mapping of conditions and state of improvements (e.g., cleared lands, structures) within the township at that time. Improvements are scattered along the Lake Range of the township from north to south with concentrations in the town site of Penetangor (now Kincardine) and in the western portion of the township along Concession Roads 1 and 2, south of the Durham Road and Concession Road 2 and 3, north of the road (Bridgland 1850). Survey mapping shows little improvement along the Durham Road which is notable given the fact that it served as an early colonization route.

In summary, while the early surveyor's field notes do not specifically note any First Peoples' or other occupation within the study area, there is potential for historic-era settlements to exist.

2.3.3 Historic Métis

The Historic Saugeen Métis are descendants of the Métis who traded at Saugeen (see Wilson McArthur 2005). Pierre Piché was considered this first Métis in the area, trading in about 1816. The Ojibwa invited Piché to share the resources within the Saugeen territory, but also required him to “share” in the protection of these same resources and the environment for mutual benefit. The Historic Saugeen Métis are descended from unions between European traders and native women. The Lake Huron



watershed Métis lived, fished, hunted, trapped and harvested the lands and waters of the Bruce Peninsula, the Lake Huron proper shoreline and its watershed (Saugeen Métis 2013). These are considered the traditional Métis territory.

2.3.4 Historic Euro-Canadian and Municipal Settlement

The study area comprises Lots 1, 2, 3, and 4, Concession 1 South of the Durham Road (SDR) in the Geographic Township of Kincardine, Bruce County, Ontario. A brief discussion of early municipal settlement is provided below, along with a summary of historic land use. This will provide a general context for identifying features of archaeological potential.

Prior to the formation of Bruce County, this region was part of the “Queen’s Bush,” an extensive tract of land surrendered by local Ojibwa populations to the British through the Treaty of Manitowaning in 1836 (Robertson 1906:11). Some accounts suggest that the first Europeans to traverse through Bruce County were French explorer Samuel de Champlain and Jesuit missionaries who traveled here in the 17th century. It is reported that the first Euro-Canadian settlers to establish homes in Bruce County were William Withers and Allan Cameron (Robertson 1906:429). In the spring of 1848 these pioneers settled at the mouth of Penetangore River located in present day Kincardine.

The census of 1851 reported that there were no more than 499 families living in Bruce County, many of whom lived in temporary shanties. These shanties were typical dwellings for early settlers while their land was cleared, and were often a stipulation of the land grant process. The population of the county grew quickly into the 1860s, which was facilitated by the construction of a series of stone roads that provided access between the various settlements within the County.

Early on, the focal point for both residence and industry was the Lake Huron shoreline. The mouth of the Penetangore River was an attractive locale for docking and shipping. Its readiness for access by water gave Kincardine Township the earliest and largest pioneer settlement in the county. For the first 10 years after its formation Kincardine was the leading township in Bruce County. Unlike the other Bruce County townships Kincardine Township was surveyed in three sections at different times (Robertson 1906:429). The first survey in 1848 was the town plot that was formally dubbed “Penetangor.” This name was later changed to Kincardine when it was incorporated in 1858. The second survey was the 1848-49 Durham Road Survey by A.P. Borough, PLS (Robertson 1906:429).

Historic Durham Road (now Hwy 9) forms the northern boundary of the study area. The 1848-1849 Durham Road was planned as a model for “colonized roads” of the mid-nineteenth century (Kincardine News 1969). The construction of the road would make a major contribution to the development of Grey and Bruce Counties by opening up the interior lands for habitation. The original Durham Road survey laid out the road and



three concessions on either side of it, with the creation of 50 acre lots which could be granted free to settlers; other lands were withheld for sale and purchase at a later date (Kincardine News 1969). Once the road was surveyed, the lots alongside it were some of the first to be offered for sale; these were occupied quickly and generally by 1850 (Roberston 1906:429) (H. Belden & Co 1880). John Dingman and Major William Daniel were the first settlers on the Durham Road. Also in 1849 “free grant” lots were made to many settlers on the south side of the Durham Road, with grantees including George Ryckman, Samuel Taylor, William Fanning, Robert Stewart, and John Sellery. Many families who settled along the Durham Road were Highland Scotch by birth or descent (Roberston 1906).

The 1880 Map of Kincardine Township by H. Belden & Co. does not list landowners for Lots 1 through 4 of Concession 1 South of the Durham Road, nor does it show any structures within the lot limits (Map 8). This information is contrary to that provided in the AMICK 2005 which places the 2005 subject property in Concession 2 rather than Concession 1. The lack of both a landowner name and structure on each of the lots is not an indication that the lands were unsettled, as historic atlas maps are not always accurate renderings of land use conditions of the time. Landowners often had to pay a subscribers fee to be shown in the atlas and many families may have simply chosen not to do so. The fact that other occupants of Concession 1 SDR are listed in the 1871 census and that BbHj-37 (Clements Site) documented a reported ca. 1840-1860 domestic site provides further evidence for early pioneer settlement along the Durham Road.

2.3.5 Modern Land Use

The study area incorporates a number of modern land uses. The northwest and central-west portion has undergone commercial development and contains a number of businesses (Canadian Tire, Sobey’s, Meridian Credit Union, Boston Pizza, Holiday Inn Hotel and a professional office building) and their associated infrastructure including access roads, parking lots, utilities, landscaping and drainage (Images 1 to 7). These are all accessed off of Highway 21 via Durham Street, with a north-south arterial route (Millennium Way) present along the east side of the commercial complex (Images 8 and 9). Evidence of significant underground servicing is present throughout the commercial zone (Images 1 to 7), along the rights-of-way for both major adjacent highways and the arterial roads, all of which are also ditched in places. A deep drainage ditch has been cut along the south side of the commercial zone (Image 10) and a ditch and berm are present adjacent to Highway 21. An earth berm runs along a treed property line extending south from Highway 9 and separates the commercial zone from residential/farm lots to the east (Image 7). A wood pole hydro line runs along a field edge east of the commercial properties. Regardless of the presence of standing buildings, a small portion of the northwest corner of the commercial complex and study area is grassed and undeveloped (Image 11). It is not known whether this area was disturbed during the construction of the adjacent commercial areas.



To the east of the commercial area along Highway 9 are three rural residential properties with laneways off of the highway (Images 12 to 14). These contain structures (houses, barns, sheds, outbuildings), laneways and areas of manicured lawn. Farm machinery roads extend southward into the associated agricultural fields.

The remainder of the study area is comprised of active or former agricultural fields (cropped, hay fields, now vacant lands) (Images 15 to 17) as well as a natural area associated with a tributary of the Penetangore River (Image 18) which includes some wet and steeply sloped lands. Throughout the study area there are several seasonal/relic watercourses and swales running east to west across the fields (Image 16 and 17).

2.4 Analysis and Conclusions

As noted in Section 2.1, the Province of Ontario has identified numerous factors that signal the potential of a property to contain archaeological resources. Based on the archaeological and historical context reviewed above, the study area contains or is in proximity to features signalling archaeological potential, namely: 1) watercourses (active and seasonal); 2) 19th century thoroughfares and colonization roads (Hwy. 21 - Goderich Road and Hwy. 9 - Durham Road); 3) the 19th century settled town core of Kincardine (see Map 8); and 4) registered and known archaeological sites. Therefore, based on a mapping review, some portions of the study area have potential for either First Peoples or EuroCanadian sites.

Nonetheless, some lands within the study area have also witnessed significant prior disturbance and do not retain archaeological potential. Most notable in this regard are the commercial complexes and rights-of-way. More isolated disturbances are present within the residential/farm lots (where buildings and laneways are present). However, due to restrictions on property access, a formal property inspection could not be undertaken to visually confirm extent of disturbance. Other areas within the property are also of low potential, namely the watercourse and its sloped valley lands.

Based on our generalized mapping review, roughly 11.38% (8.8 ha) of the project area is considered to be disturbed and does not retain potential for the discovery of intact archaeological resources. An additional 3.24% is also considered to have low potential due to wet (2.85%; 2.2 ha) or steeply sloped (0.39%; 0.3 ha) conditions. A total of 16.6 ha or 21.47% was previously surveyed. The remaining 63.9% is considered to have archaeological potential, with 50.06% (38.7 ha) consisting of former or active agricultural lands and 13.84% (10.7 ha) consisting of treed or lawn areas. Areas of varying archaeological potential are shown on Map 9 and on the proponent map shown in Map 10. However, this mapping was done without the benefit of complete property access and a formal property inspection to meet provincial standards. Therefore, these evaluations of potential are considered preliminary and are for general planning purposes. Confirmation in the field is required once more detailed servicing plans are made.



Two separate parcels within the study area have been previously subject to archaeological assessment. The entire Millennium Way extension was surveyed by TMHC in 2006, received provincial clearance, and the road extension was built. Therefore this section can be entirely eliminated from archaeological concern. The lands subject to Stage 1 assessment by AMICK in 2005 were only partially surveyed and one archaeological site was found, with a requirement for Stage 3 survey. All of the surveyed lands that are 70 metres or more from distant from the Stage 2 limit of BbHj-37 have been cleared of archaeological concern, with further assessment required for site area proper and the lands that were not surveyed during the 2005 study.

Table 2: Documentary Records

- Field notes and maps November 20 and 22, 2013
- Photograph log and images: November 20 (P1010334-355), November 22 (P1010383-435)
- Records on file at Timmins Martelle Heritage Consultants Inc., 1600 Attawandaron Road, London, ON N6G 3M6

2.5 Recommendations

Based on the information compiled in the background study, the following recommendations are made:

- 1) The previously assessed lands in the 2006 TMHC survey of the Millennium Way road extension are of no further archaeological concern and no additional assessment is recommended.
- 2) Registered site BbHj-37, recorded by AMICK during a 2005 partial survey of a proposed development property within the study area, requires Stage 3 testing to current MTCS standards. Based on the information provided in the consultant report for this project, the site would be classified as a post-contact site of cultural heritage value or interest.¹ The proposed excavation strategy should follow that defined for small post-contact sites of established cultural heritage value or interest (MTCS 2011; Table 3.1. Standards 3 and 4), with initial test units placed at 10 metre intervals across the surface scatter and an additional 40% of units placed in areas of interest. As the Stage 2 reporting indicated a maximum site size of roughly 60 by 60 metres, methodological provisions for Stage 3 testing of large sites (MTCS 2011; Section 3.31, Subsection 3.3.1 Standard 1) might also be applicable. Until Stage 3 testing is undertaken, all lands within 70 metres of the Stage 2 site limits have further archaeological concern and are protected from land alterations (other than typical agricultural cultivation) by the provisions of

¹ Note that this evaluation is based on a date range of ca. 1840-1860. No land registry information is available to confirm or refute this.



- the *Ontario Heritage Act* which prohibit disturbance to registered archaeological sites.
- 3) The remaining lands surveyed by AMICK in 2005 require no further archaeological assessment.
 - 4) All former and active agricultural lands within the study area that were not previously surveyed demonstrate potential for the discovery of archaeological resources. Based on provincial standards these require ploughing and a pedestrian or “walk-over” survey at a five metre interval. Ploughed surfaces must be well-weathered by heavy rainfall and the ploughed surface must be clean of vegetation resulting in at least 80% surface visibility.
 - 5) The low-lying, wet and steeply sloped lands associated with the tributary of the Penetangore River are considered to have low archaeological potential and do not require further assessment. However, given that a formal field inspection could not be undertaken, the precise limits of the these could not be mapped and therefore a detailed field inspection will minimally be required prior to any future servicing work can take place in these areas.
 - 6) The previously disturbed lands within the commercial zones and residential/farm lots do not retain potential to house intact archaeological resources and therefore no further work is recommended in these areas. However, given that a formal field inspection could not be undertaken, the precise limits of the these could not be mapped and therefore a detailed field inspection will minimally be required prior to any future servicing work can take place in these areas.
 - 7) The treed lands associated with the Penetangore River tributary and the lawn areas within the residential/farm lots have potential for the discovery of archaeological resources. Based on provincial standards, these lands must be subject to a test pit survey at a five metre interval. Where test pitting is conducted each test pit should measure approximately 30 cm (shovel-width) in diameter and be excavated into the first five centimetres of subsoil. The soil from each test pit should be passed through 6 mm hardware cloth in an effort to retain any artifacts that might be present. When the screening process is completed, the soil strata should be examined and the pits filled in as best as possible and re-capped with sod.

These recommendations are subject to report review and acceptance by the Ministry of Tourism, Culture and Sport.



4.0 SUMMARY

A Stage 1 background study was undertaken for a roughly 77.3 ha study area that was selected by the Municipality of Kincardine for the preparation of a Servicing Master Plan for the Kincardine Business Park in the Town of Kincardine. The study area includes agricultural lands, residential and farm lots and natural areas, in addition to a developed commercial block along Highway 21. The background research indicated that the study area was in proximity to features signalling archaeological potential, namely: 1) watercourses; 2) 19th century thoroughfares and colonization roads (Goderich Road and Durham Road); 3) the 19th century town core of Kincardine; and 4) registered or known archaeological sites. Therefore, lands within the study area have archaeological potential for both First Peoples and historic era EuroCanadian sites. The background study also indicated that some lands within the study area have already been subject to Stage 2 survey and cleared of archaeological concern. Furthermore, one 19th century site identified in a previous study is present within the study area and requires Stage 3 testing. The previously unsurveyed agricultural and undeveloped lands within the study area retain archaeological potential and warrant Stage 2 assessment involving pedestrian or test pit survey. The developed lands and lands containing built features do not retain archaeological potential and require no further archaeological assessment, as do the low potential low-lying and sloped valley lands of the Penetangore River tributary. Because property access was restricted and a complete and formal property could not be undertaken, areas of low potential should be subject to more detailed field inspection in the future if and when plans to service these areas are put in place.

5.0 ADVICE ON COMPLIANCE WITH LEGISLATION

This report is submitted to the Ministry of Tourism, Culture and Sport as a condition of licensing in accordance with Part VI of the *Ontario Heritage Act*, R.S.O 1990, c 0.18. The report is reviewed to ensure that it complies with the standards and guidelines that are issued by the minister, and that the archaeological fieldwork and report recommendations ensure the conservation, protection and preservation of the cultural heritage of Ontario. When all matters relating to archaeological sites within the project area of a development proposal have been addressed to the satisfaction of the Ministry of Tourism, Culture and Sport, a letter will be issued by the ministry stating that there are no further concerns with regard to alterations to archaeological sites by the proposed development.

It is an offence under Sections 48 and 69 of the *Ontario Heritage Act* for any party other than a licensed archaeologist to make any alteration to a known archaeological site or to remove any artifact or other physical evidence of past human use or activity from the site, until such time as a licensed archaeologist has completed archaeological fieldwork on the site, submitted a report to the minister stating that the site has no further cultural heritage value or interest, and the report has been filed in the



Ontario Public Register of Archaeology Reports referred to in Section 65.1 of the *Ontario Heritage Act*.

Should previously undocumented (i.e., unknown or deeply buried) archaeological resources be discovered, there may be a new archaeological site and therefore subject to Section 48(1) of the *Ontario Heritage Act*. The proponent or person discovering the archaeological resources must cease alteration of the site immediately and engage a licensed consultant archaeologist to carry out archaeological fieldwork, in compliance with Section 48(1) of the *Ontario Heritage Act*. Further, archaeological sites recommended for further archaeological fieldwork or protection remain subject to Section 48 (1) of the *Ontario Heritage Act* and may not be altered, or have artifacts removed from them, except by a person holding an archaeological licence.

The *Funeral, Burial and Cremation Services Act, 2002, S.O. 2002, c.33* (when proclaimed in force) requires that any person discovering human remains must notify the police or coroner and the Registrar of Cemeteries at the Ministry of Small Business and Consumer Services. The Registrar of Cemeteries, Cemeteries Regulation Unit can be reached at (416)326-8404 or (416)326-8393.

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7.0 IMAGES



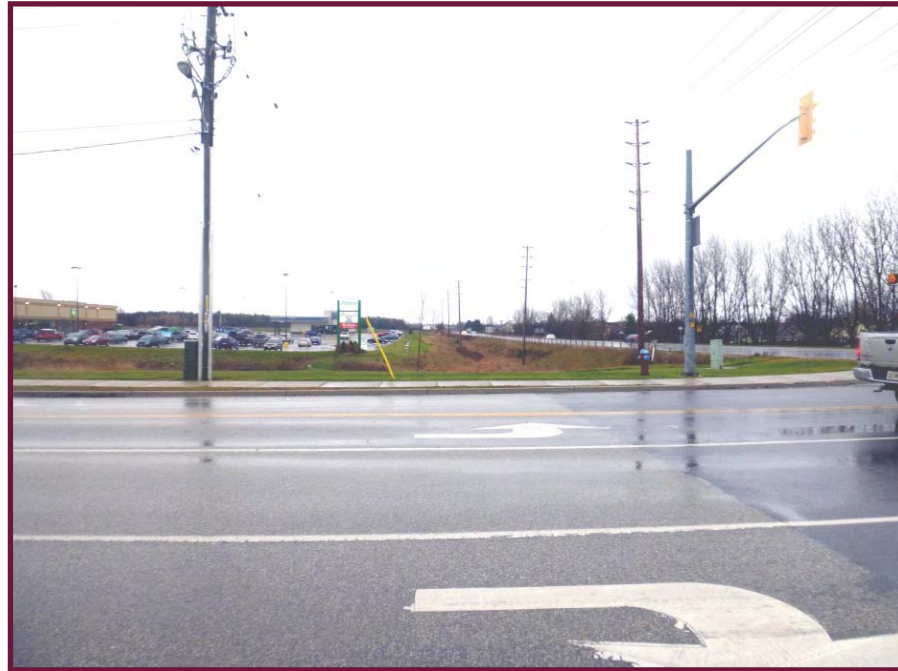


Image 1: Overview of Commercial Lands Along Highway 21, South of Durham Street (looking south)



Image 2: Commercial Lands on Highway 21 North of Durham Street (looking north)



Image 3: Canadian Tire Store Along Highway 21 (looking northeast)



Image 4: Commercial Lands South of Durham Street (looking southeast)



Image 5: Transformer Station in Northwest Corner of Study Area (looking northeast)



Image 6: Underground Services in Commercial Lands South of Durham Road (looking east)





Image 7: Landscaped Earth Berm East of Commercial Lands on Highway 9 (looking south)



Image 8: Commercial Complex Access Roads - Intersection of Durham Street and Millennium Way (looking east)



Image 9: Northern Extension of Millennium Way (looking north)



Image 10: Drainage Ditch South of Commercial Lands off Highway 21 (looking west)



Image 11: Grassed, Undeveloped Lands Within Commercial Complex off Highway 21 (looking south)



Image 12: Manicured Lawn and Treed Area in Front of Residential Property on Highway 9 (looking south)





**Image 13: Residential/Farm Lot off Highway 9
(looking southwest)**



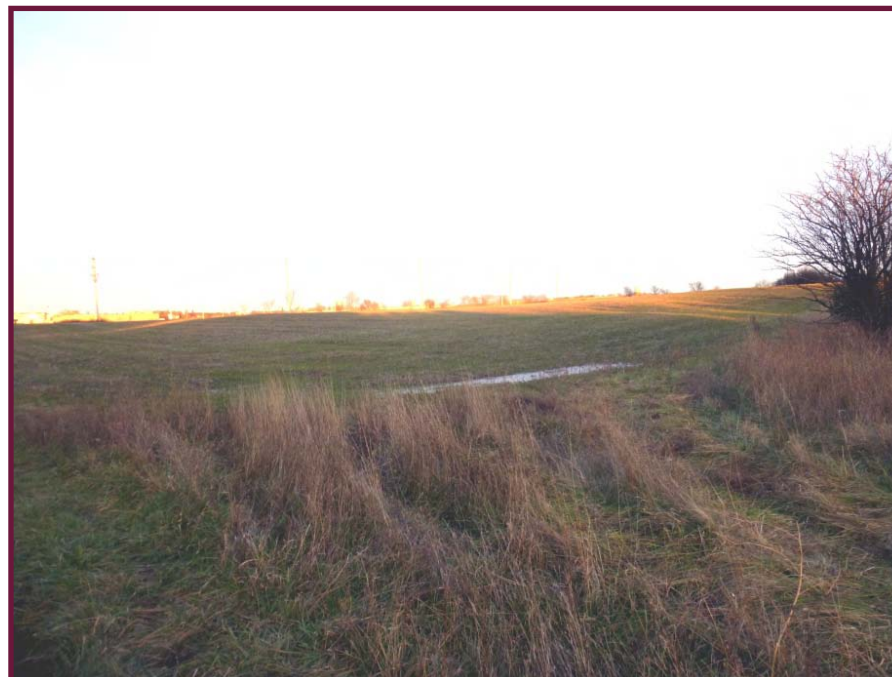
**Image 14: Residential/Farm Lot in Northeast Corner of Study Area
(looking southwest)**



**Image 15: Agricultural Field in Northeast Portion of Study Area
(looking south)**



**Image 16: Agricultural Field East of Commercial Lands
(looking southeast)**



**Image 17: Agricultural Field in Southern Portion of Study Area
(looking northeast)**

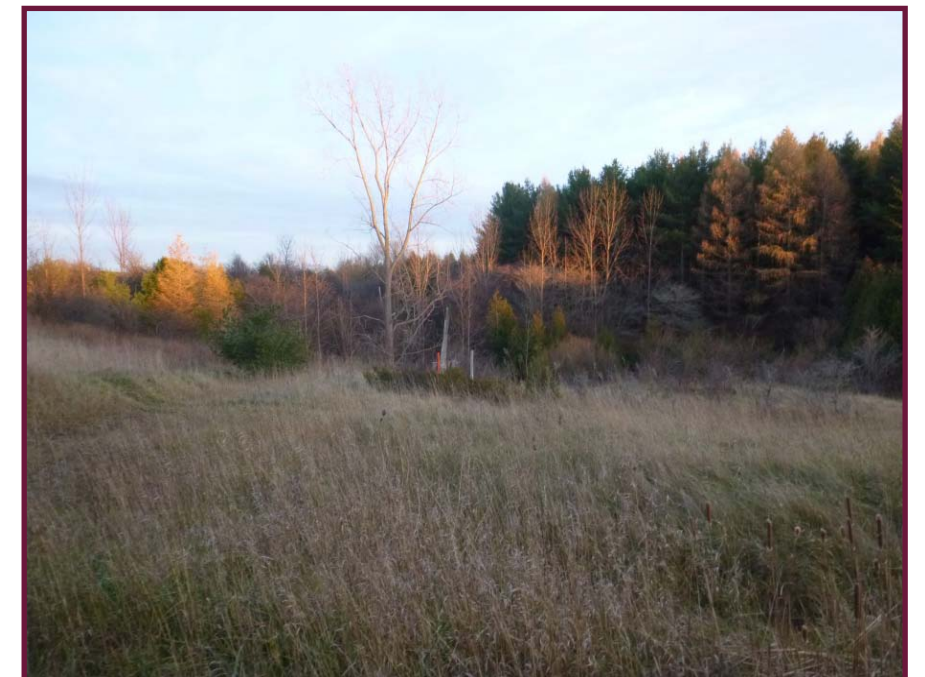
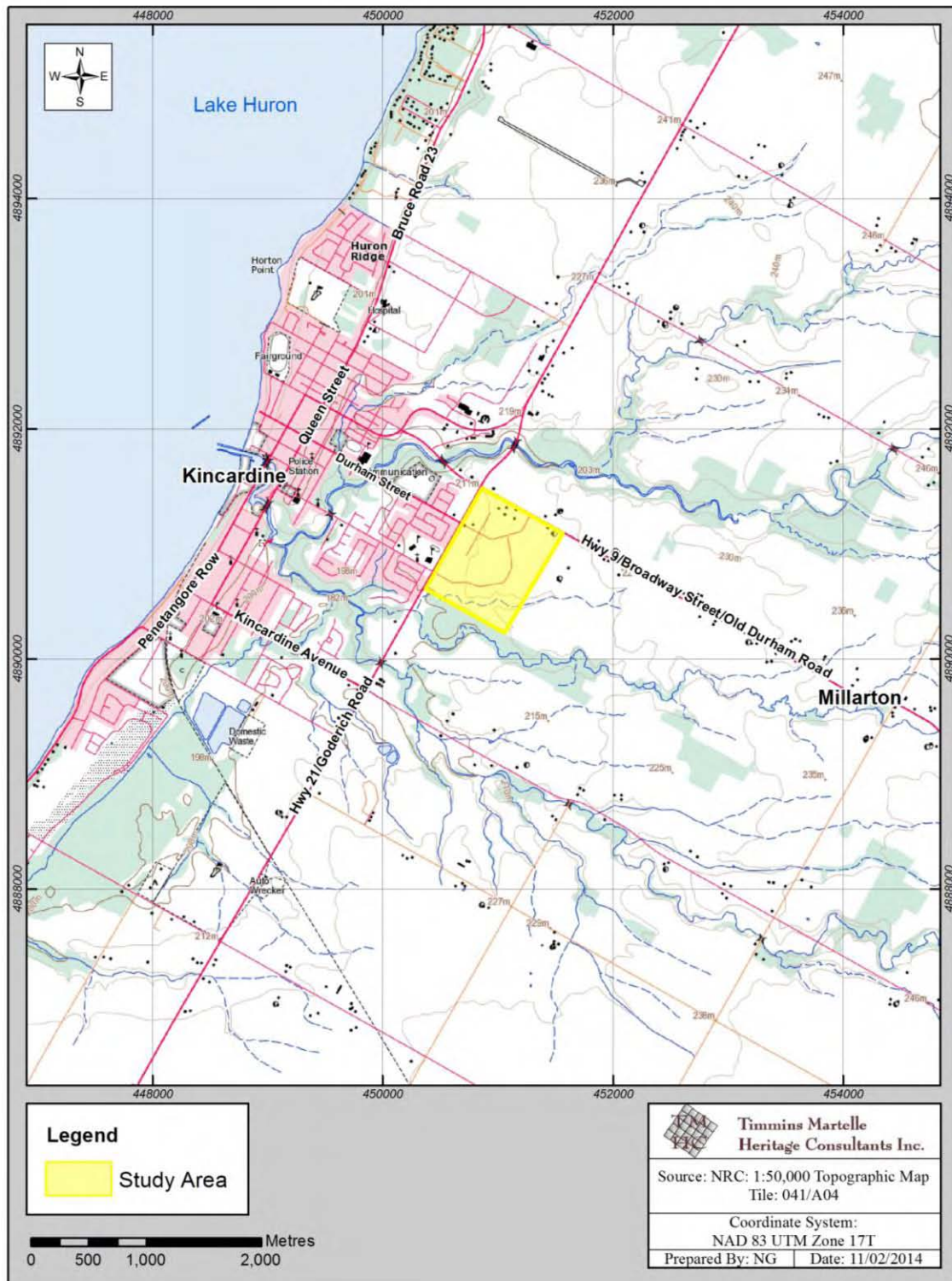


Image 18: Penentangore River Tributary Treed and Sloped Valley Lands in South Portion of Study Area (looking east)



8.0 MAPS





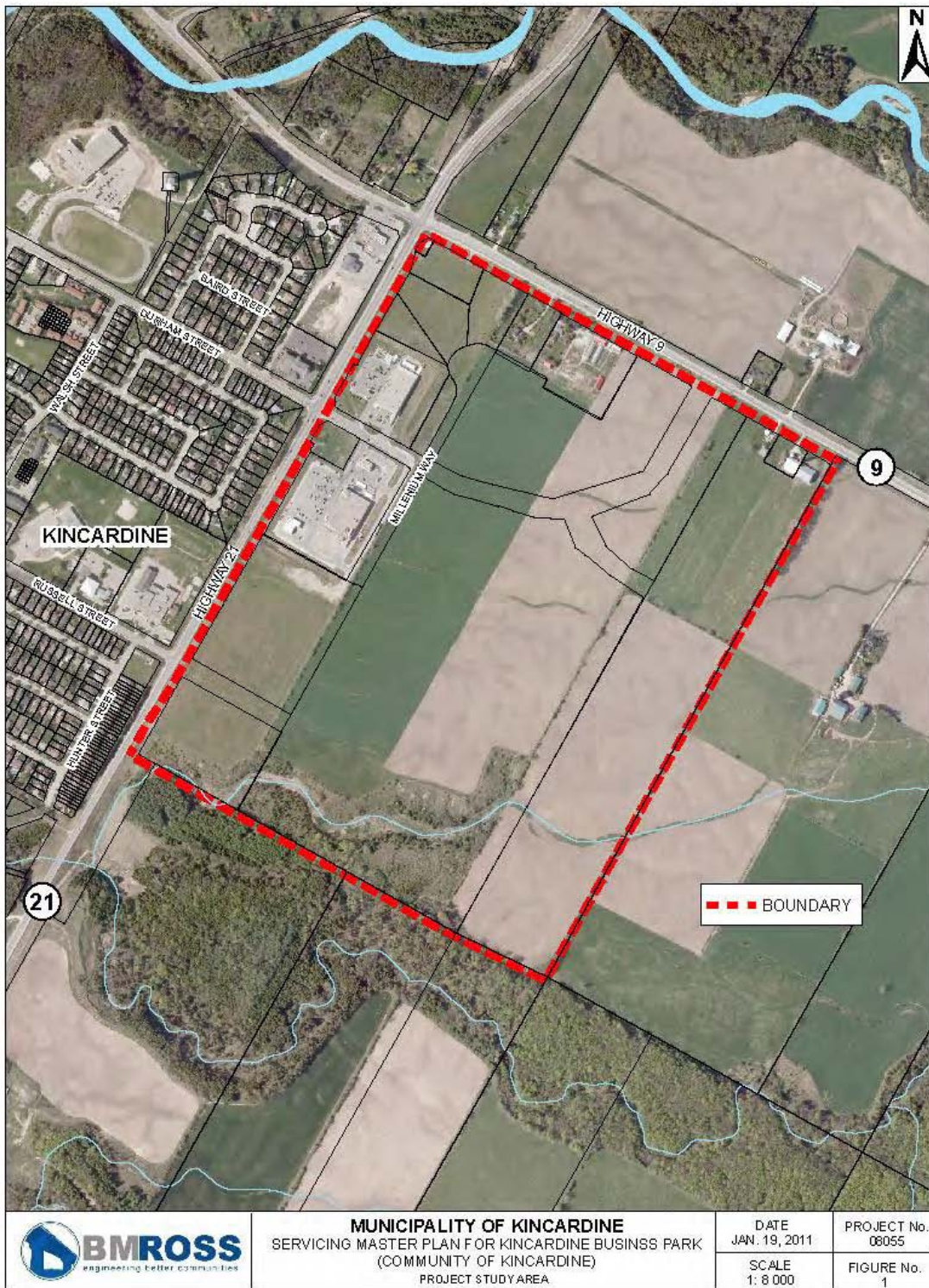
Map 1: Location of the Study Area in Kincardine, ON





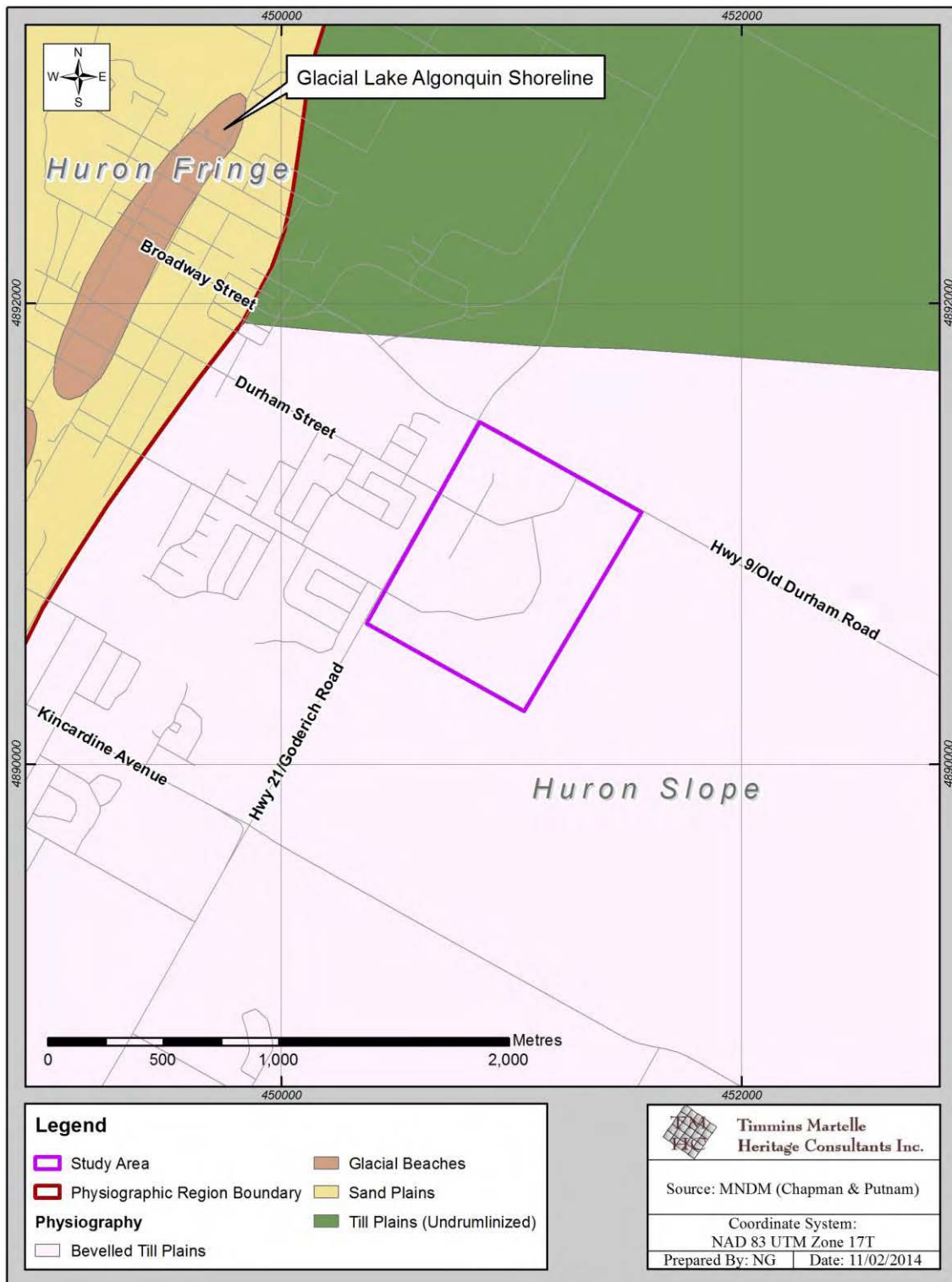
**Map 2: Aerial Photograph Showing the Location of the Study Area in
Kincardine, ON**





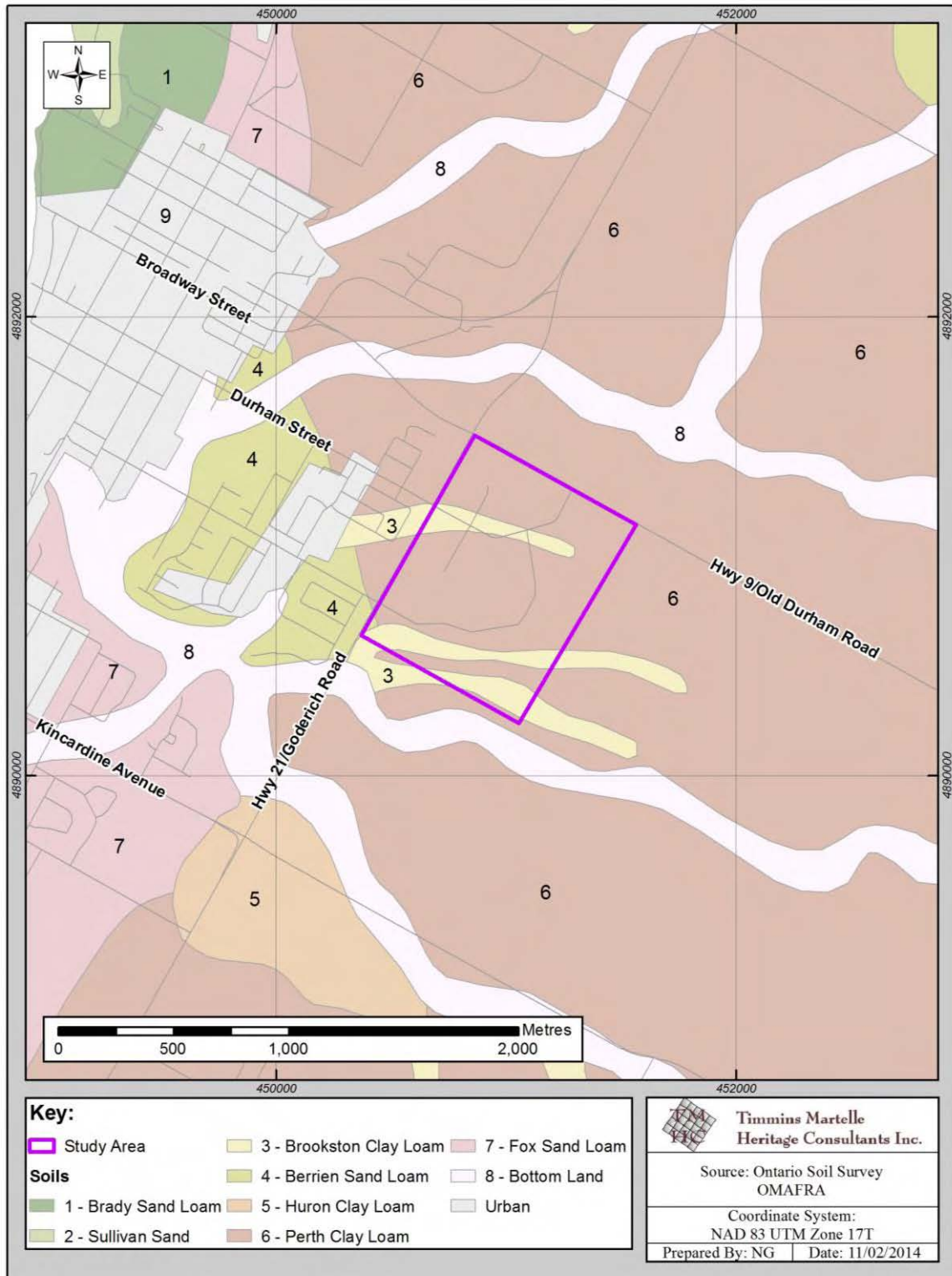
Map 3: Proponent Map Showing the Limits of the Study Area for the Servicing Master Plan





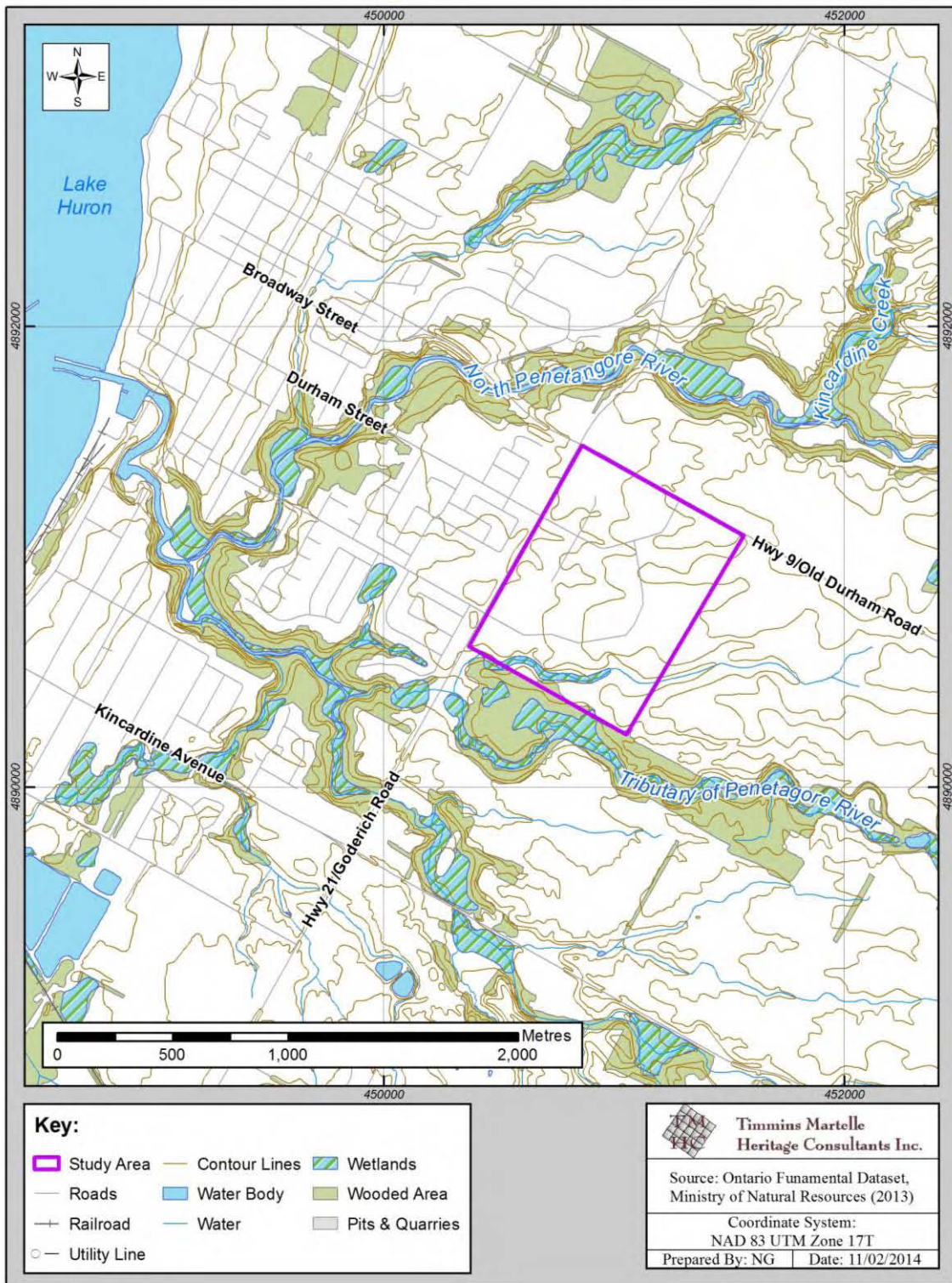
Map 4: Physiography Within the Vicinity of the Study Area





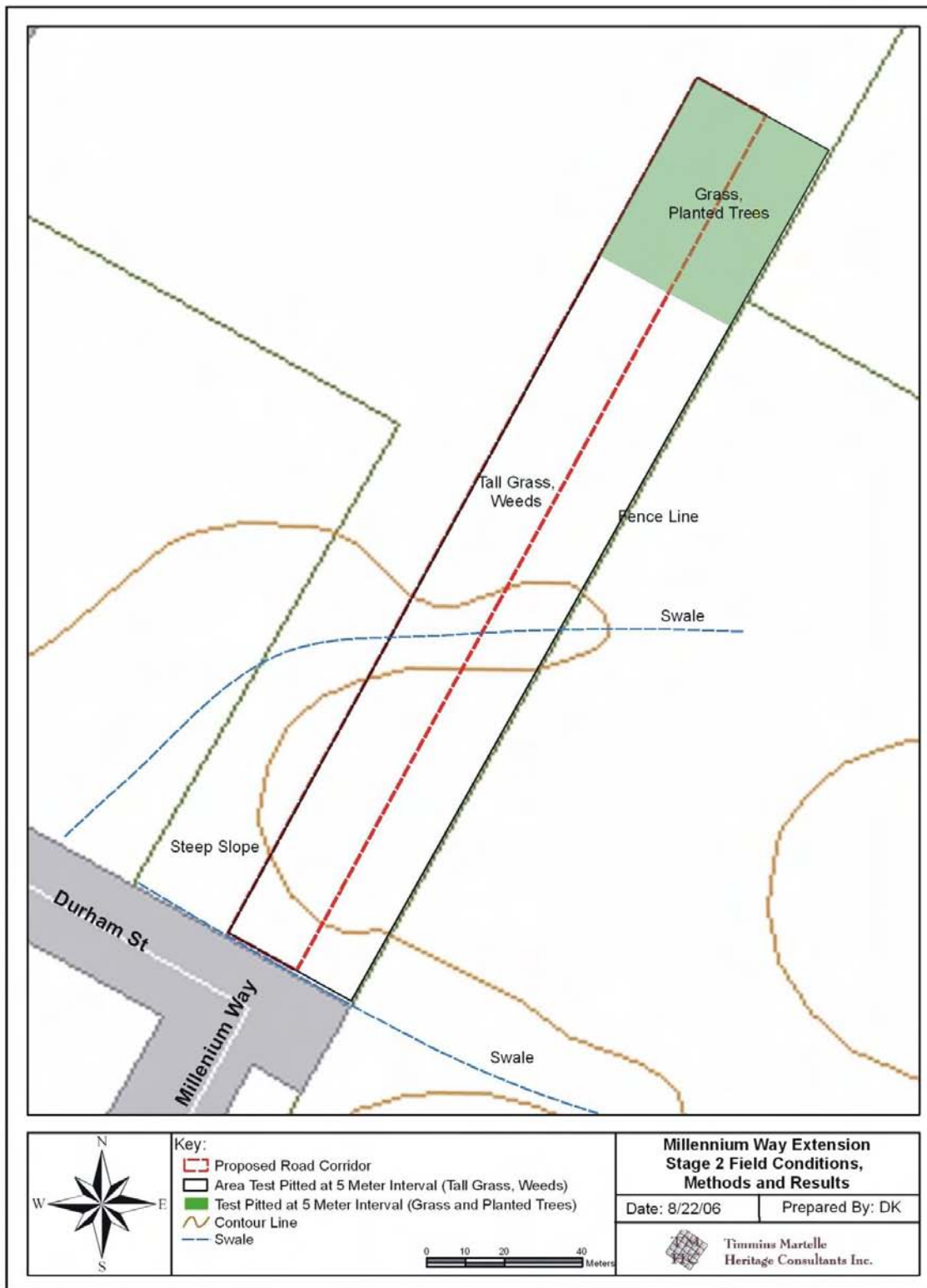
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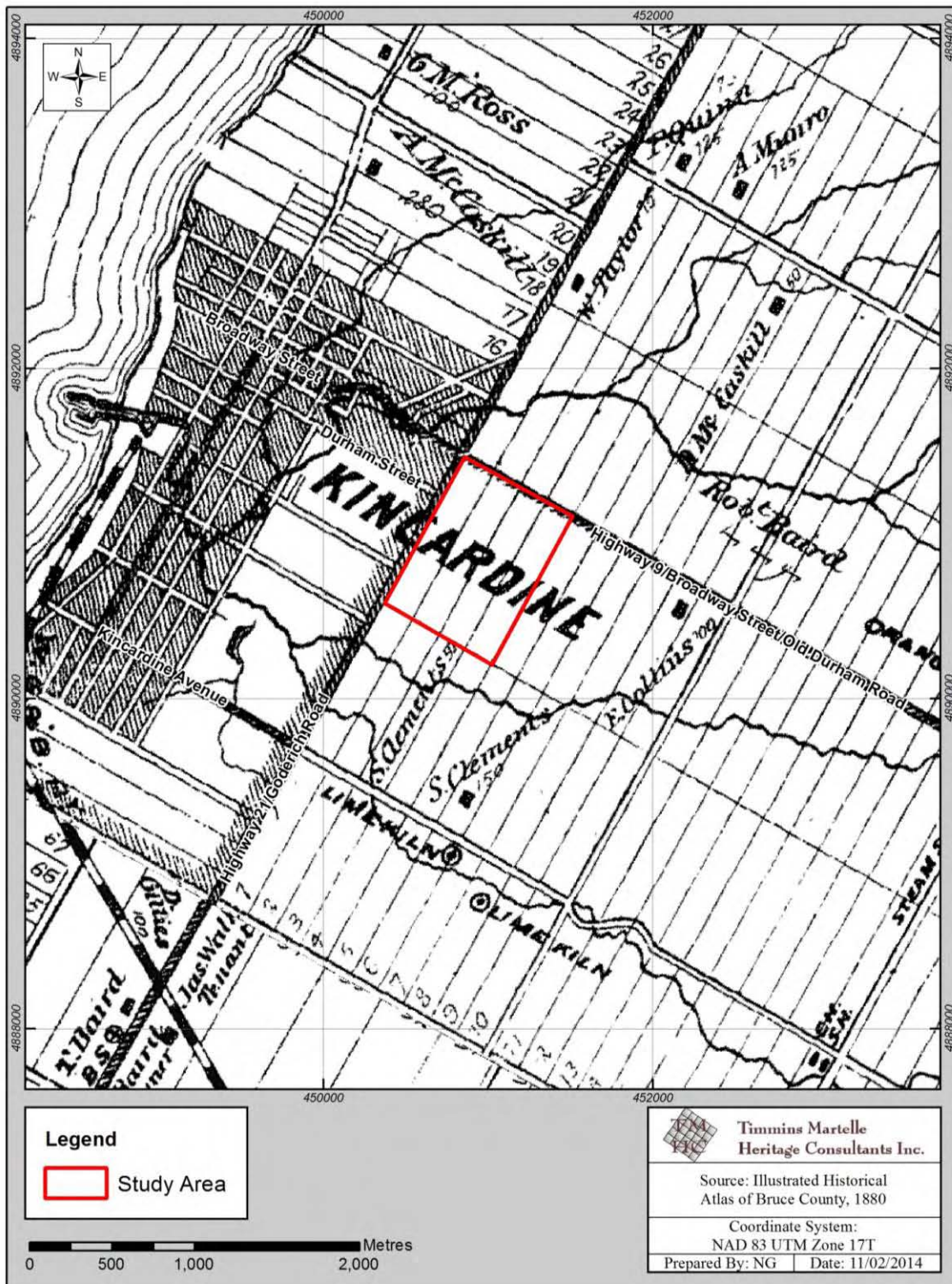
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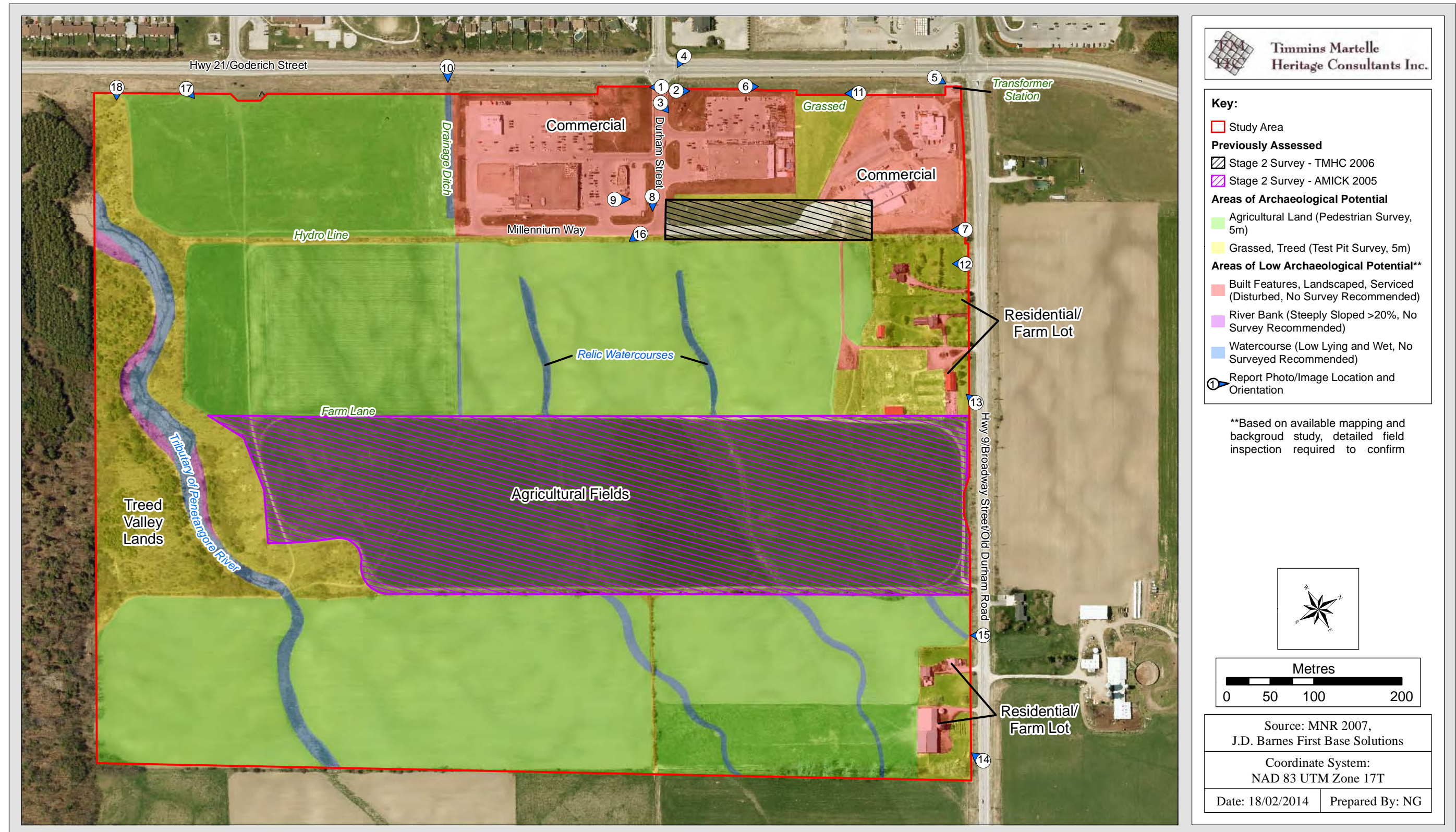
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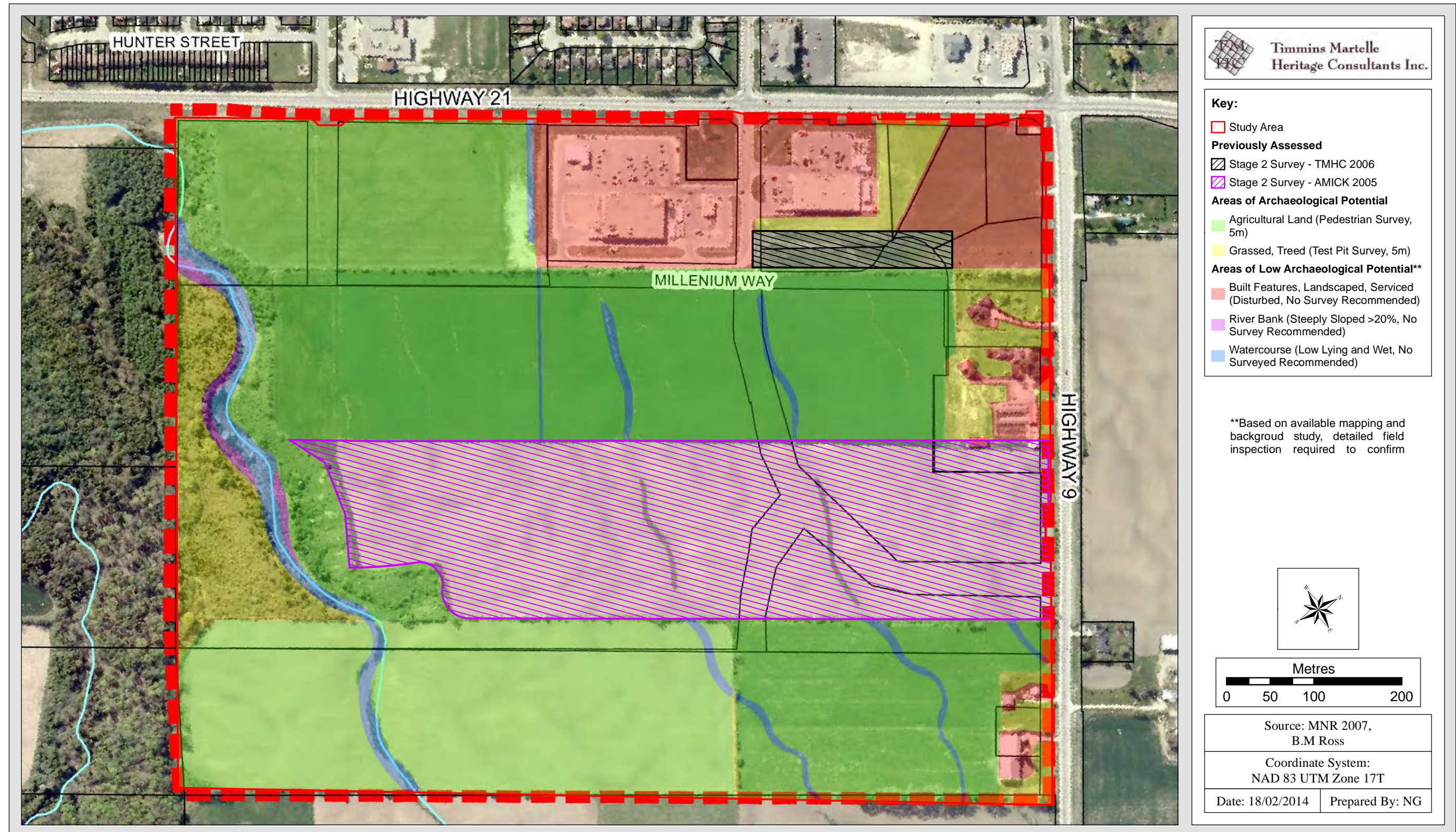
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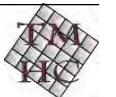


Map 9: Areas of Archaeological Potential Established by Stage 1 Background Study





Map 10: Areas of Archaeological Potential Established by Stage 1 Background Study - Shown on Proponent Mapping



APPENDIX 2
SERVICING PLAN

MUNICIPALITY OF KINCARDINE

**KINCARDINE BUSINESS PARK
SERVICING PLAN**

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engineering better communities

MUNICIPALITY OF KINCARDINE

KINCARDINE BUSINESS PARK SERVICING PLAN

DRAFT

September 19, 2011
Revised June 29, 2016

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DRAFT

**MUNICIPALITY OF KINCARDINE
KINCARDINE BUSINESS PARK
SERVICING PLAN**

1.0 INTRODUCTION

The Municipality of Kincardine wishes to determine a practical approach to provide servicing for the balance of the Business Park. The Business Park is primarily located southeast of the intersection of Highway 9 and Highway 21. The balance of the remaining undeveloped lands is about 70 gross ha, however, the Holtby Drain prevents development of the southerly lands and reduces the developable land area to under 60 Ha.

Generally, the Business Park area includes the first four farm lots east of Highway 21 and south of Highway 9 together with a small parcel on the north side of Highway 9. All four farm lots have been designated as Business Park in the Municipality's official plan. The first lot was purchased by Kincardine who became the developer of the northerly two thirds of the lot, most of which has been built-out with Commercial facilities.

The purpose of this study is to outline how the balance of the four farm lots can be provided with sanitary servicing, potable water, storm drainage, stormwater management, and road systems from a Master Plan perspective.

This report has been prepared primarily focused on the four farm lots southeast of Highway 9 and Highway 21 although some consideration has been given to the lands located north of Highway 9.

2.0 TRANSPORTATION AND ROAD PATTERN

2.1 Road Pattern

The County of Bruce Planning Department has completed a recommended pattern for development and installation of new roads throughout the Business Park area. This road pattern, as slightly modified by BMROSS, including the preferred road widths, is shown on Figure TR1. It is anticipated that these roads will be constructed as development progresses.

The Ministry of Transportation (MTO) has provided comments based on the road pattern presented on Figure TR1 and have suggested that it may be appropriate to modify the orientation of Russell Street. The suggested MTO road concept has been provided for comparative purposes as Figure TR2.

The Ministry has noted possible issues with the road, labeled ‘Private Drive’, connecting Millennium Way and the extension of Russell Street and has suggested that Private Drive is situated too close to the intersection of Highway 21 and Russell Street and that future left-turning movements from Russell St. onto Private Drive, will slow and possibly block traffic flow through the Highway 21-Russell St. intersection.

Following discussions with the Municipality, the MTO, and the property owners within the Business Park the preferred internal road layout of Russell Street can be finalized.

Regardless of the final configuration of the internal road system, it is proposed that the Business Park will access the existing road network at the following locations:

- Highway 21 at Durham Street
- Highway 21 at Russell Street
- Highway 9 at an extension of Durham Street

2.2 Road Cross Section

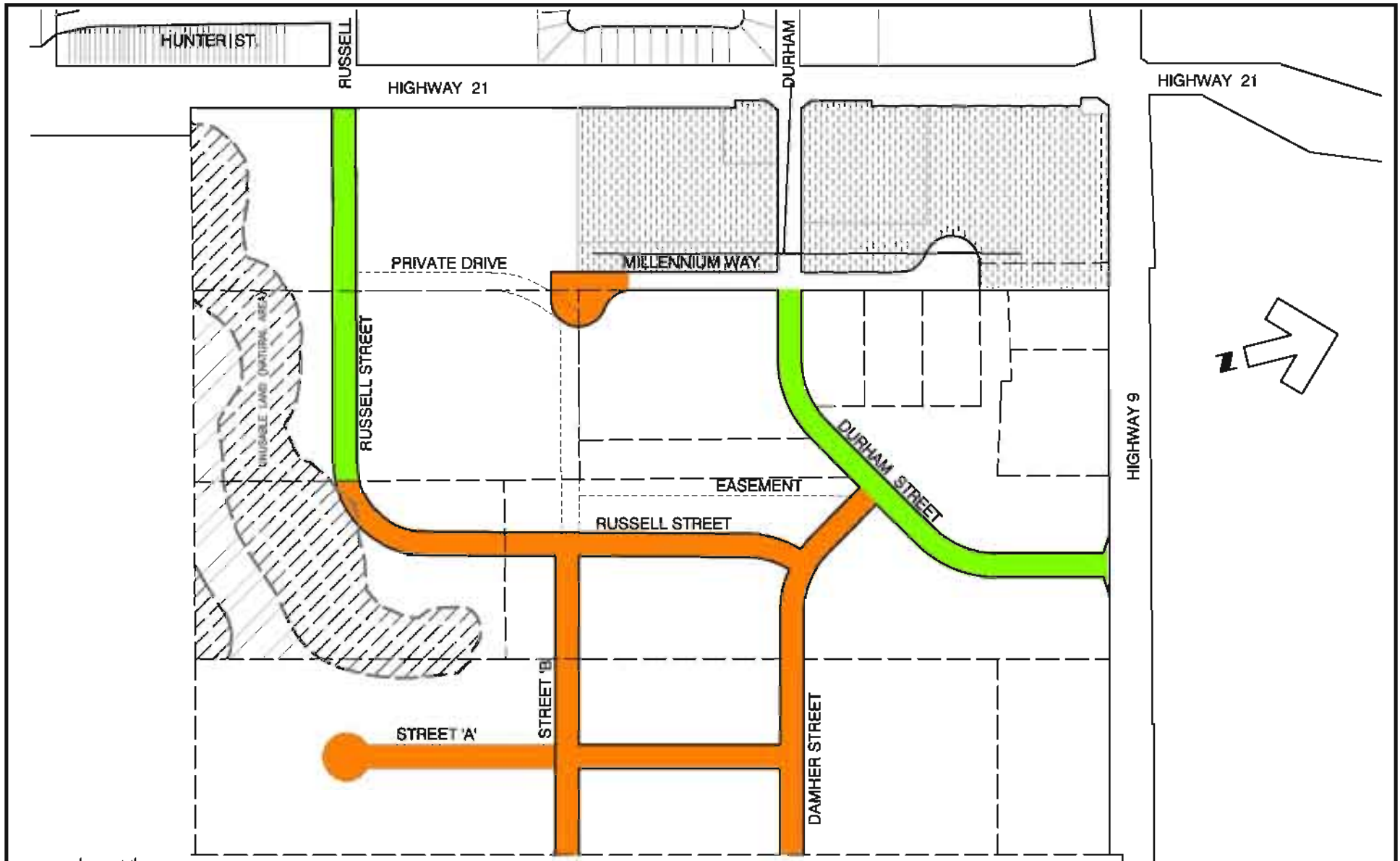
Although subject to change as part of future geotechnical recommendations to be completed for final design it is anticipated that at a minimum the road cross section for each street type will consist of the following:

- i. 10.5 metre Wide Road
 - 50mm HL3, 50mm HL4, 150mm Granular A, 400mm Granular B
- ii. 8.5 metre Wide Road
 - 40mm HL3, 40mm HL4, 150mm Granular A, 300mm Granular B


All roads are to be constructed with a minimum of 2% cross fall, adequate sub-grade drainage, curb and gutter, sidewalk on one side (where warranted), grass boulevard restoration, street lighting, and required utilities.

2.3 Development Grading and Road Layout

Preliminary grading and drainage of the development area has been completed to match existing topography. Figure TR-3 has been provided to illustrate the conceptual finished road elevations and overall intent of grading at key locations throughout the Business Park.



Legend

-  Existing commercial Area
-  Future 10.5m wide road (26m min. wide road allowance)
-  Future 8.5m wide road (20m min. wide road allowance)



**Municipality of Kincardine
Kincardine Business Park
Servicing - Transportation**

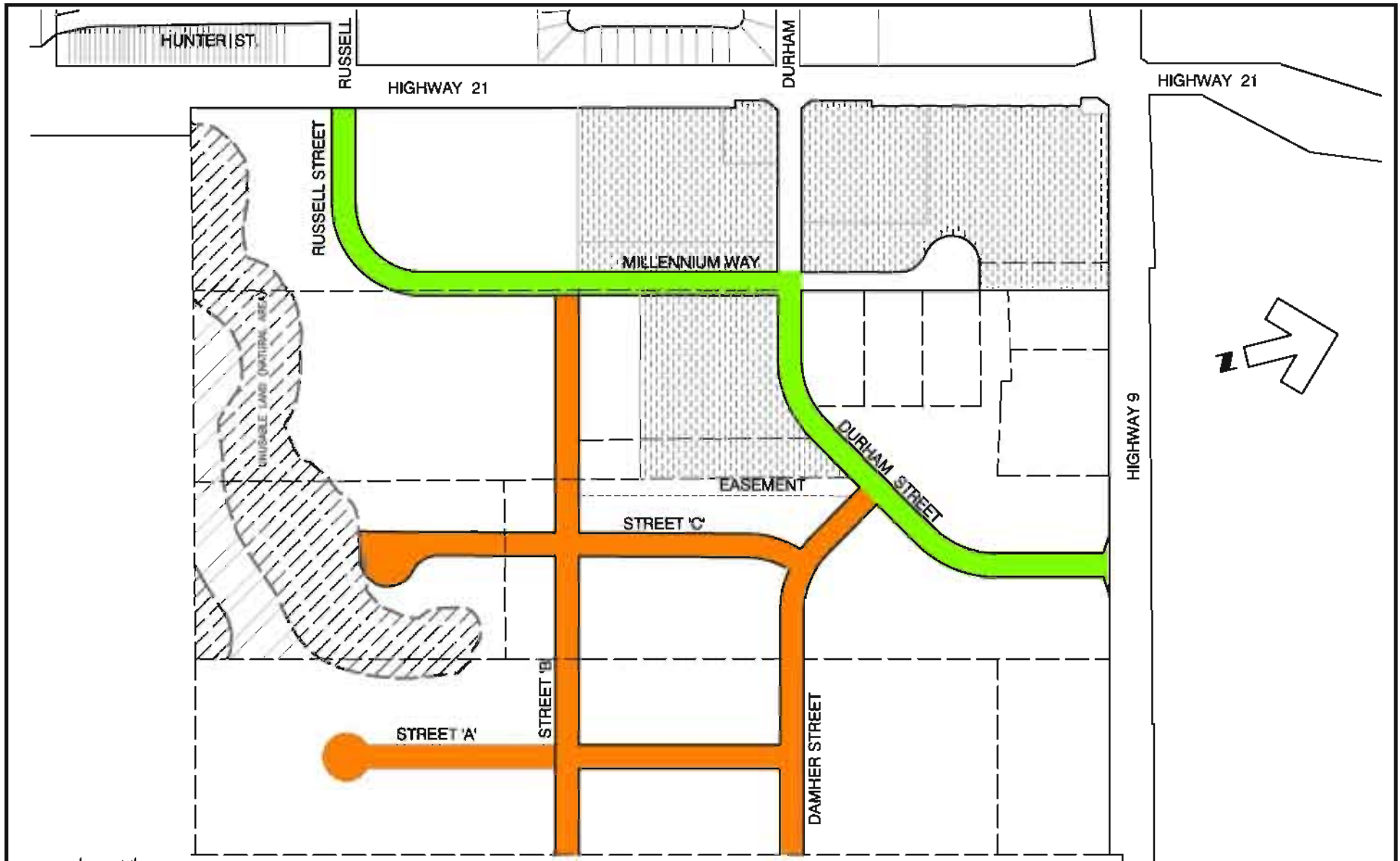
Proposed Road Layout and
Net Developable Land Areas

DATE
June 2016

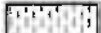


PROJECT No.
08055

SCALE
1:6,000

FIGURE No.
TR1



Legend

-  Existing commercial Area
-  Future 10.5m wide road (26m min. wide road allowance)
-  Future 8.5m wide road (20m min. wide road allowance)



Municipality of Kincardine
Kincardine Business Park
 Servicing - Transportation
 MTO Road Concept

DATE June 2016	PROJECT No. 08055
SCALE 1:6,000	FIGURE No. TR2

2.4 Traffic Impact Study

A traffic impact study associated with the proposed Business Park was undertaken by Paradigm Transportation Solutions Limited. The current version of the Traffic Impact Study is an update to a previous study completed by Paradigm. This latest study, finalized in November 2015, examined updated traffic counts, as well as comments from the MTO. Impacts based on forecasted background traffic and increased traffic volume as a result of development of the Business Park, were examined for the following intersections:

- Highway 21 and Highway 9/Broadway Street
- Highway 21 and Durham Street
- Highway 21 and Russell Street
- Highway 21 and Kincardine Avenue/South Line
- Durham Street and Millennium Way
- Highway 9 and the future Durham Street extension

Impacts and measures to accommodate traffic were examined for 5-year, 10-year and 15-year forecast periods. Traffic counts for Durham Street, Russell Street, Millennium Way, and Kincardine Avenue are from July 2013. The traffic count for Highway 9 is from October 2012. To determine the peak hour traffic volume generated by the Business Park, the following land use codes (from the Institute of Transportation Engineers Trip Generation Manual 9th Edition) were used: Hotel, Building Materials and Lumber Store, Shopping Centre, and Specialty Retail Centre.

It is forecasted that the Business Park will generate 424 total new trips in the AM Peak hour and 983 in the PM Peak. Growth in the background traffic volumes was assumed to be 2% over the forecast periods.

2.4.1 Forecasted Traffic Conditions

2020 Forecast Period

- The increase in background traffic is expected to result in a similar Level of Service (LOS) as the existing conditions, with slight increases in delays to left turns from westbound Highway 9 onto Highway 21 during the PM peak hour (LOS E).
- With the additional traffic resulting from the development of the Business Park, the following deficiencies were identified:
 - Westbound traffic on Highway 9 turning left onto Highway 21 will operate a LOS of F.
 - At the intersection of Russell Street and Highway 21, the east and westbound movements are forecasted to operate at LOS F and well above a volume to capacity ratio of 1.0 during the peak PM hour.

2025

- The increase in background traffic will result in similar conditions as the 2020 background traffic, with the left turn from westbound Highway 9 onto Highway 21 operating at LOS E.
- With the additional Business Park traffic, the following deficiencies were identified:

- The left turn movement from westbound Highway 9 onto Highway 21 will be at LOS F during the peak PM hour.
- At the intersection of Russell Street and Highway 21, the east and westbound movements are forecasted to operate at LOS F and well above a volume to capacity ratio of 1.0 during the peak PM hour.
- Eastbound movements at Highway 21 and Kincardine Avenue/South Line will operate at LOS F during the peak PM hour, however, the volume to capacity ratio will be expected to be below 1.0

2030

- The increase in background traffic is, again, expected to have similar impacts as the previous time periods; however, the delay for a left turn from westbound Highway 9 onto Highway 21 at the peak PM hour will result in a decline of the LOS from E to F.
- With the additional Business Park traffic, the following deficiencies were identified:
 - The left turn movement from westbound Highway 9 onto Highway 21 will be at LOS F during the peak PM hour.
 - At the intersection of Russell Street and Highway 21, the east and westbound movements are forecasted to operate at LOS F and well above a volume to capacity ratio of 1.0 during the peak PM hour.
 - Eastbound movements at Highway 21 and Kincardine Avenue/South Line will operate at LOS F during the peak PM hour, however, the volume to capacity ratio will be expected to be below 1.0

2.4.2 Remedial Measures and Recommended Improvements

Signals

- Warranted at Russell Street and Highway 21 by 2020
 - Also recommend construction of separate westbound left turn lane (on Russell Street from the Business Park) and a southbound (on Highway 21) left turn lane.
- Not warranted at Kincardine Avenue and Highway 21.

Left Turn Lane Warrants

- Assessed for the intersection of the future Durham Street extension and Highway 9. A left turn lane on Durham Street was not warranted.

Right Turn Lanes

- Given 2020 traffic levels, right turn lanes should be considered on Highway 21 at its intersections with Durham and Russell Streets.

Signal Changes

- At the intersection of Highways 21 and 9, it is recommended that by 2020 an advanced turn signal for left turns from westbound Highway 9 onto Highway 21 be implemented.

- At the intersection of Highway 21 and Durham Street, it is recommended that by 2030 an advanced turn signal for left turns from westbound Durham Street onto Highway 21 be implemented.
- Implementation of a left turn signal from westbound Russell Street onto Highway 21 and a southbound left turn from Highway 21 onto Russell Street is advised with the installation of a the previously recommended new signal.

3.0 WATER SERVICING

Water servicing of the development area is anticipated to occur through the extension of the existing municipal water distribution system. The primary source of supply for the lands will be from the existing 300 mm watermain at Russell Street and the 300mm on Durham Street at Millenium Way.

A preliminary review of the water distribution system was completed and was based on hydrant flow tests undertaken at the intersection of Highway 21 / Durham Street and Highway 21 / Russell Street.

3.1 WaterCAD Model

A WaterCAD model was created in order to analyze the watermain extensions to the development lands. For the purpose of the model, the following assumptions were made:

- Water supply from the existing eastern terminus on Russell Street and from the intersection of Durham Street and Millenium Way are treated as two independent sources. (Note: This is assumed to simplify the model and is assumed to be reasonable because of the relatively high number of connecting watermains upstream of each location.)
- The water supply at each connection location was modelled as a pump, with curve characteristics based on theoretical flow and pressure values calculated from the hydrant flow tests. See below for theoretical flow and pressure values.
- Available flow and pressure in this area is based on no pumps at the WTP operational (i.e., because this was the case during the hydrant tests).

Appendix B provides technical details related to the modelling completed using WaterCAD.

Based on the results of the infrastructure review, the following observations were noted:

- The existing water infrastructure in Kincardine can accommodate the growth of the Business Park lands while maintaining fire flow supply and quantity;
- Pressures within the development area, under most flow demands, typically fall between 250 and 330kPa (36 to 48 PSI). MOE guidelines would suggest that these pressures should preferably be in the range of 350 to 550 kPa (50 to 80 PSI).

- A booster pumping system will be required in conjunction with the later phases of construction to ensure that adequate pressures are provided under development densities. The Municipality should establish pressure monitoring to track system operation as development proceeds to better determine the appropriate timing to construct the pressure boosting facilities.

3.2 Booster Pumping System

Operating pressures in the area of the Russell Street extension, without additional pressure boosting, appear to be higher than other areas of the development lands. This is attributable to the lower ground elevations for this area of the Business Park. It is anticipated that booster pumping facilities would be more advantageous in the area of Millenium Way and Durham Street and could be phased in as part of a pressure monitoring program within the development.

From the results of the hydrant flow testing, it is assumed that the new pressure zone can be continually fed by the existing municipal system at a rate of at least 70 L/s. This is sufficient to meet design average and maximum day demands, and nearly sufficient to meet design peak day demands, assuming that adequate booster pumping is provided within the new pressure zone, but in terms of available supply for fire protection probably represents a "worst case" for storage considerations because it corresponds to maintaining a residual pressure of 300 kPa in the existing system, which is significantly higher than the 140 kPa minimum allowable under fire conditions. The "best case" for minimizing storage requirements corresponds to having 190 L/s available from the existing system.

From the 2008 MOE Design Guidelines for Drinking-Water Systems Table 8.1, at a design fire flow of 150 L/s, the storage requirement is based on a duration of between 2 and 3 hours. For the purposes of this analysis, a 2.5 hour storage requirement has been assumed.

Based on the calculations summarized in Appendix B, under the "worst case" scenario approximately 1200 m³ of storage is required while under minimum storage design conditions, no storage would be required.

It is recommended that the need for storage be re-evaluated as the initial phases of development proceed and the actual development demands become apparent.

3.3 Distribution System

As shown on Figure WM1, the proposed watermain distribution system will be installed within the proposed road allowance throughout the development area with sizing ranging from 150mm to 300mm.



Legend

- 1 Area Identification - Water Demand
- Water Demand Areas

- 200 Watermain and Pipe Diameter (mm)
- Proposed Booster Pumping Station



Municipality of Kincardine
Kincardine Business Park
 Servicing - Water
 Detailed Area Plan -
 Proposed Watermain Layout

DATE June 2016	PROJECT No. 08055
SCALE 1:4,000	FIGURE No. WM1

4.0 SANITARY SERVICING

The purpose of this portion of the study is to review the ability of the existing sanitary sewer collection system, in the Park Street Pumping Station tributary area, to receive flows from the proposed Business Park.

There are two potential corridors available for sanitary outlet from the Business Park area:

- Durham Street – Existing sanitary sewer connection.
- Russell Street – Proposed sanitary sewer connection.

Both corridors are within the same tributary area of the Park Street Sewage Pumping Station and both routes ultimately meet at the Scott Street portion of the sewer system.

Historical study work completed for the area, and further confirmed through the analysis summarized herein, determined that sanitary sewage flows for the remainder of the Business Park area would be better directed to a new sewage outlet along Russell Street to Scott Street as capacity in the downstream portion of the Durham Street corridor is limited.

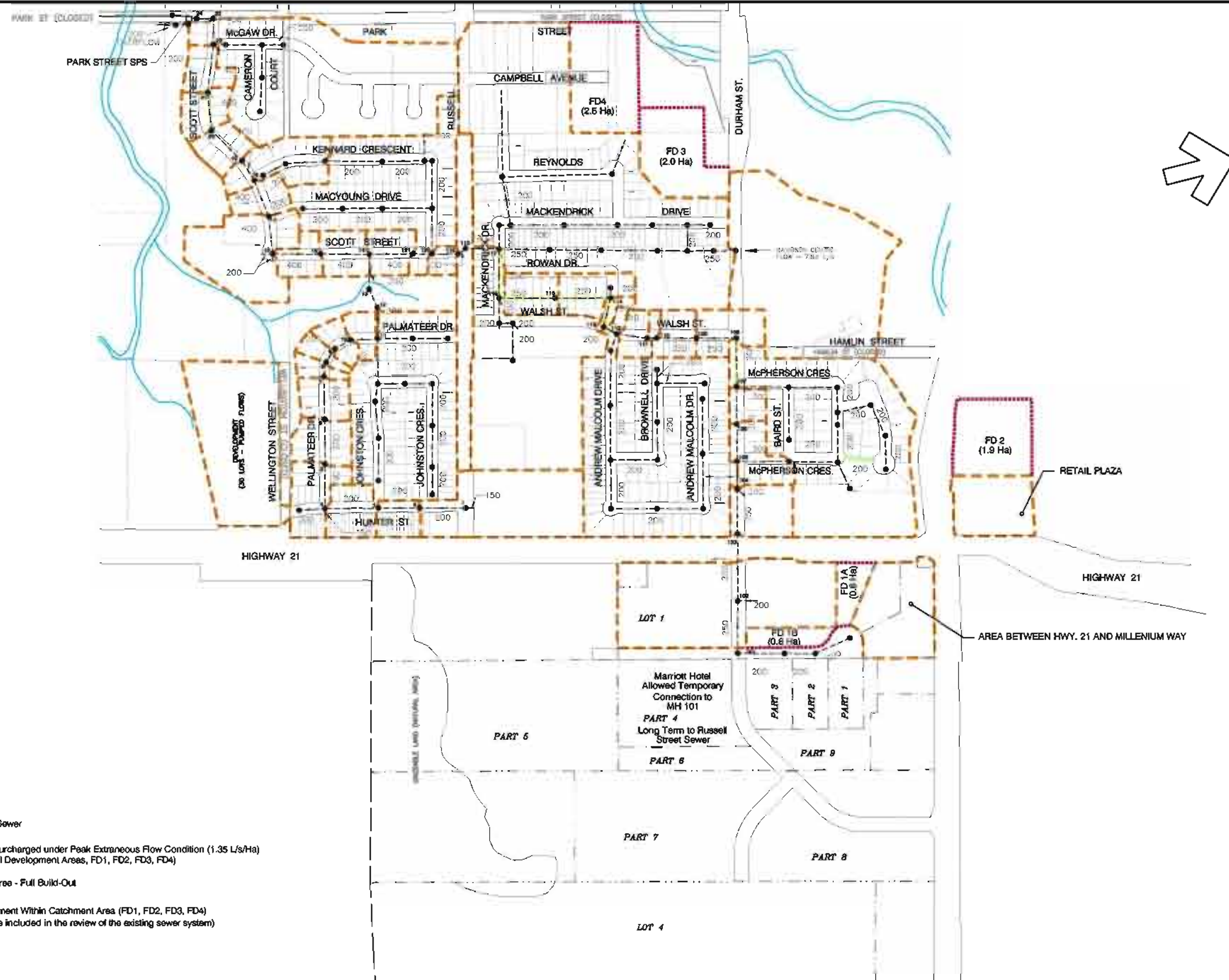
Given the capacity limitations of the Durham Street corridor, any further development requests, beyond what is currently connected to the Durham Street sewer should be considered on a case by case basis.

The following summarizes the existing and proposed data and provides the necessary technical evaluation in support of the use of the Park Street sewage system.

4.1 Existing Collection System

The existing sanitary sewer collection system for the Park Street tributary area was constructed in the 1970s to service the expanding residential growth in Kincardine. At the time, no consideration for an expanded service area, beyond the Highway 21 corridor, was included in those original designs. Figure SA1 shows the current service area that is tributary to the Park Street system. At this time the existing collection system services, in addition to the residential development, the following:

- Davidson Recreation Centre, two schools, one church
- Commercial development along the westerly side of Highway 21
- Business Park development consisting of Canadian Tire, Tim Horton's, Sobey's, a bank, Holiday Inn Express, Boston Pizza, and dentist office.
- Currently under construction and not yet contributing sewage is a proposed carwash and the new Marriott Hotel. The Marriott hotel sanitary sewage connection to the Durham Street outlet is considered temporary until such time that additional sanitary sewer extensions may be completed to the Russell Street corridor.



Legend

- MH Numbering
- Existing Sanitary Sewer
- Existing Sewers Surcharged under Peak Extraneous Flow Condition (1.35 L/s/Ha) (Includes Potential Development Areas, FD1, FD2, FD3, FD4)
- Existing Service Area - Full Build-Out
- Potential Development Within Catchment Area (FD1, FD2, FD3, FD4) (These areas were included in the review of the existing sewer system)

	Municipality of Kincardine Kincardine Business Park Servicing - Sanitary		DATE June 2016	PROJECT No. 08055
	Existing Conditions and Associated Drainage Areas		SCALE 1:7,500	FIGURE No. SA1

4.2 Existing Collection System Sewage Flows

Existing sewer capacities are assessed by comparing the actual carrying capacity of the various sewer sections to the expected peak flow rates that must be conveyed in these sections. For the existing Park Street sewage pumping station drainage area the total sewage flows are comprised of:

- A domestic sewage flow component. (Residential and Commercial); and an
- Extraneous sewage flow (infiltration and inflow) component.

For the purpose of this investigation, peaked values for the various sewage flow components have been calculated on an area flow basis in litres per second per hectare (L/s/ha) based on calculations summarized below.

4.3 Sewage Flow Data

In 2011, a review of the sanitary sewage system was completed based on sewage flow data from the late 2000's. This information is presented below in Table 1A:

Table 1A
Sewage Flow Data for 2006 to 2009

Year	Pumped Volume m³	Average Day m³/day	Max. Day m³/day
2006	350577	960	3177
2007	299313	820	4536
2008	392465	1075	6454
2009	326686	895	5053
Avg.	340,000	940	6454

For comparison purposes, sanitary sewage data for more recent years was reviewed and summarized below in Table 1B:

Table 1B
Sewage Flow Data for 2012 to 2015

Year	Pumped Volume m³	Average Day m³/day	Max. Day m³/day
2012	322,163	880	2294
2013	345,870	949	9012
2014	344,601	943	3121
2015	293,944	806	2234
Total	325,000	895	9012

Based on a review of the above it is evident that the average day flow has not changed significantly from past years of record. A high flow event was recorded however in 2013 that exceeded the event recorded in 2008.

4.4 Existing Domestic Sewage Flows

A domestic sewage flow component is defined as the total wastewater flow exclusive of any extraneous (infiltration/inflow) component.

From the data provided in Table 1A and 1B, a domestic sewage flow component of approximately 900 m³/day seems to be an appropriate average day flow for the more recent years of record considered.

4.5 Existing Maximum Extraneous Sewage Flows

Based on the above information, maximum day flow events were observed in 2008 (January thaw/rain event) with a value of 6454 m³/day (75 L/s) and in 2013 (January thaw/rain event) with a value of 9012 m³/day (104 L/s). As reported by Kincardine Operation staff, during the 2008 event it was necessary to run 3 pumps to avoid a bypass.

The Operation staff noted that events, such as the one in 2013, have occurred where 3 pumps have not been able to keep up with the peak flow and a "bypass" resulted. During these "bypass" events, the recorded data does not accurately represent the max. daily flow as the wetwell transducer (during the submerged period) will not accurately record the wetwell volume during the bypass period.

Given the above information, the most reliable data available is the January 2008 event where a bypass almost occurred but did not. However, in order to provide a conservative approach to the evaluation of the sewage collection system it is suggested that the flow event from the 2013 data be used to estimate the peak flow for the existing tributary area.

The total drainage area tributary to the Park Street SPS, near the end of 2015, was in the order of 100 Ha.

For the sake of round numbers the following values are suggested:

- Average Domestic Sewage Flow = 900 m³/day
- Peak Extraneous Flow Value = 9000 m³/day

As part of the recommendations of this study, the Municipality should complete an investigation to determine (where possible) the source(s) of the extraneous flow and reduce or eliminate the source, where possible.

4.6 Existing Total Sewage Flows – Calculation of Area Flow Rate Extreme Extraneous Flow Conditions

Using the values stated above, an existing total peak sewage flow value can be calculated for the existing drainage area as follows:

$$Q \text{ peak (L/s/ha)} = \frac{(\text{Avg. Domestic Q} \times 4.0) + (\text{Max Extraneous Q}) \times 1000}{(\text{Drainage Area (ha)} \times 24 \times 60 \times 60)} \times \frac{1000}{1}$$

Where:

$$\text{Average Domestic Sewage Flow} = 900 \text{ m}^3/\text{day}$$

$$\text{Domestic Peak Factor} = 4.0 \times \text{Avg.}$$

$$\text{Total Peak Extraneous Flow Value} = 9000 \text{ m}^3/\text{day}$$

$$\text{Drainage Area} = 100 \text{ Ha}$$

$$\begin{aligned} \text{Max Extraneous Q} &= \text{Recorded high max day} - \text{Avg. Domestic day} \\ &= 9000 \text{ m}^3/\text{day} - 900 \text{ m}^3/\text{day} \\ &= 8100 \text{ m}^3/\text{day} \end{aligned}$$

Therefore:

$$\begin{aligned} Q \text{ peak (L/s)} &= \frac{(900 \times 4.0) + (8100)}{100 \times 24 \times 3600} \times \frac{1000}{1} \\ &= \mathbf{1.35 \text{ L/s/ha}} \text{ (Based on existing flow information)} \end{aligned}$$

By comparison, standard MOECC Design Guidelines for sewage flow in L/s/ha would be calculated as follows:

$$Q \text{ peak (L/s/ha)} = \frac{\text{Avg. Domestic Q} \times 4.0}{1 \text{ ha} \times 24 \times 60 \times 60} + \text{Extraneous Q allowance}$$

Where:

$$\begin{aligned} \text{Avg. Domestic Q} &= 450 \text{ L/capita/day} \times 40 \text{ persons/ha} \\ &= 18,000 \text{ L/day/ha} \end{aligned}$$

$$\text{Domestic Peak Factor} = 4.0 \times \text{Avg.}$$

$$\text{Max Extraneous Q} = 0.2 \text{ L/s/ha}$$

Therefore:

$$\begin{aligned} Q \text{ peak (L/s)} &= \frac{18,000 \times 4.0}{1 \times 24 \times 3600} + 0.2 \\ &= \mathbf{1.03 \text{ L/s/ha}} \text{ (Based on MOECC design guidelines)} \end{aligned}$$

From the above calculation, it can be seen that the recorded domestic and peak extraneous flows are in the area of 30% more than standard MOECC design guidelines. This demonstrates the significance of the high extraneous flow events on the calculation of remaining sewer capacity and the need for the municipality to be vigilant in pursuing the reduction of these extraneous flows.

For the purpose of this report the unit peak flow rate of 1.35 L/s/ha will be used in capacity considerations and the evaluation of sewer and pipe capacities.

4.7 Existing Collection System

The existing collection system for the Park Street Pumping Station has been analyzed assuming that the tributary area has been built-out. Total peak sewage flows have been applied to the system based on the unit peak flow rate of noted above. The evaluation of the existing system includes the following:

- Existing Tributary Area: 100 Ha
- Area FD1A: 0.6 Ha (Area immediately north of Canadian Tire)
- Area FD1B: 0.6 Ha (Proposed Carwash site)
- Area FD2: 1.9 Ha (Residential west of Liquor Store Retail plaza)
- Area FD3: 2.0 Ha (Possible Residential west of MacKendrick Dr.)
- Area FD4: 2.5 Ha (Planned Residential at north end of Campbell St.)

Future development areas, to the east of Millenium Drive, within the Business Park, have not been included in this analysis as the purpose of the review was to determine what areas of the sewer system do or do not presently have available capacity.

Appendix C includes the existing sanitary sewer design sheets for the drainage areas noted on SA1 and identifies the design flows under current peak domestic and the maximum extraneous flow event discussed above.

4.7.1 Existing System Analysis and Areas of Concern

Assuming build-out of the current tributary area, and inclusion of areas FD1 to FD4, Figure SA1 identifies the existing sewers which will theoretically experience surcharging. These areas are identified as follows:

- Scott Street (21-22):

This single section of sewer is predicted to have minor surcharging that is less than 100 mm above the top of the pipe. The sewer is at a depth of over 5.0 m in this location and the calculated amount of surcharging should not negatively impact the system.

- Walsh and Mackendrick (115-117):

This section of sewer is predicted to have minor surcharging ranging from 200 mm to 300 mm above the top of pipe. As the sewer is at a depth ranging from 3.8 m to 6.0 m the surcharging is not expected to negatively impact development that are connected to the pipe.

- Durham Street (107-108):

This single section of sewer is predicted to have minor surcharging that is less than 200mm above the top of the pipe. As the sewer is at a depth of over 3.6 m in this location the calculated surcharging should not negatively impact the system.

4.7.2 Existing System Observations and Opportunities

Based on the analysis and modelling of the existing system, the following observations and opportunities are summarized:

- The Durham Street sewer is not of sufficient depth to provide sanitary outlet for the southerly half of the Business Park lands.
- It is suggested that areas beyond those identified on Figure SA1 be excluded from the Durham Street sanitary sewer corridor so that the limited capacity available on Walsh and Mackendrick is not reduced further.
- The existing sewer on Scott Street is at a depth ranging from 3.2 m to 7.5 m and as such some degree of surcharging within this section of sewer (structures 118 to 121 and structures 14 to 24) can be tolerated.

Following a review of the above observations, the preferred and most practical means of servicing the Business Park area appears to be through the construction of a new trunk sewer along Russell Street, from Highway 21 to Scott, with outlet to the existing sanitary sewer at the Russell and Scott Street intersection.

The Municipality of Kincardine completed the design of this sewer in 2005 and received MOECC approval for the construction from Scott Street to east of Highway 21 at that time. Unfortunately, the approval contains a construction window which limits its validity to only 5 years. Since the sewer has not been constructed an amendment application in the future will be necessary to allow construction of the Russell Street sewer to proceed.

Given the contemplated development densities for the Business Park, additional assessment was undertaken, as part of this study, to review the impact of adding sewage flow to the Scott Street sanitary sewers and the Park Street sewage pumping station. The following provides details related to this review.

4.8 Scott Street Sewer – Impact from Business Park

4.8.1 Business Park Design Flows

Review of design flows for the full development of the Business Park are based upon MOECC guidelines. It is recognized, however, that the MOECC guidelines may be conservative given that the possible uses within the Business Park area may ultimately consist of “dry” type industry and big box shopping centres which typically do not generate significant sewage amounts.

The Business Park is to consist of a mix of various development types including the following:

- Residential (R)
- Highway Service Commercial (HSC)
- Large Format Commercial (LFC)
- Light Industrial (LI)

Sewage Criteria for each development type is summarized below:

Residential Population Density = 35 ppHa
 Residential Sewage Flow = 450 L/cap/day

Land Use	Average Sewage Flow	Peaking Factor	Infiltration Allowance
R	0.18 L/Ha/s	Harmon	0.2 L/Ha/s
HSC	0.28 L/Ha/s	2.0	0.2 L/Ha/s
LFC	0.28 L/Ha/s	2.0	0.2 L/Ha/s
LI	0.35 L/Ha/s	3.5	0.2 L/Ha/s

Figure SA2 provides an illustration of the various development types and areas within the Business Park areas as well as the limit of the current tributary area.

The stages referred to herein should not be confused with suggested phasing. The development stages have been defined as a way to define the tributary areas considered as part of the collection system analysis and were somewhat arbitrarily established.

A summary of the possible future development areas (as illustrated in Figure SA2) are summarized below:

- Stage 1A

Represents the remaining potential development areas that are immediately adjacent to, or within, the current tributary drainage area for the Park Street SPS.

- Stage 1B

Represents the most westerly half of the Business Park that is not yet developed.

- Stage 2

Stage 2 is represented by the easterly half of the Business Park lands.

- Stage 3

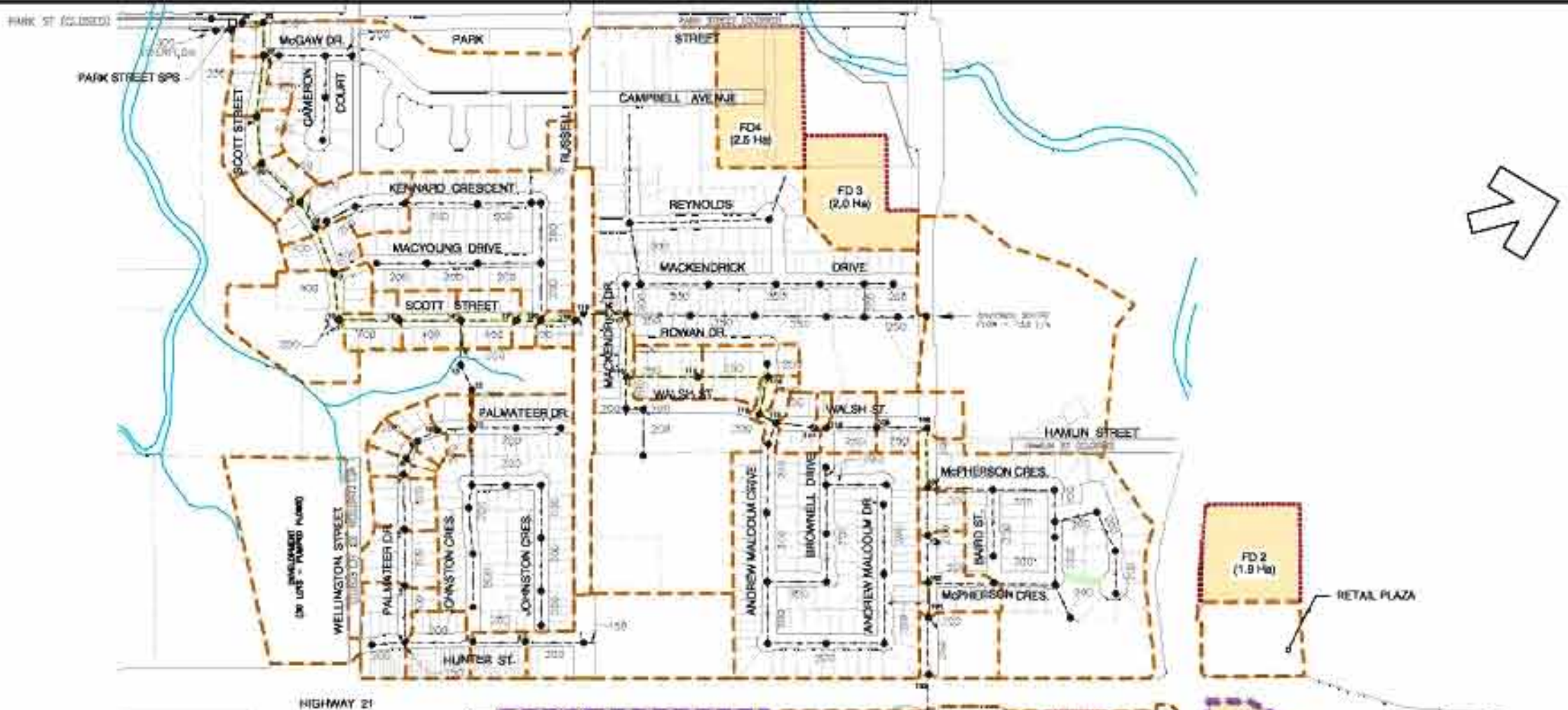
Stage 3 represents the area north of Highway 9 which is currently not included in the official plan area of the Municipality. This area was included in the collection system review to determine the feasibility of including it in the tributary area of a new sewer.

A detailed summary of the development types that each Stage is comprised of is summarized below in the following table:

Stage	Development Type (Ha)				Summary (Ha)
	R	HSC	LFC	LI	
1A	6.4	1.2	0.0	0.0	7.6
1B	2.2	15.1	16.3	0.0	33.6
2	0.0	9.7	2.2	20.8	32.7
3	0.0	7.6	7.6	7.6	22.9
Total	8.6	33.6	26.1	28.4	96.8

Given the above areas and the development types, the following peak sewage flows are estimated for each area:

Stage	Total Additional Flow to Park St. SPS	
	Incremental Flows L/s	Note
Stage 1A	7.0	Flows to Outlet upstream of Scott St. and Russell St.
Stage 1B	26.0	Flows to Russell St. Sewer
Stage 2	31.0	Flows to Russell St. Sewer
Stage 3	20.0	Flows to Russell St. Sewer



Legend

- 105 M4 Numbering
- Existing Sanitary Sewer
- Existing Sewers Surcharged under Peak Extraneous Flow Condition (1.35 L/s/M²)
- Existing Service Area - Full Build-Out
- Stage 1A - Potential Development Within Tributary Area (FD1A, FC1B, FD2, FD3, FD4)
- Stage 1B Development
- Stage 2 Development
- Stage 3 - Possible Future Drainage Area - Reviewed for impacts to system only
- Area resulting in acceptable surcharging levels on Scott Street
- Area resulting in unacceptable surcharging levels on Scott Street
- Existing Trunk Sewer with more than 10% Remaining Capacity
- Existing Sewers Approaching Capacity
- Existing Sewers Surcharged



Municipality of Kincardine
Kincardine Business Park
 Servicing - Sanitary
 Future Conditions - Stage 1, 2, 3
 and Associated Drainage Areas

DATE June 2016	PROJECT No. 08055
SCALE 1:7,500	FIGURE No. SA2

4.8.2 Capacity Analysis

Appendix C includes a copy of the sanitary sewer design sheets prepared to review the impact of adding the incremental stages, summarized above, as noted on Figure SA2.

4.8.3 Development of Stage 1B

Under this scenario it is assumed that the existing tributary area is built-out in addition to the first half of the future business park lands that are not yet developed. These future flows are to be conveyed within the new sanitary sewer on Russell Street.

The addition of the predicted flows from Stage 1B of the Business Park area will result in most of the Scott Street sewer surcharging beyond what it currently experiences under wet weather flow conditions. Existing sanitary sewers from structure 14 to 22 range in depth from 3.4 to 7.5 metres. The surcharge depths correspondingly range from 0.1 metres to 0.5 metres above the top of the existing pipe. The resultant theoretical surcharge levels are not considered significant given the depth of the sewer system.

The addition of Stage 1B development can be accommodated in the Scott Street sanitary sewer.

4.8.4 Development of Stage 2

Under this scenario it is assumed that the Stage 1A and Stage 1B lands have been developed in addition to Stage 2 which complete the development of the Business Park. These future flows would be conveyed within the new sanitary sewer on Russell Street to its outlet at Scott Street. Predicted flows from Stage 1A, 1B and Stage 2 of the Business Park area will result in all of the Scott Street sewer surcharging beyond what it currently experiences under wet weather flow conditions. Existing sanitary sewers from structure 118 to 120 and from structure 15 to 24 will have acceptable surcharge depths that in theory do not come within 2.5 metres of the finished ground. Existing sanitary sewers from structure 120 to 15 are somewhat shallower with depths between 3.2 and 4.2 metres. This section of sewer may experience surcharging depths that in theory could be within 2.5 metres of the finished ground. It is recommended that monitoring of these locations be completed near the end of build-out of Stage 2 and the Business Park.

Stage 1 and Stage 2 of the Business Park area will theoretical contribute a combined sewage flow of about 59 L/s to the Park Street system and will require a 300mm sanitary sewer on Russell Street installed at a minimum grade of 0.5%.

4.8.5 Addition of Stage 3

Under this scenario about 27 Ha more of developed land area will be added beyond the Stage 1B and Stage 2 development from the north side of Highway 9. Predicted flows from all three stages of development will result in a greater level of surcharging than what would be acceptable. Theoretical depths of surcharging on Scott Street range will come within 0.5 metres of the finished grade in the shallower sections of the sewer.

The possibility of basement flooding with the inclusion of the Stage 3 area is very high along several sections of Scott Street and possibly some branch sewer sections. In order to accommodate the future Stage 3 lands, the existing sewers on Scott Street would require upgrading or an alternative relief sewer would need to be installed to remove sewage flow from the Scott Street sewers. It is understood that the soil and water table conditions in the area of Scott Street would significantly complicate construction activities and possible future sewer replacements if the Stage 3 area was to be considered.

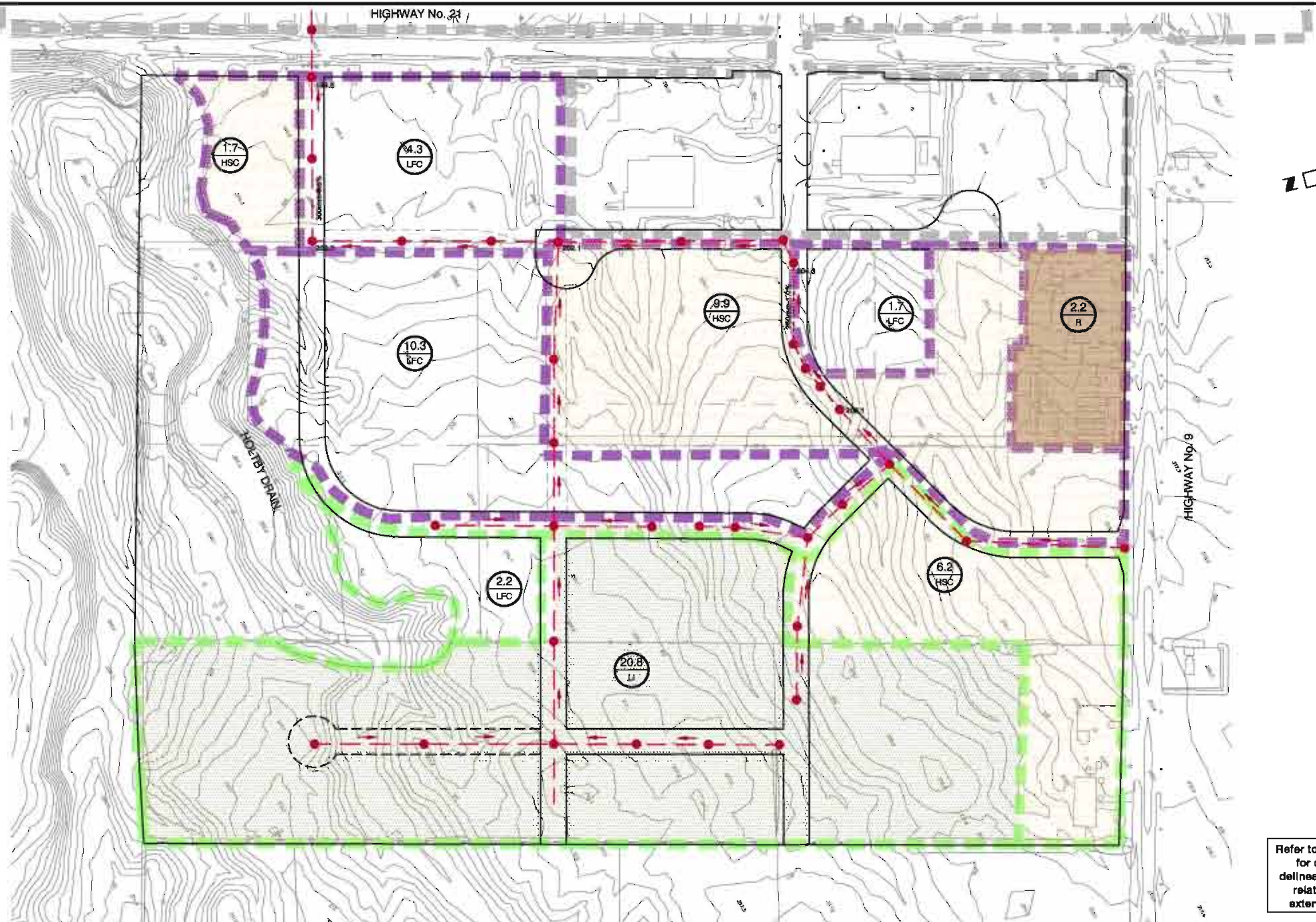
Based on the forgoing, the Municipality may wish to incorporate capacity into the proposed Russell Street Sewer and the internal pipe network of the Business Park with the understanding that Stage 3 could only proceed in the future following long term monitoring of the sewage flows within the Scott Street Sewer and/or the upgrade of the Scott Street system at some point in the future.

4.8.6 Summary of Collection System Review

It is recommended that the Municipality proceed with the construction of the Russell Street sanitary sewer as follows:










- Allow the additional development on the remaining northerly part of lot 1 to proceed with the Durham Street sewer outlet
- Consider on a case by case basis to allowing some of the future development along Millenium Way with access to the Durham Street sewer outlet.
- Construct or have constructed the Russell Street trunk sewer to provide access to the Business Park lands.

Figure SA3 shows the potential location of sanitary sewer route in the business park area.



Refer to Figure SA2 for drainage delineation details related to the external areas.

Legend

- | | | |
|--|--|--|
|  Highway Service Commercial |  Light Industrial |  Stage 1B Development Areas |
|  Large Format Commercial |  Proposed Sanitary Sewer and Invert |  Stage 2 Development Areas |
|  Residential |  Built Sanitary Sewer and Invert |  Existing Servicing Area |



Municipality of Kincardine
Kincardine Business Park
 Servicing - Sanitary
 Detailed Area Plan -
 Proposed Sanitary Sewer Layout

DATE June 2016	PROJECT No. 08055
SCALE 1:4,000	FIGURE No. SA3

4.9 Assessment of Park Street Sewage Pumping Station Capacity

4.9.1 Introduction

The Park Street Sewage Pumping Station was originally designed by BMROSS and constructed in 1976. The station was sized based on population values provided at the time by the upstream land developer.

The station is a drypit/wetwell configuration with 3 pumps in total (2 pumps in parallel providing the required capacity). The station drypit/wetwell are constructed below the control building which houses the existing 75 kW generator. All three pumps are Fairbank Morse Series 5443-32, 22.4 kW (30 Hp).

The station pumps directly to the headworks of the Kincardine sewage treatment plant through approximately 1,200 metres of 300mm dia. forcemain. A portion of the existing forcemain was installed under the Penetangore River.

4.9.2 Calculation of Existing Peak Sewage Flow to Station under Extreme Extraneous Flow Conditions

Based on the 2013 peak flow event it is estimated that the upon occasion, the pumping station sees wet weather peak flow of approximately 115 L/s. It is noted that this value assumes a 10% uncertainty factor.

Based on the expected peak sewage flow and current pump capacities, it is therefore evident that the inflow rates to the Park Street pumping station are exceeding the stations firm capacity (two pumps) under an extreme extraneous inflow period as on several occasions the operation of all 3 pumps has been required and still has not averted a bypass situation.

4.9.3 Calculation of Proposed Peak Sewage Flow to Station with Business Park Areas Included

The anticipated cumulative peak sewage flow to the Park Street Sewage Pumping Station is estimated as follows:

- Existing 115.0 L/s
- Stage 1A 122.0 L/s
- Stage 1B 148.0 L/s
- Stage 2 179.0 L/s
- Stage 3 199.0 L/s

4.10 Drawdown Testing

Drawdown testing to determine current pump capacities was conducted on April 14, 2008 which revealed the following pump operating conditions.

- Pump 1 60 L/s
- Pump 2 59 L/s
- Pump 3 55 L/s
- Pump 1 and Pump 2 85 L/s
- Pump 2 and Pump 3 82 L/s
- Pump 1 and Pump 3 82 L/s

4.11 Pumping Station Improvements

It is acknowledged that pumping station improvements are required as the development of the Business Park proceeds.

Three basic alternatives with possibilities for staging to increase the capacity of the existing pumping station to meet the cumulative peak sewage flow received at the Park Street SPS were identified and evaluated. These were:

- Install larger pumps in the existing dry pit and use the existing forcemain.
- Retain the existing pumps and twin the existing forcemain.
- Install larger pumps and twin the existing forcemain to maximize station capacity.

Detailed calculations related to the review of the station capacity and upgrade possibilities are included in Appendix D.

4.11.1 Alternative 1 – Install Larger Pumps in the Existing Dry Pit and Use the Existing Forcemain

Revised station capacity: 155 to 190 L/s (depending on motor size selected)

Probable option cost: \$840,000 to \$960,000

Discussion:

- This would involve replacing all three existing pumps with 63 kW (85 Hp) to 78 kW (105 Hp) units and will increase the capacity by 90 to 130% depending on which pump is selected.
- A substantial increase in the discharge pressure is required to move the greater flows through the existing forcemain. This results in greater power costs for operation and increased risk of forcemain failure.
- The existing standby power system will not be adequate for the larger pumps and will need to be replaced with a larger unit.

- VFD control of the larger pumps will be required to avoid excessive cycling and to maintain forcemain velocities to within the range suggested by the MOE in their guidelines.
- Modifications to the power supply and pump control system will likely be required under this option which given the age of the station is probably an appropriate maintenance upgrade at this time.

4.11.2 Alternative 2 – Retain Existing Pumps and Twin the Existing Forcemain

Revised station capacity: 115 L/s
Probable option cost: \$960,000

Discussion:

- This option involves installing a second 300mm diameter forcemain from the existing pumping station to the existing inlet structure at the lagoons. A second forcemain will allow two of the three pumps to pump through its own forcemain. This should allow each of the pumps to deliver its full single-pump capacity when operating in parallel. This would then give a station capacity of around 115 L/s. It is noted that twinning the forcemain alone does not provide sufficient capacity to accommodate the future business park development.
- Operation in this manner would mean that there would be no electrical or standby power upgrade requirements under this option.
- Modifications will be required to the existing bypass valve chamber and the lagoon inlet chamber to accommodate the second forcemain.
- Capacity could be increased further through pump replacement (see Alternative 3)

4.11.3 Alternative 3 – Replace Existing Pumps and Twin the Existing Forcemain

Revised station capacity: 230 L/s
Probable option cost: \$1,920,000

Discussion:

- This is a combination of the previous options which will maximize station capacity by replacing the existing pumps with three new pumps, each having a capacity of 115 L/s, and twinning the existing forcemain. This will give a firm station capacity of 230 L/s, with one pump acting as standby.

- Cost is high relative to the increase in station capacity that can be achieved through a straight pump replacement.

Considering the upgrade options contemplated, Alternative 1 is preferred. It allows capacity to be staged by changing the pump motor size and has less environmental impact than the forcemain twinning associated with Alternative 2 or 3.

4.12 Summary

Portions of the sewage collection system are at or near capacity under existing wet weather sewage flow conditions.

Allowing significant flows to the Durham Street outlet would result in replacement of numerous sections of sewers throughout the collection system both on the Durham Street and Russell Street outlet.

It is recommended that a Russell Street trunk sewer be constructed from Scott Street easterly to provide collection for flows from the Business Park area east of Highway 21 and south of Highway 9.

Based on the expected peak sewage flow, current pump capacities of the Park Street SPS, and occasional by-pass events, it is evident that the inflow rates to the Park Street pumping station are at times beyond the stations firm pumping capacity and requires upgrade to accommodate any significant additional flows. As summarized above, the following alternatives were considered:

- Install larger pumps in the existing dry pit and use the existing forcemain.
- Retain the existing pumps and twin the existing forcemain.
- Install larger pumps and twin the existing forcemain to maximize station capacity.

The installation of larger pumps and pumping through the existing forcemain appears to be the most practical means of increasing the pumping capacity of the Park Street SPS and will provide the benefit of upgrading the existing pump control and communication system with current more modern technology.

5.0 STORMWATER MANAGEMENT

In conjunction with the development of the Kincardine Business Park, The Municipality of Kincardine is proposing the construction of stormwater management facilities to control the stormwater runoff from the proposed development area.

Two new facilities will be required which have been designed as water quality and quantity treatment ponds (wet pond facilities) in accordance with the “Stormwater Management Planning and Design Manual” by the MOE, dated March 2003 and the requirements of the Saugeen Valley Conservation Authority (SVCA) and the Ministry of Transportation.

5.1 Existing Conditions

5.1.1 Site Topography and Soils

The site can be described as moderate sloping with underlying soils identified as being a Berrien Sandy Loam (Bes) and Perth clay loam (Pc) as classified under the hydrologic soil group “B-C”. Both these soils are further described as imperfectly drained soils.

5.1.2 Pre-Existing Drainage Conditions

Existing drainage for the general watershed area is typically in an east-west direction towards the Highway No. 21 road corridor.

The proposed Business Park is traversed by a series of main catchment groups (including the Holtby Drain) that convey flows to one of two separate outlet locations under Highway No. 21:

A) 1500mm CSP Culvert

This culvert is located at the upstream end (under Highway No. 21) of the storm sewer system along the north limit of the school property. The total drainage area tributary to this outlet is about 82 Ha.

B) 5790 x 3650 mm Multi-Plate Arch

This large multi-plate structure is located on a tributary of the Penetangore River, immediately south of the Business Park. The total drainage area upstream of this outlet is about 1840 Ha.

It is recognized that an area of commercial development exists along the Highway 21 corridor from Highway 9 southerly for about 600 meters and spans from Highway 21 to Millenium Way. These development areas have their own existing runoff control measures that have been designed, approved, and constructed through the appropriate planning process.

In order to adequately compare the original conditions that the two Highway 21 outlets would have been designed for, the pre-development hydrologic modeling has been prepared assuming that the existing commercial area was not developed.

The main catchment groups that traverse the business park lands, and their corresponding sub-catchment areas, are summarized below:

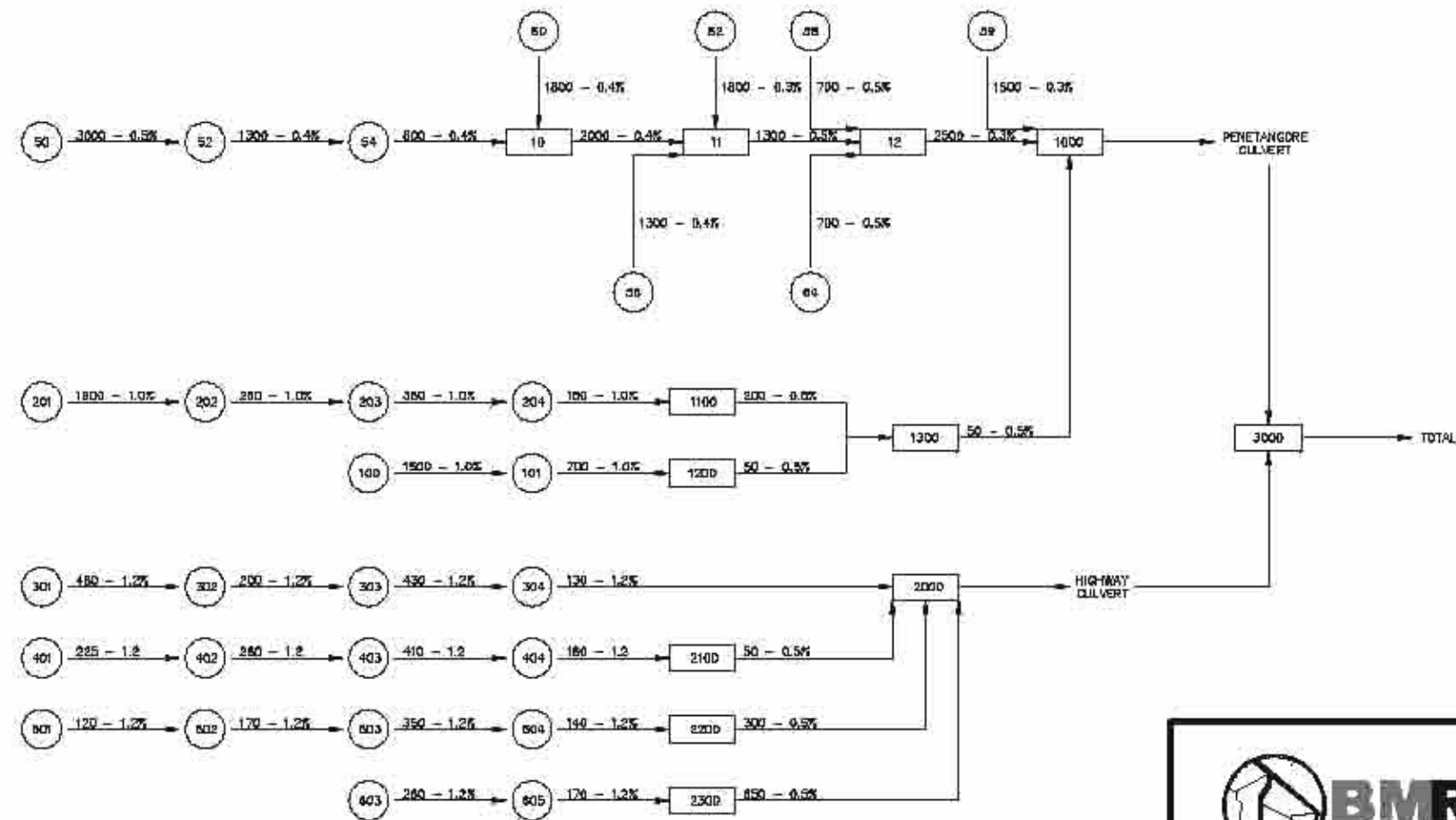
Outlet Location A – 1500mm CSP Culvert

The catchment group consisting of drainage areas 301, 302, 303, 304, 401, 402, 403, 404, 501, 502, 503, 504, 603, and 605 discharge to the Highway 21 corridor ditch and to outlet location A (1500mm CSP Culvert).

Outlet Location B – 5790 x 3650 mm Multi-Plate Arch

The catchment group consisting of drainage areas 50, 52, 54, 56, 58, 59, 60, 62, 64, 100, 101, 201, 202, 203, 204 discharge to the Highway 21 Multi-Plate Arch on the tributary of the Pentangore. Catchments 201 through 204 represent the drainage limits for the Holtby Drain and total approximately 194 Ha.

Figures ST1 and ST 2 illustrate the pre-existing drainage features for the area.



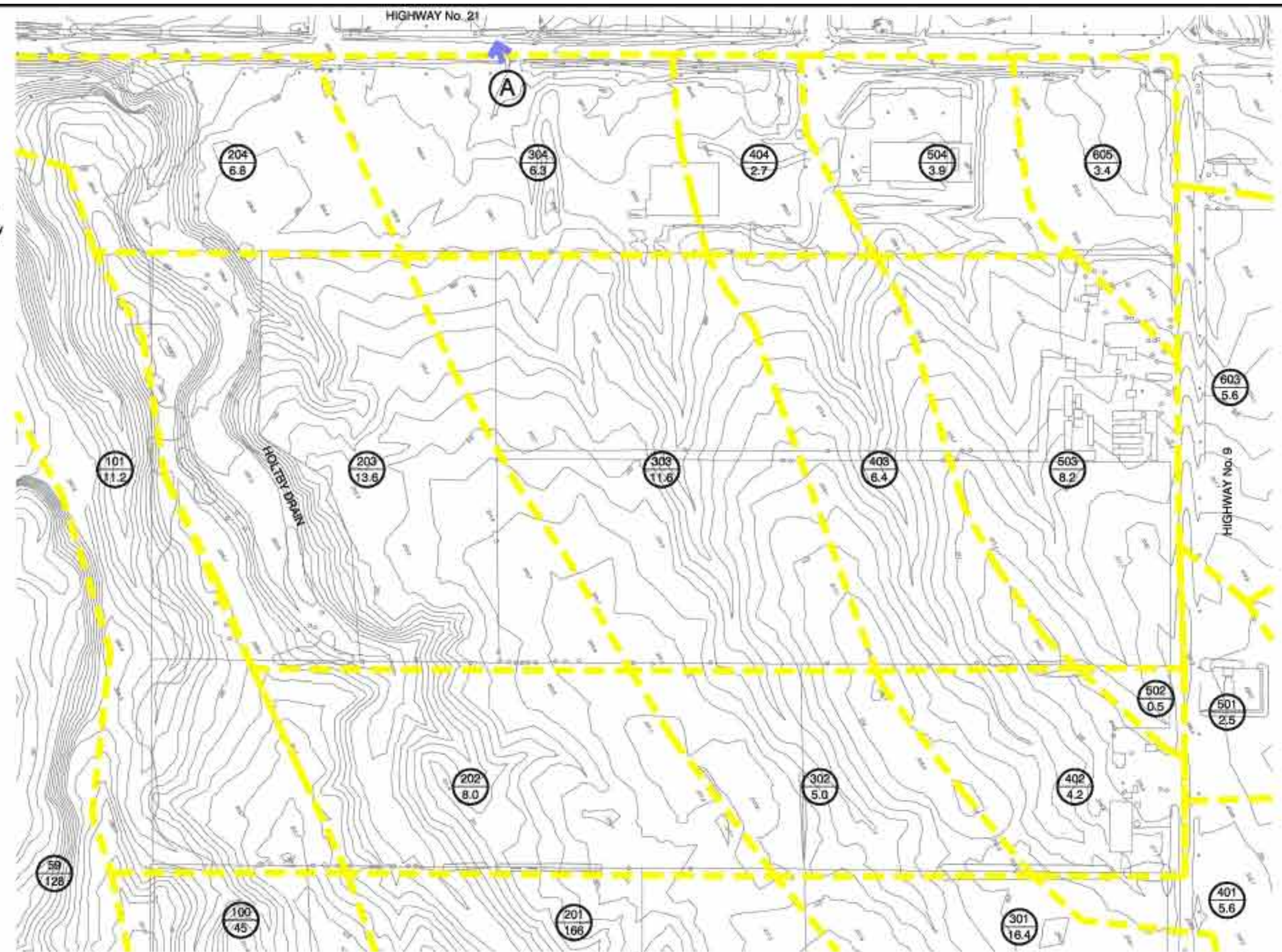
- Legend**
- Pre-Existing Drainage Catchment Areas
 - Delineation of Primary Catchment Groups
 - Existing Open Channel Drain
 - Miduss Drainage Catchment (I.D. / Area in Hectares)
 - Catchment Area / I.D.
 - Conveyance (Channel / Pipe)
 - Confluence Location

BMROSS engineering better communities	Municipality of Kincardine Kincardine Business Park Servicing - Stormwater Management	DATE June 2016	PROJECT No. 08055
	Pre-Existing Drainage Areas and Miduss Modelling Schematic	SCALE 1:35,000	FIGURE No. ST1

(B)

(A)

- Storm Outlets**
- (A) Storm Sewer
1500mm CSP Culvert
 - (B) Penetangore Tributary
5790 x 3630mm Arch
Culvert (Multi-Plate)



Legend

- Pre-Existing Drainage Catchment Areas
- Midusa Drainage Catchment
(I.D. / Area in Hectares)

Refer to Figure ST1
for drainage
delineation details
related to the
external areas.

**Municipality of Kincardine
Kincardine Business Park**
Servicing - Stormwater Management
Detailed Area Plan -
Pre-Existing Drainage Areas
and Midusa Modelling Schematic

DATE June 2016	PROJECT No. 08055
SCALE 1:4,000	FIGURE No. ST2

5.2 Stormwater Management Criteria

The stormwater management plan for the Kincardine Business Park has been developed to minimize any impacts to the downstream drainage systems and watercourses.

The stormwater management criteria for the area has been developed based on previous development proposals and past discussions with the SVCA. The criteria for both Quantity and Quality control measures are summarized below:

5.2.1 Quantity Control Criteria

Provide suitable attenuation storage so that the peak flows are not exceeded. The following locations will be used for comparison purposes:

- i. Holtby Drain (immediately prior to its convergence with the Penetangore tributary)
- ii. Highway 21 Outlet A - CSP culvert (school site)
- iii. Highway 21 Outlet B - Multi-plate Arch culvert (Penetangore tributary)
- iv. Combined Flow at both Highway 21 outlet locations.

5.2.2 Quality Control Criteria

The following summarizes the water quality control requirements for each of the two outlet locations:

- a) 1500mm CSP Culvert – All runoff shall meet MOE “Enhanced” Level criteria (80% TSS removal) prior to discharge to any open watercourse.
- b) 5790 x 3650 mm Multi-Plate Arch – All runoff shall meet MOE “Enhanced” Level criteria (80% TSS removal) prior to discharge to any open watercourse.

All of the above is to be addressed and designed in accordance with the “Stormwater Management Planning and Design Manual” by the MOE, dated March 2003.

5.2.3 Consideration of External Lands

The new stormwater management facilities will provide for quantity and quality control of stormwater discharge from the proposed development areas within the Business Park lands.

Although some of the external drainage areas, generally east of the Business Park, will be conveyed through the proposed stormwater management facilities, the external lands have been modeled in their current state (i.e., agricultural usage) and remain unchanged under the future development conditions. Future development of these external lands will require a further review of stormwater management for each particular area.

5.2.4 Methodology for Computing Stormwater Run-off

Pre and post development modelling was prepared using Miduss V2 (Allen A. Smith Inc., 17 Lyndale Drive, Dundas, Ontario, L9H 3L4) to simulate the following synthetic design storms and rainfall events:

- Goderich 6 hr, SCS Type II for the 1:2 through 1:100 year return periods

The total rainfall data used in the analysis of the plan was derived from the Goderich Weather Station.

Figure Nos. ST1, ST2, ST3, and ST4 include the following key information used in the development of the Miduss models:

- Miduss Model Schematics for the individual catchments for the existing and proposed drainage area conditions;
- Sub-catchment numbers and drainage boundaries for the existing and proposed drainage area conditions.

Additional input parameter and rainfall summary information is provided in Appendix E.

The initial abstraction values used in the Miduss model are based on a calculated value of 0.1s for all drainage areas. The resulting initial abstraction values range from 5.20 to 8.02 mm for the pervious area which is consistent with that recommended in the Miduss model and the MOE Guidelines. The impervious initial abstraction used results in a value of 0.52 mm which is conservative and will result in similarly conservative flow values.

A summary of the curve number (CN) and manning values used in the model are contained within Appendix E along with the model input parameters noted above. The values used are consistent with standard practice.

Miduss modelling results for the existing and proposed drainage area conditions are presented in Section 4.7 and a printed and digital copy of the Output files have been provided in Appendix F.

It is noted that only printed versions of the 1:5, 1:25, and 1:100 flow events have been provided in the Appendix to minimize the report size.

5.3 Stormwater Management Plan

Two new stormwater management facilities are proposed as part of the plan for the Business Park. The possibility of limiting the new facilities to a single pond was reviewed, however, due to topographical and property constraints a single facility was not feasible.

In addition to the two new ponds noted, the existing dry pond (corner of Durham Street and Highway 2, referred to as Pond 1) will be used to control a portion of the development area.

The following describes the proposed stormwater management plan, in more detail, for those drainage areas located within the Business Park. Figure ST4 can be referred to for details related to the noted catchment areas.

5.3.1 Existing Commercial Area (406, 500, 605, 750, 751)

The existing commercial areas identified as catchments 406, 500, 605, 750, and 751 have been constructed with their own stormwater management facilities. Brief details related to the controls provided for each area are summarized as follows:

5.3.1.1 Areas 406, 500:

Runoff from areas 406 and 500 discharge to the existing SWM facility identified as Pond 1. The pond was originally designed and constructed as a dry pond in conjunction with the Canadian Tire development and in recent years was expanded to include the Sobeys grocery store. The pond is located at the south-east corner of the intersection of Highway 21 and Durham Street and it provides basic water quality along with pre to post water quantity control for the noted catchment areas as well as a portion of the currently undeveloped Business Park area. The pond outlets directly to the ditch located within the Highway 21 road corridor.

5.3.1.2 Areas 750, 751:

These areas have been constructed with roof top control devices to limit the discharge rate to the ditch within the Highway 21 road corridor.

5.3.1.3 Area 605:

This is the latest area of development within the existing commercial lands and currently includes a Boston Pizza, a Holiday Inn Express, and a couple other vacant lease buildings. This catchment area has been designed with on-site quality and quantity control facilities which discharge directly to the ditch along Highway 21.

5.3.2 Catchment Area 604

This area is currently developed with a combination of residential and agricultural type buildings and the area has been developed for some time and was never provided with any type of development control. Future development intensification of these lands will need to address potential impacts related to the runoff characteristics generated from the site.

5.3.3 Catchment Area 405

The existing SWM facility (noted as Pond 1) was designed to accommodate runoff from these future development lands. On-site quality controls however, will be required and it is anticipated that quality control can be provided through the installation of oil-grit separators, or similar type treatment devices, on the property. It is anticipated that both major and minor storm runoff events will be conveyed to Pond 1.

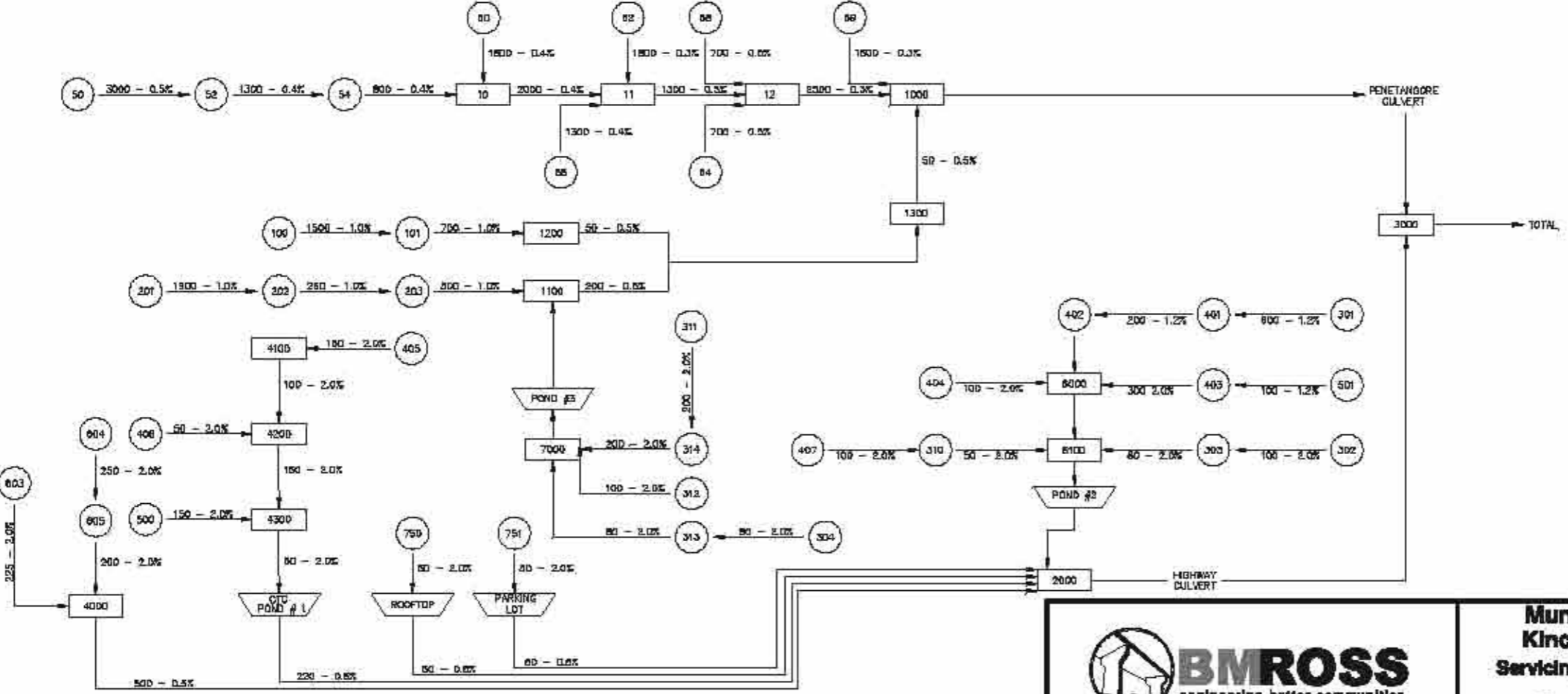
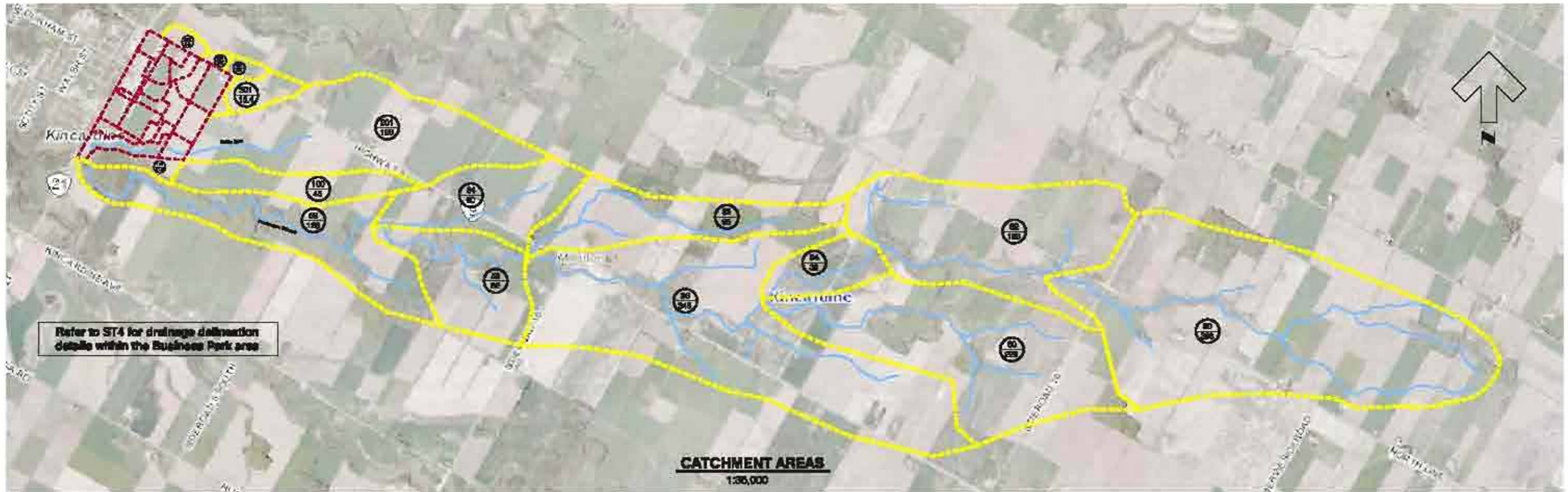
5.3.4 Catchment Areas 302, 303, 310, 402, 403, 404, 407

These future development areas are all tributary to the proposed SWM facility noted as Pond 2. The proposed pond has been designed as a wet pond with forebay and main pond features summarized in more detail in later sections of this report. The pond is to outlet into the Highway 21 ditch. As noted, the external lands tributary to Pond 2 have been included in the design based on their current development levels (i.e., 0% impervious).

5.3.8 Catchment Areas 304, 311, 312, 313, 314

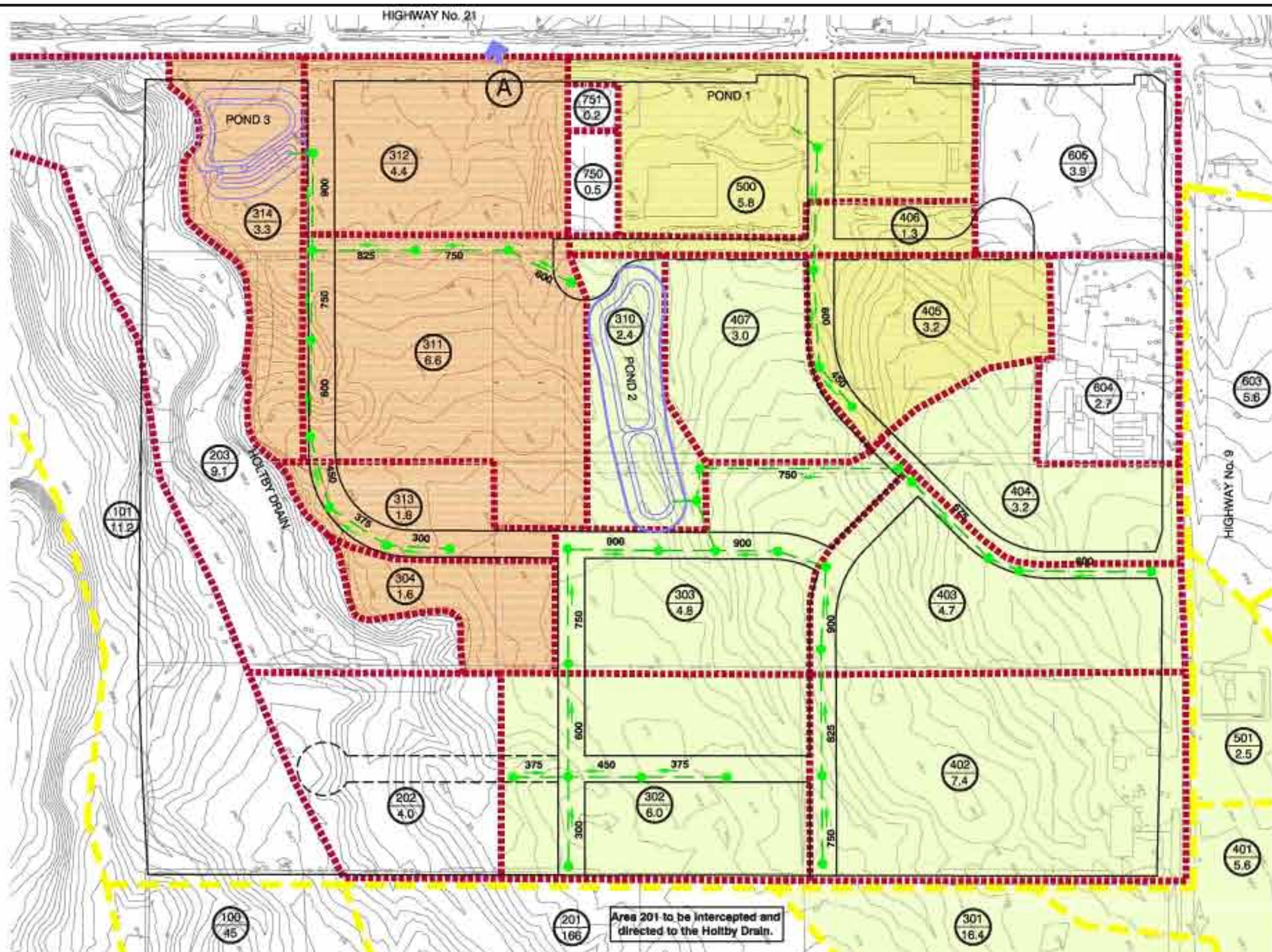
These future development areas are all tributary to the proposed SWM facility noted as Pond 3. The proposed pond has been designed as a wet pond with forebay and main pond features summarized in more detail in later sections of this report. The pond is to outlet immediately downstream of the Holtby Drain.

Details related to the design of Pond 2 and Pond 3 are provided in further detail in the following sections related to their design quality and quantity control capabilities. As noted Pond 1 is an existing facility and no modifications to the pond are proposed at this time.



- Legend**
- Pre-Existing Drainage Catchment Areas
 - Post Development Drainage Catchment Areas (Business Park Area)
 - Existing Open Channel Drain
 - 121
135 Miduse Drainage Catchment (L.D. / Area in Hectares)
 - 09 Catchment Area / L.D.
 - $2000 - 0.4\%$ Conveyance (Channel / Pipe)
 - 3000 Confluence Location

	Municipality of Kincardine Kincardine Business Park Servicing - Stormwater Management		DATE June 2016	PROJECT No. 08055
	Post Development Drainage Areas and Miduse Modelling Schematic		SCALE 1:35,000	FIGURE No. ST3



- Storm Outlets**
- (A) Storm Sewer
1500mm CSP Culvert
 - (B) Penetangore Tributary
5790 x 3550mm Arch
Culvert (Multi-Plate)

- Legend**
- Pre-Existing Drainage Catchment Area
 - Post Development Drainage Catchment Areas
 - 151
135 Miduss Drainage Catchment
(I.D. / Area in Hectares)
 - Proposed Storm Sewer and Pipe Size (mm)
1200
 - Pond 1 - Tributary Area
 - Pond 2 - Tributary Area
 - Pond 3 - Tributary Area

Area 201 to be intercepted and directed to the Holtby Drain.

Refer to Figure ST3 for drainage delineation details related to the external areas.



**Municipality of Kincardine
Kincardine Business Park**
Servicing - Stormwater Management
Detailed Area Plan -
Post Development Drainage Areas
and Miduss Modelling Schematic

DATE June 2016	PROJECT No. 08055
SCALE 1:4,000	FIGURE No. ST4

5.4 Water Quality Control

As noted in the MOE guidelines, the preferred facility type from drainage areas over 10 Ha is an extended detention wet pond facility. This is the most practical strategy for providing stormwater management within the drainage area for the business park.

Each facility will be designed to include the following:

- Permanent pool area.
- Wet pond quality and quantity control area for extended detention.
- Outlet structure with control gates for possible pond isolation.
- Maintenance access to the forebay and outlet structure.
- Landscaping.

Details and characteristics of each new pond are summarized below:

Pond 2 - Stormwater Management Facility

Design parameters for the facility have been based on the following:

- Drainage area impervious level for lands within the proposed Business Park (31.5 Ha) are to be based on an average value of 64%. It is noted, however that the impervious level for the various catchments varies from between 50% and 75%. The detailed Miduss input parameter sheets (refer to Appendix) should be referred to for the specific impervious value of each catchment area. The external tributary lands (24.5 Ha) have been modeled based on their current impervious level of 0%.
 - Proposed Business Park Area: 31.5 Ha
 - Average Impervious Level: 64%
 - External Drainage Area: 24.5 Ha
 - Average Impervious Level: 0%
 - Total Drainage Area: 56.0 Ha
 - Net Impervious Level: 36%
- Level 1 receiving stream and 35% impervious level.
- End-of-pipe, extended detention, wet pond configuration.
- From Table 3.2, an interpolated storage volume of 143 m³/Ha results (40m³/Ha extended detention and 103 m³/Ha of permanent pool).

Based on these parameters, the minimum storage requirements for Pond 2 include a permanent pool volume of 5,740 m³ and an extended detention volume of 2,240 m³. A 37 hour extended detention time will be provided by means of a 200 mm diameter orifice outlet.

Pond 3 - Stormwater Management Facility

Design parameters for the facility have been based on the following:

- Drainage area impervious level for lands within the proposed Industrial Park (18.0 Ha) are to be based on an average value of 73%. The majority of the areas have been designed with an impervious level of 75%, however, there is one catchment with an impervious level of 50%. The detailed Miduss input parameter sheets (Appendix A) should be referred to for the specific impervious value of each catchment area. There are no external lands that are tributary to this facility.
 - Proposed Business Park Area: 17.7 Ha
 - Average Impervious Level: 69%
- Level 1 receiving stream and 69% impervious level.
- End-of-pipe, extended detention, wet pond configuration.
- From Table 3.2, an interpolated storage volume of 223 m³/Ha results (40m³/Ha extended detention and 183 m³/Ha of permanent pool).

Based on these parameters, the minimum storage requirements for Pond 3 include a permanent pool volume of 3,233 m³ and an extended detention volume of 708 m³. A 22 hour extended detention time will be provided by means of a 200 mm diameter orifice outlet.

Confirmation of pond storage requirements, actual pond volumes, forebay sizing, cleanout frequency and drawdown timing is provided in Appendix G.

5.5 Water Quantity Control

Both of the proposed Stormwater Management Facilities have been designed with an extended detention volume component for pre to post development control of the 1:2 through to the 1:100 storm events.

Pre and post hydrologic models were developed as follows:

- Pre-development flows were assessed considering the entire watershed area for each of the two outlets under Highway 21. The assessment included the existing tributary of the Penetangore. This approach ensures that a full review of the flows downstream of the Business Park was completed.
- Post-development flows were assessed considering development within the proposed Industrial Park and all external drainage areas for the two outlets under Highway 21 as completed for the pre-development area. It is noted that a significant portion of the external lands are conveyed within the tributary of the Penetangore and are not within the development boundaries of the Business Park.

a) Minor Drainage System

Minor system surface flow will be directed into each SWM facility from all sub-catchment areas within the Business Park. Typically the minor system will be conveyed within a new storm sewer system designed to accommodate the 1:5 year storm event. Storm sewers are proposed to outlet to the end-of-pipe wet pond SWM facilities shown on Figure ST4.

b) Major Storm System

Major system surface flow will be directed into each SWM facility from all sub-catchment areas within the Business Park. Typically the major system will be conveyed within the finished road surface.

c) Modelling Results

The following tables summarize the results for both the pre-existing condition and the proposed development state. For comparative purposes, flow values at the following locations have been included in the summaries:

- i. Holtby Drain (immediately prior to its convergence with the Penetangore tributary)
 - ii. Highway 21 Outlet A - CSP culvert (school site)
 - iii. Highway 21 Outlet B - Multi-plate Arch culvert (Penetangore tributary)
 - iv. Combined Flow at both Highway 21 outlet locations.
- Table 2 presents the pre-existing site flows for the 2 yr through 100 yr rainfall events.
 - Table 3 presents the post development site flows for the 2 yr through 100 yr rainfall events.
 - Table 4 presents the comparison between Table 2 and Table 3 (as a percentage increase or decrease).

Table 2
Pre-Existing Miduss Flows (m³/s)

Storm Event (year)	Holtby Drain at Confluence with Penetangore Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	3.3	1.9	16.9	17.4
5	7.8	4.5	41.7	43.0
10	11.6	6.6	63.0	65.0
25	17.1	9.4	94.6	97.6
50	21.5	11.6	120.8	124.7
100	26.2	13.6	149.0	153.6

Table 3
Post-Development Miduss Flows (m³/s)

Storm Event (year)	Holtby Drain at Confluence with Penetangore Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	3.1	0.6	16.8	17.1
5	7.4	1.3	41.5	42.3
10	11.1	2.0	62.7	64.4
25	16.3	3.6	94.1	97.2
50	20.5	4.8	120.2	124.5
100	25.5	6.1	148.4	153.7

Table 4
Comparison Miduss Flows (% Change)

Storm Event (year)	Holtby Drain at Confluence with Penetangore Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	-4.9	-69.1	-0.3	-2.0
5	-5.3	-71.2	-0.4	-1.7
10	-4.6	-69.7	-0.5	-1.0
25	-4.9	-61.6	-0.5	-0.4
50	-4.8	-58.5	-0.5	-0.2
100	-2.7	-55.3	-0.4	0.1

Discussion related to the above results is summarized below for each location considered:

- Holtby Drain

Under all storm flow events (i.e., 2 through 100 year storms) there appears to be a nominal decrease in the peak flow events experienced under the developed state of the Business Park.

- 1500mm CSP Culvert under Highway 21

The proposed plan will significantly reduce flows to this outlet under Highway 21 as compared to the pre-existing condition (i.e., no commercial development). This is typically due to the fact that some of the predevelopment drainage areas are being redirected to the new stormwater management facility proposed for the Business Park.

- Multi-Plate Arch

The proposed plan will result in essentially no change to the peak flows experienced under 2 through 100 year flow events and the developed state.

- Combined Total at Highway 21

The proposed plan will not result in an increase, under all flow events, for the combined drainage area upstream of Highway 21.

5.7 Construction Sediment and Erosion Control

Before commencing stripping operations on the site, erosion and sediment controls are to be installed.

Monthly Erosion and Sediment Control Inspection Reports (Report Sheet included as Appendix H) are to be completed and made available to interested parties. These reports are to be based on bi-weekly inspections and after significant storm events (>13 mm). These reports are to be submitted until the site has been stabilized.

5.8 Monitoring and Maintenance Program

The facility has been designed to reduce maintenance requirements. General maintenance and monitoring for the facility should be in compliance with the “Stormwater Management Planning and Design Manual” by the MOE, March 2003, and would include the following:

- Inspection of the facility initially and after each significant rainfall event for the first two years following construction. It is proposed that inspections then be carried out after the first two years on an annual basis.
- Cleaning of debris from the outlet structure.
- Replacement of any plantings that have died.
- Removal of accumulated sediments from the forebay. It is expected that the cleaning of the forebay will be required approximately every 12 years and 6.5 years for Pond 2 and Pond 3, respectively (refer to Appendix G for calculations).

5.9 Summary of Stormwater Management Plan

1. This report outlines the provisions of Stormwater Management Facilities for the Business Park to be located at Highway 9 and 21 in Kincardine.
2. Through the study process, it was determined that two new end-of-pipe Extended Detention Wet Pond Facilities would provide a suitable strategy for providing stormwater management for the area. In addition, the existing dry pond, at the intersection of Durham Street and Highway 21 will be utilized for a portion of the development lands.

The proposed facilities have been designed in compliance with the criteria established in the MOE “Stormwater Management Planning and Design Manual”, dated March 2003.

3. The SWM facilities have been designed to provide:
 - Quality and Quantity control of the developed business park lands and any existing external lands at their current impervious level.
4. Details regarding monitoring and maintenance of the SWM facilities as well as sediment and erosion control measures during and after construction phases, has been outlined in this report.
5. Modelling results demonstrate that peak flow rates from the developed lands will generally not change significantly from that of the pre-existing condition for the area.

Based on the recommendations contained in this Stormwater Management Report, it is concluded that the construction of the proposed Extended Detention Wet Pond Facilities will provide suitable quality and quantity treatment of stormwater run-off from the development area and not adversely impact the receiving channels downstream of Highway No. 21.

6.0 POSSIBLE DEVELOPMENT PHASING

It is anticipated that the completion of the development of the business park will take a number of years and will therefore need to follow a phased-in infrastructure plan. Further discussions need to be undertaken with the various property owners to ascertain what areas of the Business Park may need to proceed in advance of others.

Figure PH-1 provides a suggested phasing scenario for the Business Park with the progression logically being from west to east to maximize upon the existing infrastructure that's exists adjacent to the Highway 21 corridor. Three (3) phases have been proposed as shown in the figure.

It is anticipated that by the completed of the second phase of the project, all required external infrastructure improvements and proposed works should be completed.

External Projects

- PHASE 1**
- (A) Sanitary Sewer
Russell - Hwy. 21 to Scott
 - (B) Park Street Sewage PS
Upgrades
- PHASE 2**
- (C) Signalization
- Russell St / Hwy. 21
 - (D) North Bound Right
Turn Lanes on Hwy. 21
- Russell St
- Durham St
 - (E) Left Turn Protective/
Permissive Phase
- Hwy. 21 / Hwy. 9
- Hwy. 21 / Durham St



Legend

- New Road
- Phase 1 Servicing
- Phase 2 Servicing
- Phase 3 Servicing
- Proposed Storm Sewer and Pipe Size (mm)
- Proposed Sanitary Sewer
- Watermain and Pipe Diameter (mm)
- Existing Topography and Contours
- Proposed Stormwater Management Facility
- Proposed Booster Pumping Station



**Municipality of Kincardine
Kincardine Business Park**
Suggested Phasing
Servicing Plan
Completed Phases

DATE June 2016	PROJECT No. 08055
SCALE 1:4,000	FIGURE No. PH1

7.0 PROBABLE COSTS

Preliminary estimated costs to provide full servicing and road construction for the Business Park have been prepared and are presented based upon recent tenders for similar works. All costs include allowances for local sanitary collection, external sanitary collection and pumping upgrades, water distribution and pressure boosting facilities, storm sewer collection, storm water management, road construction, street lighting, engineering, and contingencies.

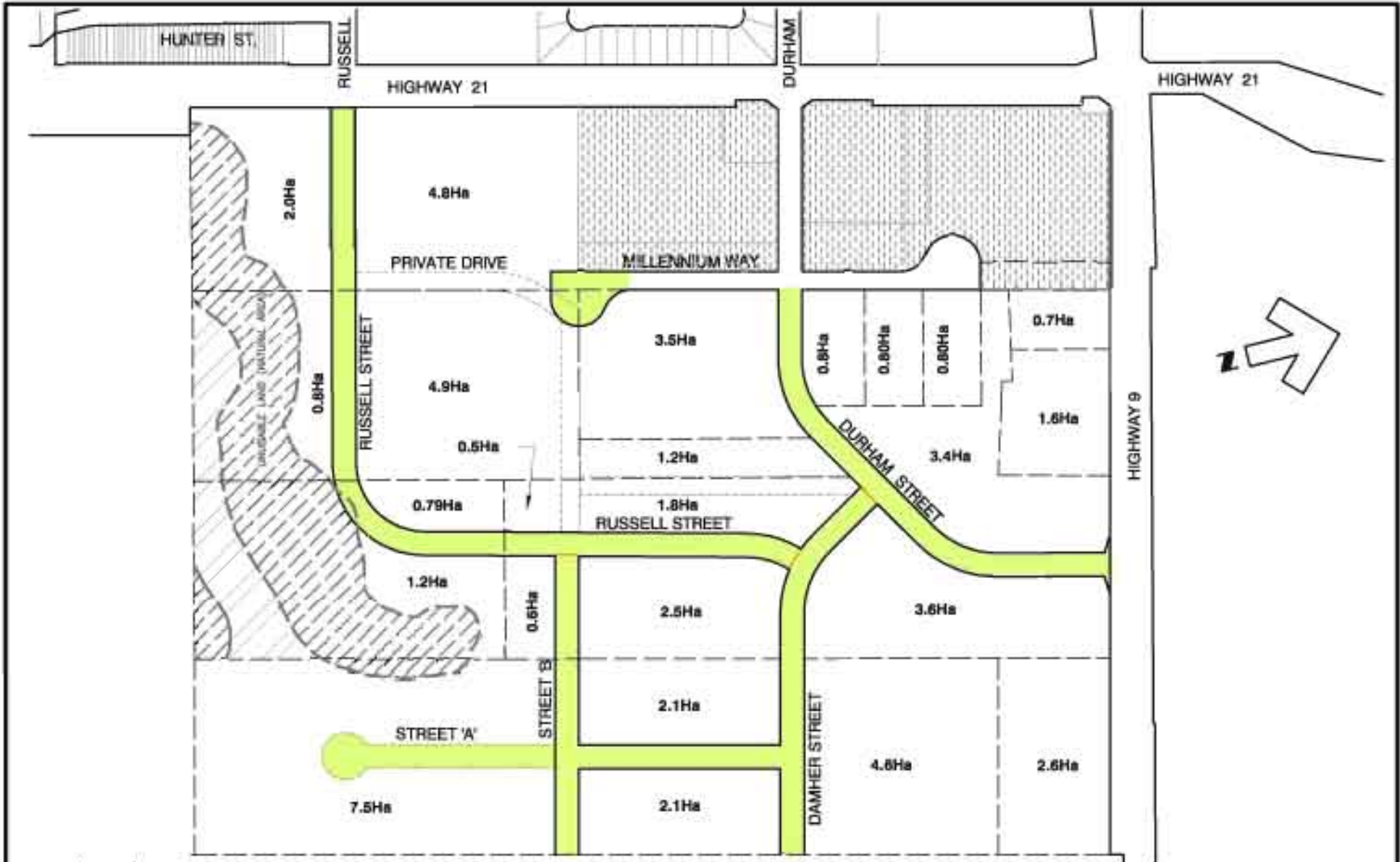
The anticipated total costs and estimated cost per hectare are summarized in the following table. Appendix I provides further breakdown and additional details of the costs shown.

Table 5
Estimated Probable Costs



Servicing Component	Cost			
	Phase 1	Phase 2	Phase 3	Total
Internal Servicing				
Road System	\$1,082,000	\$1,744,000	\$1,176,000	\$4,002,000
Storm Collection System	\$710,000	\$880,000	\$354,000	\$1,944,000
Stormwater Management Facilities	\$384,000	\$302,000	\$0	\$686,000
Sanitary Collection System	\$389,000	\$315,000	\$257,000	\$961,000
Water Distribution System	\$501,000	\$348,000	\$237,000	\$1,086,000
Subtotal - Internal Servicing	\$3,066,000	\$3,589,000	\$2,024,000	\$8,679,000
External / Other Servicing				
Russell Street Sanitary Sewer	\$627,000	\$0	\$0	\$627,000
Park Street Pumping Station Upgrades	\$950,000	\$0	\$0	\$950,000
Hwy. 21 Improvements	\$0	\$617,000	\$0	\$617,000
Water Booster Station	\$0	\$799,000	\$0	\$799,000
Subtotal - External / Other Servicing	\$1,577,000	\$1,416,000	\$0	\$2,993,000
TOTAL - Internal / External / Other Servicing	\$4,643,000	\$5,005,000	\$2,024,000	\$11,672,000

HST has not been included in the costs presented.

As shown on Figure CS1, there is approximately 52 net developable hectares (total area – road allowance and SWM blocks) within the Business Park land area. Based on the above, it is estimated the approximate cost per Developable hectare is approximately \$230,000.



Legend

-  Existing commercial Area
-  Proposed Road Allowances
- 7.5Ha** Net Developable Land Area



Municipality of Kincardine
Kincardine Business Park
 Servicing - Cost Sharing
 Net Developable Land Area

DATE June 2016	PROJECT No. 08055
SCALE 1:6,000	FIGURE No. CS1

8.0 SUMMARY

Based on the findings presented in this report, it is suggested that the Business Park area can be adequately serviced by municipal water, sewage, storm drainage, and road system. It is anticipated that the majority of the servicing can be phased depending on development interests. The following important items, related to servicing are noted:

- The installation of a new sanitary sewer, external to the development, is required on Russell Street from Highway 21 to Scott Street;
- Upgrades at the Park Street Sewage Pumping Station will be required;
- Pressure Boosting facilities will be required as development proceeds within the Business Park;
- The lands north of Highway 9 will result in significant (and unacceptable) surcharging in the existing Park Street sewers;
- Transportation improvements including signalization at Durham as well as right turn lanes on Highway 21 at Russell and Durham will be required as development proceeds;
- Further discussion with the MTO and property owners is warranted related to the internal configuration of Russell Street;
- Further investigation will be required, as the nature of development becomes more well-known, to determine the need to expand Highway 21 to four lanes between Highway 9 and the Russell Street intersection.
- It is possible to phase-in servicing depending on the nature of development interests for the area.
- The municipality and the developers will need to reach some consensus as to how the services on the balance of the Business Park will be funded.

All of which is respectfully submitted.

B. M. ROSS AND ASSOCIATES LIMITED

Per _____
Dale Erb, P. Eng.

DLE/

Per _____
Bruce W. Potter, P. Eng.

APPENDIX A

TRANSPORATION STUDY PARADIGM TRANSPORTATION SOLUTIONS



Kincardine Business Park Traffic Impact Study

Paradigm Transportation Solutions Limited

November 2015

Project Number

140720

November 2015

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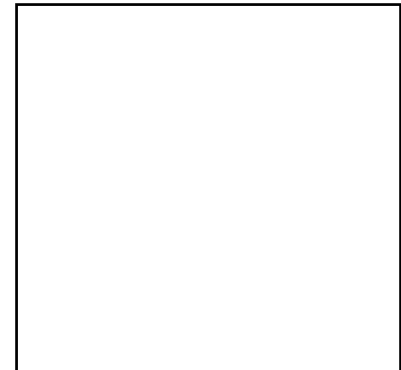
Kincardine Business Park Draft Traffic Impact Study

List of Revisions

Version	Date	Author	Description
1	April 2015	J Mallett	For comments
2	November 2015	J Mallett	For submission

Signatures and Seals

Signature



Engineer's Seal

Disclaimer

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Executive Summary

Content

A commercial subdivision is proposed to be built on the southeast corner of the intersection of Highway 21 and Highway 9 in Kincardine, Ontario. The subdivision is planned to have a mix of commercial uses including, but not limited to retail, hotels and restaurants. The subdivision will access Highway 21 at Durham Street and Russell Street and will access Highway 9 at a Durham Street extension.

Development Concept

The location of the development is on the southeast corner of the intersection of Highway 21 and Highway 9 in Kincardine, Ontario. The development has had some development occur on it already with a Sobey's, Tim Hortons, Canadian Tire, Boston Pizza, Meridian, a Holiday Inn Express and a Dentist Office. The remainder of the developable land to be considered in this study is approximately 17.77 hectares. The land uses for the remaining land include retail, hotel, car wash, and building supply and sales. The site will access the existing road network on Highway 21 at Durham Street and Russell Street and on Highway 9 at an extension of Durham Street.

The remainder of the site to the east is not considered in this report. During pre-study communication with the MTO, it was determined that the development plans for lands to the east are too unknown and the time frame too long to make reasonable forecasts. When development plans for those lands are known, additional study is expected to be done.

For the purposes of forecasting in this study, it was assumed that the completion date will be five years from the writing of this report (2020).

Conclusions

Based on the analyses contained in the report, it is concluded that:

- ▶ The intersections within the study area operate within acceptable levels.
- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F during the PM peak hour at the 2030 background horizon, the 2020 total horizon, 2025 total horizon, and 2030 total horizon.
- ▶ The westbound left-turn movement on Durham Street at Highway 21 is forecast to operate at LOS F during the PM peak hour at the 2030 total horizon.



- ▶ The sidestreet operations of the intersection of Highway 21 and Russell Street operate at LOS F during the PM peak hour at the 2020 total horizon, 2025 total horizon, and during both peak hours at the 2030 total horizon.
- ▶ The eastbound movements on Kincardine Avenue at Highway 21 are forecast to operate at LOS F during the PM peak hour at the 2025 and 2030 total horizons.

The following improvements are warranted:

- ▶ A westbound protected / permissive left-turn phase is forecast to be warranted at the intersection of Highway 21 and Highway 9 at the 2020 horizon.
- ▶ A westbound protected / permissive left-turn phase is forecast to be warranted at the intersection of Highway 21 and Durham Street at the 2030 horizon.
- ▶ A signal is forecast to be warranted by the 2020 horizon at the intersection of Highway 21 and Russell Street. Along with signalization, westbound and southbound left-turn lanes should be constructed as well as westbound and southbound protected / permissive left-turn phases.
- ▶ A northbound right turn lane is forecast to be warranted on Highway 21 at Durham Street.
- ▶ A northbound right turn lane is forecast to be warranted on Highway 21 at Russell Street.

Recommendations

Based on the foregoing analyses, it is recommended that the planning applications be approved as proposed with the following conditions related to transportation system improvements:

- ▶ A westbound protected / permissive phase be implemented at the intersection of Highway 21 and Highway 9.
- ▶ A westbound protected / permissive phase be implemented at the intersection of Highway 21 and Durham Street.
- ▶ A northbound right-turn lane be constructed on Highway 21 at Durham Street.
- ▶ A signal be constructed at the intersection of Highway 21 and Russell Street with a westbound and southbound left-turn lanes, a northbound right-turn lane and westbound and southbound protected / permissive left-turn phases.



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1 Introduction

1.1 Background

A commercial subdivision is proposed to be built on the southeast corner of the intersection of Highway 21 and Highway 9 in Kincardine, Ontario. The subdivision is planned to have a mix of commercial uses including, but not limited to retail, hotels and restaurants. The subdivision will access Highway 21 at Durham Street and Russell Street and will access Highway 9 at a Durham Street extension. The location of the development is shown in **Figure 1.1**.

A draft Traffic Impact Study (TIS) was originally prepared in June 2011 for this property. This updated TIS has been prepared based on updates to the site, traffic volumes and comments received from the Ministry of Transportation (MTO). A pre-study meeting was held with representation from the MTO, Municipality of Kincardine, BM Ross and Paradigm on 31 March 2014 where a scope outline was agreed upon.

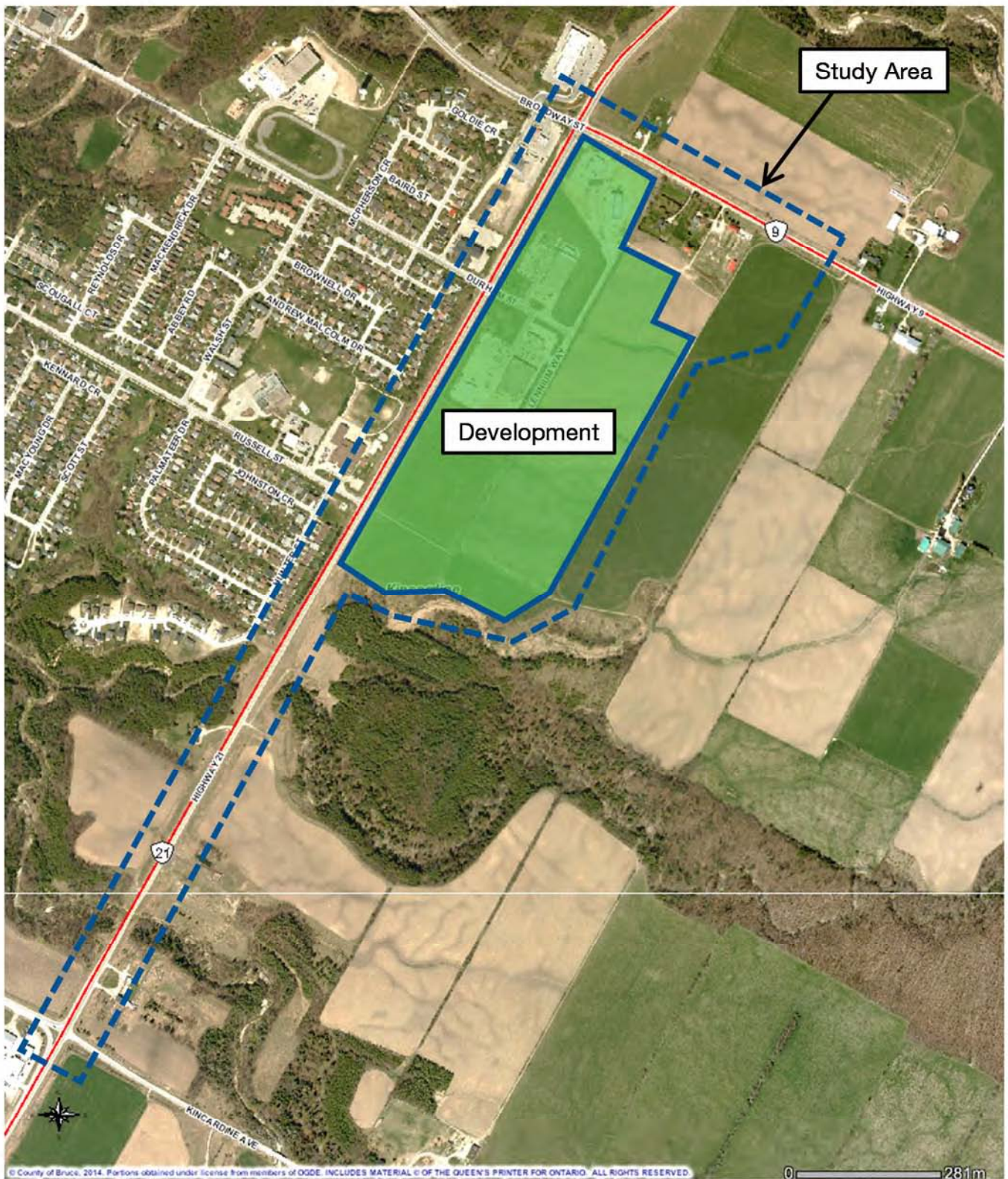
1.1 Purpose and Scope

Paradigm Transportation Solutions Limited was retained to conduct a traffic impact study for the proposed subdivision. The purpose of the study is to determine the impact of the development on the following intersections:

- ▶ Highway 21 and Highway 9 / Broadway Street
- ▶ Highway 21 and Durham Street
- ▶ Highway 21 and Russell Street
- ▶ Highway 21 and Kincardine Avenue / South Line
- ▶ Durham Street and Millennium Way
- ▶ Highway 9 and Durham Street

The scope of the study includes determination of the current traffic and site conditions in the vicinity of the development, additional traffic that will be generated by the development, analyses of the impact of the traffic and development of recommendations on the measures required in order to accommodate this traffic in a satisfactory manner for a planning horizon of the assumed opening year (five years from present) and five and ten years from opening year. The AM and PM peak hours were used for analysis in this report.





Development Location

Kincardine Business Park TIS
140720

Figure 1.1

2 Existing Conditions

This section documents current traffic conditions, operational deficiencies, and constraints experienced by the public traveling at the intersections within the study area. The operational deficiencies and constraints identified at this stage will provide input to the problem statement and will be fundamental to the process of defining alternative solutions.

2.1 Existing Roads

The location of the planned subdivision is on the southeast corner of the intersection of Highway 21 and Highway 9 in Kincardine, Ontario. Highway 21 is a two lane provincial highway with a speed limit of 80 km/h.

Highway 9 is also a two-lane provincial highway with a speed limit of 80 km/h. West of Highway 21, Highway 9 becomes the municipal road Broadway Street.

Durham Street is a two-lane municipal road with a speed limit of 50 km/h. Durham Street is proposed to extend east and northward through the subject development to intersect with Highway 9.

The intersections of Highway 21 with Highway 9 / Broadway Street and Durham Street are signalized.

2.2 Transit, Cycling and Pedestrian Services

There is no transit service or dedicated bicycle facilities within the study area. There are sidewalks on one side of Durham Street and Millennium Way.

2.3 Base Year Traffic Volumes

Existing turning movement volumes for the intersections along Highway 21 were provided by the Ministry of Transportation. The counts at Durham Street, Russell Street and Kincardine Avenue were conducted in July 2013 and the count at Highway 9 was conducted in October 2012. The intersection of Durham Street and Millennium Way was counted by Paradigm Transportation Solutions Limited in July 2013. The existing AM and PM peak hour traffic volumes are shown in **Figure 2.1**.

2.4 Base Year Traffic Operations

Intersection level of service (LOS) is a recognized method of quantifying the average delay experienced by drivers at intersections. It is based on the delay experienced by individual vehicles executing the various movements. The delay is related to the number of vehicles desiring to make a particular movement, compared to the estimated capacity for that movement. The



capacity is based on a number of criteria related to the opposing traffic flows and intersection geometry.

The highest possible rating is LOS A, under which the average total delay is equal or less than 10.0 seconds per vehicle. When the average delay exceeds 80 seconds for signalized intersections, 50 seconds for unsignalized intersections or when the volume to capacity ratio is greater than 1.0, the movement is classed as LOS F and remedial measures are usually implemented, if they are feasible. LOS E is usually used as a guideline for the determination of road improvement needs on through lanes, while LOS F may be acceptable for left-turn movements at peak times, depending on delays.

The operations of intersections in the study area were evaluated with the existing turning movement volumes using Synchro 9.

The intersection analysis considered two separate measures of performance:

- ▶ The volume to capacity ratio for each intersection; and
- ▶ The LOS for each turning movement. LOS is based on the average control delay per vehicle.

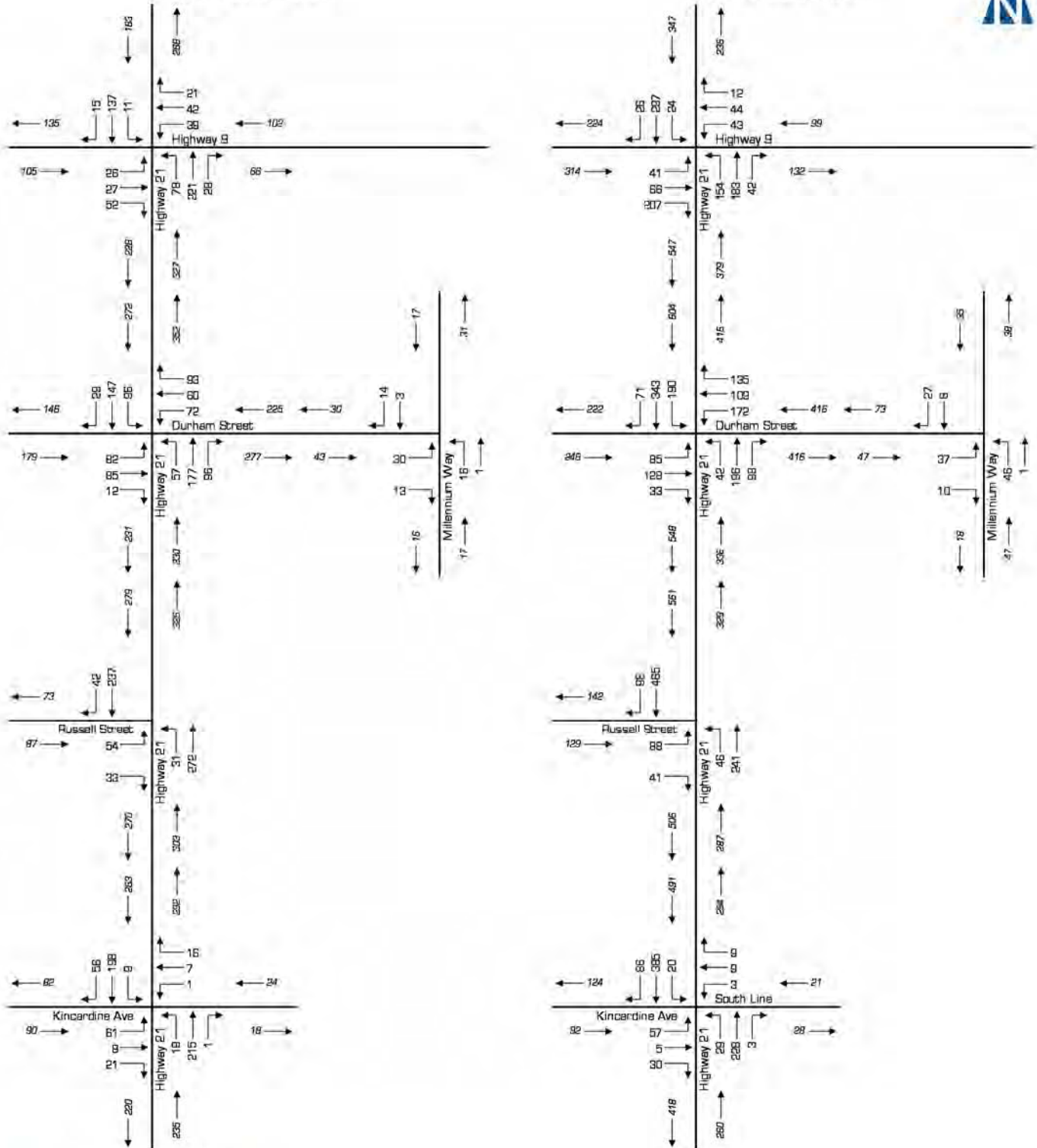
The operation of the intersections within the study area was evaluated using Synchro 9 with the existing turning movement volumes. The analysis shows that the movements at all intersections operate well under existing conditions. A summary of the operations and detailed Synchro outputs are provided in **Appendix A**.





AM Peak Hour

PM Peak Hour



Base Year Traffic Volumes

3 Development Concept

The location of the development is on the southeast corner of the intersection of Highway 21 and Highway 9 in Kincardine, Ontario. The development has had some development occur on it already with a Sobey's, Tim Hortons, Canadian Tire, Boston Pizza, Meridian, a Holiday Inn Express and a Dentist Office. The remainder of the developable land to be considered in this study is approximately 17.77 hectares. The land uses for the remaining land include retail, hotel, car wash, and building supply and sales. The site will access the existing road network on Highway 21 at Durham Street and Russell Street and on Highway 9 at an extension of Durham Street. The proposed site concept plan is shown in **Figure 3.1**.

The remainder of the site to the east is not considered in this report. During pre-study communication with the MTO, it was determined that the development plans for lands to the east are too unknown and the time frame too long to make reasonable forecasts. When development plans for those lands are known, additional study is expected to be done.

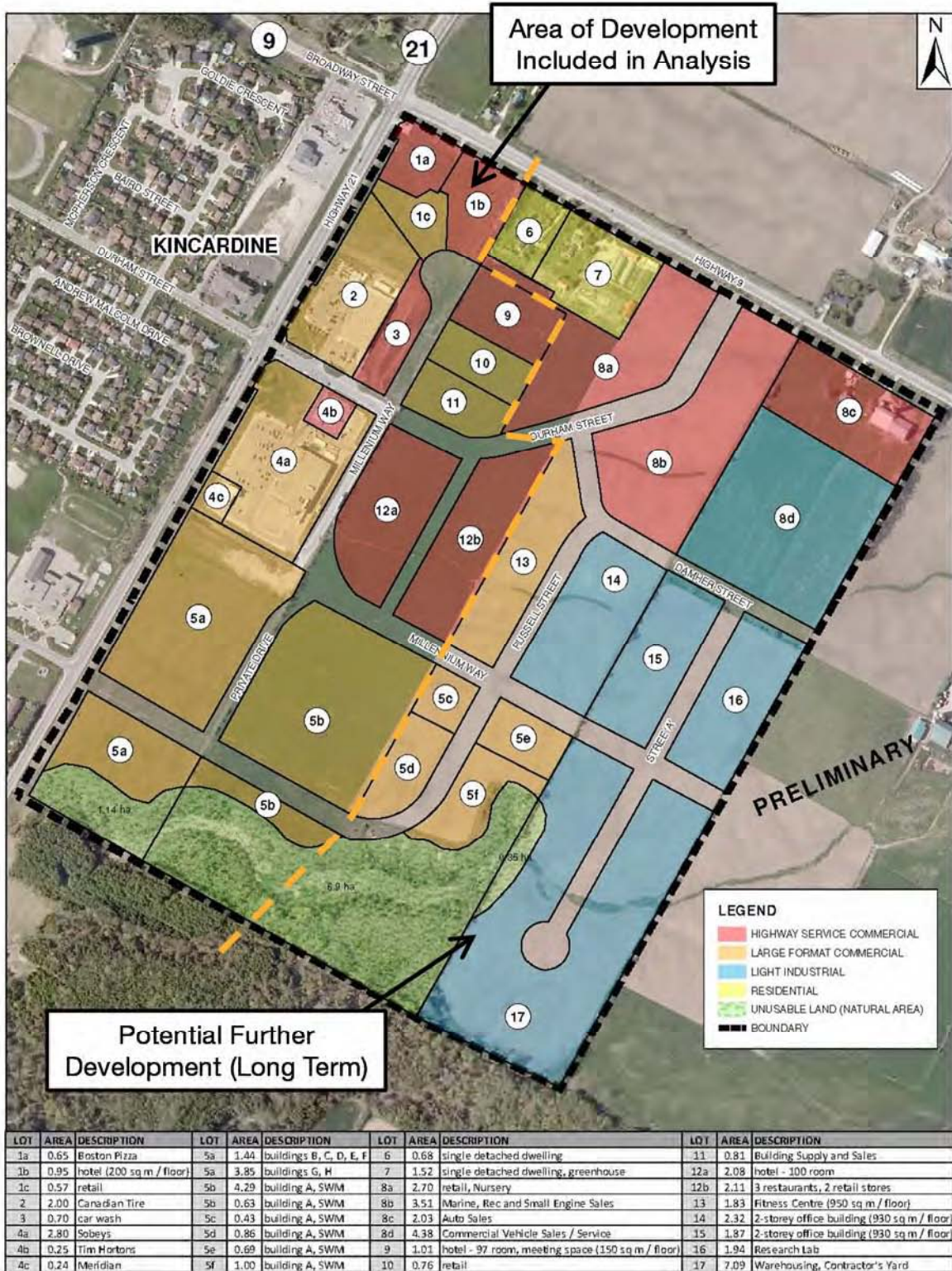
For the purposes of forecasting in this study, it was assumed that the completion date will be five years from the writing of this report (2020).

3.1 Development Trip Generation

The analysis of the first phase of the development includes lots 5a, 5b, 9, 10, 11, 12a, and 12b. Based on the best estimate of land use at the time of this report, the types of land use include retail, hotels, and building supplies and sales. The Institute of Transportation Engineers (ITE) Trip Generation Manual 9th Edition was used to estimate the peak hour traffic volumes that will be generated by the components of this development. The following land use codes were used:

- ▶ **LUC 310 (Hotel):** Hotels are places of lodging that provide sleeping accommodations and supporting facilities such as restaurants, cocktail lounges, meeting and banquet rooms or convention facilities, limited recreational facilities (pool, fitness room), and/or other retail and service shops.
- ▶ **LUC 812 (Building Materials and Lumber Store):** A building materials and lumber store is a free-standing building that sells hardware, building materials and lumber. The lumber may be stored in the main building, yard, or storage shed. The buildings contained in this land use are less than 30,000 square feet gross floor area.
- ▶ **LUC 820 (Shopping Centre):** Integrated group of commercial establishments that is planned, developed, owned and managed as a unit. The composition is related to its market area in terms of size, location and type of store. Provides on-site parking facilities sufficient to serve its parking demands.





- **LUC 826 (Specialty Retail Centre):** Includes gasoline/service station with convenience markets where the primary business is the fueling of motor vehicles. These stations may also have ancillary facilities for servicing and repairing motor vehicles. Some commonly sold convenience items are newspapers, coffee or other beverages and snack items usually consumed in the car. Generally located at intersections or interchanges.

The gross floor area (GFA) of the retail uses were determined by assuming a 25% coverage of the total area of the lots. The estimated trip generation for the development is displayed in **Table 3.1**. For this development, it is expected that 424 and 983 new trips will be generated in the AM and PM peak hour, respectively.

TABLE 3.1: DEVELOPMENT TRIP GENERATION

Block	Land Use	ITE Land Use Code	Area	Units	AM Peak Hour				PM Peak Hour			
					Rate	Total	In	Out	Rate	Total	In	Out
5a North	Retail	820 Shopping Centre Passby	3.85 ha	103.6 x 1000 ft ²	0.92 n/a	95 0	59 0	36 0	3.71 34%	384 131	184 65	200 65
5a South	Retail	820 Shopping Centre Passby	1.44 ha	38.8 x 1000 ft ²	0.92 n/a	36 0	22 0	14 0	3.71 34%	144 49	69 24	75 24
5b North	Retail	820 Shopping Centre Passby	4.29 ha	115.4 x 1000 ft ²	0.92 n/a	106 0	66 0	40 0	3.71 34%	428 146	206 73	223 73
5Bb South	Retail	820 Shopping Centre Passby	0.63 ha	17.0 x 1000 ft ²	0.92 n/a	16 0	10 0	6 0	3.71 34%	63 21	30 11	33 11
9	Hotel	310 Hotel Passby	1.01 ha	97 rooms	0.53 n/a	51 0	30 0	21 0	0.60 n/a	58 0	30 0	29 0
10	Retail	820 Shopping Centre Passby	0.76 ha	20.5 x 1000 ft ²	0.92 n/a	19 0	12 0	7 0	3.71 34%	76 26	36 13	39 13
11	Building Supplies and Sales	812 Building Materials and Lumber Store Passby	0.81 ha	21.8 x 1000 ft ²	2.60 n/a	57 0	38 0	19 0	4.49 n/a	98 0	46 0	52 0
12a	Retail	826 Specialty Retail Centre Passby	1.27 ha	20.0 x 1000 ft ²	n/a n/a	0 0	0 0	0 0	2.71 n/a	54 0	24 0	30 0
12b	Hotel	310 Hotel Passby	0.84 ha	84 rooms	0.53 n/a	45 0	26 0	18 0	0.60 n/a	50 0	26 0	25 0
Total Trips						424	263	161		1356	651	705
Total Passby						0	0	0		372	186	186
Net New Trips						424	263	161		983	465	519

3.2 Development Trip Distribution and Assignment

The trip distribution was based on the proximity of nearby residential areas and weighting the existing turning movement volumes at the intersections on Highway 21. The trip distributions of new trips used in this study are summarized in **Table 3.2**. Passby traffic distribution, which is the diversion of existing traffic into the site, was based on the existing traffic volumes at the intersection Highway 21 and Highway 9. The distribution used for passby traffic is summarized in **Table 3.3**.



TABLE 3.2: NEW TRIP DISTRIBUTION

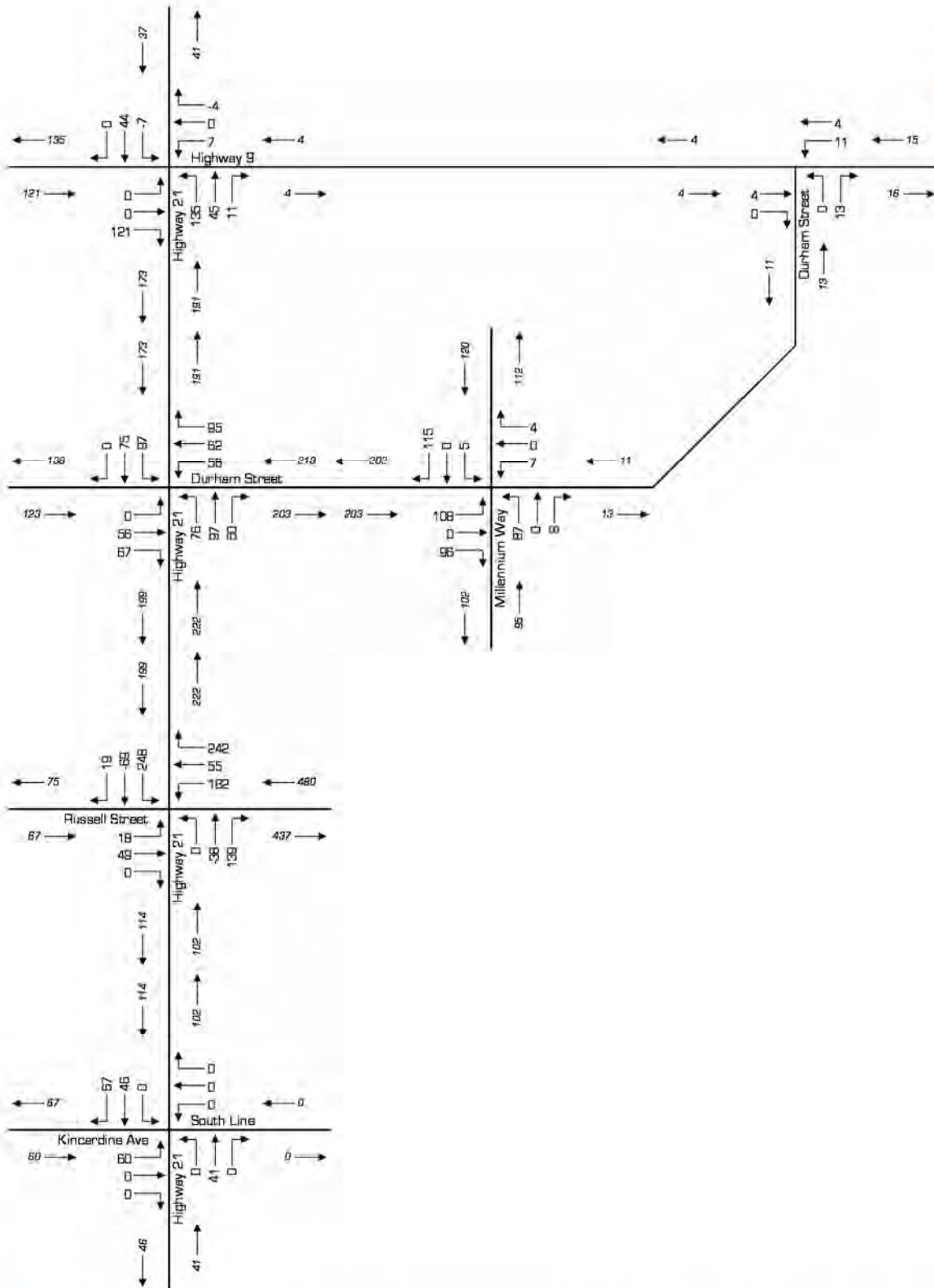
Direction	Distribution
West (Broadway)	26%
West (Durham)	27%
West (Russell)	14%
West (Kincardine Ave)	13%
South (Hwy 21)	9%
East (Hwy 9)	3%
North (Hwy 21)	8%

TABLE 3.3: PASSBY TRIP DISTRIBUTION

Direction	Distribution
North (21) to East (9)	4%
North (21) to South (21)	49%
South (21) to East (9)	7%
South (21) to North (21)	30%
East (9) to North (21)	2%
East (9) to South (21)	7%

Figure 3.2a and **Figure 3.2b** show the site generated traffic forecasts, (including the passby traffic for the PM peak hour). The new generated traffic and passby traffic for the PM peak hour are shown separately in **Appendix B**.





Development PM Peak Hour Traffic Volume Forecasts

4 Evaluation of Future Traffic Conditions

The assessment of future traffic conditions contained in this section includes estimates of future background and total traffic and analysis for planning horizons of expected completion (2020) and five and ten years from completion (2025 and 2030, as required by the MTO requirements for Traffic Impact Studies. The likely future traffic volumes in the vicinity of the development will likely consist of increased non-site traffic volumes (background traffic) and the traffic generated by the proposed development (site traffic).

4.1 2020 Horizon

4.1.1 2020 Background Traffic Growth

The non-site traffic increase is generalized traffic growth in the Kincardine area. As requested by MTO in the pre-study consultations, a 2% per year growth rate was used to forecast background traffic volumes. The 2020 background traffic is shown in **Figure 4.1**.

4.1.2 2020 Background Traffic Operations

Based on the forecasted 2016 background traffic volumes, LOS analyses have been conducted using Synchro 8 to determine the AM and PM peak hour conditions for the intersections within the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. The analysis indicates that the operations will be nearly identical to the existing conditions, with slight increases to delay, particularly to the westbound left-turn movement at Highway 21 and Highway 9 during the PM peak hour, which is forecast to operate at LOS E. A summary of the 2020 background traffic operations and the detailed Synchro reports are included in **Appendix C**.

4.1.3 Total 2020 Traffic Volumes

The total 2020 traffic volumes, which are the background volumes added to the site generated volumes are shown in **Figure 4.2a** and **Figure 4.2b**.

4.1.4 Total 2020 Traffic Operations

Based on the forecasted 2020 total traffic volumes, LOS analyses have been conducted using Synchro 9 and the AM and PM peak hour conditions for the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. A summary of the 2020 total traffic operations and the detailed Synchro reports are included in **Appendix D**. The analysis indicates the following deficiencies in traffic operations are forecast to occur:



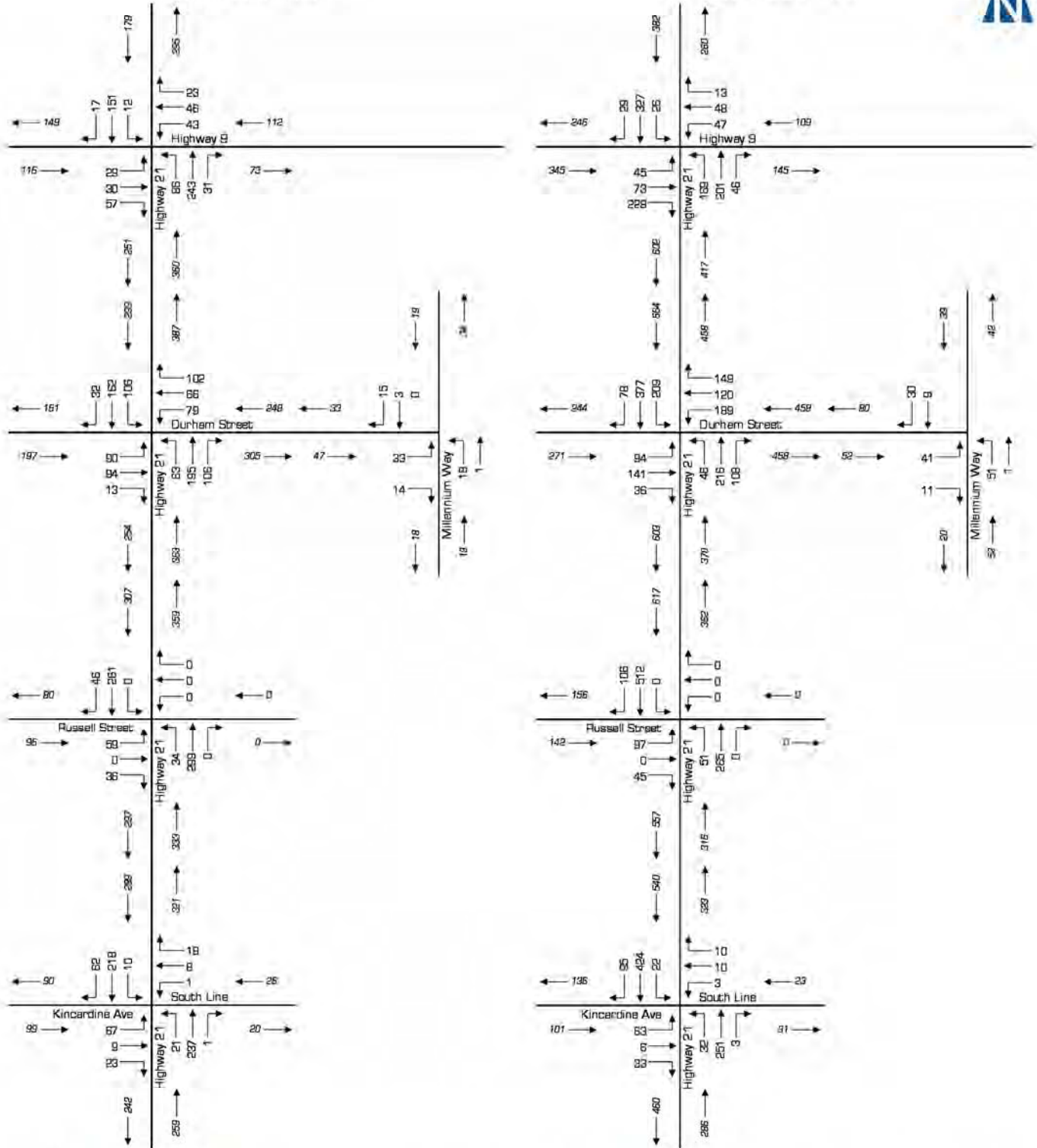
- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F during the PM peak hour.
- ▶ The sidestreet (east and westbound) movements on Russell Street at Highway 21 are forecast to operate at LOS F and well above a V/C ratio of 1.0 during the PM peak hour.



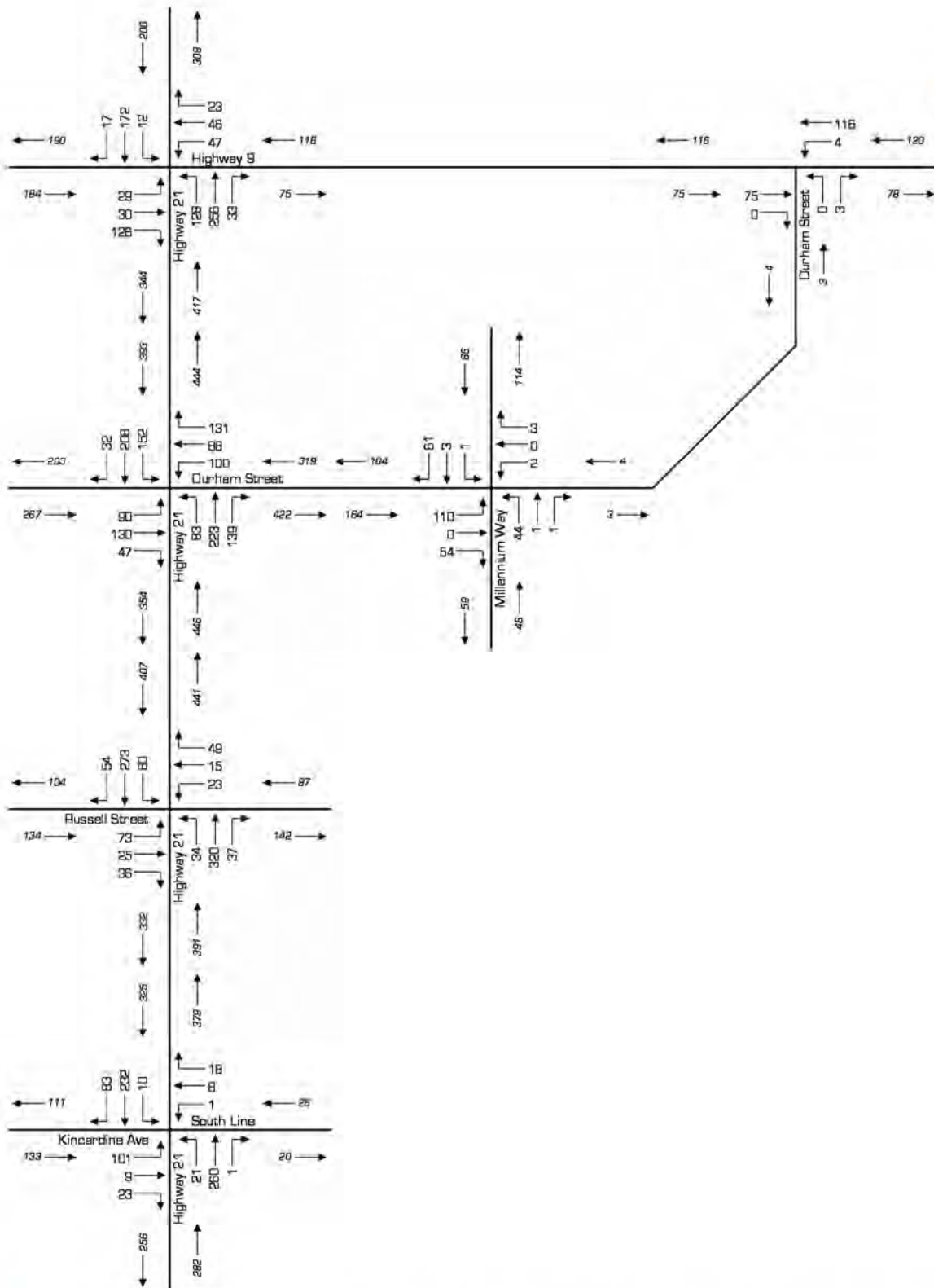


AM Peak Hour

PM Peak Hour



2020 Background Traffic Volume Forecasts



2020 Total AM Peak Hour Traffic Volume Forecasts

4.2 2025 Horizon

4.2.1 2025 Background Traffic Growth

Similar to the 2020 horizon year, the 2025 background traffic was determined by applying a 2% growth rate to the existing volumes. The 2025 background traffic is shown in **Figure 4.3**.

4.2.2 2025 Background Traffic Operations

Based on the forecast 2024 background traffic volumes, LOS analyses have been conducted using Synchro 9 to determine the AM and PM peak hour conditions for the intersections within the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. The analysis indicates that the operations will be nearly identical to the 2020 background conditions, with the westbound left-turn movement at Highway 21 and Highway 9 during the PM peak hour forecast operating at LOS E. A summary of the 2025 background traffic operations and the detailed Synchro reports are included in **Appendix E**.

4.2.3 Total 2025 Traffic Volumes

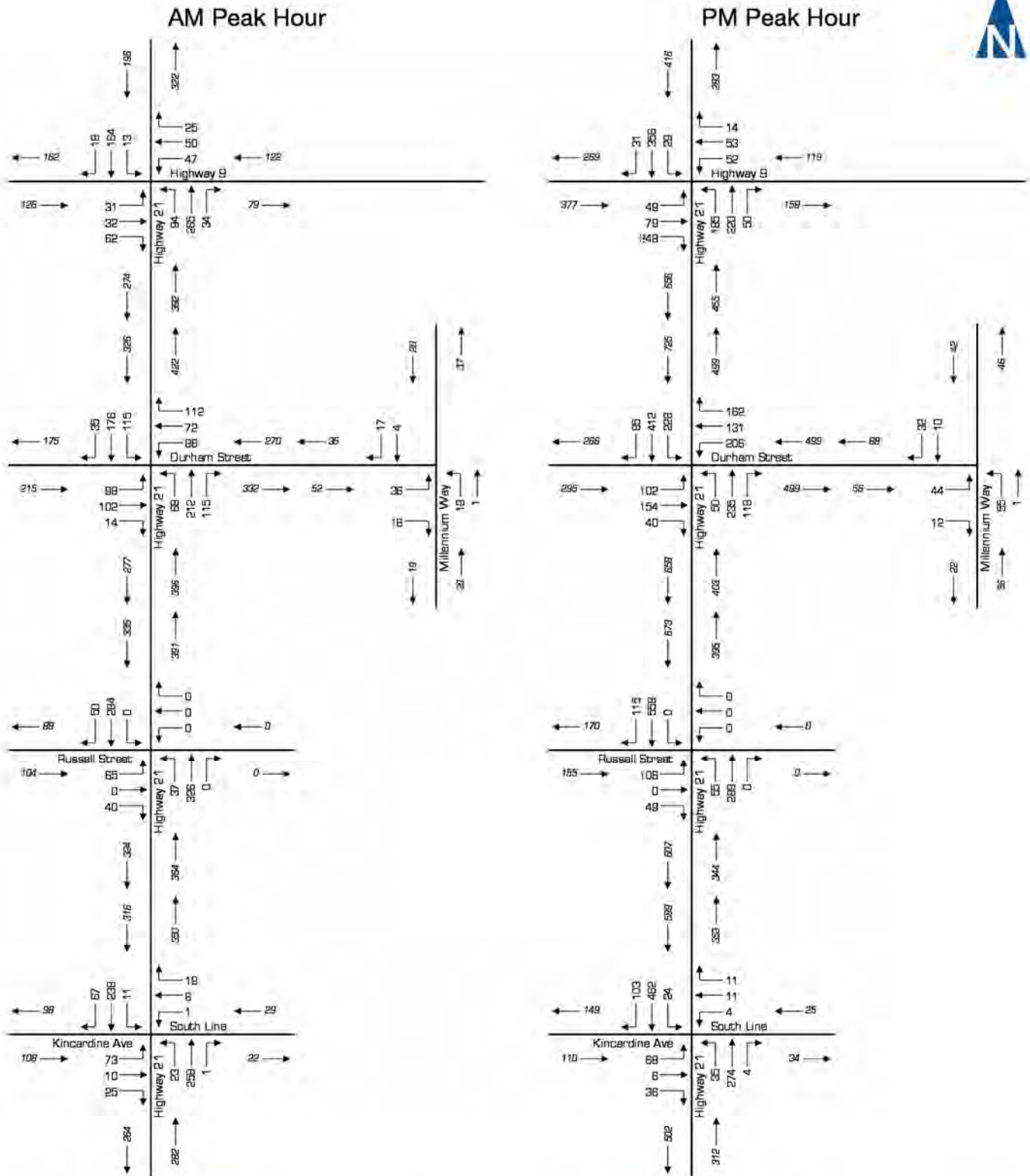
The total 2025 traffic volumes, which are the background volumes added to the site generated volumes are shown in **Figure 4.4a** and **Figure 4.4b**.

4.2.4 Total 2025 Traffic Operations

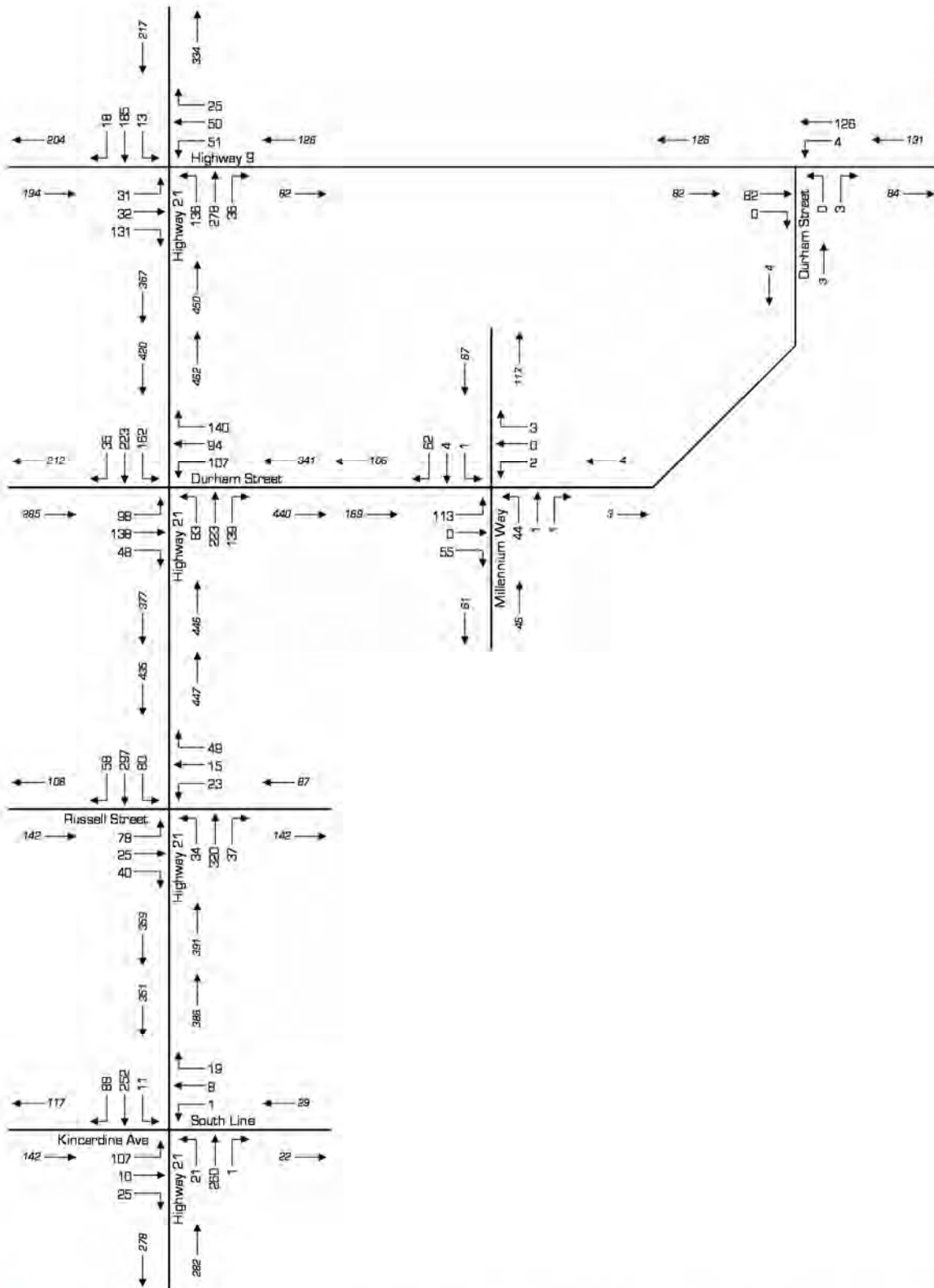
Based on the forecasted 2025 total traffic volumes, LOS analyses have been conducted using Synchro 9 and the AM and PM peak hour conditions for the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. A summary of the 2025 total traffic operations and the detailed Synchro reports are included in **Appendix F**. The analysis indicates the following deficiencies in traffic operations are forecast to occur:

- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F during the PM peak hour.
- ▶ The sidestreet (east and westbound) movements on Russell Street at Highway 21 are forecast to operate at LOS F and well above a V/C ratio of 1.0 during the PM peak hour.
- ▶ The eastbound movements on Kincardine Avenue at Highway 21 are forecast to operate at LOS F during the PM peak hour, but below a V/C ratio of 1.0.





2025 Background Traffic Volume Forecasts



2025 Total AM Peak Hour Traffic Volume Forecasts

4.3 2030 Horizon

4.3.1 2030 Background Traffic Growth

Similar to the 2020 and 2025 horizon years, the 2030 background traffic was determined by applying a 2% growth rate to the existing volumes. The 2030 background traffic is shown in **Figure 4.5**.

4.3.2 2030 Background Traffic Operations

Based on the forecast 2030 background traffic volumes, LOS analyses have been conducted using Synchro 9 to determine the AM and PM peak hour conditions for the intersections within the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. The analysis indicates that the operations will be mostly similar to the 2020 and 2025 background conditions, but with the delay for the westbound left-turn movement at Highway 21 and Highway 9 during the PM peak hour forecast to increase to LOS F from E. Also notable is the increase of the forecast eastbound operations on Russell Street to be LOS E. A summary of the 2030 background traffic operations and the detailed Synchro reports are included in **Appendix G**.

4.3.3 Total 2030 Traffic Volumes

The total 2030 traffic volumes, which are the background volumes added to the site generated volumes are shown in **Figure 4.6a** and **Figure 4.6b**.

4.2.4 Total 2030 Traffic Operations

Based on the forecasted 2030 total traffic volumes, LOS analyses have been conducted using Synchro 9 and the AM and PM peak hour conditions for the study area. No changes to the existing geometry or signal phasing structure or cycle lengths were made in the analysis, but the signal timings were otherwise optimized by Synchro. A summary of the 2030 total traffic operations and the detailed Synchro reports are included in **Appendix H**. The analysis indicates the following deficiencies in traffic operations are forecast to occur:

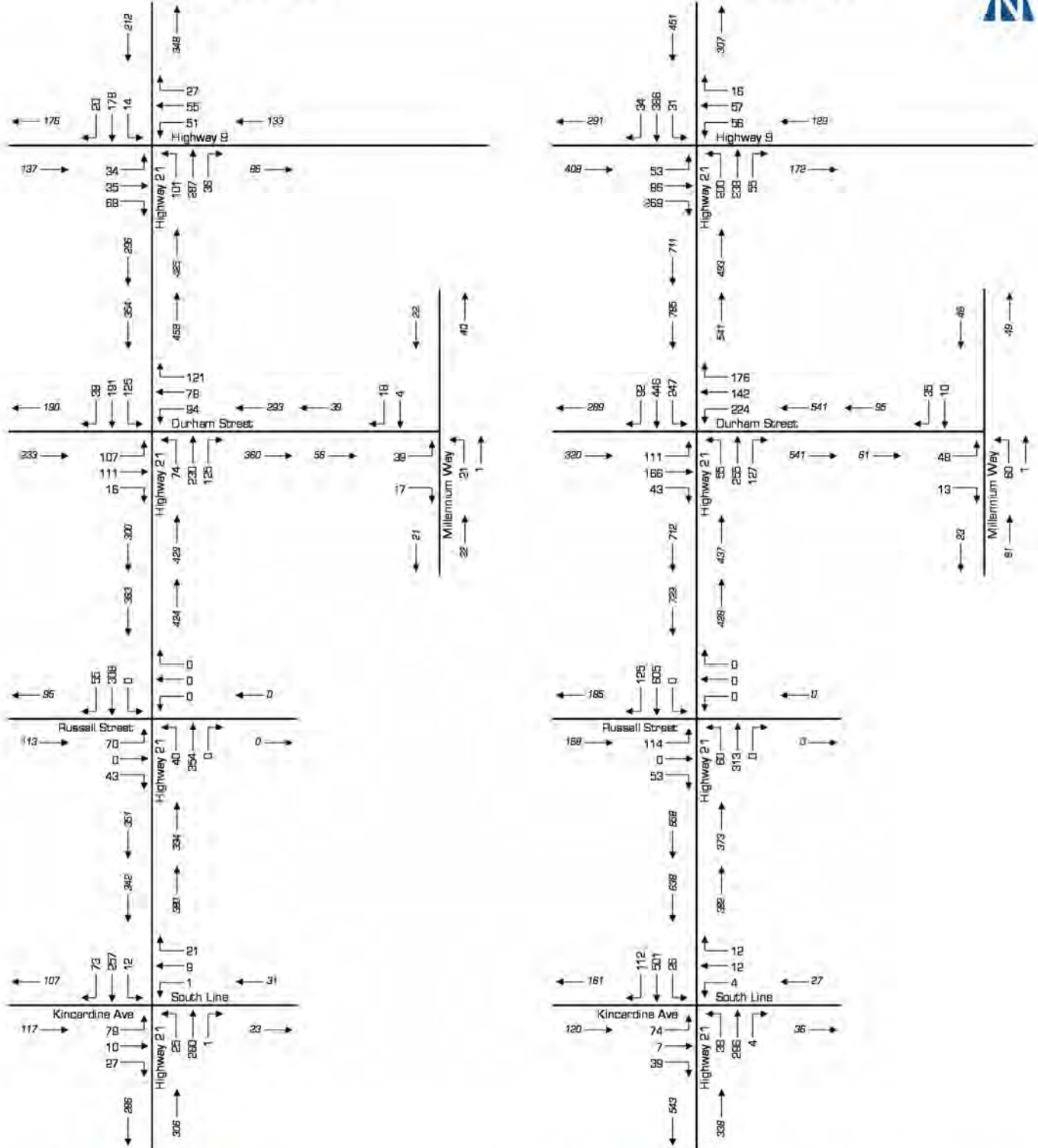
- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F during the PM peak hour.
- ▶ The sidestreet (east and westbound) movements on Russell Street at Highway 21 are forecast to operate at LOS F and well above a V/C ratio of 1.0 during the PM peak hour.
- ▶ The eastbound movements on Kincardine Avenue at Highway 21 are forecast to operate at LOS F during the PM peak hour, but below a V/C ratio of 1.0.



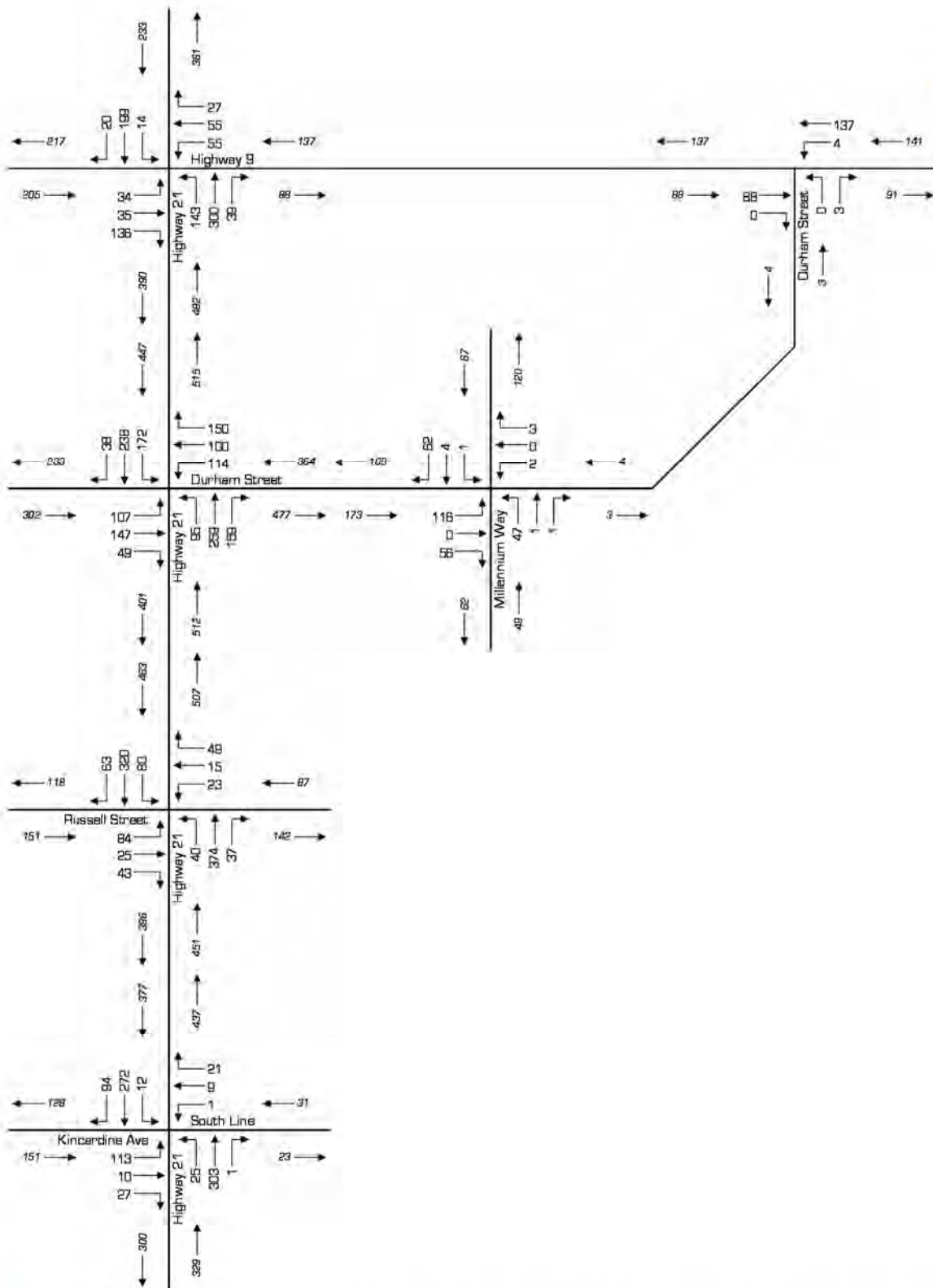


AM Peak Hour

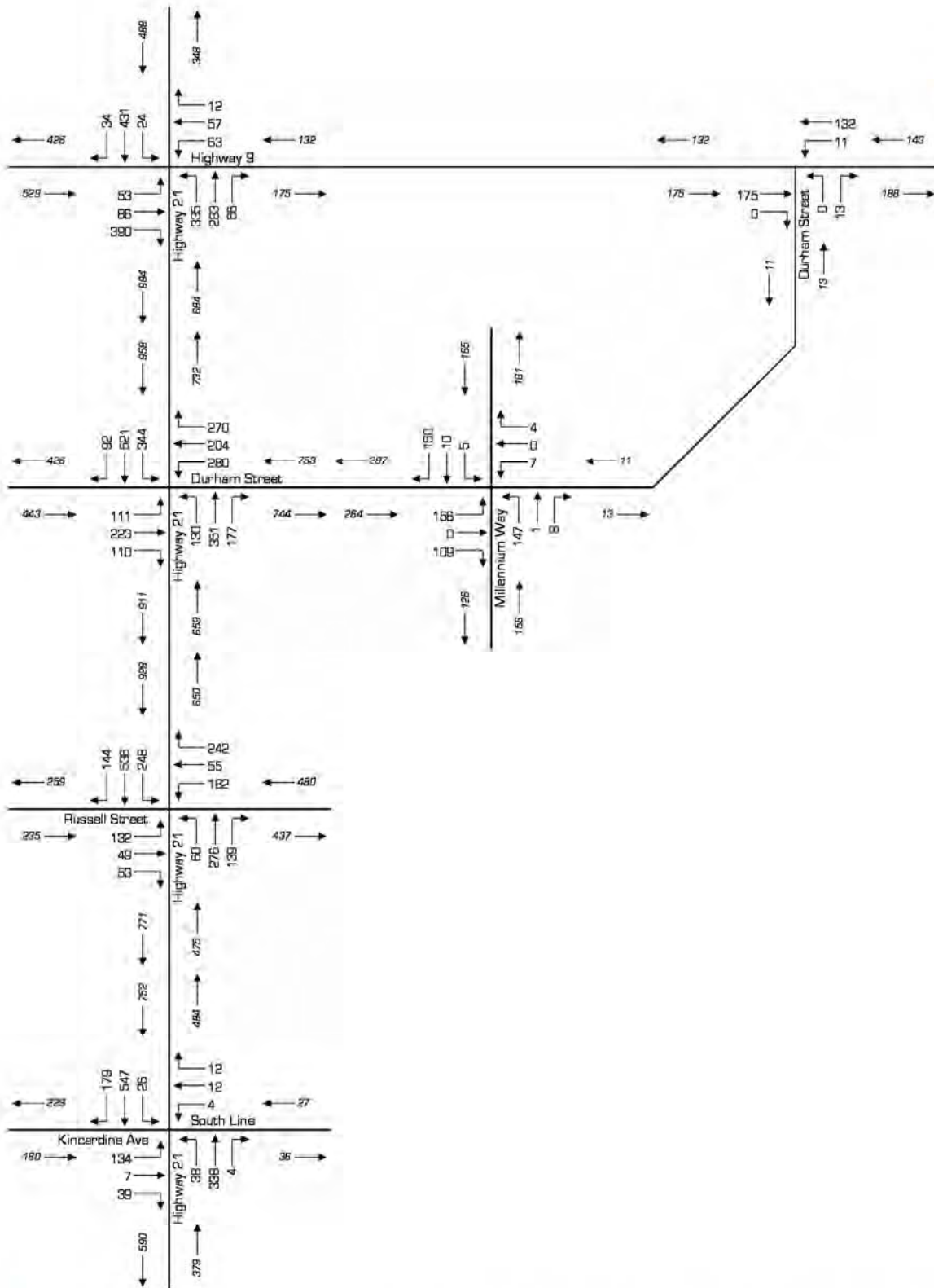
PM Peak Hour



2030 Background Traffic Volume Forecasts



2030 Total AM Peak Hour Traffic Volume Forecasts



2030 Total PM Peak Hour Traffic Volume Forecasts

5 Remedial Measures

The following sections review what, if any, measures should be implemented to mitigate the increases in delay resulting from the development of the site.

5.1 Signal Warrants

5.1.1 Highway 21 and Russell Street

The intersection of Highway 21 and Russell Street was checked if signals will be warranted at any of the forecast horizon years. **Table 5.1** summarizes the results of the signal warrant analyses and the signal warrant worksheets are included in **Appendix I**.

The analysis indicates that a signal will be warranted at the intersection of Highway 21 and Russell Street by the development by the 2020 horizon year. A separate westbound left-turn lane should be constructed as a part of this intersection as the left-turn volumes are forecast to represent nearly half the westbound volume. Also, as part of the reconfiguration of this intersection from a 3-legged stop-controlled intersection to a 4-legged signalized intersection, a southbound left-turn lane should be constructed, which can be placed in the existing shadow lane of the northbound left-turn lane.

TABLE 5.1: SIGNAL WARRANT ANALYSIS SUMMARY

	2020	2025	2030
Background	Not Warranted	Not Warranted	Not Warranted
Total	Warranted	Warranted	Warranted

5.1.2 Highway 21 and Kincardine Avenue

The intersection of Highway 21 and Kincardine Avenue was also checked if signal would be warranted. The analysis shows that at the 2030 total horizon, a signal is not warranted at this intersection (and therefore, not warranted at the other horizons, which have lower volumes). The signal warrant worksheet is included in **Appendix I**. Despite the poor level of service for the eastbound movements, the sidestreet volumes are not high enough to warrant a signal.

5.2 Left-Turn Lane Warrants

The need for a left-turn lane was analyzed for the westbound direction on Highway 9 at the future Durham Street extension. Left-turn lane warrants are based on the Ministry of Transportation Geometric Design Standards manual. Warrants are based on the percentage of vehicles turning left in the advancing volume and warrants start at 5%. Based on the percentage of left-turning vehicles forecast for the future horizons, the AM peak hours will use the 5% nomograph and the PM peak hours will use the 10%



nomograph. A design speed of 20 km/h over the speed limit of 80 km/h was assumed. The results of the left-turn lane warrant analysis are shown in **Figure 5.1**. The results are that a left-turn lane is not warranted at this intersection.

5.3 Right-Turn Lanes

While there is not a concrete rule on when a right-turn lane is warranted, generally when the right-turn volume reaches 100 vehicles per hour, a right-turn lane should be considered. By 2020, the northbound right-turn volumes on Highway 21 at Durham Street is forecast to reach 139 vph and 159 vph during the AM and PM peak hours, respectively. Also, the northbound right-turn volume on Highway 21 at Russell Street is forecast to reach 139 vph during the PM peak hour. Therefore, right-turn lanes should be considered on Highway 21 at both Durham Street and Russell Street

5.4 Signalized Intersections

The intersections of Highway 21 with Highway 9 and Durham Street are forecasted to have movements operate poorly by the 2030 total horizon:

- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F at the 2030 background PM peak hour, and the 2020, 2025, and 2030 total PM peak hour horizons.
- ▶ The westbound left-turn movement on Durham Street at Highway 21 is forecast to operate at LOS F at the 2030 total PM peak hour horizon.

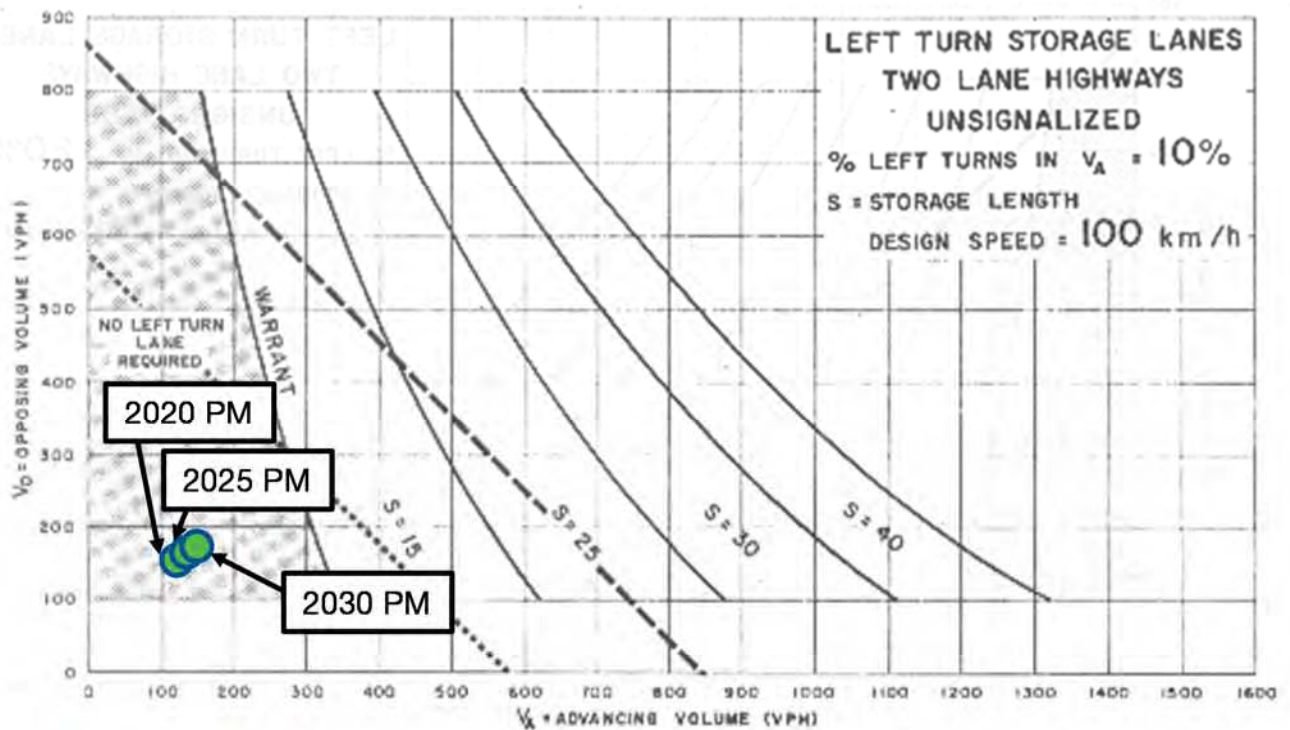
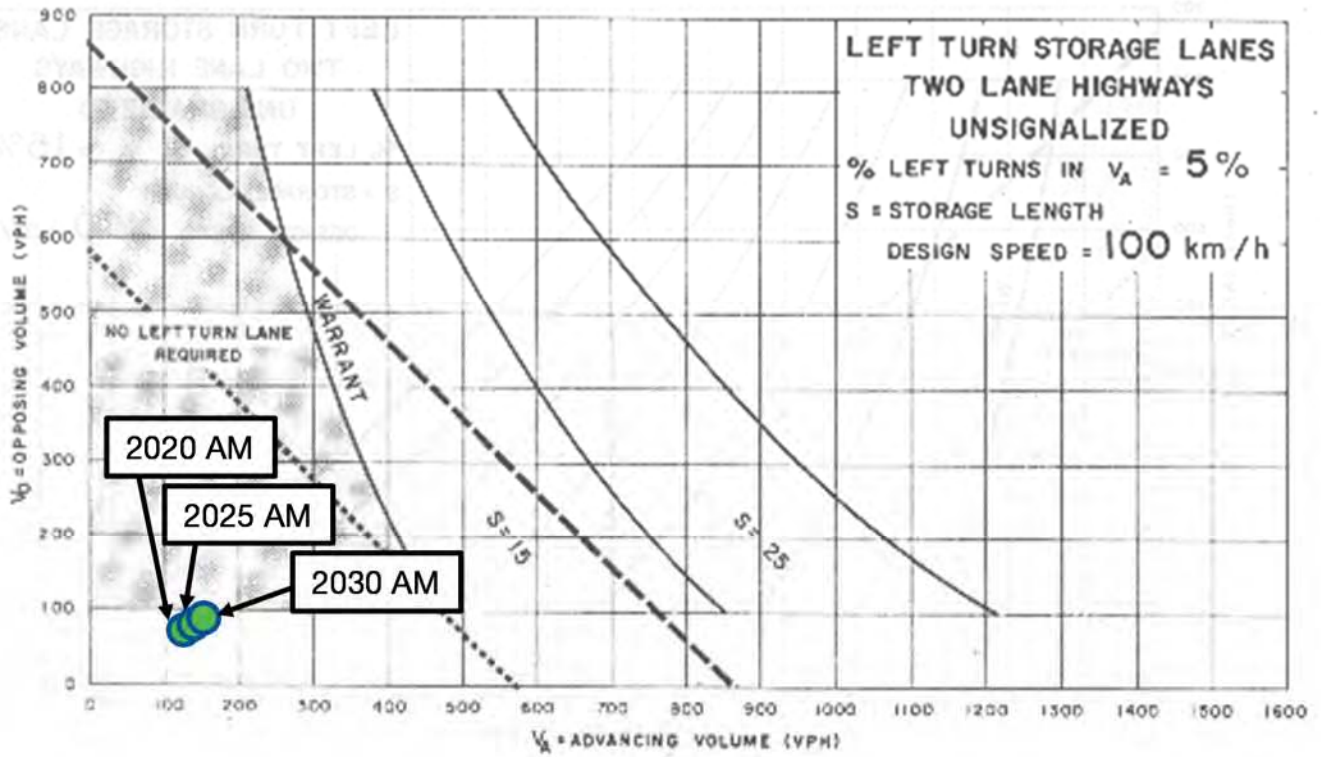
To improve operations, the following changes should be made to the signals, based on the 2021 total horizon:

- ▶ At Highway 21 and Highway 9, a westbound left-turn protected/permmissive phase should be implemented by the 2020 horizon.
- ▶ At Highway 21 and Durham Street, a westbound left-turn protected/permmissive phase should be implemented by the 2030 horizon.

5.5 Traffic Operations With Improvements

The traffic operations with the 2030 total horizon volumes were analysed in Synchro 9, with the improvements noted above. It was found that the traffic is forecast to operate in a satisfactory manor with the improvement. Of note, the new signal at Highway 21 and Russell Street was found to operate best with a westbound and southbound protected / permmissive left-turn phases in addition to the improvements noted in Section 5.1.1. A summary of the 2030 total traffic operations and the detailed Synchro reports are included in **Appendix J**.





Left-turn Lane Warrant Nomographs Highway 9 and Durham Street

6 Conclusions and Recommendations

6.1 Conclusions

Based on the analyses contained in the report, it is concluded that:

- ▶ The intersections within the study area operate within acceptable levels.
- ▶ The westbound left-turn movement on Highway 9 at Highway 21 is forecast to operate at LOS F during the PM peak hour at the 2030 background horizon, the 2020 total horizon, 2025 total horizon, and 2030 total horizon.
- ▶ The westbound left-turn movement on Durham Street at Highway 21 is forecast to operate at LOS F during the PM peak hour at the 2030 total horizon.
- ▶ The sidestreet operations of the intersection of Highway 21 and Russell Street operate at LOS F during the PM peak hour at the 2020 total horizon, 2025 total horizon, and during both peak hours at the 2030 total horizon.
- ▶ The eastbound movements on Kincardine Avenue at Highway 21 are forecast to operate at LOS F during the PM peak hour at the 2025 and 2030 total horizons.

The following improvements are warranted:

- ▶ A westbound protected / permissive left-turn phase is forecast to be warranted at the intersection of Highway 21 and Highway 9 at the 2020 horizon.
- ▶ A westbound protected / permissive left-turn phase is forecast to be warranted at the intersection of Highway 21 and Durham Street at the 2030 horizon.
- ▶ A signal is forecast to be warranted by the 2020 horizon at the intersection of Highway 21 and Russell Street. Along with signalization, westbound and southbound left-turn lanes should be constructed as well as westbound and southbound protected / permissive left-turn phases.
- ▶ A northbound right turn lane is forecast to be warranted on Highway 21 at Durham Street.
- ▶ A northbound right turn lane is forecast to be warranted on Highway 21 at Russell Street.



6.2 Recommendations

Based on the foregoing analyses, it is recommended that the planning applications be approved as proposed with the following conditions related to transportation system improvements:

- ▶ A westbound protected / permissive phase be implemented at the intersection of Highway 21 and Highway 9.
- ▶ A westbound protected / permissive phase be implemented at the intersection of Highway 21 and Durham Street.
- ▶ A northbound right-turn lane be constructed on Highway 21 at Durham Street.
- ▶ A signal be constructed at the intersection of Highway 21 and Russell Street with a westbound and southbound left-turn lanes, a northbound right-turn lane and westbound and southbound protected / permissive left-turn phases.





Appendix A

Base Year Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall
				Eastbound				Westbound				Northbound				Southbound				
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS Delay V/C Queue	D 39 0.19 12.8	C 21 0.36 18.4	C 21 0.36 18.4	C 25	D 41 0.27 17.0	D 39 0.22 17.9	A 4 0.11 2.3	C 32	A 4 0.09 8.4	A 4 0.20 22.0	A 4 0.20 22.0	A 4 0.02 2.0	A 4 0.11 12.8	A 0 0.01 0.2	A 3	B 11	
	2 - Highway 21 & Durham Street	Signal	LOS Delay V/C Queue	D 52 0.53 31.8	D 43 0.44 33.6	D 43 0.44 33.6	D 47	D 50 0.48 28.7	D 41 0.27 24.0	B 12 0.36 14.2	C 32	A 8 0.08 11.2	A 8 0.27 40.4	A 8 0.27 40.4	A 3 0.13 9.2	A 5 0.13 17.0	A 1 0.03 2.4	A 4	B 19	
	3 - Durham Street & Millennium Way	TWSC	LOS Delay V/C Queue	A 5 0.02 0.5		A 5 0.02 0.5	A 5						A 10 0.02 0.6	A 10 0.02 0.6		A 10 0.02 0.4	A 9 0.02 0.4	A 9 0.02 0.4	A 9	7
	4 - Highway 21 & Russell Street	TWSC	LOS Delay V/C Queue	B 13 0.18 5.2		B 13 0.18 5.2	B 13						A 8 0.03 0.7	A 0 0.17 0.0		A 1	A 0 0.15 0.0	A 0 0.03 0.0	A 0	2
	5 - Highway 21 & Kincardine Avenue	TWSC	LOS Delay V/C Queue	B 14 0.17 5.0	B 14 0.17 5.0	B 14 0.17 5.0	B 14	B 11 0.04 1.0	B 11 0.04 1.0	B 11 0.04 1.0	B 11	A 8 0.02 0.4	A 0 0.14 0.0	A 0 0.14 0.0	A 1	A 0 0.01 0.2	A 0 0.01 0.2	A 0 0.04 0.0	A 0	3
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS Delay V/C Queue	C 34 0.22 15.8	C 26 0.73 44.9	C 26 0.73 44.9	C 27	E 64 0.59 18.7	C 32 0.17 16.1	A 0 0.04 0.0	D 42	A 7 0.23 23.5	A 6 0.20 28.0	A 6 0.20 28.0	A 6 0.03 4.9	A 7 0.25 39.6	A 1 0.02 1.8	A 6	B 15	
	2 - Highway 21 & Durham Street	Signal	LOS Delay V/C Queue	C 34 0.33 27.3	C 33 0.43 43.6	C 33 0.43 43.6	C 34	E 58 0.78 55.5	C 33 0.29 32.2	A 7 0.32 14.0	C 34	B 16 0.09 13.6	B 16 0.34 66.3	B 16 0.34 66.3	B 16 0.27 27.9	A 10 0.31 57.1	A 3 0.07 6.3	A 8	C 20	
	3 - Durham Street & Millennium Way	TWSC	LOS Delay V/C Queue	A 6 0.02 0.6		A 6 0.02 0.6	A 6						A 10 0.06 1.6	A 10 0.06 1.6		A 9 0.04 0.9	A 9 0.04 0.9	A 9	8	
	4 - Highway 21 & Russell Street	TWSC	LOS Delay V/C Queue	C 21 0.39 14.5		C 21 0.39 14.5	C 21						A 9 0.05 1.3	A 0 0.15 0.0		A 1	A 0 0.30 0.0	A 0 0.06 0.0	A 0	3
	5 - Highway 21 & Kincardine Avenue	TWSC	LOS Delay V/C Queue	C 18 0.24 7.2	C 18 0.24 7.2	C 18 0.24 7.2	C 18	C 16 0.06 1.6	C 16 0.06 1.6	C 16 0.06 1.6	C 16	A 9 0.03 0.7	A 0 0.15 0.0	A 0 0.15 0.0	A 1 0.02 0.4	A 1 0.02 0.4	A 0 0.05 0.0	A 1	3	



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Existing AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	26	27	52	39	42	21	78	221	28	11	137	15
Future Volume (vph)	26	27	52	39	42	21	78	221	28	11	137	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.901				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1640	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.727			0.701			0.662			0.593		
Satd. Flow (perm)	1303	1640	0	1332	1827	1380	1187	1766	0	939	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		57				52		11				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			694.0			358.0			262.4	
Travel Time (s)		17.0			31.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	28	29	57	42	46	23	85	240	30	12	149	16
Shared Lane Traffic (%)												
Lane Group Flow (vph)	28	86	0	42	46	23	85	270	0	12	149	16
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	10.3	10.3		10.3	10.3	10.3	70.2	70.2		70.2	70.2	70.2
Actuated g/C Ratio	0.11	0.11		0.11	0.11	0.11	0.78	0.78		0.78	0.78	0.78
v/c Ratio	0.19	0.36		0.27	0.22	0.11	0.09	0.20		0.02	0.11	0.01
Control Delay	39.1	20.6		41.2	38.8	3.7	4.0	3.9		3.7	3.8	0.0
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	39.1	20.6		41.2	38.8	3.7	4.0	3.9		3.7	3.8	0.0
LOS	D	C		D	D	A	A	A		A	A	A
Approach Delay		25.2			32.4			3.9			3.4	
Approach LOS		C			C			A			A	
Queue Length 50th (m)	4.7	4.9		7.2	7.8	0.0	3.8	12.4		0.5	6.6	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Existing AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	82	85	12	72	60	93	57	177	96	96	147	29
Future Volume (vph)	82	85	12	72	60	93	57	177	96	96	147	29
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.981				0.850		0.947				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1852	0	1770	1863	1509	1805	1664	0	1626	1712	1583
Flt Permitted	0.715			0.689			0.656			0.562		
Satd. Flow (perm)	1332	1852	0	1283	1863	1509	1246	1664	0	962	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		7				101		35				38
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8				358.0
Travel Time (s)		10.1			13.6			22.0				16.1
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	89	92	13	78	65	101	62	192	104	104	160	32
Shared Lane Traffic (%)												
Lane Group Flow (vph)	89	105	0	78	65	101	62	296	0	104	160	32
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	12.7	12.7		12.7	12.7	12.7	66.0	66.0		78.8	73.5	73.5
Actuated g/C Ratio	0.13	0.13		0.13	0.13	0.13	0.66	0.66		0.79	0.74	0.74
v/c Ratio	0.53	0.44		0.48	0.27	0.36	0.08	0.27		0.13	0.13	0.03
Control Delay	51.6	42.5		49.8	41.3	11.5	8.1	7.9		3.2	4.6	1.4
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	51.6	42.5		49.8	41.3	11.5	8.1	7.9		3.2	4.6	1.4
LOS	D	D		D	D	B	A	A		A	A	A
Approach Delay		46.7			31.7			7.9			3.7	
Approach LOS		D			C			A			A	
Queue Length 50th (m)	17.4	18.9		15.1	12.3	0.0	4.2	19.8		3.6	7.8	0.0

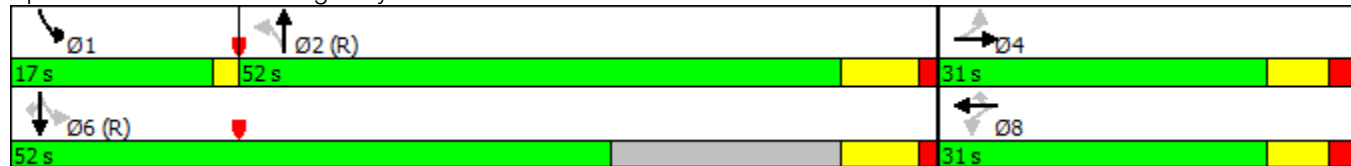


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	31.8	33.6		28.7	24.0	14.2	11.2	40.4		9.2	17.0	2.4
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	326	459		314	456	445	822	1110		857	1257	1173
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.27	0.23		0.25	0.14	0.23	0.08	0.27		0.12	0.13	0.03

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.53
Intersection Signal Delay:	19.0
Intersection LOS:	B
Intersection Capacity Utilization:	62.1%
ICU Level of Service:	B
Analysis Period (min):	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	30	13	16	1	3	14
Future Volume (vph)	30	13	16	1	3	14
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.960			0.887		
Flt Protected	0.966			0.955		
Satd. Flow (prot)	1649	0	0	1468	1685	0
Flt Permitted	0.966			0.955		
Satd. Flow (perm)	1649	0	0	1468	1685	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	23%	25%	0%	0%	0%
Adj. Flow (vph)	33	14	17	1	3	15
Shared Lane Traffic (%)						
Lane Group Flow (vph)	47	0	0	18	18	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	17.6%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Existing AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	30	13	16	1	3	14
Future Volume (Veh/h)	30	13	16	1	3	14
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	33	14	17	1	3	15
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		90	73	80	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		90	73	80	0
tC, single (s)	4.1		7.3	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.7	4.0	4.0	3.3
p0 queue free %	98		98	100	100	99
cM capacity (veh/h)	1636		816	805	798	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	47	18	18			
Volume Left	33	17	0			
Volume Right	14	0	15			
cSH	1636	816	1028			
Volume to Capacity	0.02	0.02	0.02			
Queue Length 95th (m)	0.5	0.5	0.4			
Control Delay (s)	5.1	9.5	8.6			
Lane LOS	A	A	A			
Approach Delay (s)	5.1	9.5	8.6			
Approach LOS		A	A			
Intersection Summary						
Average Delay			6.8			
Intersection Capacity Utilization			17.6%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	54	33	31	272	237	42
Future Volume (vph)	54	33	31	272	237	42
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.949					0.850
Flt Protected	0.970		0.950			
Satd. Flow (prot)	1678	0	1752	1776	1759	1524
Flt Permitted	0.970		0.950			
Satd. Flow (perm)	1678	0	1752	1776	1759	1524
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	3%	3%	7%	8%	6%
Adj. Flow (vph)	59	36	34	296	258	46
Shared Lane Traffic (%)						
Lane Group Flow (vph)	95	0	34	296	258	46
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	30.8%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Existing AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	54	33	31	272	237	42
Future Volume (Veh/h)	54	33	31	272	237	42
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	59	36	34	296	258	46
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	622	258	304			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	622	258	304			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	86	95	97			
cM capacity (veh/h)	433	778	1251			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	95	34	296	258	46	
Volume Left	59	34	0	0	0	
Volume Right	36	0	0	0	46	
cSH	521	1251	1700	1700	1700	
Volume to Capacity	0.18	0.03	0.17	0.15	0.03	
Queue Length 95th (m)	5.3	0.7	0.0	0.0	0.0	
Control Delay (s)	13.4	8.0	0.0	0.0	0.0	
Lane LOS	B	A				
Approach Delay (s)	13.4	0.8		0.0		
Approach LOS	B					
Intersection Summary						
Average Delay			2.1			
Intersection Capacity Utilization			30.8%	ICU Level of Service		A
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Existing AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	61	8	21	1	7	16	19	215	1	9	198	56
Future Volume (vph)	61	8	21	1	7	16	19	215	1	9	198	56
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.912			0.999				0.850
Flt Protected		0.958			0.998		0.950				0.998	
Satd. Flow (prot)	0	1747	1538	0	1729	0	1626	1726	0	0	1731	1615
Flt Permitted		0.958			0.998		0.950				0.998	
Satd. Flow (perm)	0	1747	1538	0	1729	0	1626	1726	0	0	1731	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	66	9	23	1	8	17	21	234	1	10	215	61
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	75	23	0	26	0	21	235	0	0	225	61
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	34.9%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Existing AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↗	↘		↔		↖	↗			↖	↗
Traffic Volume (veh/h)	61	8	21	1	7	16	19	215	1	9	198	56
Future Volume (Veh/h)	61	8	21	1	7	16	19	215	1	9	198	56
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	66	9	23	1	8	17	21	234	1	10	215	61
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	532	512	215	516	572	234	276			235		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	532	512	215	516	572	234	276			235		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	85	98	97	100	98	98	98			99		
cM capacity (veh/h)	432	439	817	444	422	810	1237			1344		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	98	26	21	235	225	61						
Volume Left	66	1	21	0	10	0						
Volume Right	23	17	0	1	0	61						
cSH	566	616	1237	1700	1344	1700						
Volume to Capacity	0.17	0.04	0.02	0.14	0.01	0.04						
Queue Length 95th (m)	5.0	1.1	0.4	0.0	0.2	0.0						
Control Delay (s)	13.7	11.1	8.0	0.0	0.4	0.0						
Lane LOS	B	B	A		A							
Approach Delay (s)	13.7	11.1	0.7		0.3							
Approach LOS	B	B										
Intersection Summary												
Average Delay			2.8									
Intersection Capacity Utilization			34.9%		ICU Level of Service					A		
Analysis Period (min)			15									

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Existing PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	41	66	207	43	44	12	154	183	42	24	297	26
Future Volume (vph)	41	66	207	43	44	12	154	183	42	24	297	26
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.886				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1683	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.726			0.288			0.565			0.607		
Satd. Flow (perm)	1352	1683	0	511	1863	1615	1074	1776	0	1153	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		173				52		21				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			694.0			358.0			262.4	
Travel Time (s)		17.0			31.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	45	72	225	47	48	13	167	199	46	26	323	28
Shared Lane Traffic (%)												
Lane Group Flow (vph)	45	297	0	47	48	13	167	245	0	26	323	28
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	13.9	13.9		13.9	13.9	13.9	61.8	61.8		61.8	61.8	61.8
Actuated g/C Ratio	0.15	0.15		0.15	0.15	0.15	0.69	0.69		0.69	0.69	0.69
v/c Ratio	0.22	0.73		0.59	0.17	0.04	0.23	0.20		0.03	0.25	0.02
Control Delay	33.7	25.6		64.1	32.2	0.2	7.1	5.8		6.0	6.7	1.1
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	33.7	25.6		64.1	32.2	0.2	7.1	5.8		6.0	6.7	1.1
LOS	C	C		E	C	A	A	A		A	A	A
Approach Delay		26.7			42.3			6.3			6.2	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	7.4	21.3		8.2	7.8	0.0	9.2	12.0		1.3	18.3	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Existing PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	85	128	33	172	109	135	42	196	98	190	343	71
Future Volume (vph)	85	128	33	172	109	135	42	196	98	190	343	71
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.969				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1830	0	1787	1900	1583	1805	1752	0	1787	1881	1583
Flt Permitted	0.681			0.589			0.540			0.516		
Satd. Flow (perm)	1294	1830	0	1108	1900	1583	1026	1752	0	971	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		12				147		33				77
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	92	139	36	187	118	147	46	213	107	207	373	77
Shared Lane Traffic (%)												
Lane Group Flow (vph)	92	175	0	187	118	147	46	320	0	207	373	77
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	21.7	21.7		21.7	21.7	21.7	52.7	52.7		69.8	64.5	64.5
Actuated g/C Ratio	0.22	0.22		0.22	0.22	0.22	0.53	0.53		0.70	0.64	0.64
v/c Ratio	0.33	0.43		0.78	0.29	0.32	0.09	0.34		0.27	0.31	0.07
Control Delay	34.1	33.2		57.5	32.5	6.6	16.0	15.5		7.2	9.8	2.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	34.1	33.2		57.5	32.5	6.6	16.0	15.5		7.2	9.8	2.5
LOS	C	C		E	C	A	B	B		A	A	A
Approach Delay		33.5			34.4			15.6			8.2	
Approach LOS		C			C			B			A	
Queue Length 50th (m)	15.9	28.8		36.1	20.2	0.0	4.4	31.5		12.6	30.6	0.0

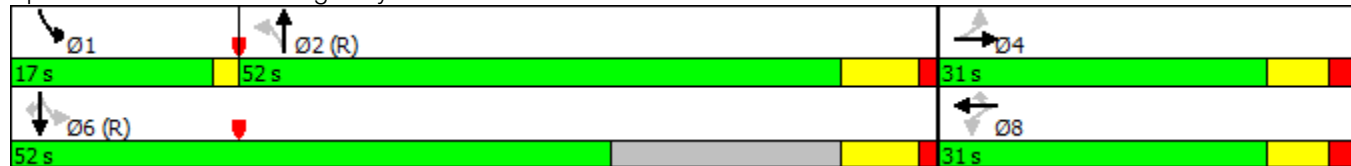


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	27.3	43.6		55.5	32.2	14.0	13.6	66.3		27.9	59.1	6.3
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	334	482		286	491	518	550	954		800	1238	1068
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.28	0.36		0.65	0.24	0.28	0.08	0.34		0.26	0.30	0.07

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.78
Intersection Signal Delay:	20.4
Intersection LOS:	C
Intersection Capacity Utilization:	76.0%
ICU Level of Service:	D
Analysis Period (min):	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	37	10	46	1	8	27
Future Volume (vph)	37	10	46	1	8	27
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.971				0.897	
Flt Protected	0.962			0.953		
Satd. Flow (prot)	1664	0	0	1811	1704	0
Flt Permitted	0.962			0.953		
Satd. Flow (perm)	1664	0	0	1811	1704	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	20%	0%	0%	0%	0%
Adj. Flow (vph)	40	11	50	1	9	29
Shared Lane Traffic (%)						
Lane Group Flow (vph)	51	0	0	51	38	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	19.3%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
3: Millienium Way & Durham Street

Kincardine Business Park TIS
Existing PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	37	10	46	1	8	27
Future Volume (Veh/h)	37	10	46	1	8	27
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	40	11	50	1	9	29
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		119	86	91	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		119	86	91	0
tC, single (s)	4.1		7.1	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.5	4.0	4.0	3.3
p0 queue free %	98		94	100	99	97
cM capacity (veh/h)	1617		815	788	783	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	51	51	38			
Volume Left	40	50	0			
Volume Right	11	0	29			
cSH	1617	815	998			
Volume to Capacity	0.02	0.06	0.04			
Queue Length 95th (m)	0.6	1.6	0.9			
Control Delay (s)	5.8	9.7	8.8			
Lane LOS	A	A	A			
Approach Delay (s)	5.8	9.7	8.8			
Approach LOS		A	A			
Intersection Summary						
Average Delay			8.0			
Intersection Capacity Utilization			19.3%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	88	41	46	241	465	96
Future Volume (vph)	88	41	46	241	465	96
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.957					0.850
Flt Protected	0.967		0.950			
Satd. Flow (prot)	1712	0	1770	1845	1863	1615
Flt Permitted	0.967		0.950			
Satd. Flow (perm)	1712	0	1770	1845	1863	1615
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	3%	2%	0%
Adj. Flow (vph)	96	45	50	262	505	104
Shared Lane Traffic (%)						
Lane Group Flow (vph)	141	0	50	262	505	104
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	45.2%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Existing PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	88	41	46	241	465	96
Future Volume (Veh/h)	88	41	46	241	465	96
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	96	45	50	262	505	104
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	867	505	609			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	867	505	609			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	69	92	95			
cM capacity (veh/h)	305	567	970			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	141	50	262	505	104	
Volume Left	96	50	0	0	0	
Volume Right	45	0	0	0	104	
cSH	358	970	1700	1700	1700	
Volume to Capacity	0.39	0.05	0.15	0.30	0.06	
Queue Length 95th (m)	14.6	1.3	0.0	0.0	0.0	
Control Delay (s)	21.4	8.9	0.0	0.0	0.0	
Lane LOS	C	A				
Approach Delay (s)	21.4	1.4		0.0		
Approach LOS	C					
Intersection Summary						
Average Delay			3.3			
Intersection Capacity Utilization			45.2%		ICU Level of Service	A
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Existing PM






















Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	57	5	30	3	9	9	29	228	3	20	385	86
Future Volume (vph)	57	5	30	3	9	9	29	228	3	20	385	86
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.941			0.998				0.850
Flt Protected		0.956			0.994		0.950				0.998	
Satd. Flow (prot)	0	1752	1615	0	1561	0	1805	1824	0	0	1856	1615
Flt Permitted		0.956			0.994		0.950				0.998	
Satd. Flow (perm)	0	1752	1615	0	1561	0	1805	1824	0	0	1856	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	62	5	33	3	10	10	32	248	3	22	418	93
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	67	33	0	23	0	32	251	0	0	440	93
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	53.3%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Existing PM

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	57	5	30	3	9	9	29	228	3	20	385	86
Future Volume (Veh/h)	57	5	30	3	9	9	29	228	3	20	385	86
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	62	5	33	3	10	10	32	248	3	22	418	93
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	789	777	418	778	868	250	511			251		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	789	777	418	778	868	250	511			251		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	78	98	95	99	96	99	97			98		
cM capacity (veh/h)	283	315	639	252	257	794	1065			1297		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	100	23	32	251	440	93						
Volume Left	62	3	32	0	22	0						
Volume Right	33	10	0	3	0	93						
cSH	426	363	1065	1700	1297	1700						
Volume to Capacity	0.23	0.06	0.03	0.15	0.02	0.05						
Queue Length 95th (m)	7.2	1.6	0.7	0.0	0.4	0.0						
Control Delay (s)	18.0	15.6	8.5	0.0	0.6	0.0						
Lane LOS	C	C	A		A							
Approach Delay (s)	18.0	15.6	1.0		0.5							
Approach LOS	C	C										
Intersection Summary												
Average Delay			2.8									
Intersection Capacity Utilization			53.3%	ICU Level of Service				A				
Analysis Period (min)			15									

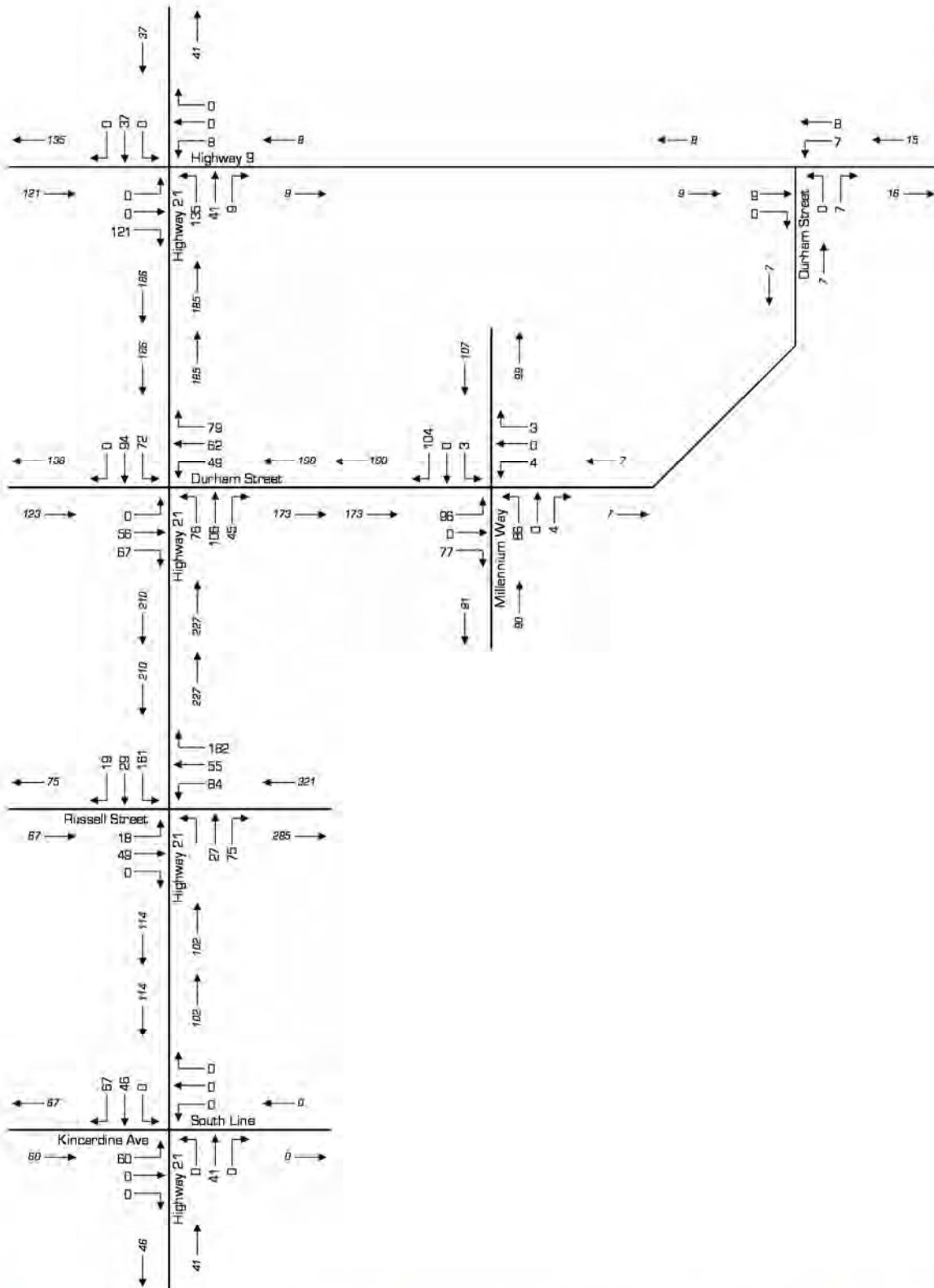


Appendix B

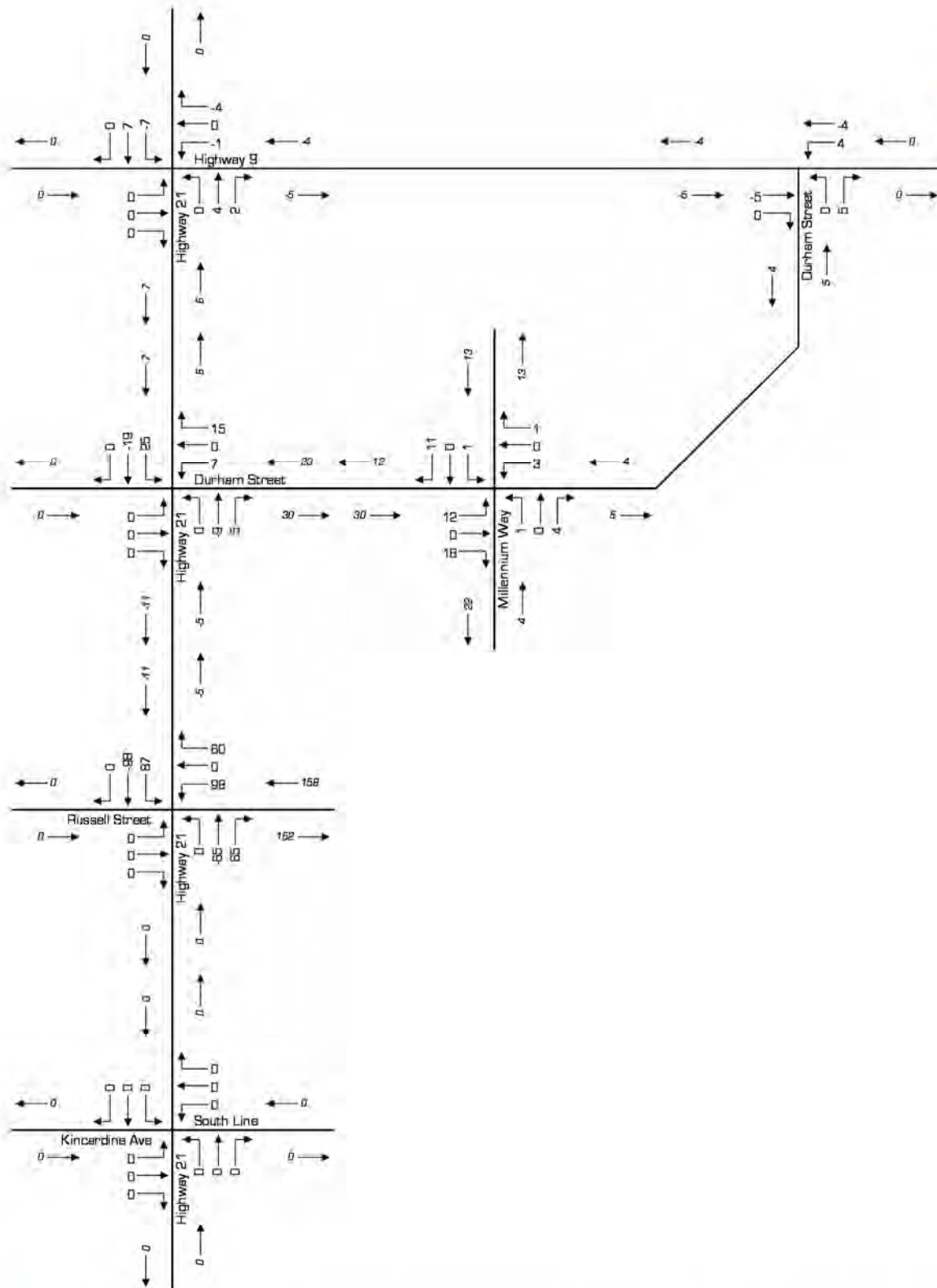
Development Generated Trip Forecasts







Development PM Peak Hour Traffic Volume Forecasts – New Trips



Development PM Peak Hour Traffic Volume Forecasts – Passby

Appendix C

2020 Background Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall		
				Eastbound				Westbound				Northbound				Southbound						
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach			
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	C	C	C	D	D	A	C	A	A	A	A	A	A	A	A	A	B	
			Delay	39	21	21	25	42	39	5	33	4	4	4	4	4	4	0	4	4	4	11
			V/C	0.21	0.39	0.39		0.31	0.23	0.12		0.10	0.22	0.22		0.02	0.12	0.01				
			Queue	13.9	19.5	19.5		18.4	19.0	2.8		9.4	25.1	25.1		2.2	14.5	0.4				
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	D	D	B	C	A	A	A	A	A	A	A	A	A	A	B
Delay			52	43	43	47	50	41	11	32	9	9	9	9	4	5	2	4	4	4	19	
V/C			0.56	0.46	0.46		0.51	0.29	0.38		0.09	0.31	0.31		0.15	0.14	0.03					
Queue			34.1	36.3	36.3		30.8	25.4	14.8		12.5	47.5	47.5		10.6	19.2	2.8					
3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A					A	A		A	A	A	A	A	A	A	7	
		Delay	5		5	5					10	10		10	9	9	9	9	9	9	9	
		V/C	0.02		0.02						0.03	0.03			0.02	0.02						
		Queue	0.5		0.5						0.6	0.6			0.5	0.5						
4 - Highway 21 & Russell Street	TWSC	LOS	B		B	B					A	A		A	A	A	A	A	A	A	2	
		Delay	14		14	14					8	0		1	0	0	0	0	0	0	0	
		V/C	0.21		0.21						0.03	0.19			0.17	0.03						
		Queue	6.4		6.4						0.7	0.0			0.0	0.0						
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	B	B	B	B	B	A	A	A	A	A	A	A	A	A	A	3	
		Delay	15	15	15	14	11	11	11	11	8	0	0	1	0	0	0	0	0	0	0	
		V/C	0.21	0.21	0.21		0.05	0.05	0.05		0.02	0.15	0.15		0.01	0.01	0.04					
		Queue	5.0	5.0	5.0		1.0	1.0	1.0		0.4	0.0	0.0		0.2	0.2	0.0					
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	E	C	A	D	A	A	A	A	A	A	A	A	A	B	
			Delay	32	28	28	28	69	31	0	44	8	7	7	7	7	8	2	7	7	16	
			V/C	0.22	0.76	0.76		0.65	0.17	0.04		0.26	0.22	0.22		0.04	0.28	0.03				
			Queue	16.3	51.1	51.1		20.3	16.5	0.0		28.3	32.9	32.9		5.6	46.9	2.4				
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	D	C	A	C	B	B	B	B	A	B	A	A	A	A	C
Delay			32	31	31	31	53	30	6	32	19	19	19	19	9	12	3	10	10	10	21	
V/C			0.32	0.42	0.42		0.77	0.28	0.32		0.10	0.40	0.40		0.33	0.35	0.08					
Queue			28.8	45.9	45.9		59.4	33.6	14.1		15.7	79.7	79.7		32.8	70.2	6.9					
3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A					A	A		A	A	A	A	A	A	A	8	
		Delay	6		6	6					10	10		10	9	9	9	9	9	9	8	
		V/C	0.03		0.03						0.07	0.07			0.04	0.04						
		Queue	0.7		0.7						1.8	1.8			1.1	1.1						
4 - Highway 21 & Russell Street	TWSC	LOS	D		D	D					A	A		A	A	A	A	A	A	A	4	
		Delay	27		27	27					9	0		1	0	0	0	0	0	0	0	
		V/C	0.49		0.49						0.06	0.17			0.33	0.07						
		Queue	20.2		20.2						1.5	0.0			0.0	0.0						
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	C	C	C	C	A	A	A	A	A	A	A	A	A	A	3	
		Delay	21	21	21	21	17	17	17	17	9	0	0	1	1	1	0	1	1	1	3	
		V/C	0.30	0.30	0.30		0.08	0.08	0.08		0.03	0.16	0.16		0.02	0.02	0.06					
		Queue	9.9	9.9	9.9		2.0	2.0	2.0		0.8	0.0	0.0		0.5	0.5	0.0					



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2020 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	29	30	57	43	46	23	86	243	31	12	151	17
Future Volume (vph)	29	30	57	43	46	23	86	243	31	12	151	17
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.902				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1641	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.724			0.695			0.653			0.578		
Satd. Flow (perm)	1298	1641	0	1320	1827	1380	1170	1766	0	915	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		62				52		12				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	32	33	62	47	50	25	93	264	34	13	164	18
Shared Lane Traffic (%)												
Lane Group Flow (vph)	32	95	0	47	50	25	93	298	0	13	164	18
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	10.5	10.5		10.5	10.5	10.5	70.1	70.1		70.1	70.1	70.1
Actuated g/C Ratio	0.12	0.12		0.12	0.12	0.12	0.78	0.78		0.78	0.78	0.78
v/c Ratio	0.21	0.39		0.31	0.23	0.12	0.10	0.22		0.02	0.12	0.01
Control Delay	39.4	20.7		41.9	38.8	4.6	4.1	4.1		3.8	3.9	0.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	39.4	20.7		41.9	38.8	4.6	4.1	4.1		3.8	3.9	0.2
LOS	D	C		D	D	A	A	A		A	A	A
Approach Delay		25.4			33.0			4.1			3.5	
Approach LOS		C			C			A			A	
Queue Length 50th (m)	5.4	5.6		8.0	8.5	0.0	4.1	13.9		0.6	7.4	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2020 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	90	94	13	79	66	102	63	195	106	106	162	32
Future Volume (vph)	90	94	13	79	66	102	63	195	106	106	162	32
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.982				0.850		0.947				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1855	0	1770	1863	1509	1805	1664	0	1626	1712	1583
Flt Permitted	0.710			0.682			0.646			0.539		
Satd. Flow (perm)	1323	1855	0	1270	1863	1509	1227	1664	0	923	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		7				111		35				38
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8				358.0
Travel Time (s)		10.1			13.6			22.0				16.1
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	98	102	14	86	72	111	68	212	115	115	176	35
Shared Lane Traffic (%)												
Lane Group Flow (vph)	98	116	0	86	72	111	68	327	0	115	176	35
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	13.3	13.3		13.3	13.3	13.3	63.6	63.6		78.2	72.9	72.9
Actuated g/C Ratio	0.13	0.13		0.13	0.13	0.13	0.64	0.64		0.78	0.73	0.73
v/c Ratio	0.56	0.46		0.51	0.29	0.38	0.09	0.31		0.15	0.14	0.03
Control Delay	52.2	42.7		50.3	41.0	10.9	8.6	8.9		3.5	4.9	1.6
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	52.2	42.7		50.3	41.0	10.9	8.6	8.9		3.5	4.9	1.6
LOS	D	D		D	D	B	A	A		A	A	A
Approach Delay		47.0			31.6			8.9			4.0	
Approach LOS		D			C			A			A	
Queue Length 50th (m)	19.1	20.9		16.7	13.5	0.0	4.7	23.4		4.2	8.9	0.0

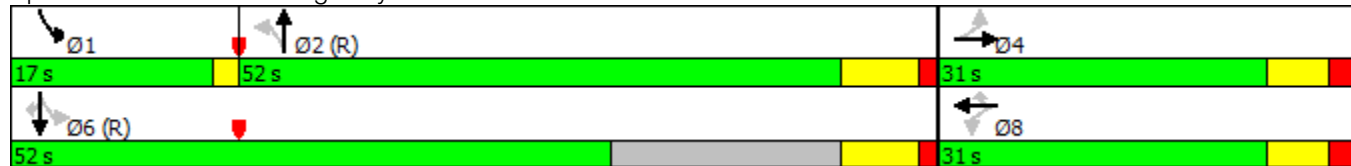


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	34.1	36.3		30.8	25.4	14.8	12.5	47.5		10.6	19.2	2.8
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	324	459		311	456	453	780	1071		827	1247	1164
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.30	0.25		0.28	0.16	0.25	0.09	0.31		0.14	0.14	0.03

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.56
Intersection Signal Delay:	19.4
Intersection LOS:	B
Intersection Capacity Utilization:	62.6%
ICU Level of Service:	B
Analysis Period (min):	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	33	14	18	1	3	15
Future Volume (vph)	33	14	18	1	3	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.960				0.886	
Flt Protected	0.966			0.955		
Satd. Flow (prot)	1650	0	0	1466	1683	0
Flt Permitted	0.966			0.955		
Satd. Flow (perm)	1650	0	0	1466	1683	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	23%	25%	0%	0%	0%
Adj. Flow (vph)	36	15	20	1	3	16
Shared Lane Traffic (%)						
Lane Group Flow (vph)	51	0	0	21	19	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	17.7%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
3: Millienium Way & Durham Street

Kincardine Business Park TIS
2020 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	33	14	18	1	3	15
Future Volume (Veh/h)	33	14	18	1	3	15
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	36	15	20	1	3	16
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		97	80	87	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		97	80	87	0
tC, single (s)	4.1		7.3	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.7	4.0	4.0	3.3
p0 queue free %	98		98	100	100	99
cM capacity (veh/h)	1636		805	797	789	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	51	21	19			
Volume Left	36	20	0			
Volume Right	15	0	16			
cSH	1636	805	1029			
Volume to Capacity	0.02	0.03	0.02			
Queue Length 95th (m)	0.5	0.6	0.5			
Control Delay (s)	5.2	9.6	8.6			
Lane LOS	A	A	A			
Approach Delay (s)	5.2	9.6	8.6			
Approach LOS		A	A			
Intersection Summary						
Average Delay			6.9			
Intersection Capacity Utilization			17.7%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	59	36	34	299	261	46
Future Volume (vph)	59	36	34	299	261	46
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.949					0.850
Flt Protected	0.970		0.950			
Satd. Flow (prot)	1678	0	1752	1776	1759	1524
Flt Permitted	0.970		0.950			
Satd. Flow (perm)	1678	0	1752	1776	1759	1524
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	3%	3%	7%	8%	6%
Adj. Flow (vph)	64	39	37	325	284	50
Shared Lane Traffic (%)						
Lane Group Flow (vph)	103	0	37	325	284	50
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	32.5%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2020 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	59	36	34	299	261	46
Future Volume (Veh/h)	59	36	34	299	261	46
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	64	39	37	325	284	50
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	683	284	334			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	683	284	334			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	84	95	97			
cM capacity (veh/h)	398	753	1220			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	103	37	325	284	50	
Volume Left	64	37	0	0	0	
Volume Right	39	0	0	0	50	
cSH	484	1220	1700	1700	1700	
Volume to Capacity	0.21	0.03	0.19	0.17	0.03	
Queue Length 95th (m)	6.4	0.8	0.0	0.0	0.0	
Control Delay (s)	14.4	8.0	0.0	0.0	0.0	
Lane LOS	B	A				
Approach Delay (s)	14.4	0.8		0.0		
Approach LOS	B					
Intersection Summary						
Average Delay			2.2			
Intersection Capacity Utilization			32.5%		ICU Level of Service	A
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2020 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	67	9	23	1	8	18	21	237	1	10	218	62
Future Volume (vph)	67	9	23	1	8	18	21	237	1	10	218	62
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.910			0.999				0.850
Flt Protected		0.958			0.998		0.950				0.998	
Satd. Flow (prot)	0	1747	1538	0	1726	0	1626	1726	0	0	1731	1615
Flt Permitted		0.958			0.998		0.950				0.998	
Satd. Flow (perm)	0	1747	1538	0	1726	0	1626	1726	0	0	1731	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	73	10	25	1	9	20	23	258	1	11	237	67
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	83	25	0	30	0	23	259	0	0	248	67
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	37.1%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2020 Background AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	67	9	23	1	8	18	21	237	1	10	218	62
Future Volume (Veh/h)	67	9	23	1	8	18	21	237	1	10	218	62
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	73	10	25	1	9	20	23	258	1	11	237	67
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	588	564	237	568	630	258	304			259		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	588	564	237	568	630	258	304			259		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	81	98	97	100	98	97	98			99		
cM capacity (veh/h)	393	408	795	406	390	785	1207			1317		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	108	30	23	259	248	67						
Volume Left	73	1	23	0	11	0						
Volume Right	25	20	0	1	0	67						
cSH	514	588	1207	1700	1317	1700						
Volume to Capacity	0.21	0.05	0.02	0.15	0.01	0.04						
Queue Length 95th (m)	6.3	1.3	0.5	0.0	0.2	0.0						
Control Delay (s)	14.9	11.5	8.0	0.0	0.4	0.0						
Lane LOS	B	B	A		A							
Approach Delay (s)	14.9	11.5	0.7		0.3							
Approach LOS	B	B										
Intersection Summary												
Average Delay			3.1									
Intersection Capacity Utilization			37.1%		ICU Level of Service					A		
Analysis Period (min)			15									

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2020 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	45	73	228	47	48	13	169	201	46	26	327	29
Future Volume (vph)	45	73	228	47	48	13	169	201	46	26	327	29
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.886				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1683	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.723			0.263			0.549			0.594		
Satd. Flow (perm)	1347	1683	0	467	1863	1615	1043	1776	0	1129	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		174				52		21				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	49	79	248	51	52	14	184	218	50	28	355	32
Shared Lane Traffic (%)												
Lane Group Flow (vph)	49	327	0	51	52	14	184	268	0	28	355	32
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	15.2	15.2		15.2	15.2	15.2	60.5	60.5		60.5	60.5	60.5
Actuated g/C Ratio	0.17	0.17		0.17	0.17	0.17	0.67	0.67		0.67	0.67	0.67
v/c Ratio	0.22	0.76		0.65	0.17	0.04	0.26	0.22		0.04	0.28	0.03
Control Delay	32.2	27.8		69.4	30.8	0.2	8.2	6.6		6.7	7.6	1.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	32.2	27.8		69.4	30.8	0.2	8.2	6.6		6.7	7.6	1.5
LOS	C	C		E	C	A	A	A		A	A	A
Approach Delay		28.4			44.0			7.3			7.0	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	7.9	26.5		8.9	8.3	0.0	11.3	14.5		1.5	22.1	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2020 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	94	141	36	189	120	149	46	216	108	209	377	78
Future Volume (vph)	94	141	36	189	120	149	46	216	108	209	377	78
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.970				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1832	0	1787	1900	1583	1805	1752	0	1787	1881	1583
Flt Permitted	0.674			0.573			0.522			0.473		
Satd. Flow (perm)	1281	1832	0	1078	1900	1583	992	1752	0	890	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		12				162		32				85
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	102	153	39	205	130	162	50	235	117	227	410	85
Shared Lane Traffic (%)												
Lane Group Flow (vph)	102	192	0	205	130	162	50	352	0	227	410	85
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	24.7	24.7		24.7	24.7	24.7	48.8	48.8		66.8	61.5	61.5
Actuated g/C Ratio	0.25	0.25		0.25	0.25	0.25	0.49	0.49		0.67	0.62	0.62
v/c Ratio	0.32	0.42		0.77	0.28	0.32	0.10	0.40		0.33	0.35	0.08
Control Delay	31.7	30.9		53.4	30.2	5.8	18.6	18.8		8.8	11.8	2.7
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	31.7	30.9		53.4	30.2	5.8	18.6	18.8		8.8	11.8	2.7
LOS	C	C		D	C	A	B	B		A	B	A
Approach Delay		31.2			31.8			18.8			9.8	
Approach LOS		C			C			B			A	
Queue Length 50th (m)	17.0	30.6		38.7	21.3	0.0	5.3	39.9		16.0	38.5	0.0

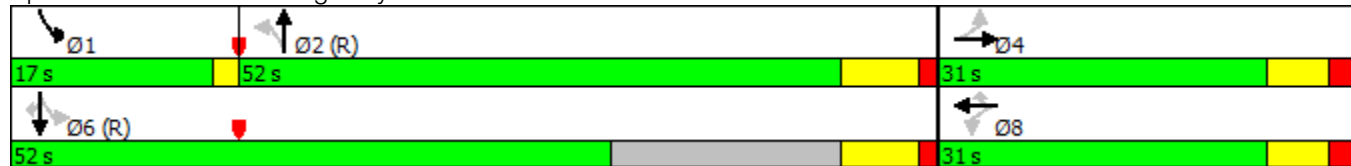


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	28.8	45.9		59.4	33.6	14.1	15.7	79.7		32.8	70.2	6.9
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	347	506		293	516	548	504	905		729	1207	1046
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.29	0.38		0.70	0.25	0.30	0.10	0.39		0.31	0.34	0.08

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	60
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.77
Intersection Signal Delay:	20.7
Intersection LOS:	C
Intersection Capacity Utilization	79.6%
ICU Level of Service	D
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	41	11	51	1	9	30
Future Volume (vph)	41	11	51	1	9	30
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.972				0.896	
Flt Protected	0.962			0.953		
Satd. Flow (prot)	1667	0	0	1811	1702	0
Flt Permitted	0.962			0.953		
Satd. Flow (perm)	1667	0	0	1811	1702	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	20%	0%	0%	0%	0%
Adj. Flow (vph)	45	12	55	1	10	33
Shared Lane Traffic (%)						
Lane Group Flow (vph)	57	0	0	56	43	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	19.5%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 2020 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	41	11	51	1	9	30
Future Volume (Veh/h)	41	11	51	1	9	30
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	45	12	55	1	10	33
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		134	96	102	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		134	96	102	0
tC, single (s)	4.1		7.1	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.5	4.0	4.0	3.3
p0 queue free %	97		93	100	99	97
cM capacity (veh/h)	1617		792	776	770	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	57	56	43			
Volume Left	45	55	0			
Volume Right	12	0	33			
cSH	1617	791	994			
Volume to Capacity	0.03	0.07	0.04			
Queue Length 95th (m)	0.7	1.8	1.1			
Control Delay (s)	5.8	9.9	8.8			
Lane LOS	A	A	A			
Approach Delay (s)	5.8	9.9	8.8			
Approach LOS		A	A			
Intersection Summary						
Average Delay			8.1			
Intersection Capacity Utilization			19.5%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	97	45	51	265	512	106
Future Volume (vph)	97	45	51	265	512	106
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.957					0.850
Flt Protected	0.967		0.950			
Satd. Flow (prot)	1712	0	1770	1845	1863	1615
Flt Permitted	0.967		0.950			
Satd. Flow (perm)	1712	0	1770	1845	1863	1615
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	3%	2%	0%
Adj. Flow (vph)	105	49	55	288	557	115
Shared Lane Traffic (%)						
Lane Group Flow (vph)	154	0	55	288	557	115
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	48.4%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2020 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	97	45	51	265	512	106
Future Volume (Veh/h)	97	45	51	265	512	106
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	105	49	55	288	557	115
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	955	557	672			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	955	557	672			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	61	91	94			
cM capacity (veh/h)	268	530	919			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	154	55	288	557	115	
Volume Left	105	55	0	0	0	
Volume Right	49	0	0	0	115	
cSH	318	919	1700	1700	1700	
Volume to Capacity	0.48	0.06	0.17	0.33	0.07	
Queue Length 95th (m)	20.0	1.5	0.0	0.0	0.0	
Control Delay (s)	26.5	9.2	0.0	0.0	0.0	
Lane LOS	D	A				
Approach Delay (s)	26.5	1.5		0.0		
Approach LOS	D					
Intersection Summary						
Average Delay	3.9					
Intersection Capacity Utilization	48.4%			ICU Level of Service	A	
Analysis Period (min)	15					

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2020 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	63	6	33	3	10	10	32	251	3	22	424	95
Future Volume (vph)	63	6	33	3	10	10	32	251	3	22	424	95
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.941			0.998				0.850
Flt Protected		0.957			0.994		0.950				0.998	
Satd. Flow (prot)	0	1755	1615	0	1564	0	1805	1824	0	0	1856	1615
Flt Permitted		0.957			0.994		0.950				0.998	
Satd. Flow (perm)	0	1755	1615	0	1564	0	1805	1824	0	0	1856	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	68	7	36	3	11	11	35	273	3	24	461	103
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	75	36	0	25	0	35	276	0	0	485	103
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	57.4%
ICU Level of Service	B
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2020 Background PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	63	6	33	3	10	10	32	251	3	22	424	95
Future Volume (Veh/h)	63	6	33	3	10	10	32	251	3	22	424	95
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	68	7	36	3	11	11	35	273	3	24	461	103
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	868	855	461	857	956	274	564			276		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	868	855	461	857	956	274	564			276		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	72	98	94	99	95	99	97			98		
cM capacity (veh/h)	246	282	605	218	226	769	1018			1270		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	111	25	35	276	485	103						
Volume Left	68	3	35	0	24	0						
Volume Right	36	11	0	3	0	103						
cSH	369	326	1018	1700	1270	1700						
Volume to Capacity	0.30	0.08	0.03	0.16	0.02	0.06						
Queue Length 95th (m)	9.9	2.0	0.9	0.0	0.5	0.0						
Control Delay (s)	20.9	17.0	8.7	0.0	0.6	0.0						
Lane LOS	C	C	A		A							
Approach Delay (s)	20.9	17.0	1.0		0.5							
Approach LOS	C	C										
Intersection Summary												
Average Delay			3.2									
Intersection Capacity Utilization			57.4%		ICU Level of Service					B		
Analysis Period (min)			15									



Appendix D

2020 Total Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall	
				Eastbound				Westbound				Northbound				Southbound					
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach		
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	B	B	C	D	D	A	C	A	A	A	A	A	A	A	A	B	
			Delay	38	17	17	20	45	38	4	34	5	5	5	5	4	5	0	4	4	12
			V/C	0.20	0.54	0.54		0.39	0.23	0.12		0.17	0.25	0.25		0.02	0.15	0.02			
			Queue	13.7	23.8	23.8		19.7	18.6	2.7		14.7	28.4	28.4		2.4	17.4	0.4			
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	E	D	A	D	B	B	B	B	A	A	A	A	A	C
			Delay	45	45	45	45	68	39	9	36	11	12	12	12	5	6	2	5	5	22
V/C			0.48	0.64	0.64		0.75	0.32	0.40		0.13	0.39	0.39		0.24	0.19	0.03				
Queue			32.3	52.6	52.6		38.1	30.4	15.5		18.9	69.6	69.6		17.7	28.5	3.2				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	B	B	B	B	A	A	A	A	A	A	7	
		Delay	5	5	5	5	3	3	3	3	13	13	13	13	9	9	9	9	9	9	
		V/C	0.07	0.07	0.07		0.00	0.00	0.00		0.10	0.10	0.10		0.07	0.07	0.07				
		Queue	1.9	1.9	1.9		0.0	0.0	0.0		2.6	2.6	2.6		1.8	1.8	1.8				
4 - Highway 21 & Russell Street	TWSC	LOS	E	E	E	E	C	C	C	C	A	A	A	A	A	A	A	A	A	8	
		Delay	38	38	38	38	20	20	20	20	8	0	0	0	3	3	0	1	2	2	
		V/C	0.59	0.59	0.59		0.28	0.28	0.28		0.03	0.23	0.23		0.07	0.07	0.03				
		Queue	26.9	26.9	26.9		9.2	9.2	9.2		0.8	0.0	0.0		1.9	1.9	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	B	B	B	B	A	A	A	A	A	A	A	A	A	4	
		Delay	18	18	18	18	12	12	12	12	8	0	0	0	0	0	0	0	0	0	
		V/C	0.32	0.32	0.32		0.05	0.05	0.05		0.02	0.17	0.17		0.01	0.01	0.05				
		Queue	11.0	11.0	11.0		1.3	1.3	1.3		0.5	0.0	0.0		0.2	0.2	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A						0	
		Delay		0	0	0	0	0	0		9	9		9	9						
		V/C		0.05	0.05		0.00	0.00			0.00				0.00						
		Queue		0.0	0.0		0.1	0.1			0.1				0.1						
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	F	C	A	D	B	A	A	B	A	B	A	A	B	
			Delay	27	23	23	23	84	26	0	52	17	10	10	13	9	11	2	10	10	
			V/C	0.16	0.79	0.79		0.77	0.12	0.02		0.56	0.30	0.30		0.03	0.35	0.03			
			Queue	15.7	66.5	66.5		30.0	15.9	0.0		68.0	44.3	44.3		4.9	58.0	2.6			
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	D	C	A	C	C	D	D	D	D	C	A	C	C	
			Delay	26	27	27	27	53	25	5	28	28	39	39	36	42	20	3	26	29	
V/C			0.23	0.47	0.47		0.82	0.27	0.35		0.42	0.82	0.82		0.90	0.54	0.11				
Queue			31.8	84.5	84.5		113.3	53.2	18.8		32.1	109.6	109.6		54.4	76.3	6.7				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	A	C	C	C	C	A	A	A	A	A		
		Delay	5	5	5	5	5	5	5	5	23	23	23	23	10	10	10	10	10		
		V/C	0.10	0.10	0.10		0.01	0.01	0.01		0.45	0.45	0.45		0.18	0.18	0.18				
		Queue	2.7	2.7	2.7		0.1	0.1	0.1		18.0	18.0	18.0		5.1	5.1	5.1				
4 - Highway 21 & Russell Street	TWSC	LOS	F	F	F	F	F	F	F	F	A	A	A	A	A	A	A	A	A		
		Delay	Err	Err	Err	9999	Err	Err	Err	Err	Err	9	0	0	1	5	5	0	4	3583	
		V/C	9.33	9.33	9.33		6.72	6.72	6.72		0.06	0.23	0.23		0.23	0.23	0.08				
		Queue	Err	Err	Err		Err	Err	Err		1.5	0.0	0.0		7.2	7.2	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	E	E	E	E	C	C	C	C	A	A	A	A	A	A	A	A	A		
		Delay	42	42	42	42	20	20	20	20	9	0	0	1	1	1	0	1	7		
		V/C	0.66	0.66	0.66		0.09	0.09	0.09		0.04	0.19	0.19		0.02	0.02	0.10				
		Queue	34.1	34.1	34.1		2.5	2.5	2.5		0.9	0.0	0.0		0.5	0.5	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A							
		Delay		0	0	0	1	1			1	9		9	9						
		V/C		0.10	0.10		0.01	0.01			0.02				0.02						
		Queue		0.0	0.0		0.2	0.2			0.4				0.4						



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2020 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	29	30	126	47	46	23	128	256	33	12	172	17
Future Volume (vph)	29	30	126	47	46	23	128	256	33	12	172	17
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.879				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1616	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.724			0.575			0.640			0.570		
Satd. Flow (perm)	1298	1616	0	1092	1827	1380	1147	1766	0	903	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		137				52		12				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0			262.4	
Travel Time (s)		17.0			22.1			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	32	33	137	51	50	25	139	278	36	13	187	18
Shared Lane Traffic (%)												
Lane Group Flow (vph)	32	170	0	51	50	25	139	314	0	13	187	18
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	10.9	10.9		10.9	10.9	10.9	64.8	64.8		64.8	64.8	64.8
Actuated g/C Ratio	0.12	0.12		0.12	0.12	0.12	0.72	0.72		0.72	0.72	0.72
v/c Ratio	0.20	0.54		0.39	0.23	0.12	0.17	0.25		0.02	0.15	0.02
Control Delay	38.3	17.0		45.0	37.8	4.4	4.8	4.8		4.1	4.5	0.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	38.3	17.0		45.0	37.8	4.4	4.8	4.8		4.1	4.5	0.2
LOS	D	B		D	D	A	A	A		A	A	A
Approach Delay		20.4			34.1			4.8			4.1	
Approach LOS		C			C			A			A	
Queue Length 50th (m)	5.4	5.5		8.8	8.5	0.0	6.5	14.9		0.6	8.5	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2020 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	90	130	47	100	88	131	83	223	139	152	208	32
Future Volume (vph)	90	130	47	100	88	131	83	223	139	152	208	32
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.960				0.850		0.942				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1800	0	1770	1863	1509	1805	1661	0	1626	1712	1583
Flt Permitted	0.695			0.495			0.617			0.479		
Satd. Flow (perm)	1295	1800	0	922	1863	1509	1172	1661	0	820	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		17				142		41				38
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8				358.0
Travel Time (s)		10.1			13.6			22.0				16.1
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	98	141	51	109	96	142	90	242	151	165	226	35
Shared Lane Traffic (%)												
Lane Group Flow (vph)	98	192	0	109	96	142	90	393	0	165	226	35
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	15.9	15.9		15.9	15.9	15.9	59.8	59.8		75.6	70.3	70.3
Actuated g/C Ratio	0.16	0.16		0.16	0.16	0.16	0.60	0.60		0.76	0.70	0.70
v/c Ratio	0.48	0.64		0.75	0.32	0.40	0.13	0.39		0.24	0.19	0.03
Control Delay	44.7	44.9		68.2	38.7	9.2	11.3	12.0		4.9	6.3	2.1
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	44.7	44.9		68.2	38.7	9.2	11.3	12.0		4.9	6.3	2.1
LOS	D	D		E	D	A	B	B		A	A	A
Approach Delay		44.8			35.9			11.9			5.4	
Approach LOS		D			D			B			A	
Queue Length 50th (m)	18.5	33.9		21.6	17.7	0.0	7.3	33.7		7.4	13.5	0.0

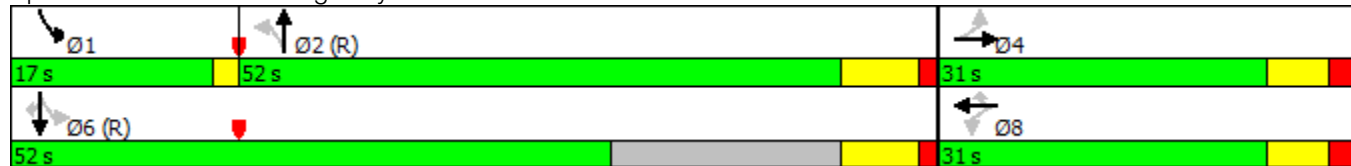


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	32.3	52.6		38.1	30.4	15.5	18.9	69.6		17.7	28.5	3.2
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	317	453		225	456	476	701	1010		741	1203	1124
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.31	0.42		0.48	0.21	0.30	0.13	0.39		0.22	0.19	0.03

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.75
Intersection Signal Delay:	21.7
Intersection LOS:	C
Intersection Capacity Utilization	74.4%
ICU Level of Service	D
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	110	0	54	2	0	3	44	1	1	1	3	61
Future Volume (vph)	110	0	54	2	0	3	44	1	1	1	3	61
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.956			0.919			0.997			0.873	
Flt Protected		0.968			0.980			0.954			0.999	
Satd. Flow (prot)	0	1634	0	0	1678	0	0	1457	0	0	1657	0
Flt Permitted		0.968			0.980			0.954			0.999	
Satd. Flow (perm)	0	1634	0	0	1678	0	0	1457	0	0	1657	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			73.4			138.6			84.1	
Travel Time (s)		13.6			5.3			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	2%	23%	2%	2%	2%	25%	0%	2%	2%	0%	0%
Adj. Flow (vph)	120	0	59	2	0	3	48	1	1	1	3	66
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	179	0	0	5	0	0	50	0	0	70	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	31.4%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2020 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	110	0	54	2	0	3	44	1	1	1	3	61
Future Volume (Veh/h)	110	0	54	2	0	3	44	1	1	1	3	61
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	120	0	59	2	0	3	48	1	1	1	3	66
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage (veh)												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	3			59			342	276	30	276	304	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	3			59			342	276	30	276	304	2
tC, single (s)	4.1			4.1			7.3	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.7	4.0	3.3	3.5	4.0	3.3
p0 queue free %	93			100			90	100	100	100	99	94
cM capacity (veh/h)	1632			1545			503	587	1045	636	566	1089
Direction, Lane #												
	EB 1	WB 1	NB 1	SB 1								
Volume Total	179	5	50	70								
Volume Left	120	2	48	1								
Volume Right	59	3	1	66								
cSH	1632	1545	510	1037								
Volume to Capacity	0.07	0.00	0.10	0.07								
Queue Length 95th (m)	1.9	0.0	2.6	1.7								
Control Delay (s)	5.1	2.9	12.8	8.7								
Lane LOS	A	A	B	A								
Approach Delay (s)	5.1	2.9	12.8	8.7								
Approach LOS			B	A								
Intersection Summary												
Average Delay			7.2									
Intersection Capacity Utilization			31.4%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2020 AM





















Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↕	↕			↕	↕
Traffic Volume (vph)	73	25	36	23	15	49	34	320	37	80	273	54
Future Volume (vph)	73	25	36	23	15	49	34	320	37	80	273	54
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.964			0.924			0.985				0.850
Flt Protected		0.973			0.987		0.950				0.989	
Satd. Flow (prot)	0	1715	0	0	1699	0	1752	1758	0	0	1762	1524
Flt Permitted		0.973			0.987		0.950				0.989	
Satd. Flow (perm)	0	1715	0	0	1699	0	1752	1758	0	0	1762	1524
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			63.0			1178.3			487.8	
Travel Time (s)		5.2			4.5			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	2%	3%	2%	2%	2%	3%	7%	2%	2%	8%	6%
Adj. Flow (vph)	79	27	39	25	16	53	37	348	40	87	297	59
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	145	0	0	94	0	37	388	0	0	384	59
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	62.1%
ICU Level of Service	B
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2020 AM

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	73	25	36	23	15	49	34	320	37	80	273	54
Future Volume (Veh/h)	73	25	36	23	15	49	34	320	37	80	273	54
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	79	27	39	25	16	53	37	348	40	87	297	59
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	954	933	297	966	972	368	356			388		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	954	933	297	966	972	368	356			388		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	58	89	95	87	93	92	97			93		
cM capacity (veh/h)	189	239	740	187	226	677	1197			1170		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	145	94	37	388	384	59						
Volume Left	79	25	37	0	87	0						
Volume Right	39	53	0	40	0	59						
cSH	249	333	1197	1700	1170	1700						
Volume to Capacity	0.58	0.28	0.03	0.23	0.07	0.03						
Queue Length 95th (m)	26.7	9.1	0.8	0.0	1.9	0.0						
Control Delay (s)	37.9	20.0	8.1	0.0	2.5	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	37.9	20.0	0.7		2.1							
Approach LOS	E	C										
Intersection Summary												
Average Delay			7.8									
Intersection Capacity Utilization			62.1%		ICU Level of Service				B			
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2020 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	101	9	23	1	8	18	21	260	1	10	232	83
Future Volume (vph)	101	9	23	1	8	18	21	260	1	10	232	83
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.910			0.999				0.850
Flt Protected		0.956			0.998		0.950				0.998	
Satd. Flow (prot)	0	1749	1538	0	1726	0	1626	1726	0	0	1730	1615
Flt Permitted		0.956			0.998		0.950				0.998	
Satd. Flow (perm)	0	1749	1538	0	1726	0	1626	1726	0	0	1730	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	110	10	25	1	9	20	23	283	1	11	252	90
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	120	25	0	30	0	23	284	0	0	263	90
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	39.7%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2020 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	101	9	23	1	8	18	21	260	1	10	232	83
Future Volume (Veh/h)	101	9	23	1	8	18	21	260	1	10	232	83
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	110	10	25	1	9	20	23	283	1	11	252	90
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	628	604	252	608	694	284	342			284		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	628	604	252	608	694	284	342			284		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	70	97	97	100	97	97	98			99		
cM capacity (veh/h)	369	387	779	381	359	760	1169			1290		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	145	30	23	284	263	90						
Volume Left	110	1	23	0	11	0						
Volume Right	25	20	0	1	0	90						
cSH	447	555	1169	1700	1290	1700						
Volume to Capacity	0.32	0.05	0.02	0.17	0.01	0.05						
Queue Length 95th (m)	11.1	1.4	0.5	0.0	0.2	0.0						
Control Delay (s)	17.7	11.9	8.1	0.0	0.4	0.0						
Lane LOS	C	B	A		A							
Approach Delay (s)	17.7	11.9	0.6		0.3							
Approach LOS	C	B										
Intersection Summary												
Average Delay			3.8									
Intersection Capacity Utilization			39.7%	ICU Level of Service		A						
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	75	0	4	116	0	3
Future Volume (vph)	75	0	4	116	0	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt					0.865	
Flt Protected				0.998		
Satd. Flow (prot)	1863	0	0	1859	1611	0
Flt Permitted				0.998		
Satd. Flow (perm)	1863	0	0	1859	1611	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	490.2			203.9	128.0	
Travel Time (s)	35.3			9.2	9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	82	0	4	126	0	3
Shared Lane Traffic (%)						
Lane Group Flow (vph)	82	0	0	130	3	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	19.3%
Analysis Period (min)	15
	ICU Level of Service A



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↻			↻	↻	
Traffic Volume (veh/h)	75	0	4	116	0	3
Future Volume (Veh/h)	75	0	4	116	0	3
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	82	0	4	126	0	3
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None		None			
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			82		216	82
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			82		216	82
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			100		100	100
cM capacity (veh/h)			1515		770	978
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	82	130	3			
Volume Left	0	4	0			
Volume Right	0	0	3			
cSH	1700	1515	978			
Volume to Capacity	0.05	0.00	0.00			
Queue Length 95th (m)	0.0	0.1	0.1			
Control Delay (s)	0.0	0.2	8.7			
Lane LOS		A	A			
Approach Delay (s)	0.0	0.2	8.7			
Approach LOS			A			
Intersection Summary						
Average Delay			0.3			
Intersection Capacity Utilization			19.3%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2020 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	45	73	349	55	48	9	304	246	57	19	371	29
Future Volume (vph)	45	73	349	55	48	9	304	246	57	19	371	29
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.876				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1664	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.723			0.197			0.500			0.557		
Satd. Flow (perm)	1347	1664	0	350	1863	1615	950	1776	0	1058	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		266				52		21				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	49	79	379	60	52	10	330	267	62	21	403	32
Shared Lane Traffic (%)												
Lane Group Flow (vph)	49	458	0	60	52	10	330	329	0	21	403	32
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	20.3	20.3		20.3	20.3	20.3	55.4	55.4		55.4	55.4	55.4
Actuated g/C Ratio	0.23	0.23		0.23	0.23	0.23	0.62	0.62		0.62	0.62	0.62
v/c Ratio	0.16	0.79		0.77	0.12	0.02	0.56	0.30		0.03	0.35	0.03
Control Delay	26.5	23.0		84.0	25.6	0.1	16.8	9.7		9.1	10.8	1.7
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	26.5	23.0		84.0	25.6	0.1	16.8	9.7		9.1	10.8	1.7
LOS	C	C		F	C	A	B	A		A	B	A
Approach Delay		23.4			52.2			13.2			10.1	
Approach LOS		C			D			B			B	
Queue Length 50th (m)	7.0	31.5		10.0	7.4	0.0	34.4	25.4		1.5	35.1	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2020 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	94	197	103	245	182	243	122	312	158	306	453	78
Future Volume (vph)	94	197	103	245	182	243	122	312	158	306	453	78
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.948				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1783	0	1787	1900	1583	1805	1753	0	1787	1881	1583
Flt Permitted	0.614			0.457			0.484			0.202		
Satd. Flow (perm)	1167	1783	0	860	1900	1583	920	1753	0	380	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		25				264		35				77
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	102	214	112	266	198	264	133	339	172	333	492	85
Shared Lane Traffic (%)												
Lane Group Flow (vph)	102	326	0	266	198	264	133	511	0	333	492	85
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	55.0	55.0		14.0	69.0	69.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	55.0%	55.0%		14.0%	69.0%	69.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	38.0	38.0		38.0	38.0	38.0	34.2	34.2		53.5	48.2	48.2
Actuated g/C Ratio	0.38	0.38		0.38	0.38	0.38	0.34	0.34		0.54	0.48	0.48
v/c Ratio	0.23	0.47		0.82	0.27	0.35	0.42	0.82		0.90	0.54	0.11
Control Delay	26.2	26.6		52.6	25.3	4.9	27.7	38.5		41.7	19.6	3.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	26.2	26.6		52.6	25.3	4.9	27.7	38.5		41.7	19.6	3.2
LOS	C	C		D	C	A	C	D		D	B	A
Approach Delay		26.5			27.9			36.3			26.2	
Approach LOS		C			C			D			C	
Queue Length 50th (m)	14.0	45.8		48.3	27.7	0.0	20.5	88.1		36.5	67.3	0.8

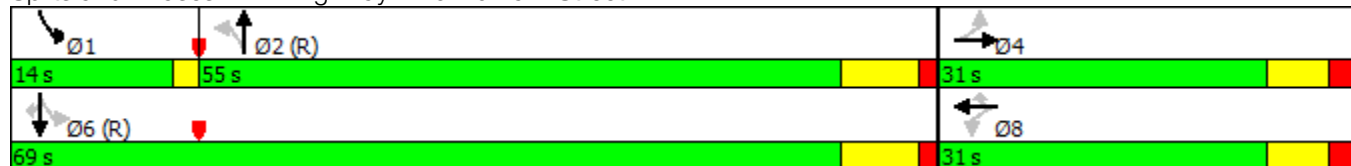


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	31.8	84.5		#113.3	53.2	18.8	32.1	109.6		#54.4	76.3	6.7
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	443	692		326	721	764	438	854		372	1160	1006
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.23	0.47		0.82	0.27	0.35	0.30	0.60		0.90	0.42	0.08

Intersection Summary

Area Type: Other
 Cycle Length: 100
 Actuated Cycle Length: 100
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 60
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.90
 Intersection Signal Delay: 29.1 Intersection LOS: C
 Intersection Capacity Utilization 93.7% ICU Level of Service F
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	149	0	107	7	0	4	138	1	8	5	9	145
Future Volume (vph)	149	0	107	7	0	4	138	1	8	5	9	145
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.944			0.955			0.992			0.877	
Flt Protected		0.972			0.968			0.955			0.999	
Satd. Flow (prot)	0	1584	0	0	1722	0	0	1798	0	0	1664	0
Flt Permitted		0.972			0.968			0.955			0.999	
Satd. Flow (perm)	0	1584	0	0	1722	0	0	1798	0	0	1664	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			77.0			138.6			84.1	
Travel Time (s)		13.6			5.5			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	20%	2%	2%	2%	0%	0%	2%	2%	0%	0%
Adj. Flow (vph)	162	0	116	8	0	4	150	1	9	5	10	158
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	278	0	0	12	0	0	160	0	0	173	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	44.9%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2020 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	149	0	107	7	0	4	138	1	8	5	9	145
Future Volume (Veh/h)	149	0	107	7	0	4	138	1	8	5	9	145
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	162	0	116	8	0	4	150	1	9	5	10	158
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage (veh)												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	4			116			563	402	58	410	458	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	4			116			563	402	58	410	458	2
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	90			99			56	100	99	99	98	85
cM capacity (veh/h)	1611			1473			340	483	1008	503	449	1088
Direction, Lane #												
	EB 1	WB 1	NB 1	SB 1								
Volume Total	278	12	160	173								
Volume Left	162	8	150	5								
Volume Right	116	4	9	158								
cSH	1611	1473	354	975								
Volume to Capacity	0.10	0.01	0.45	0.18								
Queue Length 95th (m)	2.7	0.1	18.1	5.1								
Control Delay (s)	4.7	5.0	23.3	9.5								
Lane LOS	A	A	C	A								
Approach Delay (s)	4.7	5.0	23.3	9.5								
Approach LOS			C	A								
Intersection Summary												
Average Delay			10.8									
Intersection Capacity Utilization			44.9%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2020 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↔	↔			↔	↔
Traffic Volume (vph)	115	49	45	182	55	242	51	227	139	248	443	125
Future Volume (vph)	115	49	45	182	55	242	51	227	139	248	443	125
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.971			0.932			0.943				0.850
Flt Protected		0.973			0.981		0.950				0.982	
Satd. Flow (prot)	0	1750	0	0	1703	0	1770	1746	0	0	1829	1615
Flt Permitted		0.973			0.981		0.950				0.982	
Satd. Flow (perm)	0	1750	0	0	1703	0	1770	1746	0	0	1829	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			79.2			1178.3			487.8	
Travel Time (s)		5.2			5.7			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	2%	2%	2%	2%	3%	2%	2%	2%	0%
Adj. Flow (vph)	125	53	49	198	60	263	55	247	151	270	482	136
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	227	0	0	521	0	55	398	0	0	752	136
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	98.2%
ICU Level of Service	F
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2020 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↗	↘			↖	↗
Traffic Volume (veh/h)	115	49	45	182	55	242	51	227	139	248	443	125
Future Volume (Veh/h)	115	49	45	182	55	242	51	227	139	248	443	125
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	125	53	49	198	60	263	55	247	151	270	482	136
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
							None				None	
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1672	1530	482	1530	1590	322	618			398		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1672	1530	482	1530	1590	322	618			398		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	0	37	92	0	23	63	94			77		
cM capacity (veh/h)	14	85	584	36	78	718	962			1161		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	227	521	55	398	752	136						
Volume Left	125	198	55	0	270	0						
Volume Right	49	263	0	151	0	136						
cSH	24	78	962	1700	1161	1700						
Volume to Capacity	9.43	6.71	0.06	0.23	0.23	0.08						
Queue Length 95th (m)	Err	Err	1.5	0.0	7.2	0.0						
Control Delay (s)	Err	Err	9.0	0.0	5.1	0.0						
Lane LOS	F	F	A		A							
Approach Delay (s)	Err	Err	1.1		4.3							
Approach LOS	F	F										
Intersection Summary												
Average Delay			3582.4									
Intersection Capacity Utilization			98.2%		ICU Level of Service				F			
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2020 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (vph)	123	6	33	3	10	10	32	292	3	22	470	162
Future Volume (vph)	123	6	33	3	10	10	32	292	3	22	470	162
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.941			0.999				0.850
Flt Protected		0.955			0.994		0.950				0.998	
Satd. Flow (prot)	0	1748	1615	0	1564	0	1805	1826	0	0	1857	1615
Flt Permitted		0.955			0.994		0.950				0.998	
Satd. Flow (perm)	0	1748	1615	0	1564	0	1805	1826	0	0	1857	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	134	7	36	3	11	11	35	317	3	24	511	176
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	141	36	0	25	0	35	320	0	0	535	176
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	63.1%
ICU Level of Service	B
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2020 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	123	6	33	3	10	10	32	292	3	22	470	162
Future Volume (Veh/h)	123	6	33	3	10	10	32	292	3	22	470	162
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	134	7	36	3	11	11	35	317	3	24	511	176
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
			6									
Median type												
								None			None	
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	962	949	511	951	1124	318	687			320		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	962	949	511	951	1124	318	687			320		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	36	97	94	98	94	98	96			98		
cM capacity (veh/h)	210	248	567	185	178	727	916			1223		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	177	25	35	320	535	176						
Volume Left	134	3	35	0	24	0						
Volume Right	36	11	0	3	0	176						
cSH	265	269	916	1700	1223	1700						
Volume to Capacity	0.67	0.09	0.04	0.19	0.02	0.10						
Queue Length 95th (m)	34.6	2.4	1.0	0.0	0.5	0.0						
Control Delay (s)	42.8	19.8	9.1	0.0	0.6	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	42.8	19.8	0.9		0.4							
Approach LOS	E	C										
Intersection Summary												
Average Delay			6.9									
Intersection Capacity Utilization			63.1%		ICU Level of Service					B		
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	149	0	11	112	0	13
Future Volume (vph)	149	0	11	112	0	13
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt					0.865	
Flt Protected				0.996		
Satd. Flow (prot)	1863	0	0	1859	1644	0
Flt Permitted				0.996		
Satd. Flow (perm)	1863	0	0	1859	1644	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	492.9			201.2	105.0	
Travel Time (s)	35.5			9.1	7.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	2%	0%	0%
Adj. Flow (vph)	162	0	12	122	0	14
Shared Lane Traffic (%)						
Lane Group Flow (vph)	162	0	0	134	14	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	25.0%
ICU Level of Service	A
Analysis Period (min)	15



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↻			↻	↻	
Traffic Volume (veh/h)	149	0	11	112	0	13
Future Volume (Veh/h)	149	0	11	112	0	13
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	162	0	12	122	0	14
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None			None		
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			162		308	162
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			162		308	162
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			99		100	98
cM capacity (veh/h)			1429		683	888
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	162	134	14			
Volume Left	0	12	0			
Volume Right	0	0	14			
cSH	1700	1429	888			
Volume to Capacity	0.10	0.01	0.02			
Queue Length 95th (m)	0.0	0.2	0.4			
Control Delay (s)	0.0	0.7	9.1			
Lane LOS		A	A			
Approach Delay (s)	0.0	0.7	9.1			
Approach LOS			A			
Intersection Summary						
Average Delay			0.7			
Intersection Capacity Utilization			25.0%	ICU Level of Service	A	
Analysis Period (min)			15			



Appendix E

2025 Background Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall	
				Eastbound				Westbound				Northbound				Southbound					
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach		
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	C	C	C	D	D	A	C	A	A	A	A	A	A	A	A	B	
			Delay	39	21	21	25	42	39	5	33	4	4	4	4	4	4	0	4	4	12
			V/C	0.22	0.40	0.40		0.33	0.25	0.13		0.11	0.24	0.24		0.02	0.13	0.02			
			Queue	14.6	20.3	20.3		19.5	19.8	3.4		10.4	28.4	28.4		2.4	16.0	0.6			
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	D	D	B	C	A	A	A	A	A	A	A	A	C	
			Delay	53	43	43	47	50	40	11	31	9	10	10	10	4	5	2	4	4	20
			V/C	0.58	0.48	0.48		0.53	0.30	0.39		0.10	0.34	0.34		0.17	0.15	0.03			
			Queue	36.4	38.7	38.7		32.4	26.9	15.1		14.0	54.5	54.5		11.9	21.5	3.2			
	3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A					A	A		A		A	A	A	7	
			Delay	5		5	5					10	10		10		9	9	9	7	
V/C			0.02		0.02						0.03	0.03				0.02	0.02				
Queue			0.6		0.6						0.7	0.7				0.6	0.6				
4 - Highway 21 & Russell Street	TWSC	LOS	C		C	C					A	A		A		A	A	A	2		
		Delay	16		16	16					8	0		1		0	0	0	2		
		V/C	0.25		0.25						0.03	0.21				0.18	0.03				
		Queue	7.9		7.9						0.8	0.0				0.0	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	B	B	B	B	A	A	A	A	A	A	A	A	3		
		Delay	16	16	16	16	12	12	12	12	8	0	0	1	0	0	0	0	3		
		V/C	0.25	0.25	0.25		0.05	0.05	0.05		0.02	0.17	0.17		0.01	0.01	0.04				
		Queue	7.7	7.7	7.7		1.4	1.4	1.4		0.5	0.0	0.0		0.2	0.2	0.0				
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	E	C	A	D	A	A	A	A	A	A	A	B		
			Delay	31	30	30	30	79	29	0	48	10	8	8	8	7	9	2	8	18	
			V/C	0.21	0.79	0.79		0.73	0.17	0.04		0.31	0.25	0.25		0.04	0.32	0.03			
			Queue	16.7	57.0	57.0		24.1	17.3	0.0		33.9	38.6	38.6		6.5	54.9	2.9			
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	D	C	A	C	C	C	C	B	B	A	A	B	C	
			Delay	29	28	28	28	46	27	5	28	21	23	23	23	11	14	3	12	21	
			V/C	0.30	0.39	0.39		0.73	0.26	0.30		0.13	0.49	0.49		0.41	0.42	0.10			
			Queue	30.6	49.2	49.2		65.3	35.6	14.2		16.9	89.4	89.4		37.0	80.0	7.4			
	3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A					A	A		A		A	A	A	8	
			Delay	6		6	6					10	10		10		9	9	9	8	
V/C			0.03		0.03						0.08	0.08				0.05	0.05				
Queue			0.7		0.7						2.0	2.0				1.2	1.2				
4 - Highway 21 & Russell Street	TWSC	LOS	D		D	D					A	A		A		A	A	A	5		
		Delay	35		35	35					9	0		2		0	0	0	5		
		V/C	0.59		0.59						0.07	0.18				0.36	0.07				
		Queue	28.2		28.2						1.8	0.0				0.0	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	D	D	D	D	C	C	C	C	A	A	A	A	A	A	A	A	4		
		Delay	25	25	25	25	19	19	19	19	9	0	0	1	1	1	0	1	4		
		V/C	0.37	0.37	0.37		0.10	0.10	0.10		0.04	0.18	0.18		0.02	0.02	0.07				
		Queue	13.2	13.2	13.2		2.6	2.6	2.6		1.0	0.0	0.0		0.5	0.5	0.0				



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2025 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	31	32	62	47	50	25	94	265	34	13	164	18
Future Volume (vph)	31	32	62	47	50	25	94	265	34	13	164	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.901				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1640	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.722			0.691			0.645			0.564		
Satd. Flow (perm)	1294	1640	0	1313	1827	1380	1156	1766	0	893	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		67				52		12				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	34	35	67	51	54	27	102	288	37	14	178	20
Shared Lane Traffic (%)												
Lane Group Flow (vph)	34	102	0	51	54	27	102	325	0	14	178	20
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	10.6	10.6		10.6	10.6	10.6	69.9	69.9		69.9	69.9	69.9
Actuated g/C Ratio	0.12	0.12		0.12	0.12	0.12	0.78	0.78		0.78	0.78	0.78
v/c Ratio	0.22	0.40		0.33	0.25	0.13	0.11	0.24		0.02	0.13	0.02
Control Delay	39.3	20.5		42.3	38.8	5.1	4.2	4.3		3.9	4.0	0.3
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	39.3	20.5		42.3	38.8	5.1	4.2	4.3		3.9	4.0	0.3
LOS	D	C		D	D	A	A	A		A	A	A
Approach Delay		25.2			33.3			4.3			3.6	
Approach LOS		C			C			A			A	
Queue Length 50th (m)	5.8	5.9		8.7	9.2	0.0	4.6	15.5		0.6	8.1	0.0



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	14.6	20.3		19.5	19.8	3.4	10.4	28.4		2.4	16.0	0.6
Internal Link Dist (m)		211.6			466.2			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	359	503		364	507	420	897	1374		693	1366	1265
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.09	0.20		0.14	0.11	0.06	0.11	0.24		0.02	0.13	0.02

Intersection Summary

Area Type:	Other
Cycle Length:	90
Actuated Cycle Length:	90
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	45
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.40
Intersection Signal Delay:	11.5
Intersection LOS:	B
Intersection Capacity Utilization	60.6%
ICU Level of Service	B
Analysis Period (min)	15

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2025 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	98	102	14	86	72	112	68	212	115	115	176	35
Future Volume (vph)	98	102	14	86	72	112	68	212	115	115	176	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.982				0.850		0.947				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1855	0	1770	1863	1509	1805	1664	0	1626	1712	1583
Flt Permitted	0.706			0.676			0.637			0.516		
Satd. Flow (perm)	1315	1855	0	1259	1863	1509	1210	1664	0	883	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		6				122		35				38
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	107	111	15	93	78	122	74	230	125	125	191	38
Shared Lane Traffic (%)												
Lane Group Flow (vph)	107	126	0	93	78	122	74	355	0	125	191	38
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	13.9	13.9		13.9	13.9	13.9	62.8	62.8		77.6	72.3	72.3
Actuated g/C Ratio	0.14	0.14		0.14	0.14	0.14	0.63	0.63		0.78	0.72	0.72
v/c Ratio	0.58	0.48		0.53	0.30	0.39	0.10	0.34		0.17	0.15	0.03
Control Delay	52.6	43.0		50.3	40.4	10.5	9.2	9.8		3.8	5.2	1.8
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	52.6	43.0		50.3	40.4	10.5	9.2	9.8		3.8	5.2	1.8
LOS	D	D		D	D	B	A	A		A	A	A
Approach Delay		47.4			31.1			9.7			4.3	
Approach LOS		D			C			A			A	
Queue Length 50th (m)	20.9	23.0		18.0	14.6	0.0	5.4	27.0		4.8	10.2	0.0

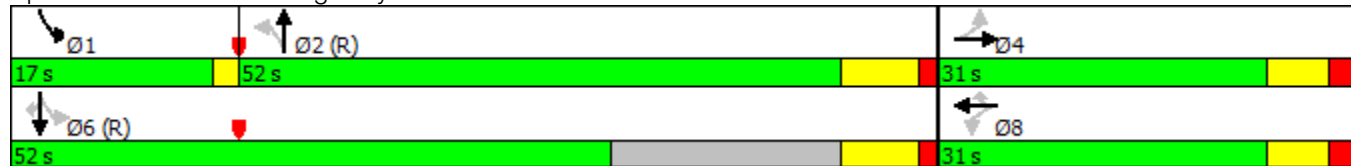


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	36.4	38.7		32.4	26.9	15.1	14.0	54.5		11.9	21.5	3.2
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	322	459		308	456	461	759	1057		796	1237	1154
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.33	0.27		0.30	0.17	0.26	0.10	0.34		0.16	0.15	0.03

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.58
Intersection Signal Delay:	19.7
Intersection LOS:	B
Intersection Capacity Utilization	63.0%
ICU Level of Service	B
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	36	16	19	1	4	17
Future Volume (vph)	36	16	19	1	4	17
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.959				0.890	
Flt Protected	0.966			0.954		
Satd. Flow (prot)	1645	0	0	1463	1691	0
Flt Permitted	0.966			0.954		
Satd. Flow (perm)	1645	0	0	1463	1691	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	23%	25%	0%	0%	0%
Adj. Flow (vph)	39	17	21	1	4	18
Shared Lane Traffic (%)						
Lane Group Flow (vph)	56	0	0	22	22	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	17.8%
	ICU Level of Service A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 2025 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	36	16	19	1	4	17
Future Volume (Veh/h)	36	16	19	1	4	17
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	39	17	21	1	4	18
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		106	86	95	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		106	86	95	0
tC, single (s)	4.1		7.3	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.7	4.0	4.0	3.3
p0 queue free %	98		97	100	99	98
cM capacity (veh/h)	1636		790	788	780	1091

Direction, Lane #	EB 1	NB 1	SB 1
Volume Total	56	22	22
Volume Left	39	21	0
Volume Right	17	0	18
cSH	1636	790	1017
Volume to Capacity	0.02	0.03	0.02
Queue Length 95th (m)	0.6	0.7	0.5
Control Delay (s)	5.1	9.7	8.6
Lane LOS	A	A	A
Approach Delay (s)	5.1	9.7	8.6
Approach LOS		A	A

Intersection Summary			
Average Delay		6.9	
Intersection Capacity Utilization	17.8%	ICU Level of Service	A
Analysis Period (min)		15	



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	65	40	37	326	284	50
Future Volume (vph)	65	40	37	326	284	50
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.949					0.850
Flt Protected	0.970		0.950			
Satd. Flow (prot)	1678	0	1752	1776	1759	1524
Flt Permitted	0.970		0.950			
Satd. Flow (perm)	1678	0	1752	1776	1759	1524
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	3%	3%	7%	8%	6%
Adj. Flow (vph)	71	43	40	354	309	54
Shared Lane Traffic (%)						
Lane Group Flow (vph)	114	0	40	354	309	54
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	34.3%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2025 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	65	40	37	326	284	50
Future Volume (Veh/h)	65	40	37	326	284	50
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	71	43	40	354	309	54
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	743	309	363			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	743	309	363			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	81	94	97			
cM capacity (veh/h)	366	729	1190			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	114	40	354	309	54	
Volume Left	71	40	0	0	0	
Volume Right	43	0	0	0	54	
cSH	450	1190	1700	1700	1700	
Volume to Capacity	0.25	0.03	0.21	0.18	0.03	
Queue Length 95th (m)	8.0	0.8	0.0	0.0	0.0	
Control Delay (s)	15.7	8.1	0.0	0.0	0.0	
Lane LOS	C	A				
Approach Delay (s)	15.7	0.8		0.0		
Approach LOS	C					
Intersection Summary						
Average Delay			2.4			
Intersection Capacity Utilization			34.3%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2025 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (vph)	73	10	25	1	8	19	23	258	1	11	238	67
Future Volume (vph)	73	10	25	1	8	19	23	258	1	11	238	67
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.909			0.999				0.850
Flt Protected		0.958			0.998		0.950				0.998	
Satd. Flow (prot)	0	1746	1538	0	1724	0	1626	1726	0	0	1731	1615
Flt Permitted		0.958			0.998		0.950				0.998	
Satd. Flow (perm)	0	1746	1538	0	1724	0	1626	1726	0	0	1731	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	79	11	27	1	9	21	25	280	1	12	259	73
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	90	27	0	31	0	25	281	0	0	271	73
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	39.4%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2025 Background AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	73	10	25	1	8	19	23	258	1	11	238	67
Future Volume (Veh/h)	73	10	25	1	8	19	23	258	1	11	238	67
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	79	11	27	1	9	21	25	280	1	12	259	73
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	638	614	259	619	686	280	332			281		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	638	614	259	619	686	280	332			281		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	78	97	97	100	98	97	98			99		
cM capacity (veh/h)	361	381	772	372	361	763	1179			1293		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	117	31	25	281	271	73						
Volume Left	79	1	25	0	12	0						
Volume Right	27	21	0	1	0	73						
cSH	473	562	1179	1700	1293	1700						
Volume to Capacity	0.25	0.06	0.02	0.17	0.01	0.04						
Queue Length 95th (m)	7.7	1.4	0.5	0.0	0.2	0.0						
Control Delay (s)	16.2	11.8	8.1	0.0	0.4	0.0						
Lane LOS	C	B	A		A							
Approach Delay (s)	16.2	11.8	0.7		0.3							
Approach LOS	C	B										
Intersection Summary												
Average Delay			3.2									
Intersection Capacity Utilization			39.4%		ICU Level of Service					A		
Analysis Period (min)			15									

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2025 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	49	79	248	52	53	14	185	220	50	29	356	31
Future Volume (vph)	49	79	248	52	53	14	185	220	50	29	356	31
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.886				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1683	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.719			0.241			0.522			0.581		
Satd. Flow (perm)	1339	1683	0	428	1863	1615	992	1776	0	1104	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		174				52		21				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	53	86	270	57	58	15	201	239	54	32	387	34
Shared Lane Traffic (%)												
Lane Group Flow (vph)	53	356	0	57	58	15	201	293	0	32	387	34
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	16.6	16.6		16.6	16.6	16.6	59.1	59.1		59.1	59.1	59.1
Actuated g/C Ratio	0.18	0.18		0.18	0.18	0.18	0.66	0.66		0.66	0.66	0.66
v/c Ratio	0.21	0.79		0.73	0.17	0.04	0.31	0.25		0.04	0.32	0.03
Control Delay	30.7	29.8		78.7	29.4	0.2	9.6	7.5		7.4	8.6	1.8
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	30.7	29.8		78.7	29.4	0.2	9.6	7.5		7.4	8.6	1.8
LOS	C	C		E	C	A	A	A		A	A	A
Approach Delay		29.9			47.6			8.4			8.0	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	8.3	31.9		9.9	9.0	0.0	13.7	17.4		1.8	26.5	0.0

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2025 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	102	154	40	206	131	162	50	235	118	228	412	85	
Future Volume (vph)	102	154	40	206	131	162	50	235	118	228	412	85	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0	
Storage Lanes	1		0	1		1	1		0	1		1	
Taper Length (m)	30.0			30.0			30.0			30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt		0.969				0.850		0.950				0.850	
Flt Protected	0.950			0.950			0.950			0.950			
Satd. Flow (prot)	1805	1830	0	1787	1900	1583	1805	1752	0	1787	1881	1583	
Flt Permitted	0.666			0.564			0.504			0.419			
Satd. Flow (perm)	1265	1830	0	1061	1900	1583	958	1752	0	788	1881	1583	
Right Turn on Red			Yes			Yes			Yes			Yes	
Satd. Flow (RTOR)		12				176		33				92	
Link Speed (k/h)		50			50			80			80		
Link Distance (m)		140.2			189.4			487.8			358.0		
Travel Time (s)		10.1			13.6			22.0			16.1		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%	
Adj. Flow (vph)	111	167	43	224	142	176	54	255	128	248	448	92	
Shared Lane Traffic (%)													
Lane Group Flow (vph)	111	210	0	224	142	176	54	383	0	248	448	92	
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm	
Protected Phases		4			8			2		1	6		
Permitted Phases	4			8		8	2			6		6	
Detector Phase	4	4		8	8	8	2	2		1	6	6	
Switch Phase													
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0	
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3	
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0	
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%	
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9	
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4	
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3	
Lead/Lag							Lag	Lag		Lead			
Lead-Lag Optimize?							Yes	Yes		Yes			
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min	
Act Effct Green (s)	28.9	28.9		28.9	28.9	28.9	43.7	43.7		62.6	57.3	57.3	
Actuated g/C Ratio	0.29	0.29		0.29	0.29	0.29	0.44	0.44		0.63	0.57	0.57	
v/c Ratio	0.30	0.39		0.73	0.26	0.30	0.13	0.49		0.41	0.42	0.10	
Control Delay	28.8	28.1		46.2	27.4	5.2	21.3	22.8		11.2	14.4	2.8	
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	
Total Delay	28.8	28.1		46.2	27.4	5.2	21.3	22.8		11.2	14.4	2.8	
LOS	C	C		D	C	A	C	C		B	B	A	
Approach Delay		28.3			27.9			22.6			12.0		
Approach LOS		C			C			C			B		
Queue Length 50th (m)	17.2	31.5		40.2	21.7	0.0	6.6	51.0		21.0	49.7	0.0	

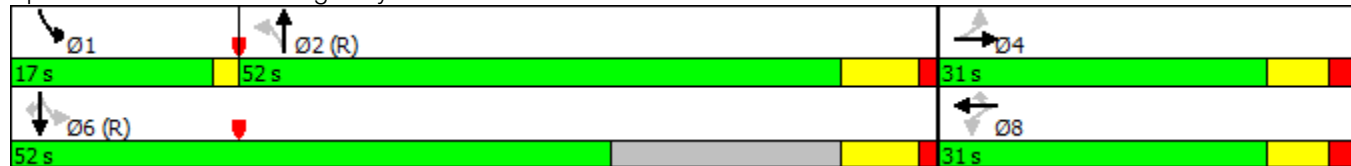


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	30.6	49.2		65.3	35.6	14.2	16.9	89.4		37.0	80.0	7.4
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	375	550		314	563	593	455	849		643	1175	1023
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.30	0.38		0.71	0.25	0.30	0.12	0.45		0.39	0.38	0.09

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	60
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.73
Intersection Signal Delay:	20.9
Intersection LOS:	C
Intersection Capacity Utilization	83.3%
ICU Level of Service	E
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	44	12	55	1	10	32
Future Volume (vph)	44	12	55	1	10	32
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.971			0.897		
Flt Protected	0.962			0.953		
Satd. Flow (prot)	1665	0	0	1811	1704	0
Flt Permitted	0.962			0.953		
Satd. Flow (perm)	1665	0	0	1811	1704	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	20%	0%	0%	0%	0%
Adj. Flow (vph)	48	13	60	1	11	35
Shared Lane Traffic (%)						
Lane Group Flow (vph)	61	0	0	61	46	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	19.8%
	ICU Level of Service A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 2025 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	44	12	55	1	10	32
Future Volume (Veh/h)	44	12	55	1	10	32
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	48	13	60	1	11	35
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		143	102	109	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		143	102	109	0
tC, single (s)	4.1		7.1	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.5	4.0	4.0	3.3
p0 queue free %	97		92	100	99	97
cM capacity (veh/h)	1617		777	768	762	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	61	61	46			
Volume Left	48	60	0			
Volume Right	13	0	35			
cSH	1617	777	989			
Volume to Capacity	0.03	0.08	0.05			
Queue Length 95th (m)	0.7	2.0	1.2			
Control Delay (s)	5.8	10.0	8.8			
Lane LOS	A	B	A			
Approach Delay (s)	5.8	10.0	8.8			
Approach LOS		B	A			
Intersection Summary						
Average Delay			8.2			
Intersection Capacity Utilization			19.8%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	106	49	55	289	558	115
Future Volume (vph)	106	49	55	289	558	115
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.957					0.850
Flt Protected	0.967		0.950			
Satd. Flow (prot)	1712	0	1770	1845	1863	1615
Flt Permitted	0.967		0.950			
Satd. Flow (perm)	1712	0	1770	1845	1863	1615
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	3%	2%	0%
Adj. Flow (vph)	115	53	60	314	607	125
Shared Lane Traffic (%)						
Lane Group Flow (vph)	168	0	60	314	607	125
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	51.6%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2025 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	106	49	55	289	558	115
Future Volume (Veh/h)	106	49	55	289	558	115
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	115	53	60	314	607	125
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	1041	607	732			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	1041	607	732			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	51	89	93			
cM capacity (veh/h)	236	496	873			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	168	60	314	607	125	
Volume Left	115	60	0	0	0	
Volume Right	53	0	0	0	125	
cSH	283	873	1700	1700	1700	
Volume to Capacity	0.59	0.07	0.18	0.36	0.07	
Queue Length 95th (m)	28.2	1.8	0.0	0.0	0.0	
Control Delay (s)	34.7	9.4	0.0	0.0	0.0	
Lane LOS	D	A				
Approach Delay (s)	34.7	1.5		0.0		
Approach LOS	D					
Intersection Summary						
Average Delay			5.0			
Intersection Capacity Utilization			51.6%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2025 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (vph)	68	6	36	4	11	11	35	274	4	24	462	103
Future Volume (vph)	68	6	36	4	11	11	35	274	4	24	462	103
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.942			0.998				0.850
Flt Protected		0.956			0.993		0.950				0.998	
Satd. Flow (prot)	0	1752	1615	0	1557	0	1805	1824	0	0	1856	1615
Flt Permitted		0.956			0.993		0.950				0.998	
Satd. Flow (perm)	0	1752	1615	0	1557	0	1805	1824	0	0	1856	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	74	7	39	4	12	12	38	298	4	26	502	112
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	81	39	0	28	0	38	302	0	0	528	112
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	61.1%
ICU Level of Service	B
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2025 Background PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (veh/h)	68	6	36	4	11	11	35	274	4	24	462	103
Future Volume (Veh/h)	68	6	36	4	11	11	35	274	4	24	462	103
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	74	7	39	4	12	12	38	298	4	26	502	112
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	946	932	502	934	1042	300	614			302		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	946	932	502	934	1042	300	614			302		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	66	97	93	98	94	98	96			98		
cM capacity (veh/h)	215	253	573	189	199	744	975			1242		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	120	28	38	302	528	112						
Volume Left	74	4	38	0	26	0						
Volume Right	39	12	0	4	0	112						
cSH	323	287	975	1700	1242	1700						
Volume to Capacity	0.37	0.10	0.04	0.18	0.02	0.07						
Queue Length 95th (m)	13.3	2.6	1.0	0.0	0.5	0.0						
Control Delay (s)	24.7	18.9	8.8	0.0	0.6	0.0						
Lane LOS	C	C	A		A							
Approach Delay (s)	24.7	18.9	1.0		0.5							
Approach LOS	C	C										
Intersection Summary												
Average Delay			3.7									
Intersection Capacity Utilization			61.1%		ICU Level of Service					B		
Analysis Period (min)			15									



Appendix F

2025 Total Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall	
				Eastbound				Westbound				Northbound				Southbound					
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach		
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	B	B	C	D	D	A	D	A	A	A	A	A	A	A	A	B	
			Delay	38	17	17	21	47	38	5	35	5	5	5	5	4	5	0	4	4	12
			V/C	0.22	0.55	0.55		0.43	0.24	0.13		0.18	0.27	0.27		0.02	0.16	0.02			
			Queue	14.4	24.5	24.5		20.9	19.5	3.3		15.7	31.6	31.6		2.5	19.0	0.6			
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	E	D	A	D	B	B	B	B	A	A	A	A	A	C
			Delay	44	44	44	44	71	38	9	36	12	13	13	13	5	7	2	6	6	22
V/C			0.50	0.64	0.64		0.78	0.33	0.40		0.13	0.40	0.40		0.26	0.20	0.03				
Queue			34.2	54.2	54.2		40.0	31.3	15.8		19.9	72.9	72.9		19.7	32.0	3.8				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	A	B	B	B	B	A	A	A	A	A		
		Delay	5	5	5	5	3	3	3	3	3	13	13	13	13	9	9	9	9	9	7
		V/C	0.08	0.08	0.08		0.00	0.00	0.00		0.10	0.10	0.10		0.07	0.07	0.07				
		Queue	2.0	2.0	2.0		0.0	0.0	0.0		2.6	2.6	2.6		1.8	1.8	1.8				
4 - Highway 21 & Russell Street	TWSC	LOS	E	E	E	E	C	C	C	C	A	A	A	A	A	A	A	A	A		
		Delay	44	44	44	44	21	21	21	21	21	8	0	0	1	2	2	0	2	2	9
		V/C	0.65	0.65	0.65		0.30	0.30	0.30		0.03	0.23	0.23		0.07	0.07	0.04				
		Queue	32.0	32.0	32.0		9.7	9.7	9.7		0.8	0.0	0.0		1.9	1.9	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	B	B	B	B	A	A	A	A	A	A	A	A	A		
		Delay	19	19	19	19	12	12	12	12	12	8	0	0	1	0	0	0	0	0	4
		V/C	0.36	0.36	0.36		0.06	0.06	0.06		0.02	0.17	0.17		0.01	0.01	0.06				
		Queue	12.7	12.7	12.7		1.4	1.4	1.4		0.5	0.0	0.0		0.2	0.2	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A							
		Delay		0	0	0	0	0	0		9	9		9	9						0
		V/C		0.05	0.05		0.00	0.00			0.00			0.00							
		Queue		0.0	0.0		0.1	0.1			0.1			0.1							
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	F	C	A	E	C	A	A	B	A	B	A	B	C	
			Delay	26	26	26	26	93	25	0	56	20	10	10	15	10	12	2	11	11	20
			V/C	0.17	0.82	0.82		0.82	0.13	0.03		0.64	0.33	0.33		0.04	0.39	0.03			
			Queue	16.1	72.6	72.6		31.2	16.7	0.0		85.0	51.5	51.5		5.6	67.5	3.1			
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	E	C	A	D	C	D	D	D	E	C	A	C	D	
			Delay	26	27	27	26	78	25	5	37	31	49	49	46	59	20	5	33	36	
V/C			0.27	0.51	0.51		0.96	0.30	0.37		0.46	0.90	0.90		0.96	0.57	0.11				
Queue			31.5	81.1	81.1		116.6	51.3	17.6		39.1	152.1	152.1		98.6	97.8	10.3				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	A	C	C	C	C	A	A	A	A	A		
		Delay	5	5	5	5	5	5	5	5	5	24	24	24	24	10	10	10	10	11	
		V/C	0.10	0.10	0.10		0.01	0.01	0.01		0.47	0.47	0.47		0.18	0.18	0.18				
		Queue	2.7	2.7	2.7		0.1	0.1	0.1		19.5	19.5	19.5		5.3	5.3	5.3				
4 - Highway 21 & Russell Street	TWSC	LOS	F	F	F	F	F	F	F	F	A	A	A	A	A	A	A	A	A		
		Delay	Err	Err	Err	Err	Err	Err	Err	Err	Err	9	0	0	1	5	5	0	4	3472	
		V/C	17.91	17.91	17.91		9.13	9.13	9.13		0.07	0.25	0.25		0.24	0.24	0.09				
		Queue	Err	Err	Err		Err	Err	Err		1.7	0.0	0.0		7.4	7.4	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	F	F	F	F	C	C	C	C	A	A	A	A	A	A	A	A	A		
		Delay	61	61	61	61	22	22	22	22	22	9	0	0	1	1	1	0	1	9	
		V/C	0.79	0.79	0.79		0.12	0.12	0.12		0.04	0.20	0.20		0.02	0.02	0.11				
		Queue	46.9	46.9	46.9		3.2	3.2	3.2		1.1	0.0	0.0		0.5	0.5	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A							
		Delay		0	0	0	1	1			1	9		9	9						1
		V/C		0.10	0.10		0.01	0.01			0.02			0.02							
		Queue		0.0	0.0		0.2	0.2			0.4			0.4							



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2025 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	31	32	131	51	50	25	136	278	36	13	185	18
Future Volume (vph)	31	32	131	51	50	25	136	278	36	13	185	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.880				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1617	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.722			0.551			0.632			0.556		
Satd. Flow (perm)	1294	1617	0	1047	1827	1380	1133	1766	0	880	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		142				52		12				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	34	35	142	55	54	27	148	302	39	14	201	20
Shared Lane Traffic (%)												
Lane Group Flow (vph)	34	177	0	55	54	27	148	341	0	14	201	20
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	11.0	11.0		11.0	11.0	11.0	64.7	64.7		64.7	64.7	64.7
Actuated g/C Ratio	0.12	0.12		0.12	0.12	0.12	0.72	0.72		0.72	0.72	0.72
v/c Ratio	0.22	0.55		0.43	0.24	0.13	0.18	0.27		0.02	0.16	0.02
Control Delay	38.4	17.0		46.9	37.9	4.9	5.0	5.1		4.2	4.6	0.3
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	38.4	17.0		46.9	37.9	4.9	5.0	5.1		4.2	4.6	0.3
LOS	D	B		D	D	A	A	A		A	A	A
Approach Delay		20.5			35.0			5.0			4.2	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	5.8	5.9		9.6	9.2	0.0	6.9	16.5		0.6	9.2	0.0

Lanes, Volumes, Timings
 1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
 Total 2025 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	14.4	24.5		20.9	19.5	3.3	15.7	31.6		2.5	19.0	0.6
Internal Link Dist (m)		211.6			466.2			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	359	551		290	507	420	814	1272		632	1263	1173
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.09	0.32		0.19	0.11	0.06	0.18	0.27		0.02	0.16	0.02

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 45
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.55
 Intersection Signal Delay: 11.7
 Intersection Capacity Utilization 75.4%
 Analysis Period (min) 15
 Intersection LOS: B
 ICU Level of Service D

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2025 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	98	138	48	107	94	140	83	223	139	162	223	35
Future Volume (vph)	98	138	48	107	94	140	83	223	139	162	223	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.961				0.850		0.942				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1803	0	1770	1863	1509	1805	1661	0	1626	1712	1583
Flt Permitted	0.691			0.479			0.608			0.475		
Satd. Flow (perm)	1287	1803	0	892	1863	1509	1155	1661	0	813	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		17				152		41				38
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	107	150	52	116	102	152	90	242	151	176	242	38
Shared Lane Traffic (%)												
Lane Group Flow (vph)	107	202	0	116	102	152	90	393	0	176	242	38
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	16.7	16.7		16.7	16.7	16.7	58.6	58.6		74.8	69.5	69.5
Actuated g/C Ratio	0.17	0.17		0.17	0.17	0.17	0.59	0.59		0.75	0.70	0.70
v/c Ratio	0.50	0.64		0.78	0.33	0.40	0.13	0.40		0.26	0.20	0.03
Control Delay	44.4	44.0		71.2	37.8	8.7	12.1	12.9		5.3	6.8	2.3
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	44.4	44.0		71.2	37.8	8.7	12.1	12.9		5.3	6.8	2.3
LOS	D	D		E	D	A	B	B		A	A	A
Approach Delay		44.1			36.3			12.7			5.9	
Approach LOS		D			D			B			A	
Queue Length 50th (m)	20.1	35.7		23.0	18.6	0.0	7.6	35.0		8.4	15.2	0.0

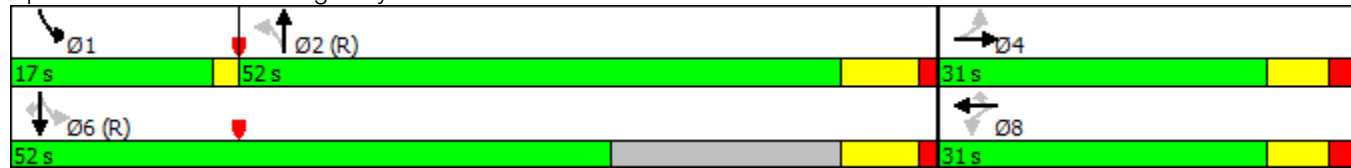


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	34.2	54.2		40.0	31.3	15.8	19.9	72.9		19.7	32.0	3.8
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	315	454		218	456	484	677	990		729	1189	1111
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.34	0.44		0.53	0.22	0.31	0.13	0.40		0.24	0.20	0.03

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.78
Intersection Signal Delay:	22.2
Intersection LOS:	C
Intersection Capacity Utilization	74.9%
ICU Level of Service	D
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	113	0	55	2	0	3	44	1	1	1	4	62
Future Volume (vph)	113	0	55	2	0	3	44	1	1	1	4	62
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.956			0.919			0.997			0.874	
Flt Protected		0.967			0.980			0.954			0.999	
Satd. Flow (prot)	0	1633	0	0	1678	0	0	1457	0	0	1658	0
Flt Permitted		0.967			0.980			0.954			0.999	
Satd. Flow (perm)	0	1633	0	0	1678	0	0	1457	0	0	1658	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			73.4			138.6			84.1	
Travel Time (s)		13.6			5.3			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	2%	23%	2%	2%	2%	25%	0%	2%	2%	0%	0%
Adj. Flow (vph)	123	0	60	2	0	3	48	1	1	1	4	67
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	183	0	0	5	0	0	50	0	0	72	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	31.8%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2025 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	113	0	55	2	0	3	44	1	1	1	4	62
Future Volume (Veh/h)	113	0	55	2	0	3	44	1	1	1	4	62
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	123	0	60	2	0	3	48	1	1	1	4	67
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage (veh)												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	3			60			350	283	30	283	312	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	3			60			350	283	30	283	312	2
tC, single (s)	4.1			4.1			7.3	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.7	4.0	3.3	3.5	4.0	3.3
p0 queue free %	92			100			90	100	100	100	99	94
cM capacity (veh/h)	1632			1544			495	581	1044	629	560	1089
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total	183	5	50	72								
Volume Left	123	2	48	1								
Volume Right	60	3	1	67								
cSH	1632	1544	502	1025								
Volume to Capacity	0.08	0.00	0.10	0.07								
Queue Length 95th (m)	2.0	0.0	2.6	1.8								
Control Delay (s)	5.2	2.9	13.0	8.8								
Lane LOS	A	A	B	A								
Approach Delay (s)	5.2	2.9	13.0	8.8								
Approach LOS			B	A								
Intersection Summary												
Average Delay			7.2									
Intersection Capacity Utilization			31.8%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2025 AM





















Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↗	↘			↖	↗
Traffic Volume (vph)	78	25	40	23	15	49	34	320	37	80	297	58
Future Volume (vph)	78	25	40	23	15	49	34	320	37	80	297	58
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.963			0.924			0.985				0.850
Flt Protected		0.973			0.987		0.950				0.990	
Satd. Flow (prot)	0	1713	0	0	1699	0	1752	1758	0	0	1762	1524
Flt Permitted		0.973			0.987		0.950				0.990	
Satd. Flow (perm)	0	1713	0	0	1699	0	1752	1758	0	0	1762	1524
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			63.0			1178.3			487.8	
Travel Time (s)		5.2			4.5			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	2%	3%	2%	2%	2%	3%	7%	2%	2%	8%	6%
Adj. Flow (vph)	85	27	43	25	16	53	37	348	40	87	323	63
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	155	0	0	94	0	37	388	0	0	410	63
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	63.9%
ICU Level of Service	B
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2025 AM

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	78	25	40	23	15	49	34	320	37	80	297	58
Future Volume (Veh/h)	78	25	40	23	15	49	34	320	37	80	297	58
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	85	27	43	25	16	53	37	348	40	87	323	63
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	980	959	323	996	1002	368	386			388		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	980	959	323	996	1002	368	386			388		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	53	88	94	86	93	92	97			93		
cM capacity (veh/h)	181	230	716	176	217	677	1167			1170		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	155	94	37	388	410	63						
Volume Left	85	25	37	0	87	0						
Volume Right	43	53	0	40	0	63						
cSH	240	320	1167	1700	1170	1700						
Volume to Capacity	0.65	0.29	0.03	0.23	0.07	0.04						
Queue Length 95th (m)	31.9	9.6	0.8	0.0	1.9	0.0						
Control Delay (s)	43.9	20.9	8.2	0.0	2.4	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	43.9	20.9	0.7		2.1							
Approach LOS	E	C										
Intersection Summary												
Average Delay			8.7									
Intersection Capacity Utilization			63.9%		ICU Level of Service					B		
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2025 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (vph)	107	10	25	1	8	19	21	260	1	11	252	88
Future Volume (vph)	107	10	25	1	8	19	21	260	1	11	252	88
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.909			0.999				0.850
Flt Protected		0.956			0.998		0.950				0.998	
Satd. Flow (prot)	0	1749	1538	0	1724	0	1626	1726	0	0	1730	1615
Flt Permitted		0.956			0.998		0.950				0.998	
Satd. Flow (perm)	0	1749	1538	0	1724	0	1626	1726	0	0	1730	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	116	11	27	1	9	21	23	283	1	12	274	96
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	127	27	0	31	0	23	284	0	0	286	96
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	42.0%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2025 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	107	10	25	1	8	19	21	260	1	11	252	88
Future Volume (Veh/h)	107	10	25	1	8	19	21	260	1	11	252	88
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	116	11	27	1	9	21	23	283	1	12	274	96
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	652	628	274	633	724	284	370			284		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	652	628	274	633	724	284	370			284		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	67	97	96	100	97	97	98			99		
cM capacity (veh/h)	354	374	758	364	344	760	1141			1290		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	154	31	23	284	286	96						
Volume Left	116	1	23	0	12	0						
Volume Right	27	21	0	1	0	96						
cSH	431	549	1141	1700	1290	1700						
Volume to Capacity	0.36	0.06	0.02	0.17	0.01	0.06						
Queue Length 95th (m)	12.8	1.4	0.5	0.0	0.2	0.0						
Control Delay (s)	18.8	12.0	8.2	0.0	0.4	0.0						
Lane LOS	C	B	A		A							
Approach Delay (s)	18.8	12.0	0.6		0.3							
Approach LOS	C	B										
Intersection Summary												
Average Delay			4.1									
Intersection Capacity Utilization			42.0%		ICU Level of Service					A		
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↻			↻	↻	
Traffic Volume (vph)	82	0	4	126	0	3
Future Volume (vph)	82	0	4	126	0	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						0.865
Flt Protected						0.999
Satd. Flow (prot)	1863	0	0	1861	1611	0
Flt Permitted						0.999
Satd. Flow (perm)	1863	0	0	1861	1611	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	490.2			203.9	128.0	
Travel Time (s)	35.3			9.2	9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	89	0	4	137	0	3
Shared Lane Traffic (%)						
Lane Group Flow (vph)	89	0	0	141	3	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	19.9% ICU Level of Service A
Analysis Period (min)	15



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↩			↩	↩	
Traffic Volume (veh/h)	82	0	4	126	0	3
Future Volume (Veh/h)	82	0	4	126	0	3
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	89	0	4	137	0	3
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None		None			
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			89		234	89
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			89		234	89
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			100		100	100
cM capacity (veh/h)			1506		752	969
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	89	141	3			
Volume Left	0	4	0			
Volume Right	0	0	3			
cSH	1700	1506	969			
Volume to Capacity	0.05	0.00	0.00			
Queue Length 95th (m)	0.0	0.1	0.1			
Control Delay (s)	0.0	0.2	8.7			
Lane LOS		A	A			
Approach Delay (s)	0.0	0.2	8.7			
Approach LOS			A			
Intersection Summary						
Average Delay			0.3			
Intersection Capacity Utilization			19.9%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2025 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	49	79	369	59	53	11	320	265	62	21	401	31
Future Volume (vph)	49	79	369	59	53	11	320	265	62	21	401	31
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.876				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1664	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.719			0.190			0.472			0.535		
Satd. Flow (perm)	1339	1664	0	337	1863	1615	897	1776	0	1016	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		266				52		20				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	53	86	401	64	58	12	348	288	67	23	436	34
Shared Lane Traffic (%)												
Lane Group Flow (vph)	53	487	0	64	58	12	348	355	0	23	436	34
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	34.0	34.0		34.0	34.0	34.0	56.0	56.0		56.0	56.0	56.0
Total Split (%)	37.8%	37.8%		37.8%	37.8%	37.8%	62.2%	62.2%		62.2%	62.2%	62.2%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	21.0	21.0		21.0	21.0	21.0	54.7	54.7		54.7	54.7	54.7
Actuated g/C Ratio	0.23	0.23		0.23	0.23	0.23	0.61	0.61		0.61	0.61	0.61
v/c Ratio	0.17	0.82		0.82	0.13	0.03	0.64	0.33		0.04	0.39	0.03
Control Delay	25.9	26.0		93.4	25.1	0.1	20.4	10.4		9.6	11.6	2.1
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	25.9	26.0		93.4	25.1	0.1	20.4	10.4		9.6	11.6	2.1
LOS	C	C		F	C	A	C	B		A	B	A
Approach Delay		26.0			55.5			15.4			10.9	
Approach LOS		C			E			B			B	
Queue Length 50th (m)	7.4	36.7		10.5	8.0	0.0	40.8	29.7		1.7	40.8	0.0

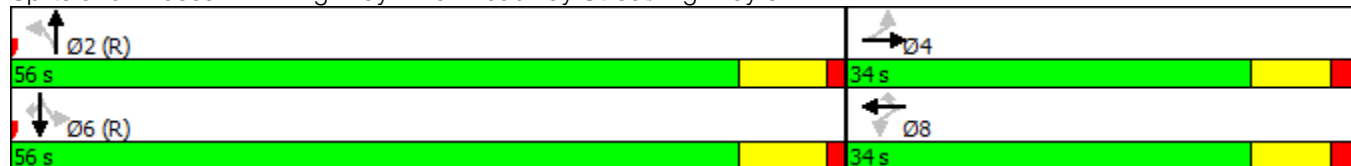


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	16.1	72.6		#31.2	16.7	0.0	#85.0	51.5		5.6	67.5	3.1
Internal Link Dist (m)		211.6			468.9			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	401	685		101	558	520	545	1087		617	1132	1000
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.13	0.71		0.63	0.10	0.02	0.64	0.33		0.04	0.39	0.03

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 55
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.82
 Intersection Signal Delay: 20.1 Intersection LOS: C
 Intersection Capacity Utilization 97.9% ICU Level of Service F
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2025 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	102	210	107	263	193	257	126	332	167	325	487	85
Future Volume (vph)	102	210	107	263	193	257	126	332	167	325	487	85
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.949				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1785	0	1787	1900	1583	1805	1753	0	1787	1881	1583
Flt Permitted	0.595			0.428			0.467			0.154		
Satd. Flow (perm)	1130	1785	0	805	1900	1583	887	1753	0	290	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		28				279		29				63
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	111	228	116	286	210	279	137	361	182	353	529	92
Shared Lane Traffic (%)												
Lane Group Flow (vph)	111	344	0	286	210	279	137	543	0	353	529	92
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	40.0	40.0		40.0	40.0	40.0	44.0	44.0		16.0	60.0	60.0
Total Split (%)	40.0%	40.0%		40.0%	40.0%	40.0%	44.0%	44.0%		16.0%	60.0%	60.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	36.9	36.9		36.9	36.9	36.9	33.3	33.3		54.6	49.3	49.3
Actuated g/C Ratio	0.37	0.37		0.37	0.37	0.37	0.33	0.33		0.55	0.49	0.49
v/c Ratio	0.27	0.51		0.96	0.30	0.37	0.46	0.90		0.96	0.57	0.11
Control Delay	25.8	26.6		78.3	25.0	4.5	31.2	49.4		59.2	20.2	5.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	25.8	26.6		78.3	25.0	4.5	31.2	49.4		59.2	20.2	5.2
LOS	C	C		E	C	A	C	D		E	C	A
Approach Delay		26.4			37.3			45.7			32.9	
Approach LOS		C			D			D			C	
Queue Length 50th (m)	16.3	51.2		~62.5	31.2	0.0	21.1	96.3		43.9	69.5	2.8

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

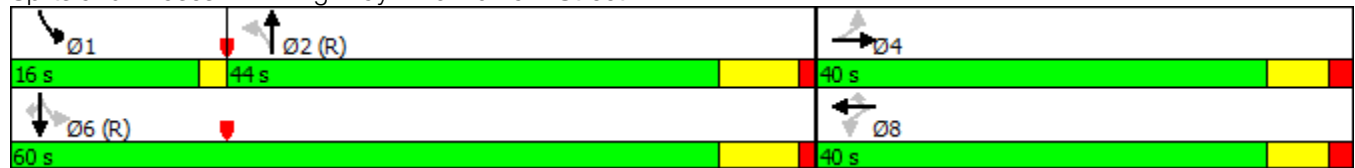


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	31.5	81.1	#116.6	51.3	17.6	39.1	#152.1		#98.6	97.8	10.3	
Internal Link Dist (m)		116.2			165.4		463.8			334.0		
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	417	676		297	701	760	325	661		367	991	864
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.27	0.51		0.96	0.30	0.37	0.42	0.82		0.96	0.53	0.11

Intersection Summary

Area Type: Other
 Cycle Length: 100
 Actuated Cycle Length: 100
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 60
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.96
 Intersection Signal Delay: 36.1 Intersection LOS: D
 Intersection Capacity Utilization 98.1% ICU Level of Service F
 Analysis Period (min) 15
 ~ Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	152	0	108	7	0	4	142	1	8	5	10	147
Future Volume (vph)	152	0	108	7	0	4	142	1	8	5	10	147
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.944			0.955			0.993			0.877	
Flt Protected		0.972			0.968			0.955			0.999	
Satd. Flow (prot)	0	1584	0	0	1722	0	0	1800	0	0	1664	0
Flt Permitted		0.972			0.968			0.955			0.999	
Satd. Flow (perm)	0	1584	0	0	1722	0	0	1800	0	0	1664	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			77.0			138.6			84.1	
Travel Time (s)		13.6			5.5			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	20%	2%	2%	2%	0%	0%	2%	2%	0%	0%
Adj. Flow (vph)	165	0	117	8	0	4	154	1	9	5	11	160
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	282	0	0	12	0	0	164	0	0	176	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	45.6%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2025 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	152	0	108	7	0	4	142	1	8	5	10	147
Future Volume (Veh/h)	152	0	108	7	0	4	142	1	8	5	10	147
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	165	0	117	8	0	4	154	1	9	5	11	160
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	4			117			572	408	58	416	465	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	4			117			572	408	58	416	465	2
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	90			99			54	100	99	99	98	85
cM capacity (veh/h)	1611			1471			333	478	1007	497	444	1088
Direction, Lane #												
	EB 1	WB 1	NB 1	SB 1								
Volume Total	282	12	164	176								
Volume Left	165	8	154	5								
Volume Right	117	4	9	160								
cSH	1611	1471	347	968								
Volume to Capacity	0.10	0.01	0.47	0.18								
Queue Length 95th (m)	2.7	0.1	19.5	5.3								
Control Delay (s)	4.7	5.0	24.4	9.5								
Lane LOS	A	A	C	A								
Approach Delay (s)	4.7	5.0	24.4	9.5								
Approach LOS			C	A								
Intersection Summary												
Average Delay			11.1									
Intersection Capacity Utilization			45.6%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2025 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕↕			↕↕		↗	↘			↕↕	↗↘
Traffic Volume (vph)	123	49	49	182	55	242	55	251	139	248	489	135
Future Volume (vph)	123	49	49	182	55	242	55	251	139	248	489	135
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.970			0.932			0.947				0.850
Flt Protected		0.973			0.981		0.950				0.983	
Satd. Flow (prot)	0	1749	0	0	1703	0	1770	1753	0	0	1831	1615
Flt Permitted		0.973			0.981		0.950				0.983	
Satd. Flow (perm)	0	1749	0	0	1703	0	1770	1753	0	0	1831	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			79.2			1178.3			487.8	
Travel Time (s)		5.2			5.7			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	2%	2%	2%	2%	3%	2%	2%	2%	0%
Adj. Flow (vph)	134	53	53	198	60	263	60	273	151	270	532	147
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	240	0	0	521	0	60	424	0	0	802	147
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	101.7%
ICU Level of Service	G
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2025 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↗	↘			↖	↗
Traffic Volume (veh/h)	123	49	49	182	55	242	55	251	139	248	489	135
Future Volume (Veh/h)	123	49	49	182	55	242	55	251	139	248	489	135
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	134	53	53	198	60	263	60	273	151	270	532	147
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1758	1616	532	1620	1688	348	679			424		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1758	1616	532	1620	1688	348	679			424		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	0	28	90	0	10	62	93			76		
cM capacity (veh/h)	8	74	547	25	67	695	913			1135		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	240	521	60	424	802	147						
Volume Left	134	198	60	0	270	0						
Volume Right	53	263	0	151	0	147						
cSH	13	57	913	1700	1135	1700						
Volume to Capacity	18.66	9.15	0.07	0.25	0.24	0.09						
Queue Length 95th (m)	Err	Err	1.7	0.0	7.4	0.0						
Control Delay (s)	Err	Err	9.2	0.0	5.2	0.0						
Lane LOS	F	F	A		A							
Approach Delay (s)	Err	Err	1.1		4.4							
Approach LOS	F	F										
Intersection Summary												
Average Delay			3470.4									
Intersection Capacity Utilization			101.7%		ICU Level of Service				G			
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2025 PM






















Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (vph)	129	6	36	4	11	11	35	315	4	24	504	171
Future Volume (vph)	129	6	36	4	11	11	35	315	4	24	504	171
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.942			0.998				0.850
Flt Protected		0.955			0.993		0.950				0.998	
Satd. Flow (prot)	0	1748	1615	0	1557	0	1805	1824	0	0	1857	1615
Flt Permitted		0.955			0.993		0.950				0.998	
Satd. Flow (perm)	0	1748	1615	0	1557	0	1805	1824	0	0	1857	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	140	7	39	4	12	12	38	342	4	26	548	186
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	147	39	0	28	0	38	346	0	0	574	186
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	66.8%
ICU Level of Service	C
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2025 PM

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	129	6	36	4	11	11	35	315	4	24	504	171
Future Volume (Veh/h)	129	6	36	4	11	11	35	315	4	24	504	171
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	140	7	39	4	12	12	38	342	4	26	548	186
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1036	1022	548	1024	1206	344	734			346		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1036	1022	548	1024	1206	344	734			346		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	24	97	93	98	92	98	96			98		
cM capacity (veh/h)	183	223	540	162	157	703	880			1196		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	186	28	38	346	574	186						
Volume Left	140	4	38	0	26	0						
Volume Right	39	12	0	4	0	186						
cSH	234	237	880	1700	1196	1700						
Volume to Capacity	0.79	0.12	0.04	0.20	0.02	0.11						
Queue Length 95th (m)	47.0	3.2	1.1	0.0	0.5	0.0						
Control Delay (s)	60.7	22.2	9.3	0.0	0.6	0.0						
Lane LOS	F	C	A		A							
Approach Delay (s)	60.7	22.2	0.9		0.5							
Approach LOS	F	C										
Intersection Summary												
Average Delay			9.3									
Intersection Capacity Utilization			66.8%	ICU Level of Service		C						
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↻			↻	↻	
Traffic Volume (vph)	162	0	11	122	0	13
Future Volume (vph)	162	0	11	122	0	13
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt					0.865	
Flt Protected				0.996		
Satd. Flow (prot)	1863	0	0	1858	1644	0
Flt Permitted				0.996		
Satd. Flow (perm)	1863	0	0	1858	1644	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	492.9			201.2	105.0	
Travel Time (s)	35.5			9.1	7.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	2%	0%	0%
Adj. Flow (vph)	176	0	12	133	0	14
Shared Lane Traffic (%)						
Lane Group Flow (vph)	176	0	0	145	14	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	25.5%
ICU Level of Service	A
Analysis Period (min)	15



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (veh/h)	162	0	11	122	0	13
Future Volume (Veh/h)	162	0	11	122	0	13
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	176	0	12	133	0	14
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None			None		
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			176		333	176
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			176		333	176
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			99		100	98
cM capacity (veh/h)			1412		660	872
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	176	145	14			
Volume Left	0	12	0			
Volume Right	0	0	14			
cSH	1700	1412	872			
Volume to Capacity	0.10	0.01	0.02			
Queue Length 95th (m)	0.0	0.2	0.4			
Control Delay (s)	0.0	0.7	9.2			
Lane LOS		A	A			
Approach Delay (s)	0.0	0.7	9.2			
Approach LOS			A			
Intersection Summary						
Average Delay			0.7			
Intersection Capacity Utilization			25.5%	ICU Level of Service	A	
Analysis Period (min)			15			



Appendix G

2030 Background Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall
				Eastbound				Westbound				Northbound				Southbound				
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	C	C	C	D	D	A	C	A	A	A	A	A	A	A	B	
			Delay	39	20	20	25	43	39	6	34	4	5	5	5	4	4	1	4	12
			V/C	0.24	0.43	0.43		0.35	0.27	0.14		0.12	0.26	0.26		0.02	0.14	0.02		
			Queue	15.2	21.5	21.5		20.6	21.5	4.0		11.4	31.6	31.6		2.5	17.6	0.8		
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	D	A	C	A	B	B	B	A	A	A	A	A	C
Delay			53	43	43	47	53	40	10	32	10	11	11	11	4	6	2	5	20	
V/C			0.61	0.50	0.50		0.59	0.31	0.40		0.11	0.37	0.37		0.19	0.17	0.04			
Queue			38.6	41.3	41.3		35.1	28.3	15.5		15.5	62.9	62.9		13.4	24.3	3.5			
3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A				A	A			A	A	A	A	A		
		Delay	5		5	5					10	10			9	9	9	9	7	
		V/C	0.03		0.03						0.03	0.03			0.02	0.02				
4 - Highway 21 & Russell Street	TWSC	LOS	C		C	C				A	A			A	A	A	A	A		
		Delay	17		17	17					8	0			0	0	0	0	3	
		V/C	0.29		0.29						0.04	0.23			0.20	0.04				
		Queue	9.7		9.7						0.9	0.0			0.0	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	B	B	B	B	A	A	A	A	A	A	A	A		
		Delay	18	18	18	18	12	12	12	12	8	0	0	1	0	0	0	0	4	
		V/C	0.29	0.29	0.29		0.06	0.06	0.06		0.02	0.18	0.18		0.01	0.01	0.05			
		Queue	9.6	9.6	9.6		1.6	1.6	1.6		0.6	0.0	0.0		0.2	0.2	0.0			
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	F	C	A	D	B	A	A	A	A	A	A	B	
			Delay	29	32	32	31	87	28	0	50	11	9	9	10	8	10	2	9	19
			V/C	0.22	0.81	0.81		0.78	0.17	0.05		0.36	0.28	0.28		0.05	0.35	0.04		
			Queue	17.3	62.9	62.9		26.7	17.9	0.3		40.1	44.9	44.9		7.3	63.8	3.3		
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	D	C	A	C	C	C	C	B	B	A	A	A	
Delay			26	25	25	25	38	25	5	24	24	29	29	29	15	18	3	15	22	
V/C			0.28	0.35	0.35		0.66	0.23	0.28		0.18	0.63	0.63		0.53	0.50	0.12			
Queue			34.5	55.4	55.4		80.9	39.6	15.3		17.6	95.0	95.0		37.4	83.2	8.1			
3 - Durham Street & Millennium Way	TWSC	LOS	A		A	A				A	A			A	A	A	A	A		
		Delay	6		6	6					10	10			9	9	9	8		
		V/C	0.03		0.03						0.09	0.09			0.05	0.05				
4 - Highway 21 & Russell Street	TWSC	LOS	E		E	E				A	A			A	A	A	A	A		
		Delay	49		49	49					10	0			0	0	0	0	7	
		V/C	0.72		0.72						0.08	0.20			0.39	0.08				
		Queue	39.8		39.8						2.0	0.0			0.0	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	D	D	D	D	C	C	C	C	A	A	A	A	A	A	A	A		
		Delay	31	31	31	31	21	21	21	21	9	0	0	1	1	1	0	1	4	
		V/C	0.46	0.46	0.46		0.12	0.12	0.12		0.04	0.19	0.19		0.02	0.02	0.07			
		Queue	18.5	18.5	18.5		3.2	3.2	3.2		1.1	0.0	0.0		0.6	0.6	0.0			



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2030 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	34	35	68	51	55	27	101	287	36	14	178	20
Future Volume (vph)	34	35	68	51	55	27	101	287	36	14	178	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.901				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1640	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.718			0.685			0.636			0.551		
Satd. Flow (perm)	1287	1640	0	1302	1827	1380	1140	1766	0	872	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		74				52		11				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	37	38	74	55	60	29	110	312	39	15	193	22
Shared Lane Traffic (%)												
Lane Group Flow (vph)	37	112	0	55	60	29	110	351	0	15	193	22
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	10.8	10.8		10.8	10.8	10.8	69.7	69.7		69.7	69.7	69.7
Actuated g/C Ratio	0.12	0.12		0.12	0.12	0.12	0.77	0.77		0.77	0.77	0.77
v/c Ratio	0.24	0.43		0.35	0.27	0.14	0.12	0.26		0.02	0.14	0.02
Control Delay	39.4	20.3		42.7	39.0	5.7	4.3	4.5		4.1	4.1	0.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	39.4	20.3		42.7	39.0	5.7	4.3	4.5		4.1	4.1	0.5
LOS	D	C		D	D	A	A	A		A	A	A
Approach Delay		25.1			33.7			4.5			3.8	
Approach LOS		C			C			A			A	
Queue Length 50th (m)	6.3	6.4		9.4	10.2	0.0	5.0	17.2		0.6	8.8	0.0



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	15.2	21.5		20.6	21.5	4.0	11.4	31.6		2.5	17.6	0.8
Internal Link Dist (m)		211.6			466.2			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	357	509		361	507	420	883	1371		675	1363	1262
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.10	0.22		0.15	0.12	0.07	0.12	0.26		0.02	0.14	0.02

Intersection Summary

Area Type:	Other
Cycle Length:	90
Actuated Cycle Length:	90
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	45
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.43
Intersection Signal Delay:	11.7
Intersection LOS:	B
Intersection Capacity Utilization:	61.4%
ICU Level of Service:	B
Analysis Period (min):	15

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2030 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	107	111	16	94	78	121	74	230	125	125	191	38
Future Volume (vph)	107	111	16	94	78	121	74	230	125	125	191	38
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.982				0.850		0.947				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1854	0	1770	1863	1509	1805	1664	0	1626	1712	1583
Flt Permitted	0.702			0.642			0.628			0.490		
Satd. Flow (perm)	1308	1854	0	1196	1863	1509	1193	1664	0	839	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		7				132		35				41
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	116	121	17	102	85	132	80	250	136	136	208	41
Shared Lane Traffic (%)												
Lane Group Flow (vph)	116	138	0	102	85	132	80	386	0	136	208	41
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	14.6	14.6		14.6	14.6	14.6	61.8	61.8		76.9	71.6	71.6
Actuated g/C Ratio	0.15	0.15		0.15	0.15	0.15	0.62	0.62		0.77	0.72	0.72
v/c Ratio	0.61	0.50		0.59	0.31	0.40	0.11	0.37		0.19	0.17	0.04
Control Delay	53.0	42.7		52.9	39.9	10.0	9.8	10.7		4.1	5.6	1.9
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	53.0	42.7		52.9	39.9	10.0	9.8	10.7		4.1	5.6	1.9
LOS	D	D		D	D	A	A	B		A	A	A
Approach Delay		47.4			31.7			10.6			4.7	
Approach LOS		D			C			B			A	
Queue Length 50th (m)	22.6	25.0		19.8	15.8	0.0	6.0	31.4		5.5	11.6	0.0

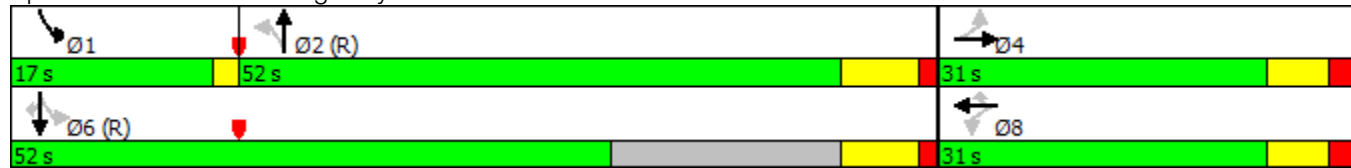


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	38.6	41.3		35.1	28.3	15.5	15.5	62.9		13.4	24.3	3.5
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	320	459		293	456	469	737	1042		763	1226	1145
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.36	0.30		0.35	0.19	0.28	0.11	0.37		0.18	0.17	0.04

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.61
Intersection Signal Delay:	20.3
Intersection LOS:	C
Intersection Capacity Utilization:	73.0%
ICU Level of Service:	C
Analysis Period (min):	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	39	17	21	1	4	18
Future Volume (vph)	39	17	21	1	4	18
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.959			0.887		
Flt Protected	0.966			0.954		
Satd. Flow (prot)	1647	0	0	1462	1685	0
Flt Permitted	0.966			0.954		
Satd. Flow (perm)	1647	0	0	1462	1685	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	23%	25%	0%	0%	0%
Adj. Flow (vph)	42	18	23	1	4	20
Shared Lane Traffic (%)						
Lane Group Flow (vph)	60	0	0	24	24	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	17.9%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millenium Way & Durham Street

Kincardine Business Park TIS
 2030 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	39	17	21	1	4	18
Future Volume (Veh/h)	39	17	21	1	4	18
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	42	18	23	1	4	20
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		115	93	102	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		115	93	102	0
tC, single (s)	4.1		7.3	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.7	4.0	4.0	3.3
p0 queue free %	97		97	100	99	98
cM capacity (veh/h)	1636		777	780	772	1091
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	60	24	24			
Volume Left	42	23	0			
Volume Right	18	0	20			
cSH	1636	777	1020			
Volume to Capacity	0.03	0.03	0.02			
Queue Length 95th (m)	0.6	0.8	0.6			
Control Delay (s)	5.1	9.8	8.6			
Lane LOS	A	A	A			
Approach Delay (s)	5.1	9.8	8.6			
Approach LOS		A	A			
Intersection Summary						
Average Delay			6.9			
Intersection Capacity Utilization			17.9%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	70	43	40	354	308	55
Future Volume (vph)	70	43	40	354	308	55
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.948					0.850
Flt Protected	0.970		0.950			
Satd. Flow (prot)	1676	0	1752	1776	1759	1524
Flt Permitted	0.970		0.950			
Satd. Flow (perm)	1676	0	1752	1776	1759	1524
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	3%	3%	7%	8%	6%
Adj. Flow (vph)	76	47	43	385	335	60
Shared Lane Traffic (%)						
Lane Group Flow (vph)	123	0	43	385	335	60
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	36.1% ICU Level of Service A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2030 Background AM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	70	43	40	354	308	55
Future Volume (Veh/h)	70	43	40	354	308	55
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	76	47	43	385	335	60
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	806	335	395			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	806	335	395			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	77	93	96			
cM capacity (veh/h)	334	705	1158			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	123	43	385	335	60	
Volume Left	76	43	0	0	0	
Volume Right	47	0	0	0	60	
cSH	418	1158	1700	1700	1700	
Volume to Capacity	0.29	0.04	0.23	0.20	0.04	
Queue Length 95th (m)	9.7	0.9	0.0	0.0	0.0	
Control Delay (s)	17.2	8.2	0.0	0.0	0.0	
Lane LOS	C	A				
Approach Delay (s)	17.2	0.8		0.0		
Approach LOS	C					
Intersection Summary						
Average Delay			2.6			
Intersection Capacity Utilization			36.1%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2030 Background AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↕			↕	↗
Traffic Volume (vph)	79	10	27	1	9	21	25	280	1	12	257	73
Future Volume (vph)	79	10	27	1	9	21	25	280	1	12	257	73
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.909							0.850
Flt Protected		0.958			0.999		0.950				0.998	
Satd. Flow (prot)	0	1748	1538	0	1725	0	1626	1728	0	0	1731	1615
Flt Permitted		0.958			0.999		0.950				0.998	
Satd. Flow (perm)	0	1748	1538	0	1725	0	1626	1728	0	0	1731	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	86	11	29	1	10	23	27	304	1	13	279	79
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	97	29	0	34	0	27	305	0	0	292	79
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	41.5%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2030 Background AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔	↔		↔		↔	↔			↔	↔
Traffic Volume (veh/h)	79	10	27	1	9	21	25	280	1	12	257	73
Future Volume (Veh/h)	79	10	27	1	9	21	25	280	1	12	257	73
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	86	11	29	1	10	23	27	304	1	13	279	79
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	691	664	279	669	742	304	358			305		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	691	664	279	669	742	304	358			305		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	74	97	96	100	97	97	98			99		
cM capacity (veh/h)	330	355	753	342	334	740	1152			1267		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	126	34	27	305	292	79						
Volume Left	86	1	27	0	13	0						
Volume Right	29	23	0	1	0	79						
cSH	432	532	1152	1700	1267	1700						
Volume to Capacity	0.29	0.06	0.02	0.18	0.01	0.05						
Queue Length 95th (m)	9.6	1.6	0.6	0.0	0.2	0.0						
Control Delay (s)	17.9	12.2	8.2	0.0	0.4	0.0						
Lane LOS	C	B	A		A							
Approach Delay (s)	17.9	12.2	0.7		0.3							
Approach LOS	C	B										
Intersection Summary												
Average Delay			3.5									
Intersection Capacity Utilization			41.5%	ICU Level of Service	A							
Analysis Period (min)			15									

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
2030 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	53	86	269	56	57	16	200	238	55	31	386	34
Future Volume (vph)	53	86	269	56	57	16	200	238	55	31	386	34
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.886				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1683	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.717			0.222			0.494			0.567		
Satd. Flow (perm)	1336	1683	0	394	1863	1615	939	1776	0	1077	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		174				52		21				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	58	93	292	61	62	17	217	259	60	34	420	37
Shared Lane Traffic (%)												
Lane Group Flow (vph)	58	385	0	61	62	17	217	319	0	34	420	37
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	18.0	18.0		18.0	18.0	18.0	57.7	57.7		57.7	57.7	57.7
Actuated g/C Ratio	0.20	0.20		0.20	0.20	0.20	0.64	0.64		0.64	0.64	0.64
v/c Ratio	0.22	0.81		0.78	0.17	0.05	0.36	0.28		0.05	0.35	0.04
Control Delay	29.4	31.6		86.9	28.1	0.2	11.2	8.5		8.2	9.7	2.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	29.4	31.6		86.9	28.1	0.2	11.2	8.5		8.2	9.7	2.2
LOS	C	C		F	C	A	B	A		A	A	A
Approach Delay		31.3			50.3			9.6			9.0	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	8.9	37.3		10.6	9.4	0.0	16.4	20.8		2.1	31.5	0.0

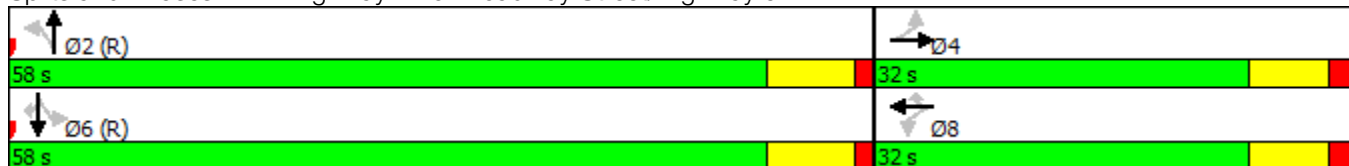


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	17.3	62.9		#26.7	17.9	0.3	40.1	44.9		7.3	63.8	3.3
Internal Link Dist (m)		211.6			468.9			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	376	598		110	524	491	605	1152		694	1201	1058
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.15	0.64		0.55	0.12	0.03	0.36	0.28		0.05	0.35	0.03

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 50
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.81
 Intersection Signal Delay: 18.9 Intersection LOS: B
 Intersection Capacity Utilization 90.2% ICU Level of Service E
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
2030 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	111	166	43	224	142	176	55	255	127	247	446	92
Future Volume (vph)	111	166	43	224	142	176	55	255	127	247	446	92
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.969				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1830	0	1787	1900	1583	1805	1752	0	1787	1881	1583
Flt Permitted	0.659			0.565			0.487			0.335		
Satd. Flow (perm)	1252	1830	0	1063	1900	1583	925	1752	0	630	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		12				191		32				92
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	121	180	47	243	154	191	60	277	138	268	485	100
Shared Lane Traffic (%)												
Lane Group Flow (vph)	121	227	0	243	154	191	60	415	0	268	485	100
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	34.8	34.8		34.8	34.8	34.8	36.6	36.6		56.7	51.4	51.4
Actuated g/C Ratio	0.35	0.35		0.35	0.35	0.35	0.37	0.37		0.57	0.51	0.51
v/c Ratio	0.28	0.35		0.66	0.23	0.28	0.18	0.63		0.53	0.50	0.12
Control Delay	26.0	25.0		38.1	24.6	4.8	24.1	29.4		15.1	18.1	3.4
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	26.0	25.0		38.1	24.6	4.8	24.1	29.4		15.1	18.1	3.4
LOS	C	C		D	C	A	C	C		B	B	A
Approach Delay		25.4			23.8			28.8			15.4	
Approach LOS		C			C			C			B	
Queue Length 50th (m)	17.5	31.8		41.1	21.8	0.0	8.3	64.6		26.6	62.7	0.8

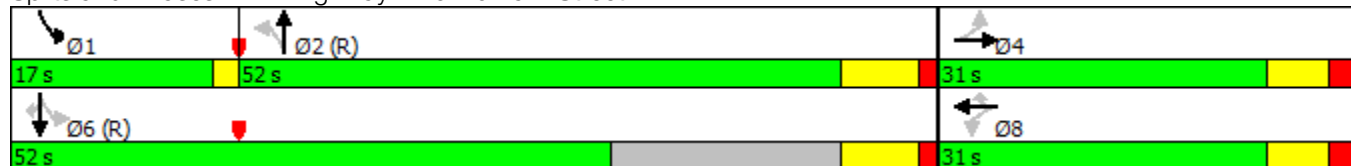


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	34.5	55.4		#80.9	39.6	15.3	17.6	95.0		37.4	83.2	8.1
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	435	644		369	661	675	413	800		530	1160	1011
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.28	0.35		0.66	0.23	0.28	0.15	0.52		0.51	0.42	0.10

Intersection Summary

Area Type: Other
 Cycle Length: 100
 Actuated Cycle Length: 100
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 60
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.66
 Intersection Signal Delay: 21.9 Intersection LOS: C
 Intersection Capacity Utilization 86.9% ICU Level of Service E
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	48	13	60	1	10	35
Future Volume (vph)	48	13	60	1	10	35
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.971			0.895		
Flt Protected	0.962			0.953		
Satd. Flow (prot)	1665	0	0	1811	1700	0
Flt Permitted	0.962			0.953		
Satd. Flow (perm)	1665	0	0	1811	1700	0
Link Speed (k/h)	50			50	50	
Link Distance (m)	189.4			138.6	84.1	
Travel Time (s)	13.6			10.0	6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	20%	0%	0%	0%	0%
Adj. Flow (vph)	52	14	65	1	11	38
Shared Lane Traffic (%)						
Lane Group Flow (vph)	66	0	0	66	49	0
Sign Control	Free			Stop	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	20.2%
	ICU Level of Service A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 2030 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	48	13	60	1	10	35
Future Volume (Veh/h)	48	13	60	1	10	35
Sign Control	Free			Stop	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	52	14	65	1	11	38
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None					
Median storage (veh)						
Upstream signal (m)	189					
pX, platoon unblocked						
vC, conflicting volume	0		154	111	118	0
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	0		154	111	118	0
tC, single (s)	4.1		7.1	6.5	6.5	6.2
tC, 2 stage (s)						
tF (s)	2.2		3.5	4.0	4.0	3.3
p0 queue free %	97		91	100	99	97
cM capacity (veh/h)	1617		760	758	751	1091
Direction, Lane #						
	EB 1	NB 1	SB 1			
Volume Total	66	66	49			
Volume Left	52	65	0			
Volume Right	14	0	38			
cSH	1617	760	990			
Volume to Capacity	0.03	0.09	0.05			
Queue Length 95th (m)	0.8	2.3	1.2			
Control Delay (s)	5.8	10.2	8.8			
Lane LOS	A	B	A			
Approach Delay (s)	5.8	10.2	8.8			
Approach LOS		B	A			
Intersection Summary						
Average Delay			8.2			
Intersection Capacity Utilization			20.2%	ICU Level of Service	A	
Analysis Period (min)			15			



Lane Group	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (vph)	114	53	60	313	605	125
Future Volume (vph)	114	53	60	313	605	125
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	15.0			45.0
Storage Lanes	1	0	1			1
Taper Length (m)	7.5		30.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.957					0.850
Flt Protected	0.967		0.950			
Satd. Flow (prot)	1712	0	1770	1845	1863	1615
Flt Permitted	0.967		0.950			
Satd. Flow (perm)	1712	0	1770	1845	1863	1615
Link Speed (k/h)	50			80	80	
Link Distance (m)	71.8			1178.3	487.8	
Travel Time (s)	5.2			53.0	22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	3%	2%	0%
Adj. Flow (vph)	124	58	65	340	658	136
Shared Lane Traffic (%)						
Lane Group Flow (vph)	182	0	65	340	658	136
Sign Control	Stop			Free	Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	54.7%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
2030 Background PM



Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	114	53	60	313	605	125
Future Volume (Veh/h)	114	53	60	313	605	125
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	124	58	65	340	658	136
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type				None	None	
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume	1128	658	794			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	1128	658	794			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	40	88	92			
cM capacity (veh/h)	207	464	827			
Direction, Lane #	EB 1	NB 1	NB 2	SB 1	SB 2	
Volume Total	182	65	340	658	136	
Volume Left	124	65	0	0	0	
Volume Right	58	0	0	0	136	
cSH	252	827	1700	1700	1700	
Volume to Capacity	0.72	0.08	0.20	0.39	0.08	
Queue Length 95th (m)	39.9	2.0	0.0	0.0	0.0	
Control Delay (s)	49.4	9.7	0.0	0.0	0.0	
Lane LOS	E	A				
Approach Delay (s)	49.4	1.6		0.0		
Approach LOS	E					
Intersection Summary						
Average Delay			7.0			
Intersection Capacity Utilization			54.7%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2030 Background PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	74	7	39	4	12	12	38	296	4	26	501	112
Future Volume (vph)	74	7	39	4	12	12	38	296	4	26	501	112
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.941			0.998				0.850
Flt Protected		0.957			0.993		0.950				0.998	
Satd. Flow (prot)	0	1754	1615	0	1558	0	1805	1824	0	0	1856	1615
Flt Permitted		0.957			0.993		0.950				0.998	
Satd. Flow (perm)	0	1754	1615	0	1558	0	1805	1824	0	0	1856	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	80	8	42	4	13	13	41	322	4	28	545	122
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	88	42	0	30	0	41	326	0	0	573	122
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	64.8%
ICU Level of Service	C
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
2030 Background PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↔		↖	↖			↕	↗
Traffic Volume (veh/h)	74	7	39	4	12	12	38	296	4	26	501	112
Future Volume (Veh/h)	74	7	39	4	12	12	38	296	4	26	501	112
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	80	8	42	4	13	13	41	322	4	28	545	122
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1024	1009	545	1011	1129	324	667			326		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1024	1009	545	1011	1129	324	667			326		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	57	96	92	98	93	98	96			98		
cM capacity (veh/h)	186	226	542	163	175	722	932			1217		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	130	30	41	326	573	122						
Volume Left	80	4	41	0	28	0						
Volume Right	42	13	0	4	0	122						
cSH	281	257	932	1700	1217	1700						
Volume to Capacity	0.46	0.12	0.04	0.19	0.02	0.07						
Queue Length 95th (m)	18.5	3.1	1.1	0.0	0.6	0.0						
Control Delay (s)	30.6	20.9	9.0	0.0	0.7	0.0						
Lane LOS	D	C	A		A							
Approach Delay (s)	30.6	20.9	1.0		0.5							
Approach LOS	D	C										
Intersection Summary												
Average Delay			4.4									
Intersection Capacity Utilization			64.8%		ICU Level of Service					C		
Analysis Period (min)			15									



Appendix H

2030 Total Traffic Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall	
				Eastbound				Westbound				Northbound				Southbound					
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach		
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	B	B	C	D	D	A	D	A	A	A	A	A	A	A	A	B	
			Delay	38	17	17	21	50	38	6	36	5	5	5	5	4	5	1	4	4	12
			V/C	0.23	0.56	0.56		0.48	0.26	0.13		0.19	0.29	0.29		0.02	0.17	0.02			
			Queue	14.9	25.3	25.3		22.5	21.1	3.9		17.0	35.5	35.5		2.7	20.9	0.8			
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	E	D	A	D	B	B	B	B	A	A	A	A	A	C
			Delay	44	43	43	43	73	37	8	36	13	15	15	15	6	7	3	7	7	23
V/C			0.51	0.64	0.64		0.81	0.33	0.41		0.16	0.47	0.47		0.30	0.22	0.04				
Queue			35.9	55.9	55.9		42.2	32.5	15.7		23.6	93.7	93.7		22.3	36.1	4.1				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	B	B	B	B	A	A	A	A	A	A	7	
		Delay	5	5	5	5	3	3	3	3	13	13	13	13	9	9	9	9	9	9	
		V/C	0.08	0.08	0.08		0.00	0.00	0.00		0.11	0.11	0.11		0.07	0.07	0.07				
		Queue	2.0	2.0	2.0		0.0	0.0	0.0		2.9	2.9	2.9		1.8	1.8	1.8				
4 - Highway 21 & Russell Street	TWSC	LOS	F	F	F	F	D	D	D	D	A	A	A	A	A	A	A	A	A	12	
		Delay	70	70	70	70	25	25	25	25	8	0	0	0	2	2	0	2	2	12	
		V/C	0.81	0.81	0.81		0.34	0.34	0.34		0.04	0.26	0.26		0.08	0.08	0.04				
		Queue	46.1	46.1	46.1		11.8	11.8	11.8		1.0	0.0	0.0		2.0	2.0	0.0				
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	C	C	C	C	B	B	B	B	A	A	A	A	A	A	A	A	A	5	
		Delay	22	22	22	22	13	13	13	13	8	0	0	0	0	0	0	0	0	0	
		V/C	0.43	0.43	0.43		0.07	0.07	0.07		0.02	0.19	0.19		0.01	0.01	0.06				
		Queue	16.9	16.9	16.9		1.7	1.7	1.7		0.6	0.0	0.0		0.3	0.3	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A						0	
		Delay		0	0	0	0	0		0	9		9		9						
		V/C		0.06	0.06		0.00	0.00			0.00		0.00		0.00						
		Queue		0.0	0.0		0.1	0.1			0.1		0.1								
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	C	C	C	F	C	A	E	C	B	B	C	B	B	A	B	C	
			Delay	24	24	24	24	104	24	0	60	29	12	12	20	11	13	3	12	23	
			V/C	0.17	0.83	0.83		0.87	0.13	0.03		0.75	0.36	0.36		0.05	0.43	0.04			
			Queue	16.9	81.1	81.1		35.0	17.4	0.0		109.0	57.5	57.5		6.2	75.8	3.5			
	2 - Highway 21 & Durham Street	Signal	LOS	C	C	C	C	F	C	A	E	C	D	D	D	E	B	A	D	D	
			Delay	28	30	30	29	152	27	5	65	31	52	52	48	71	19	5	37	46	
V/C			0.32	0.57	0.57		1.19	0.34	0.40		0.48	0.92	0.92		1.00	0.59	0.12				
Queue			34.9	88.2	88.2		131.8	54.9	19.3		40.5	166.6	166.6		112.5	104.7	11.0				
3 - Durham Street & Millennium Way	TWSC	LOS	A	A	A	A	A	A	A	A	D	D	D	D	A	A	A	A	A		
		Delay	5	5	5	5	5	5	5	5	26	26	26	26	10	10	10	10	10		
		V/C	0.11	0.11	0.11		0.01	0.01	0.01		0.50	0.50	0.50		0.19	0.19	0.19				
		Queue	2.8	2.8	2.8		0.1	0.1	0.1		21.5	21.5	21.5		5.4	5.4	5.4				
4 - Highway 21 & Russell Street	TWSC	LOS	F	F	F	F	F	F	F	F	A	A	A	A	A	A	A	A	A		
		Delay	Err	Err	Err	Err	Err	Err	Err	Err	Err	10	0	0	1	5	5	0	5	Err	
		V/C	Err	Err	Err	Err	14.16	14.16	14.16	Err	Err	0.08	0.27	0.27		0.24	0.24	0.09			
		Queue	Err	Err	Err	Err	Err	Err	Err	Err	Err	1.9	0.0	0.0		7.6	7.6	0.0			
5 - Highway 21 & Kincardine Avenue	TWSC	LOS	F	F	F	F	D	D	D	D	A	A	A	A	A	A	A	A	A		
		Delay	97	97	97	97	25	25	25	25	10	0	0	0	1	1	1	0	1	14	
		V/C	0.97	0.97	0.97		0.15	0.15	0.15		0.05	0.22	0.22		0.02	0.11	0.11				
		Queue	65.3	65.3	65.3		4.0	4.0	4.0		1.2	0.0	0.0		0.6	0.6	0.0				
6 - Highway 9 & Durham Street	TWSC	LOS		A	A	A	A	A		A	A		A	A							
		Delay		0	0	0	1	1		1	9		9		9						
		V/C		0.11	0.11		0.01	0.01			0.02		0.02		0.02						
		Queue		0.0	0.0		0.2	0.2			0.4		0.4								



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2030 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	34	35	136	55	55	27	143	300	39	14	199	20
Future Volume (vph)	34	35	136	55	55	27	143	300	39	14	199	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.881				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1618	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.718			0.523			0.623			0.542		
Satd. Flow (perm)	1287	1618	0	994	1827	1380	1117	1766	0	858	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		148				52		12				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	37	38	148	60	60	29	155	326	42	15	216	22
Shared Lane Traffic (%)												
Lane Group Flow (vph)	37	186	0	60	60	29	155	368	0	15	216	22
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	32.0	32.0		32.0	32.0	32.0	58.0	58.0		58.0	58.0	58.0
Total Split (%)	35.6%	35.6%		35.6%	35.6%	35.6%	64.4%	64.4%		64.4%	64.4%	64.4%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	11.3	11.3		11.3	11.3	11.3	64.4	64.4		64.4	64.4	64.4
Actuated g/C Ratio	0.13	0.13		0.13	0.13	0.13	0.72	0.72		0.72	0.72	0.72
v/c Ratio	0.23	0.56		0.48	0.26	0.13	0.19	0.29		0.02	0.17	0.02
Control Delay	38.3	17.0		49.6	38.0	5.5	5.2	5.4		4.4	4.8	0.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	38.3	17.0		49.6	38.0	5.5	5.2	5.4		4.4	4.8	0.5
LOS	D	B		D	D	A	A	A		A	A	A
Approach Delay		20.6			36.3			5.3			4.4	
Approach LOS		C			D			A			A	
Queue Length 50th (m)	6.3	6.4		10.5	10.2	0.0	7.3	18.2		0.6	10.1	0.0

Lanes, Volumes, Timings
 1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
 Total 2030 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	14.9	25.3		22.5	21.1	3.9	17.0	35.5		2.7	20.9	0.8
Internal Link Dist (m)		211.6			466.2			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	357	556		276	507	420	799	1267		614	1259	1169
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.10	0.33		0.22	0.12	0.07	0.19	0.29		0.02	0.17	0.02

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 45
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.56
 Intersection Signal Delay: 12.1 Intersection LOS: B
 Intersection Capacity Utilization 77.2% ICU Level of Service D
 Analysis Period (min) 15

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2030 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	107	147	49	114	100	150	95	259	159	172	238	38
Future Volume (vph)	107	147	49	114	100	150	95	259	159	172	238	38
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.963				0.850		0.943				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1807	0	1770	1863	1509	1805	1662	0	1626	1712	1583
Flt Permitted	0.687			0.466			0.599			0.422		
Satd. Flow (perm)	1280	1807	0	868	1863	1509	1138	1662	0	722	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		16				163		40				41
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	116	160	53	124	109	163	103	282	173	187	259	41
Shared Lane Traffic (%)												
Lane Group Flow (vph)	116	213	0	124	109	163	103	455	0	187	259	41
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	31.0	31.0		31.0	31.0	31.0	52.0	52.0		17.0	52.0	52.0
Total Split (%)	31.0%	31.0%		31.0%	31.0%	31.0%	52.0%	52.0%		17.0%	52.0%	52.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	17.8	17.8		17.8	17.8	17.8	57.1	57.1		73.7	68.4	68.4
Actuated g/C Ratio	0.18	0.18		0.18	0.18	0.18	0.57	0.57		0.74	0.68	0.68
v/c Ratio	0.51	0.64		0.81	0.33	0.41	0.16	0.47		0.30	0.22	0.04
Control Delay	43.5	42.9		72.8	36.7	8.1	13.4	15.2		6.2	7.4	2.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	43.5	42.9		72.8	36.7	8.1	13.4	15.2		6.2	7.4	2.5
LOS	D	D		E	D	A	B	B		A	A	A
Approach Delay		43.1			36.3			14.9			6.5	
Approach LOS		D			D			B			A	
Queue Length 50th (m)	21.7	37.6		24.5	19.6	0.0	9.2	45.5		9.5	17.4	0.0

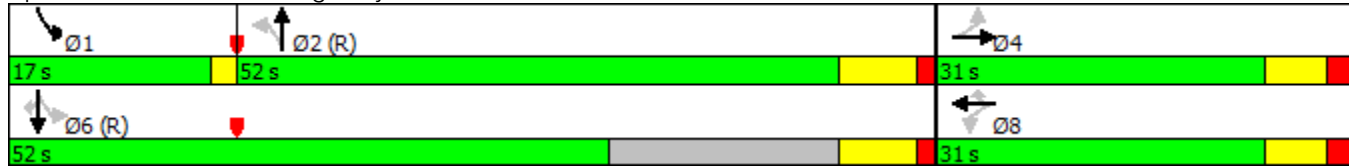


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	35.9	55.9		42.2	32.2	15.7	23.6	93.7		22.3	36.1	4.1
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	317	459		214	461	496	649	966		667	1175	1099
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.37	0.46		0.58	0.24	0.33	0.16	0.47		0.28	0.22	0.04

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	55
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.81
Intersection Signal Delay:	22.6
Intersection LOS:	C
Intersection Capacity Utilization:	75.4%
ICU Level of Service:	D
Analysis Period (min):	15

Splits and Phases: 2: Highway 21 & Durham Street





Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	116	0	56	2	0	3	47	1	1	1	4	62
Future Volume (vph)	116	0	56	2	0	3	47	1	1	1	4	62
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.956			0.919			0.997			0.874	
Flt Protected		0.967			0.980			0.954			0.999	
Satd. Flow (prot)	0	1634	0	0	1678	0	0	1456	0	0	1658	0
Flt Permitted		0.967			0.980			0.954			0.999	
Satd. Flow (perm)	0	1634	0	0	1678	0	0	1456	0	0	1658	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			73.4			138.6			84.1	
Travel Time (s)		13.6			5.3			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	2%	23%	2%	2%	2%	25%	0%	2%	2%	0%	0%
Adj. Flow (vph)	126	0	61	2	0	3	51	1	1	1	4	67
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	187	0	0	5	0	0	53	0	0	72	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	32.4%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2030 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	116	0	56	2	0	3	47	1	1	1	4	62
Future Volume (Veh/h)	116	0	56	2	0	3	47	1	1	1	4	62
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	126	0	61	2	0	3	51	1	1	1	4	67
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	3			61			357	290	30	290	318	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	3			61			357	290	30	290	318	2
tC, single (s)	4.1			4.1			7.3	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.7	4.0	3.3	3.5	4.0	3.3
p0 queue free %	92			100			90	100	100	100	99	94
cM capacity (veh/h)	1632			1542			489	575	1044	622	554	1089
Direction, Lane #												
	EB 1	WB 1	NB 1	SB 1								
Volume Total	187	5	53	72								
Volume Left	126	2	51	1								
Volume Right	61	3	1	67								
cSH	1632	1542	496	1023								
Volume to Capacity	0.08	0.00	0.11	0.07								
Queue Length 95th (m)	2.0	0.0	2.9	1.8								
Control Delay (s)	5.2	2.9	13.1	8.8								
Lane LOS	A	A	B	A								
Approach Delay (s)	5.2	2.9	13.1	8.8								
Approach LOS			B	A								
Intersection Summary												
Average Delay			7.3									
Intersection Capacity Utilization			32.4%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 AM





















Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕↕			↕↕		↗	↘			↕↕	↗
Traffic Volume (vph)	84	25	43	23	15	49	40	374	37	80	320	63
Future Volume (vph)	84	25	43	23	15	49	40	374	37	80	320	63
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.962			0.924			0.987				0.850
Flt Protected		0.973			0.987		0.950				0.990	
Satd. Flow (prot)	0	1711	0	0	1699	0	1752	1760	0	0	1761	1524
Flt Permitted		0.973			0.987		0.950				0.990	
Satd. Flow (perm)	0	1711	0	0	1699	0	1752	1760	0	0	1761	1524
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			63.0			1178.3			487.8	
Travel Time (s)		5.2			4.5			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	2%	3%	2%	2%	2%	3%	7%	2%	2%	8%	6%
Adj. Flow (vph)	91	27	47	25	16	53	43	407	40	87	348	68
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	165	0	0	94	0	43	447	0	0	435	68
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	68.5%
ICU Level of Service	C
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 AM

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	84	25	43	23	15	49	40	374	37	80	320	63
Future Volume (Veh/h)	84	25	43	23	15	49	40	374	37	80	320	63
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	91	27	47	25	16	53	43	407	40	87	348	68
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
								None			None	
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1076	1055	348	1096	1103	427	416			447		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1076	1055	348	1096	1103	427	416			447		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	40	87	93	83	91	92	96			92		
cM capacity (veh/h)	152	200	693	146	187	628	1138			1113		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	165	94	43	447	435	68						
Volume Left	91	25	43	0	87	0						
Volume Right	47	53	0	40	0	68						
cSH	206	276	1138	1700	1113	1700						
Volume to Capacity	0.80	0.34	0.04	0.26	0.08	0.04						
Queue Length 95th (m)	45.7	11.7	0.9	0.0	2.0	0.0						
Control Delay (s)	68.8	24.7	8.3	0.0	2.4	0.0						
Lane LOS	F	C	A		A							
Approach Delay (s)	68.8	24.7	0.7		2.0							
Approach LOS	F	C										
Intersection Summary												
Average Delay			12.0									
Intersection Capacity Utilization			68.5%		ICU Level of Service					C		
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2030 AM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	113	10	27	1	9	21	25	303	1	12	272	94
Future Volume (vph)	113	10	27	1	9	21	25	303	1	12	272	94
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.909							0.850
Flt Protected		0.956			0.999		0.950				0.998	
Satd. Flow (prot)	0	1750	1538	0	1725	0	1626	1728	0	0	1730	1615
Flt Permitted		0.956			0.999		0.950				0.998	
Satd. Flow (perm)	0	1750	1538	0	1725	0	1626	1728	0	0	1730	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	13%	5%	0%	0%	0%	11%	10%	0%	0%	10%	0%
Adj. Flow (vph)	123	11	29	1	10	23	27	329	1	13	296	102
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	134	29	0	34	0	27	330	0	0	309	102
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	44.2%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2030 AM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (veh/h)	113	10	27	1	9	21	25	303	1	12	272	94
Future Volume (Veh/h)	113	10	27	1	9	21	25	303	1	12	272	94
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	123	11	29	1	10	23	27	329	1	13	296	102
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	733	706	296	711	808	330	398			330		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	733	706	296	711	808	330	398			330		
tC, single (s)	7.1	6.6	6.2	7.1	6.5	6.2	4.2			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.1	3.3	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	60	97	96	100	97	97	98			99		
cM capacity (veh/h)	308	335	736	320	306	717	1113			1241		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	163	34	27	330	309	102						
Volume Left	123	1	27	0	13	0						
Volume Right	29	23	0	1	0	102						
cSH	377	501	1113	1700	1241	1700						
Volume to Capacity	0.43	0.07	0.02	0.19	0.01	0.06						
Queue Length 95th (m)	16.9	1.7	0.6	0.0	0.3	0.0						
Control Delay (s)	22.5	12.7	8.3	0.0	0.4	0.0						
Lane LOS	C	B	A		A							
Approach Delay (s)	22.5	12.7	0.6		0.3							
Approach LOS	C	B										
Intersection Summary												
Average Delay			4.6									
Intersection Capacity Utilization			44.2%		ICU Level of Service					A		
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	88	0	4	137	0	3
Future Volume (vph)	88	0	4	137	0	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt					0.865	
Flt Protected				0.999		
Satd. Flow (prot)	1863	0	0	1861	1611	0
Flt Permitted				0.999		
Satd. Flow (perm)	1863	0	0	1861	1611	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	490.2			203.9	128.0	
Travel Time (s)	35.3			9.2	9.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	96	0	4	149	0	3
Shared Lane Traffic (%)						
Lane Group Flow (vph)	96	0	0	153	3	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	20.4%
ICU Level of Service	A
Analysis Period (min)	15



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	→			←	←	←
Traffic Volume (veh/h)	88	0	4	137	0	3
Future Volume (Veh/h)	88	0	4	137	0	3
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	96	0	4	149	0	3
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None			None		
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			96		253	96
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			96		253	96
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			100		100	100
cM capacity (veh/h)			1498		734	960
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	96	153	3			
Volume Left	0	4	0			
Volume Right	0	0	3			
cSH	1700	1498	960			
Volume to Capacity	0.06	0.00	0.00			
Queue Length 95th (m)	0.0	0.1	0.1			
Control Delay (s)	0.0	0.2	8.8			
Lane LOS		A	A			
Approach Delay (s)	0.0	0.2	8.8			
Approach LOS			A			
Intersection Summary						
Average Delay			0.2			
Intersection Capacity Utilization			20.4%	ICU Level of Service	A	
Analysis Period (min)			15			

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2030 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	53	86	390	63	57	12	335	283	66	24	431	34
Future Volume (vph)	53	86	390	63	57	12	335	283	66	24	431	34
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.877				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1666	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.717			0.172			0.439			0.508		
Satd. Flow (perm)	1336	1666	0	305	1863	1615	834	1776	0	965	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		265				52		20				48
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0				262.4
Travel Time (s)		17.0			22.2			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	58	93	424	68	62	13	364	308	72	26	468	37
Shared Lane Traffic (%)												
Lane Group Flow (vph)	58	517	0	68	62	13	364	380	0	26	468	37
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		17.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	35.0	35.0		35.0	35.0	35.0	55.0	55.0		55.0	55.0	55.0
Total Split (%)	38.9%	38.9%		38.9%	38.9%	38.9%	61.1%	61.1%		61.1%	61.1%	61.1%
Yellow Time (s)	5.4	5.4		5.4	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.6	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		7.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag												
Lead-Lag Optimize?												
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	23.2	23.2		23.2	23.2	23.2	52.5	52.5		52.5	52.5	52.5
Actuated g/C Ratio	0.26	0.26		0.26	0.26	0.26	0.58	0.58		0.58	0.58	0.58
v/c Ratio	0.17	0.83		0.87	0.13	0.03	0.75	0.36		0.05	0.43	0.04
Control Delay	24.4	26.2		104.2	23.5	0.1	28.5	11.9		10.5	13.3	2.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	24.4	26.2		104.2	23.5	0.1	28.5	11.9		10.5	13.3	2.5
LOS	C	C		F	C	A	C	B		B	B	A
Approach Delay		26.0			59.8			20.0			12.4	
Approach LOS		C			E			C			B	
Queue Length 50th (m)	7.6	40.3		10.9	8.0	0.0	52.1	36.7		2.2	50.4	0.0

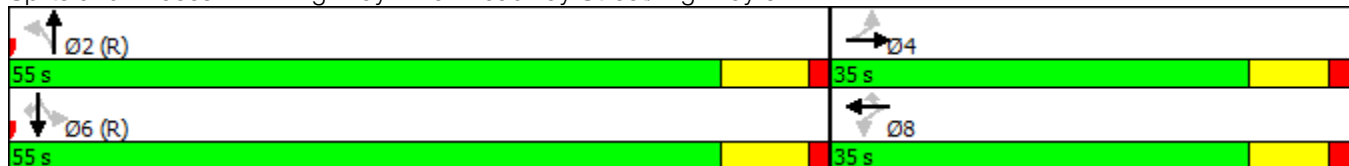


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	16.9	81.1		#35.0	17.4	0.0	#109.0	57.5		6.2	75.8	3.5
Internal Link Dist (m)		211.6			468.9			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	415	700		94	579	538	486	1044		562	1086	962
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.14	0.74		0.72	0.11	0.02	0.75	0.36		0.05	0.43	0.04

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 60
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.87
 Intersection Signal Delay: 22.6 Intersection LOS: C
 Intersection Capacity Utilization 102.0% ICU Level of Service G
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2030 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	111	223	110	280	204	270	130	351	177	344	521	92
Future Volume (vph)	111	223	110	280	204	270	130	351	177	344	521	92
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		0.0	30.0		30.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.950				0.850		0.950				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1787	0	1787	1900	1583	1805	1752	0	1787	1881	1583
Flt Permitted	0.572			0.390			0.452			0.135		
Satd. Flow (perm)	1087	1787	0	734	1900	1583	859	1752	0	254	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		26				293		29				65
Link Speed (k/h)		50			50			80				80
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	121	242	120	304	222	293	141	382	192	374	566	100
Shared Lane Traffic (%)												
Lane Group Flow (vph)	121	362	0	304	222	293	141	574	0	374	566	100
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		8	8	8	2	2		1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		10.0	10.0	10.0	20.0	20.0		5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		16.5	16.5	16.5	27.3	27.3		7.0	27.3	27.3
Total Split (s)	39.0	39.0		39.0	39.0	39.0	44.0	44.0		17.0	61.0	61.0
Total Split (%)	39.0%	39.0%		39.0%	39.0%	39.0%	44.0%	44.0%		17.0%	61.0%	61.0%
Yellow Time (s)	4.5	4.5		4.5	4.5	4.5	5.9	5.9		2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		2.0	2.0	2.0	1.4	1.4		0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		6.5	6.5	6.5	7.3	7.3		2.0	7.3	7.3
Lead/Lag							Lag	Lag		Lead		
Lead-Lag Optimize?							Yes	Yes		Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min		None	C-Min	C-Min
Act Effct Green (s)	34.8	34.8		34.8	34.8	34.8	34.4	34.4		56.7	51.4	51.4
Actuated g/C Ratio	0.35	0.35		0.35	0.35	0.35	0.34	0.34		0.57	0.51	0.51
v/c Ratio	0.32	0.57		1.19	0.34	0.40	0.48	0.92		1.00	0.59	0.12
Control Delay	28.1	29.5		151.7	26.8	4.7	31.2	51.7		71.1	19.4	5.2
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	28.1	29.5		151.7	26.8	4.7	31.2	51.7		71.1	19.4	5.2
LOS	C	C		F	C	A	C	D		E	B	A
Approach Delay		29.1			65.3			47.7			36.7	
Approach LOS		C			E			D			D	
Queue Length 50th (m)	18.6	57.2		~78.9	34.4	0.0	21.5	102.6		51.6	72.6	3.2

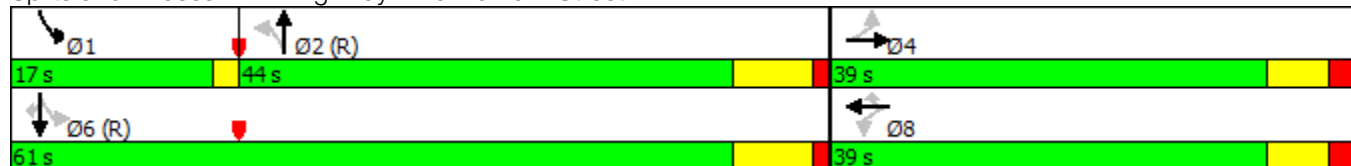


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	34.9	88.2		#131.8	54.9	18.3	40.5	#166.6		#112.5	104.7	11.0
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0			30.0		30.0
Base Capacity (vph)	377	638		255	660	741	315	661		373	1010	880
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.32	0.57		1.19	0.34	0.40	0.45	0.87		1.00	0.56	0.11

Intersection Summary

Area Type: Other
 Cycle Length: 100
 Actuated Cycle Length: 100
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 70
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 1.19
 Intersection Signal Delay: 45.7 Intersection LOS: D
 Intersection Capacity Utilization 102.5% ICU Level of Service G
 Analysis Period (min) 15
 ~ Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 2: Highway 21 & Durham Street



Lanes, Volumes, Timings
3: Millienium Way & Durham Street

Kincardine Business Park TIS
Total 2030 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (vph)	156	0	109	7	0	4	147	1	8	5	10	150
Future Volume (vph)	156	0	109	7	0	4	147	1	8	5	10	150
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.945			0.955			0.993			0.877	
Flt Protected		0.971			0.968			0.955			0.999	
Satd. Flow (prot)	0	1585	0	0	1722	0	0	1800	0	0	1664	0
Flt Permitted		0.971			0.968			0.955			0.999	
Satd. Flow (perm)	0	1585	0	0	1722	0	0	1800	0	0	1664	0
Link Speed (k/h)		50			50			50			50	
Link Distance (m)		189.4			77.0			138.6			84.1	
Travel Time (s)		13.6			5.5			10.0			6.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	20%	2%	2%	2%	0%	0%	2%	2%	0%	0%
Adj. Flow (vph)	170	0	118	8	0	4	160	1	9	5	11	163
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	288	0	0	12	0	0	170	0	0	179	0
Sign Control		Free			Free			Stop			Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	46.4%
ICU Level of Service	A
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
 3: Millienium Way & Durham Street

Kincardine Business Park TIS
 Total 2030 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Volume (veh/h)	156	0	109	7	0	4	147	1	8	5	10	150
Future Volume (Veh/h)	156	0	109	7	0	4	147	1	8	5	10	150
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	170	0	118	8	0	4	160	1	9	5	11	163
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage (veh)												
Upstream signal (m)		189										
pX, platoon unblocked												
vC, conflicting volume	4			118			586	419	59	426	476	2
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	4			118			586	419	59	426	476	2
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	89			99			51	100	99	99	97	85
cM capacity (veh/h)	1611			1470			325	470	1007	488	437	1088
Direction, Lane #												
	EB 1	WB 1	NB 1	SB 1								
Volume Total	288	12	170	179								
Volume Left	170	8	160	5								
Volume Right	118	4	9	163								
cSH	1611	1470	337	966								
Volume to Capacity	0.11	0.01	0.50	0.19								
Queue Length 95th (m)	2.8	0.1	21.6	5.4								
Control Delay (s)	4.8	5.0	26.0	9.6								
Lane LOS	A	A	D	A								
Approach Delay (s)	4.8	5.0	26.0	9.6								
Approach LOS			D	A								
Intersection Summary												
Average Delay			11.7									
Intersection Capacity Utilization			46.4%		ICU Level of Service				A			
Analysis Period (min)			15									

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↕	↕			↕	↕
Traffic Volume (vph)	132	49	53	182	55	242	60	276	139	248	536	144
Future Volume (vph)	132	49	53	182	55	242	60	276	139	248	536	144
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		0.0	0.0		45.0
Storage Lanes	0		0	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.969			0.932			0.950				0.850
Flt Protected		0.973			0.981		0.950				0.984	
Satd. Flow (prot)	0	1747	0	0	1703	0	1770	1758	0	0	1833	1615
Flt Permitted		0.973			0.981		0.950				0.984	
Satd. Flow (perm)	0	1747	0	0	1703	0	1770	1758	0	0	1833	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		71.8			79.2			1178.3			487.8	
Travel Time (s)		5.2			5.7			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	2%	2%	2%	2%	3%	2%	2%	2%	0%
Adj. Flow (vph)	143	53	58	198	60	263	65	300	151	270	583	157
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	254	0	0	521	0	65	451	0	0	853	157
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	105.3%
ICU Level of Service	G
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕		↗	↘			↖	↗
Traffic Volume (veh/h)	132	49	53	182	55	242	60	276	139	248	536	144
Future Volume (Veh/h)	132	49	53	182	55	242	60	276	139	248	536	144
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	143	53	58	198	60	263	65	300	151	270	583	157
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
								None			None	
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1846	1704	583	1713	1786	376	740			451		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1846	1704	583	1713	1786	376	740			451		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	0	17	89	0	0	61	92			76		
cM capacity (veh/h)	0	64	512	16	57	671	867			1109		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	254	521	65	451	853	157						
Volume Left	143	198	65	0	270	0						
Volume Right	58	263	0	151	0	157						
cSH	0	37	867	1700	1109	1700						
Volume to Capacity	Err	14.08	0.08	0.27	0.24	0.09						
Queue Length 95th (m)	Err	Err	1.9	0.0	7.6	0.0						
Control Delay (s)	Err	Err	9.5	0.0	5.3	0.0						
Lane LOS	F	F	A		A							
Approach Delay (s)	Err	Err	1.2		4.5							
Approach LOS	F	F										
Intersection Summary												
Average Delay			Err									
Intersection Capacity Utilization			105.3%		ICU Level of Service				G			
Analysis Period (min)			15									

Lanes, Volumes, Timings
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2030 PM



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕	↗		↕		↖	↖			↕	↗
Traffic Volume (vph)	134	7	39	4	12	12	38	338	4	26	547	179
Future Volume (vph)	134	7	39	4	12	12	38	338	4	26	547	179
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		50.0	0.0		0.0	60.0		0.0	0.0		45.0
Storage Lanes	0		1	0		0	1		0	0		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt			0.850		0.941			0.998				0.850
Flt Protected		0.955			0.993		0.950				0.998	
Satd. Flow (prot)	0	1748	1615	0	1558	0	1805	1824	0	0	1857	1615
Flt Permitted		0.955			0.993		0.950				0.998	
Satd. Flow (perm)	0	1748	1615	0	1558	0	1805	1824	0	0	1857	1615
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		244.8			293.0			246.9			1178.3	
Travel Time (s)		17.6			21.1			11.1			53.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	4%	0%	0%	33%	22%	0%	0%	4%	0%	5%	2%	0%
Adj. Flow (vph)	146	8	42	4	13	13	41	367	4	28	595	195
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	154	42	0	30	0	41	371	0	0	623	195
Sign Control		Stop			Stop			Free			Free	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	71.1%
ICU Level of Service	C
Analysis Period (min)	15

HCM Unsignalized Intersection Capacity Analysis
5: Highway 21 & Kincardine Avenue

Kincardine Business Park TIS
Total 2030 PM



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↖	↗		↔		↖	↗			↖	↗
Traffic Volume (veh/h)	134	7	39	4	12	12	38	338	4	26	547	179
Future Volume (Veh/h)	134	7	39	4	12	12	38	338	4	26	547	179
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	146	8	42	4	13	13	41	367	4	28	595	195
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type												
Median storage (veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	1120	1104	595	1106	1297	369	790			371		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1120	1104	595	1106	1297	369	790			371		
tC, single (s)	7.1	6.5	6.2	7.4	6.7	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.8	4.2	3.3	2.2			2.2		
p0 queue free %	7	96	92	97	91	98	95			98		
cM capacity (veh/h)	157	198	508	138	137	681	839			1171		
Direction, Lane #												
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	196	30	41	371	623	195						
Volume Left	146	4	41	0	28	0						
Volume Right	42	13	0	4	0	195						
cSH	202	210	839	1700	1171	1700						
Volume to Capacity	0.97	0.14	0.05	0.22	0.02	0.11						
Queue Length 95th (m)	65.5	3.9	1.2	0.0	0.6	0.0						
Control Delay (s)	97.2	25.0	9.5	0.0	0.7	0.0						
Lane LOS	F	C	A		A							
Approach Delay (s)	97.2	25.0	0.9		0.5							
Approach LOS	F	C										
Intersection Summary												
Average Delay			14.1									
Intersection Capacity Utilization			71.1%		ICU Level of Service					C		
Analysis Period (min)			15									



Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	175	0	11	132	0	13
Future Volume (vph)	175	0	11	132	0	13
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt					0.865	
Flt Protected				0.996		
Satd. Flow (prot)	1863	0	0	1858	1644	0
Flt Permitted				0.996		
Satd. Flow (perm)	1863	0	0	1858	1644	0
Link Speed (k/h)	50			80	50	
Link Distance (m)	492.9			201.2	105.0	
Travel Time (s)	35.5			9.1	7.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	2%	0%	0%
Adj. Flow (vph)	190	0	12	143	0	14
Shared Lane Traffic (%)						
Lane Group Flow (vph)	190	0	0	155	14	0
Sign Control	Free			Free	Stop	

Intersection Summary

Area Type:	Other
Control Type:	Unsignalized
Intersection Capacity Utilization	26.0%
ICU Level of Service	A
Analysis Period (min)	15



Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↻			↻	↻	
Traffic Volume (veh/h)	175	0	11	132	0	13
Future Volume (Veh/h)	175	0	11	132	0	13
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	190	0	12	143	0	14
Pedestrians						
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None		None			
Median storage (veh)						
Upstream signal (m)						
pX, platoon unblocked						
vC, conflicting volume			190		357	190
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			190		357	190
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			99		100	98
cM capacity (veh/h)			1396		640	857
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	190	155	14			
Volume Left	0	12	0			
Volume Right	0	0	14			
cSH	1700	1396	857			
Volume to Capacity	0.11	0.01	0.02			
Queue Length 95th (m)	0.0	0.2	0.4			
Control Delay (s)	0.0	0.7	9.3			
Lane LOS			A			
Approach Delay (s)	0.0	0.7	9.3			
Approach LOS			A			
Intersection Summary						
Average Delay			0.6			
Intersection Capacity Utilization			26.0%	ICU Level of Service		A
Analysis Period (min)			15			



Appendix I

Signal Warrant Analyses





Signal Justification Calculation for Forecasted Volumes (OTM Book 12 - Justification 7)



Horizon Year: 2020 Background
 Region/City/Township: Kincardine

Major Street: Highway 21
 Minor Street: Russell Street

North/South?: Y

Number of Approach Lanes: 1
 Tee Intersection?: Y
 Flow Conditions: Free

Warrant Results		
150% Satisfied	No	Justification for new intersections with forecast traffic
120% Satisfied	No	Justification for existing intersections with forecast traffic

PM Forecast Only? N

Time Period	Major Street Highway 21						Minor Street Russell Street					
	Northbound			Southbound			Eastbound			Westbound		
	Left	Through	Right	Left	Through	Right	Left	Through	Right	Left	Through	Right
AM Peak Hour	34	299	0	0	261	46	59	0	36	0	0	0
PM Peak Hour	51	265	0	0	512	106	97	0	45	0	0	0
Average Hourly Volume	21	141	0	0	193	38	39	0	20	0	0	0

Warrant	AHV
1A - All	453
1B - Minor	59
2A - Major	394
2B - Cross	39

Warrant 1 - Minimum Vehicular Volume

1A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
All Approaches		480	720	600	900	453	
						% Fulfilled	94.3%

1B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Minor Street Approaches		180	255	180	255	59	
						% Fulfilled	32.9%

Warrant 2 - Delay To Cross Traffic

2A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Major Street Approaches		480	720	600	900	394	
						% Fulfilled	82.0%

2B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Traffic Crossing Major Street		50	75	50	75	39	
						% Fulfilled	78.0%



Signal Justification Calculation for Forecasted Volumes (OTM Book 12 - Justification 7)



Horizon Year: 2030 Background
 Region/City/Township: Kincardine

Major Street: Highway 21
 Minor Street: Russell Street

North/South?: Y

Number of Approach Lanes: 1
 Tee Intersection?: Y
 Flow Conditions: Free

PM Forecast Only? N

Warrant Results		
150% Satisfied	No	Justification for new intersections with forecast traffic
120% Satisfied	No	Justification for existing intersections with forecast traffic

Time Period	Major Street Highway 21						Minor Street Russell Street					
	Northbound			Southbound			Eastbound			Westbound		
	Left	Through	Right	Left	Through	Right	Left	Through	Right	Left	Through	Right
AM Peak Hour	40	354	0	0	308	55	70	0	43	0	0	0
PM Peak Hour	60	313	0	0	605	125	114	0	53	0	0	0
Average Hourly Volume	25	167	0	0	228	45	46	0	24	0	0	0

Warrant	AHV
1A - All	535
1B - Minor	70
2A - Major	465
2B - Cross	46

Warrant 1 - Minimum Vehicular Volume

1A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
All Approaches		480	720	600	900	535	
						% Fulfilled	111.5%

1B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Minor Street Approaches		180	255	180	255	70	
						% Fulfilled	38.9%

Warrant 2 - Delay To Cross Traffic

2A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Major Street Approaches		480	720	600	900	465	
						% Fulfilled	96.9%

2B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Traffic Crossing Major Street		50	75	50	75	46	
						% Fulfilled	92.0%



Signal Justification Calculation for Forecasted Volumes (OTM Book 12 - Justification 7)



Horizon Year: 2020 Total
 Region/City/Township: Kincardine

Major Street: Highway 21
 Minor Street: Russell Street

North/South?: Y

Number of Approach Lanes: 1
 Tee Intersection?: N
 Flow Conditions: Free

Warrant Results		
150% Satisfied	Yes	Justification for new intersections with forecast traffic
120% Satisfied	Yes	Justification for existing intersections with forecast traffic

PM Forecast Only? N

Time Period	Major Street Highway 21						Minor Street Russell Street					
	Northbound			Southbound			Eastbound			Westbound		
	Left	Through	Right	Left	Through	Right	Left	Through	Right	Left	Through	Right
AM Peak Hour	34	320	39	83	273	54	73	25	36	24	16	51
PM Peak Hour	51	227	139	248	443	125	115	49	45	182	55	242
Average Hourly Volume	21	137	45	83	179	45	47	19	20	52	18	73

Warrant	AHV
1A - All	737
1B - Minor	228
2A - Major	509
2B - Cross	117

Warrant 1 - Minimum Vehicular Volume

1A	Approach Lanes	1		2 or more		Average Hourly Volume
	Flow Conditions	Free	Restricted	Free	Restricted	
		X				
	All Approaches	480	720	600	900	737
		% Fulfilled				153.6%

1B	Approach Lanes	1		2 or more		Average Hourly Volume
	Flow Conditions	Free	Restricted	Free	Restricted	
		X				
	Minor Street Approaches	120	170	120	170	228
		% Fulfilled				190.2%

Warrant 2 - Delay To Cross Traffic

2A	Approach Lanes	1		2 or more		Average Hourly Volume
	Flow Conditions	Free	Restricted	Free	Restricted	
		X				
	Major Street Approaches	480	720	600	900	509
		% Fulfilled				106.0%

2B	Approach Lanes	1		2 or more		Average Hourly Volume
	Flow Conditions	Free	Restricted	Free	Restricted	
		X				
	Traffic Crossing Major Street	50	75	50	75	117
		% Fulfilled				234.0%



Signal Justification Calculation for Forecasted Volumes (OTM Book 12 - Justification 7)



Horizon Year: 2030 Total
 Region/City/Township: Kincardine

Major Street: Highway 21
 Minor Street: Kincardine Street

North/South?: Y

Number of Approach Lanes: 1
 Tee Intersection?: N
 Flow Conditions: Free

Warrant Results		
150% Satisfied	No	Justification for new intersections with forecast traffic
120% Satisfied	No	Justification for existing intersections with forecast traffic

PM Forecast Only? N

Time Period	Major Street Highway 21						Minor Street Kincardine Street					
	Northbound			Southbound			Eastbound			Westbound		
	Left	Through	Right	Left	Through	Right	Left	Through	Right	Left	Through	Right
AM Peak Hour	25	303	1	12	272	94	113	10	27	1	9	21
PM Peak Hour	38	338	4	26	547	179	134	7	39	4	12	12
Average Hourly Volume	16	160	1	10	205	68	62	4	17	1	5	8

Warrant	AHV
1A - All	557
1B - Minor	97
2A - Major	460
2B - Cross	68

Warrant 1 - Minimum Vehicular Volume

1A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
All Approaches		480	720	600	900	557	
						% Fulfilled	116.0%

1B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Minor Street Approaches		120	170	120	170	97	
						% Fulfilled	81.0%

Warrant 2 - Delay To Cross Traffic

2A	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Major Street Approaches		480	720	600	900	460	
						% Fulfilled	95.8%

2B	Approach Lanes	1		2 or more		Average Hourly Volume	
	Flow Conditions	Free	Restricted	Free	Restricted		
		X					
Traffic Crossing Major Street		50	75	50	75	68	
						% Fulfilled	136.5%



Appendix J

2030 Total Traffic with Improvements Operations Reports





Analysis Period	Intersection	Control Type	MOE	Direction / Movement / Approach																Overall
				Eastbound				Westbound				Northbound				Southbound				
				Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	Left	Through	Right	Approach	
AM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	D	B	B	C	C	C	A	C	B	B	B	B	A	A	A	A	B
			Delay	39	18	18	21	25	26	3	21	11	11	11	11	9	10	0	9	14
			V/C	0.24	0.57	0.57		0.21	0.14	0.08		0.23	0.34	0.34		0.03	0.20	0.02		
			Queue	15.0	25.4	25.4		16.1	17.0	3.2		27.0	56.9	56.9		4.3	33.1	0.0		
	2 - Highway 21 & Durham Street	Signal	LOS	D	D	D	D	C	C	A	B	C	C	A	B	B	B	A	B	C
			Delay	48	48	48	48	26	25	5	17	23	25	6	19	11	14	1	12	22
			V/C	0.56	0.70	0.70		0.37	0.19	0.28		0.21	0.39	0.22		0.30	0.27	0.04		
			Queue	37.8	58.8	58.8		27.8	25.9	12.6		31.5	76.2	17.0		32.7	50.4	1.3		
	4 - Highway 21 & Russell Street	Signal	LOS	D	D	D	D	C	B	B	B	B	B	A	B	A	A	A	A	B
Delay			45	45	45	45	24	11	11	15	13	15	0	14	7	9	2	8	16	
V/C			0.69	0.69	0.69		0.09	0.19	0.19		0.07	0.40	0.04		0.14	0.30	0.07			
Queue			43.6	43.6	43.6		8.6	11.5	11.5		10.7	77.8	0.0		13.1	53.0	4.0			
PM Peak Hour	1 - Highway 21 & Highway 9	Signal	LOS	C	D	D	D	C	C	A	C	D	B	B	B	B	B	A	B	C
			Delay	32	50	50	48	25	23	0	22	43	14	14	28	11	15	0	14	30
			V/C	0.20	0.95	0.95		0.35	0.11	0.02		0.87	0.40	0.40		0.05	0.47	0.04		
			Queue	19.9	126.0	126.0		17.9	17.4	0.0		114.0	57.5	57.5		6.2	75.8	0.0		
	2 - Highway 21 & Durham Street	Signal	LOS	D	E	E	D	D	C	A	C	D	D	B	D	C	C	A	C	C
			Delay	40	55	55	51	49	22	4	26	43	42	15	35	31	27	7	26	32
			V/C	0.45	0.84	0.84		0.87	0.29	0.36		0.56	0.69	0.34		0.78	0.64	0.13		
			Queue	39.5	103.0	103.0		88.2	49.0	15.6		49.9	112.5	33.3		92.2	138.7	12.9		
	4 - Highway 21 & Russell Street	Signal	LOS	D	D	D	D	C	A	A	B	C	C	A	C	B	C	A	B	C
Delay			54	54	54	54	23	7	7	13	26	27	6	21	16	21	4	17	21	
V/C			0.84	0.84	0.84		0.45	0.44	0.44		0.22	0.47	0.24		0.49	0.62	0.18			
Queue			74.9	74.9	74.9		39.3	24.8	24.8		20.0	70.6	15.2		44.4	118.4	12.7			



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2030 AM with Improvements



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	34	35	136	55	55	27	143	300	39	14	199	20
Future Volume (vph)	34	35	136	55	55	27	143	300	39	14	199	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.881				0.850		0.983				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1703	1618	0	1805	1827	1380	1703	1766	0	1504	1759	1615
Flt Permitted	0.718			0.380			0.623			0.523		
Satd. Flow (perm)	1287	1618	0	722	1827	1380	1117	1766	0	828	1759	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		148				52		10				97
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			490.2			358.0				262.4
Travel Time (s)		17.0			22.1			16.1				11.8
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	6%	9%	2%	0%	4%	17%	6%	6%	4%	20%	8%	0%
Adj. Flow (vph)	37	38	148	60	60	29	155	326	42	15	216	22
Shared Lane Traffic (%)												
Lane Group Flow (vph)	37	186	0	60	60	29	155	368	0	15	216	22
Turn Type	Perm	NA		pm+pt	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4		3	8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		3	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		4.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		8.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	29.0	29.0		10.0	39.0	39.0	51.0	51.0		51.0	51.0	51.0
Total Split (%)	32.2%	32.2%		11.1%	43.3%	43.3%	56.7%	56.7%		56.7%	56.7%	56.7%
Yellow Time (s)	5.4	5.4		3.0	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.0	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		4.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag	Lag	Lag		Lead								
Lead-Lag Optimize?	Yes	Yes		Yes								
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	11.0	11.0		23.7	20.7	20.7	55.0	55.0		55.0	55.0	55.0
Actuated g/C Ratio	0.12	0.12		0.26	0.23	0.23	0.61	0.61		0.61	0.61	0.61
v/c Ratio	0.24	0.57		0.21	0.14	0.08	0.23	0.34		0.03	0.20	0.02
Control Delay	39.0	17.5		24.5	25.7	3.3	10.5	10.6		9.3	9.6	0.1
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	39.0	17.5		24.5	25.7	3.3	10.5	10.6		9.3	9.6	0.1
LOS	D	B		C	C	A	B	B		A	A	A
Approach Delay		21.1			20.9			10.6			8.7	
Approach LOS		C			C			B			A	
Queue Length 50th (m)	6.3	6.4		8.2	8.6	0.0	12.0	30.0		1.0	16.5	0.0

Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2030 AM with Improvements



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	15.0	25.4		16.1	17.0	3.2	27.0	56.9		4.3	33.1	0.0
Internal Link Dist (m)		211.6			466.2			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	314	507		283	649	524	682	1082		505	1074	1024
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.12	0.37		0.21	0.09	0.06	0.23	0.34		0.03	0.20	0.02

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 55
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.57
 Intersection Signal Delay: 13.5 Intersection LOS: B
 Intersection Capacity Utilization 75.3% ICU Level of Service D
 Analysis Period (min) 15

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2030 AM with Improvements



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	107	147	49	114	100	150	95	259	159	172	238	38
Future Volume (vph)	107	147	49	114	100	150	95	259	159	172	238	38
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		30.0	30.0		30.0
Storage Lanes	1		0	1		1	1		1	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.963				0.850			0.850			0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1807	0	1770	1863	1509	1805	1696	1599	1626	1712	1583
Flt Permitted	0.687			0.354			0.599			0.516		
Satd. Flow (perm)	1280	1807	0	659	1863	1509	1138	1696	1599	883	1712	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		16				163			163			82
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	5%	2%	2%	7%	0%	12%	1%	11%	11%	2%
Adj. Flow (vph)	116	160	53	124	109	163	103	282	173	187	259	41
Shared Lane Traffic (%)												
Lane Group Flow (vph)	116	213	0	124	109	163	103	282	173	187	259	41
Turn Type	Perm	NA		pm+pt	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm
Protected Phases		4		3	8			2		1	6	
Permitted Phases	4			8		8	2		2	6		6
Detector Phase	4	4		3	8	8	2	2	2	1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		4.0	10.0	10.0	20.0	20.0	20.0	5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		8.0	16.5	16.5	27.3	27.3	27.3	7.0	27.3	27.3
Total Split (s)	30.0	30.0		13.0	43.0	43.0	43.0	43.0	43.0	14.0	57.0	57.0
Total Split (%)	30.0%	30.0%		13.0%	43.0%	43.0%	43.0%	43.0%	43.0%	14.0%	57.0%	57.0%
Yellow Time (s)	4.5	4.5		3.0	4.5	4.5	5.9	5.9	5.9	2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		1.0	2.0	2.0	1.4	1.4	1.4	0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		4.0	6.5	6.5	7.3	7.3	7.3	2.0	7.3	7.3
Lead/Lag	Lag	Lag		Lead			Lag	Lag	Lag	Lead		
Lead-Lag Optimize?	Yes	Yes		Yes			Yes	Yes	Yes	Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min	C-Min	None	C-Min	C-Min
Act Effct Green (s)	16.2	16.2		33.0	30.5	30.5	42.7	42.7	42.7	61.0	55.7	55.7
Actuated g/C Ratio	0.16	0.16		0.33	0.30	0.30	0.43	0.43	0.43	0.61	0.56	0.56
v/c Ratio	0.56	0.70		0.37	0.19	0.28	0.21	0.39	0.22	0.30	0.27	0.04
Control Delay	48.2	48.2		25.7	24.6	4.7	23.4	24.7	5.6	11.4	14.0	0.6
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	48.2	48.2		25.7	24.6	4.7	23.4	24.7	5.6	11.4	14.0	0.6
LOS	D	D		C	C	A	C	C	A	B	B	A
Approach Delay		48.2			16.7			18.5			11.9	
Approach LOS		D			B			B			B	
Queue Length 50th (m)	22.1	38.4		18.0	16.2	0.0	12.9	38.6	1.2	15.7	26.3	0.0

Lanes, Volumes, Timings
 2: Highway 21 & Durham Street

Kincardine Business Park TIS
 Total 2030 AM with Improvements



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	37.8	58.8		27.8	25.9	12.6	31.5	76.2	17.0	32.7	50.4	1.3
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0		30.0	30.0		30.0
Base Capacity (vph)	300	436		336	689	661	500	746	794	633	961	925
Starvation Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Reduced v/c Ratio	0.39	0.49		0.37	0.16	0.25	0.21	0.38	0.22	0.30	0.27	0.04

Intersection Summary

Area Type:	Other
Cycle Length:	100
Actuated Cycle Length:	100
Offset:	0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
Natural Cycle:	60
Control Type:	Actuated-Coordinated
Maximum v/c Ratio:	0.70
Intersection Signal Delay:	21.8
Intersection LOS:	C
Intersection Capacity Utilization	73.0%
ICU Level of Service	C
Analysis Period (min)	15

Splits and Phases: 2: Highway 21 & Durham Street

Ø1 14 s	Ø2 (R) 43 s	Ø3 13 s	Ø4 30 s
Ø6 (R) 57 s	Ø8 43 s		

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 AM with Improvements



Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕↕		↖↗	↖↗		↖↗	↕	↖↗	↖↗	↕	↖↗
Traffic Volume (vph)	84	25	43	23	15	49	40	374	37	80	320	63
Future Volume (vph)	84	25	43	23	15	49	40	374	37	80	320	63
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		0.0	15.0		30.0	0.0		45.0
Storage Lanes	0		0	1		0	1		1	1		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.962			0.885				0.850			0.850
Flt Protected		0.973		0.950			0.950			0.950		
Satd. Flow (prot)	0	1711	0	1770	1649	0	1752	1776	1583	1770	1759	1524
Flt Permitted		0.791		0.603			0.552			0.433		
Satd. Flow (perm)	0	1391	0	1123	1649	0	1018	1776	1583	807	1759	1524
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		20			53				133			85
Link Speed (k/h)		50			50			80				80
Link Distance (m)		71.8			63.0			1178.3			487.8	
Travel Time (s)		5.2			4.5			53.0			22.0	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	5%	2%	3%	2%	2%	2%	3%	7%	2%	2%	8%	6%
Adj. Flow (vph)	91	27	47	25	16	53	43	407	40	87	348	68
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	165	0	25	69	0	43	407	40	87	348	68
Turn Type	Perm	NA		pm+pt	NA		Perm	NA	Perm	pm+pt	NA	Perm
Protected Phases		4		3	8			2		1	6	
Permitted Phases	4			8			2		2	6		6
Detector Phase	4	4		3	8		2	2	2	1	6	6
Switch Phase												
Minimum Initial (s)	4.0	4.0		4.0	4.0		4.0	4.0	4.0	4.0	4.0	4.0
Minimum Split (s)	22.0	22.0		8.0	22.0		23.9	23.9	23.9	8.0	23.9	23.9
Total Split (s)	26.0	26.0		8.0	34.0		48.0	48.0	48.0	8.0	56.0	56.0
Total Split (%)	28.9%	28.9%		8.9%	37.8%		53.3%	53.3%	53.3%	8.9%	62.2%	62.2%
Yellow Time (s)	4.0	4.0		3.0	4.0		5.9	5.9	5.9	3.0	5.9	5.9
All-Red Time (s)	2.0	2.0		1.0	2.0		1.4	1.4	1.4	1.0	1.4	1.4
Lost Time Adjust (s)		0.0		0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)		6.0		4.0	6.0		7.3	7.3	7.3	4.0	7.3	7.3
Lead/Lag	Lag	Lag		Lead			Lag	Lag	Lag	Lead		
Lead-Lag Optimize?	Yes	Yes		Yes			Yes	Yes	Yes	Yes		
Recall Mode	None	None		None	None		C-Max	C-Max	C-Max	None	C-Max	C-Max
Act Effct Green (s)		14.4		19.6	17.6		51.2	51.2	51.2	62.4	59.1	59.1
Actuated g/C Ratio		0.16		0.22	0.20		0.57	0.57	0.57	0.69	0.66	0.66
v/c Ratio		0.69		0.09	0.19		0.07	0.40	0.04	0.14	0.30	0.07
Control Delay		45.4		24.2	11.1		13.1	15.0	0.1	6.9	9.1	1.8
Queue Delay		0.0		0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0
Total Delay		45.4		24.2	11.1		13.1	15.0	0.1	6.9	9.1	1.8
LOS		D		C	B		B	B	A	A	A	A
Approach Delay		45.4			14.6			13.6			7.8	
Approach LOS		D			B			B			A	
Queue Length 50th (m)		25.1		3.8	2.5		3.3	38.4	0.0	3.8	21.2	0.0

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 AM with Improvements

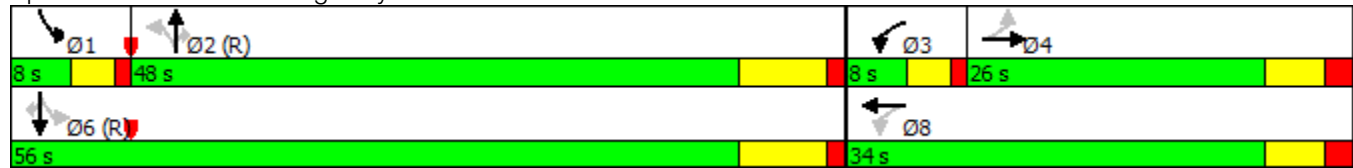


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)		43.6		8.6	11.5		10.7	77.8	0.0	13.1	53.0	4.4
Internal Link Dist (m)		47.8			39.0			1154.3			463.8	
Turn Bay Length (m)							15.0		30.0			45.0
Base Capacity (vph)		324		273	549		578	1009	957	621	1154	1029
Starvation Cap Reductn		0		0	0		0	0	0	0	0	0
Spillback Cap Reductn		0		0	0		0	0	0	0	0	0
Storage Cap Reductn		0		0	0		0	0	0	0	0	0
Reduced v/c Ratio		0.51		0.09	0.13		0.07	0.40	0.04	0.14	0.30	0.07

Intersection Summary























Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 65
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.69
 Intersection Signal Delay: 15.5 Intersection LOS: B
 Intersection Capacity Utilization 53.8% ICU Level of Service A
 Analysis Period (min) 15

Splits and Phases: 4: Highway 21 & Russell Street



Lanes, Volumes, Timings
1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
Total 2030 PM with Improvements

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	53	86	390	63	57	12	335	283	66	24	431	34
Future Volume (vph)	53	86	390	63	57	12	335	283	66	24	431	34
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	65.0		0.0	80.0		100.0	115.0		0.0	100.0		75.0
Storage Lanes	1		0	1		1	1		0	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.877				0.850		0.972				0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1666	0	1687	1863	1615	1805	1776	0	1805	1863	1615
Flt Permitted	0.717			0.168			0.413			0.489		
Satd. Flow (perm)	1336	1666	0	298	1863	1615	785	1776	0	929	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		228				52		20				97
Link Speed (k/h)		50			80			80				80
Link Distance (m)		235.6			492.9			358.0			262.4	
Travel Time (s)		17.0			22.2			16.1			11.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	2%	0%	0%	7%	2%	0%	0%	4%	4%	0%	2%	0%
Adj. Flow (vph)	58	93	424	68	62	13	364	308	72	26	468	37
Shared Lane Traffic (%)												
Lane Group Flow (vph)	58	517	0	68	62	13	364	380	0	26	468	37
Turn Type	Perm	NA		pm+pt	NA	Perm	Perm	NA		Perm	NA	Perm
Protected Phases		4		3	8			2			6	
Permitted Phases	4			8		8	2			6		6
Detector Phase	4	4		3	8	8	2	2		6	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		4.0	10.0	10.0	20.0	20.0		20.0	20.0	20.0
Minimum Split (s)	17.0	17.0		10.0	17.0	17.0	27.3	27.3		27.3	27.3	27.3
Total Split (s)	25.0	25.0		10.0	35.0	35.0	55.0	55.0		55.0	55.0	55.0
Total Split (%)	27.8%	27.8%		11.1%	38.9%	38.9%	61.1%	61.1%		61.1%	61.1%	61.1%
Yellow Time (s)	5.4	5.4		3.0	5.4	5.4	5.9	5.9		5.9	5.9	5.9
All-Red Time (s)	1.6	1.6		1.0	1.6	1.6	1.4	1.4		1.4	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.0	7.0		4.0	7.0	7.0	7.3	7.3		7.3	7.3	7.3
Lead/Lag	Lag	Lag		Lead								
Lead-Lag Optimize?	Yes	Yes		Yes								
Recall Mode	None	None		None	None	None	C-Min	C-Min		C-Min	C-Min	C-Min
Act Effct Green (s)	19.8	19.8		30.8	27.8	27.8	47.9	47.9		47.9	47.9	47.9
Actuated g/C Ratio	0.22	0.22		0.34	0.31	0.31	0.53	0.53		0.53	0.53	0.53
v/c Ratio	0.20	0.95		0.35	0.11	0.02	0.87	0.40		0.05	0.47	0.04
Control Delay	32.0	49.9		25.3	22.6	0.1	42.8	13.5		10.8	15.3	0.1
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	32.0	49.9		25.3	22.6	0.1	42.8	13.5		10.8	15.3	0.1
LOS	C	D		C	C	A	D	B		B	B	A
Approach Delay		48.1			21.8			27.8			14.0	
Approach LOS		D			C			C			B	
Queue Length 50th (m)	8.9	~57.5		8.4	8.0	0.0	54.7	36.7		2.2	50.4	0.0

Lanes, Volumes, Timings
 1: Highway 21 & Broadway Street/Highway 9

Kincardine Business Park TIS
 Total 2030 PM with Improvements

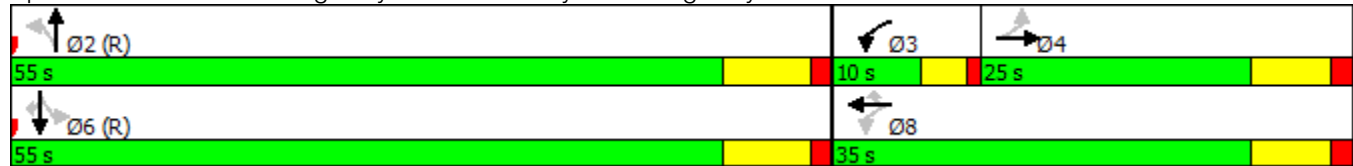


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	19.9	#126.0		17.9	17.4	0.0	#114.0	57.5		6.2	75.8	0.0
Internal Link Dist (m)		211.6			468.9			334.0			238.4	
Turn Bay Length (m)	65.0			80.0		100.0	115.0			100.0		75.0
Base Capacity (vph)	294	544		194	592	549	423	966		501	1004	915
Starvation Cap Reductn	0	0		0	0	0	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0		0	0	0
Reduced v/c Ratio	0.20	0.95		0.35	0.10	0.02	0.86	0.39		0.05	0.47	0.04

Intersection Summary
























- Area Type: Other
- Cycle Length: 90
- Actuated Cycle Length: 90
- Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
- Natural Cycle: 80
- Control Type: Actuated-Coordinated
- Maximum v/c Ratio: 0.95
- Intersection Signal Delay: 29.6
- Intersection LOS: C
- Intersection Capacity Utilization 94.6%
- ICU Level of Service F
- Analysis Period (min) 15
- ~ Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 1: Highway 21 & Broadway Street/Highway 9



Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2030 PM with Improvements

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	111	223	110	280	204	270	130	351	177	344	521	92
Future Volume (vph)	111	223	110	280	204	270	130	351	177	344	521	92
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	25.0		0.0	50.0		50.0	100.0		30.0	30.0		30.0
Storage Lanes	1		0	1		1	1		1	1		1
Taper Length (m)	30.0			30.0			30.0			30.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.950				0.850			0.850			0.850
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1805	1787	0	1787	1900	1583	1805	1827	1599	1787	1881	1583
Flt Permitted	0.620			0.198			0.443			0.302		
Satd. Flow (perm)	1178	1787	0	372	1900	1583	842	1827	1599	568	1881	1583
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		23				293			111			76
Link Speed (k/h)		50			50			80			80	
Link Distance (m)		140.2			189.4			487.8			358.0	
Travel Time (s)		10.1			13.6			22.0			16.1	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	0%	0%	3%	1%	0%	2%	0%	4%	1%	1%	1%	2%
Adj. Flow (vph)	121	242	120	304	222	293	141	382	192	374	566	100
Shared Lane Traffic (%)												
Lane Group Flow (vph)	121	362	0	304	222	293	141	382	192	374	566	100
Turn Type	Perm	NA		pm+pt	NA	Perm	Perm	NA	Perm	pm+pt	NA	Perm
Protected Phases		4		3	8			2		1	6	
Permitted Phases	4			8		8	2		2	6		6
Detector Phase	4	4		3	8	8	2	2	2	1	6	6
Switch Phase												
Minimum Initial (s)	10.0	10.0		4.0	10.0	10.0	20.0	20.0	20.0	5.0	20.0	20.0
Minimum Split (s)	16.5	16.5		8.0	16.5	16.5	27.3	27.3	27.3	7.0	27.3	27.3
Total Split (s)	36.0	36.0		17.0	53.0	53.0	38.0	38.0	38.0	17.0	55.0	55.0
Total Split (%)	33.3%	33.3%		15.7%	49.1%	49.1%	35.2%	35.2%	35.2%	15.7%	50.9%	50.9%
Yellow Time (s)	4.5	4.5		3.0	4.5	4.5	5.9	5.9	5.9	2.0	5.9	5.9
All-Red Time (s)	2.0	2.0		1.0	2.0	2.0	1.4	1.4	1.4	0.0	1.4	1.4
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)	6.5	6.5		4.0	6.5	6.5	7.3	7.3	7.3	2.0	7.3	7.3
Lead/Lag	Lag	Lag		Lead			Lag	Lag	Lag	Lead		
Lead-Lag Optimize?	Yes	Yes		Yes			Yes	Yes	Yes	Yes		
Recall Mode	None	None		None	None	None	C-Min	C-Min	C-Min	None	C-Min	C-Min
Act Effct Green (s)	24.9	24.9		45.9	43.4	43.4	32.5	32.5	32.5	56.1	50.8	50.8
Actuated g/C Ratio	0.23	0.23		0.42	0.40	0.40	0.30	0.30	0.30	0.52	0.47	0.47
v/c Ratio	0.45	0.84		0.87	0.29	0.36	0.56	0.69	0.34	0.78	0.64	0.13
Control Delay	40.1	54.8		48.9	22.4	3.6	43.1	42.2	15.4	30.6	26.6	6.5
Queue Delay	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total Delay	40.1	54.8		48.9	22.4	3.6	43.1	42.2	15.4	30.6	26.6	6.5
LOS	D	D		D	C	A	D	D	B	C	C	A
Approach Delay		51.1			25.5			35.2			26.1	
Approach LOS		D			C			D			C	
Queue Length 50th (m)	22.8	71.6		44.3	31.8	0.0	27.7	78.9	13.9	50.0	95.3	2.9

Lanes, Volumes, Timings
2: Highway 21 & Durham Street

Kincardine Business Park TIS
Total 2030 PM with Improvements

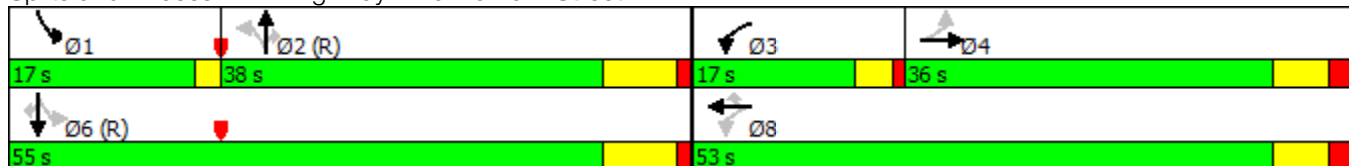


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)	39.5	103.0		#88.2	49.0	15.6	49.9	112.5	33.3	#92.2	138.7	12.9
Internal Link Dist (m)		116.2			165.4			463.8			334.0	
Turn Bay Length (m)	25.0			50.0		50.0	100.0		30.0	30.0		30.0
Base Capacity (vph)	321	504		348	818	848	257	559	566	481	885	785
Starvation Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Spillback Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Storage Cap Reductn	0	0		0	0	0	0	0	0	0	0	0
Reduced v/c Ratio	0.38	0.72		0.87	0.27	0.35	0.55	0.68	0.34	0.78	0.64	0.13

Intersection Summary






















Area Type: Other
 Cycle Length: 108
 Actuated Cycle Length: 108
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 70
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.87
 Intersection Signal Delay: 32.0 Intersection LOS: C
 Intersection Capacity Utilization 99.0% ICU Level of Service F
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 2: Highway 21 & Durham Street



Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 PM with Improvements

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	132	49	53	182	55	242	60	276	139	248	536	144
Future Volume (vph)	132	49	53	182	55	242	60	276	139	248	536	144
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0		0.0	0.0		30.0	15.0		30.0	0.0		45.0
Storage Lanes	0		0	1		0	1		1	1		1
Taper Length (m)	7.5			7.5			30.0			7.5		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.969			0.878				0.850			0.850
Flt Protected		0.973		0.950			0.950			0.950		
Satd. Flow (prot)	0	1747	0	1770	1635	0	1770	1845	1583	1770	1863	1615
Flt Permitted		0.657		0.584			0.445			0.440		
Satd. Flow (perm)	0	1179	0	1088	1635	0	829	1845	1583	820	1863	1615
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		17			263				138			133
Link Speed (k/h)		50			50			80				80
Link Distance (m)		71.8			79.2			1178.3				487.8
Travel Time (s)		5.2			5.7			53.0				22.0
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	3%	2%	2%	2%	2%	2%	2%	3%	2%	2%	2%	0%
Adj. Flow (vph)	143	53	58	198	60	263	65	300	151	270	583	157
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	254	0	198	323	0	65	300	151	270	583	157
Turn Type	Perm	NA		pm+pt	NA		Perm	NA	Perm	pm+pt	NA	Perm
Protected Phases		4		3	8			2		1	6	
Permitted Phases	4			8			2		2	6		6
Detector Phase	4	4		3	8		2	2	2	1	6	6
Switch Phase												
Minimum Initial (s)	4.0	4.0		4.0	4.0		4.0	4.0	4.0	4.0	4.0	4.0
Minimum Split (s)	22.0	22.0		8.0	22.0		23.3	23.3	23.3	8.0	23.3	23.3
Total Split (s)	32.0	32.0		9.0	41.0		35.0	35.0	35.0	14.0	49.0	49.0
Total Split (%)	35.6%	35.6%		10.0%	45.6%		38.9%	38.9%	38.9%	15.6%	54.4%	54.4%
Yellow Time (s)	4.0	4.0		3.0	4.0		5.9	5.9	5.9	3.0	5.9	5.9
All-Red Time (s)	2.0	2.0		1.0	2.0		1.4	1.4	1.4	1.0	1.4	1.4
Lost Time Adjust (s)		0.0		0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0
Total Lost Time (s)		6.0		4.0	6.0		7.3	7.3	7.3	4.0	7.3	7.3
Lead/Lag	Lag	Lag		Lead			Lag	Lag	Lag	Lead		
Lead-Lag Optimize?	Yes	Yes		Yes			Yes	Yes	Yes	Yes		
Recall Mode	None	None		None	None		C-Max	C-Max	C-Max	None	C-Max	C-Max
Act Effct Green (s)		22.1		33.1	31.1		31.4	31.4	31.4	48.9	45.6	45.6
Actuated g/C Ratio		0.25		0.37	0.35		0.35	0.35	0.35	0.54	0.51	0.51
v/c Ratio		0.84		0.45	0.44		0.22	0.47	0.24	0.49	0.62	0.18
Control Delay		54.1		23.3	6.5		25.8	27.1	6.3	15.5	20.6	4.2
Queue Delay		0.0		0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0
Total Delay		54.1		23.3	6.5		25.8	27.1	6.3	15.5	20.6	4.2
LOS		D		C	A		C	C	A	B	C	A
Approach Delay		54.1			12.9			20.9			16.7	
Approach LOS		D			B			C			B	
Queue Length 50th (m)		40.1		24.3	7.1		8.8	44.8	1.7	26.2	76.0	2.2

Lanes, Volumes, Timings
4: Highway 21 & Russell Street

Kincardine Business Park TIS
Total 2030 PM with Improvements

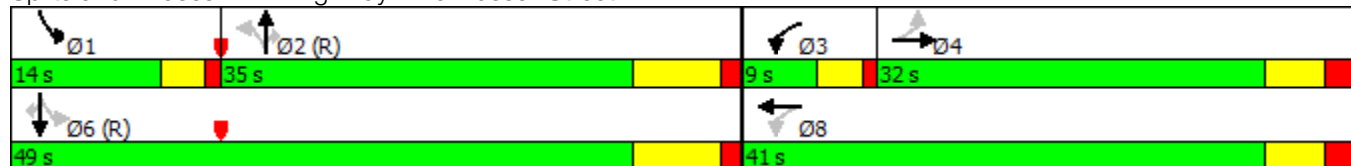


Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Queue Length 95th (m)		#74.9		39.3	24.8		20.0	70.6	15.2	44.4	118.4	12.7
Internal Link Dist (m)		47.8			55.2			1154.3			463.8	
Turn Bay Length (m)							15.0		30.0			45.0
Base Capacity (vph)		352		437	796		289	644	642	557	944	884
Starvation Cap Reductn		0		0	0		0	0	0	0	0	0
Spillback Cap Reductn		0		0	0		0	0	0	0	0	0
Storage Cap Reductn		0		0	0		0	0	0	0	0	0
Reduced v/c Ratio		0.72		0.45	0.41		0.22	0.47	0.24	0.48	0.62	0.18

Intersection Summary

Area Type: Other
 Cycle Length: 90
 Actuated Cycle Length: 90
 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green
 Natural Cycle: 65
 Control Type: Actuated-Coordinated
 Maximum v/c Ratio: 0.84
 Intersection Signal Delay: 20.9
 Intersection LOS: C
 Intersection Capacity Utilization 84.6%
 ICU Level of Service E
 Analysis Period (min) 15
 # 95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Splits and Phases: 4: Highway 21 & Russell Street



APPENDIX B

WATERCAD DISCUSSION AND PRELIMINARY DESIGN NOTES

**Municipality of Kincardine
Kincardine Business Park Water Supply
Calculations and Notes**

Job # :	08055
Date :	August 17, 2011
Revised :	May 2016

1.0 Background

There is development proposed within the lands known as the Kincardine Business Park, generally east of Highway 21 and south of Highway 9. The notes below provide a summary of analysis completed to investigate the current flows and pressures that can be provided to this area.

2.0 Hydrant Flow Tests

On June 14, 2011, hydrant flow tests were carried out by staff of BMROSS and the Municipality. Refer to the attached maps and summary sheets for location details. Results of the flow tests are provided below. During the tests, no high-lift pumps at the WTP were operational (i.e., pressure from standpipe only).

Hydrant No. K-148

Static Pressure	390 kPa
Flowing Pressure	310 kPa
Available Flow (at flowing pressure)	71 L/s
Theoretical Flow at 140 kPa	190 L/s

Hydrant No. K-144

Static Pressure	385 kPa
Flowing Pressure	300 kPa
Available Flow (at flowing pressure)	70 L/s
Theoretical Flow at 140 kPa	203 L/s

During the day of the hydrant flow tests, the following average pressure data is available for the WTP:

Average P at plant with no high-lift pumps operating	=	91 psi
		627 kPa
Average P at plant with one high-lift pump operating	=	109 psi
		752 kPa

Hydrant flow test data for the hydrant at the intersection of Russell Street and Highway 21 was obtained from a May 8, 2007 test report included in "Functional Servicing Report in Support of Zoning By-Law Amendment", prepared by Counterpoint Engineering Inc. and dated September 7, 2007.

Hydrant No. K-95

Static Pressure	415 kPa
Flowing Pressure	305 kPa
Available Flow (at flowing pressure)	71 L/s
Theoretical Flow at 140 kPa	166 L/s

3.0 **Analysis & Model Data**

3.1 **Data**

<u>Reference</u>	<u>Item</u>		
03137	WTP floor elevation @ high lift pumps	180.9 mASL	
C of A	High lift pump TDH	79 m	
	Ground elevation at hydrant K-46A	197.5 mASL	
	Ground elevation at hydrant #2	200 mASL	
	Standpipe ground elevation	207.5 mASL	
78011	Standpipe ground elevation	207.5 mASL	
Munic. staff	Standpipe LWL setpoint	37.2 m	
"	Standpipe HWL setpoint	39.2 m	
"	Standpipe LWL elevation	244.7 mASL	
"	Standpipe HWL elevation	246.7 mASL	
	Average water demand - highway service commercial	0.28 L/ha/s	
	Average water demand - large format commercial	0.28 L/ha/s	
	Average water demand - light industrial commercial	0.35 L/ha/s	
MOE Guide	Max day factor	2.00	
MOE Guide	Peak day factor	3.00	
MOE Guide	Pipe C-factor	150 mm	100
		200 - 250 mm	110
		300 - 600 mm	120

3.2 **Water Demands by Area**

See attached map for area locations.

Service Area	Hwy. Service Commercial Area (ha)	Large Format Commercial Area (ha)	Light Industrial Area (ha)	Average Day Demand (L/s)	Maximum Day Demand (L/s)	Peak Day Demand (L/s)
1	1.2	1.2	0.0	0.672	1.344	2.016
2	0.0	6.0	0.0	1.680	3.360	5.040
3	2.4	2.6	1.6	1.960	3.920	5.880
4	0.0	0.0	10.9	3.815	7.630	11.445
5	0.0	0.0	6.0	2.100	4.200	6.300
6	1.5	1.3	1.5	1.309	2.618	3.927
7	5.9	1.7	0.0	2.128	4.256	6.384
8	10.7	0.0	0.0	2.996	5.992	8.988
9	7.6	7.6	7.6	6.916	13.832	20.748
Existing	5.0	5.0	0.0	2.800	5.600	8.400

3.3 Watermain Routes

See attached map for proposed watermain routes to service development lands.

A WaterCAD model was created in order to analyze the watermain extensions to the development lands. For the purposes of the model, the following was assumed:

- Water supply from the existing eastern terminus on Russell Street and from the intersection of Durham Street and Millenium Way are treated as two independent sources. (Note: This is assumed to simplify the model and is assumed to be reasonable because of the relatively high number of connecting watermains upstream of each location.)
- The water supply at each connection location was modelled as a pump, with curve characteristics based on theoretical flow and pressure values calculated from the hydrant flow tests. See below for theoretical flow and pressure values.
- Available flow and pressure in this area is based on no pumps at the WTP operational (i.e., because this was the case during the hydrant tests).

<u>Model Pump Location</u>	<u>Q (L/s)</u>	<u>P (kPa)</u>
Pump 1 (Durham Street and Millenium Way)	0.0	385
	70.0	300
	203.0	140
Pump 2 (Russell Street and Hwy. 21)	0.0	415
	71.0	305
	166.0	140

4.0 Model Results

Ten junctions of interest were the focus of the analysis. Below is a list summarizing the junctions and their corresponding service area (refer also to the attached map).

Junction	Service Area	Avg. Day (L/s)	Max. Day (L/s)	Peak Day (L/s)
J-15	6	1.309	2.618	3.927
J-25	3	1.960	3.920	5.880
J-40	7	2.128	4.256	6.384
J-40	Existing	2.800	5.600	8.400
J-45	5	2.100	4.200	6.300
J-55	8	2.996	5.992	8.988
J-60	4	3.815	7.630	11.445
J-65	1	0.672	1.344	2.016
J-70	2	1.680	3.360	5.040
J-75	9	6.916	13.832	20.748

The average, maximum, and peak day demands listed in Section 3.0 were applied to each of the appropriate junctions. A fire flow of 150 L/s was applied to each junction at maximum day demand. Results of the analysis are summarized in the tables below. The values reported are for the condition of no high-lift pumps at the WTP operating.

Scenario A: P-65,70,75,35,40,45 at 300 mm dia., P-5,10,25 at 250 mm dia., other new w/m 200 mm dia.

Junction	P at Static (kPa)	P at Q _{AVG} (kPa)	P at Q _{MAX} (kPa)	P at Q _{PEAK} (kPa)	Available Fire Flow at 140 kPa (L/s)
J-5	417	399	381	364	
J-10	352	334	315	295	
J-15	319	300	281	260	85
J-20	304	286	266	245	
J-25	326	307	288	267	87
J-30	308	289	270	249	
J-35	384	366	348	330	
J-40	385	366	347	328	91
J-45	309	290	271	250	86
J-50	352	333	314	293	
J-55	313	294	275	254	84
J-60	315	296	277	256	86
J-65	411	393	375	357	99
J-70	391	373	355	336	95
J-75	258	238	214	186	31

Notes:

	denotes operating pressure less than 275 kPa
	denotes operating pressure above 275 kPa but less than 350 kPa
	denotes operating pressure greater than 480 kPa
	denotes fire flow of less than 150 L/s at 140 kPa minimum system pressure

**Municipality of Kincardine
Kincardine Business Park Water Supply
Preliminary Calculations and Notes**

Job # :	08055
Date :	December 4, 2013
Revised :	May 2016

1.0 Background

There is development proposed within the lands known as the Kincardine Business Park, generally east of Highway 21 and south of Highway 9. Previous work under BMROSS 08055 identified the need for booster pumping facilities to provide adequate flow & pressure within the development area. The purpose of these notes is to provide some preliminary calculations regarding booster, and potentially storage, requirements.

It is noted that at the time of any detailed design related to the watermain and booster pumping facilities, actual watermain size and pump capacity requirements will require further consideration.

2.0 Supply Characteristics at Connection to Existing System

It is anticipated that the new pressure zone would be supplied via a connection to the existing municipal system at the intersection of Durham Street and Millenium Way. Previous hydrant flow testing was conducted to confirm supply characteristics; below is a summary of design values.

Q (L/s)	P (kPa)
0	385
70	300
190	140

A second connection between the existing system and new pressure zone would be provided at the intersection of Russell Street and Highway No. 21. The connection would consist of a check valve or flow control valve, to allow the main pressure zone to supply the new zone in the event of a booster pump failure in the new zone.

3.0 Analysis & Model Data

3.1 Data

<u>Reference</u>	<u>Item</u>	
	Average water demand - highway service commercial	0.28 L/ha/s
	Average water demand - large format commercial	0.28 L/ha/s
	Average water demand - light industrial commercial	0.35 L/ha/s
MOE Guide	Max day factor	2.00
MOE Guide	Peak day factor	3.00
MOE Guide	Pipe C-factor	
	150 mm	100
	200 - 250 mm	110
	300 - 600 mm	120

3.2 Water Demands by Area

See attached map for area locations.

Service Area	Hwy. Service Commercial Area (ha)	Large Format Commercial Area (ha)	Light Industrial Area (ha)	Average Day Demand (L/s)	Maximum Day Demand (L/s)	Peak Day Demand (L/s)
1	1.2	1.2	0.0	0.672	1.344	2.016
2	0.0	6.0	0.0	1.680	3.360	5.040
3	2.4	2.6	1.6	1.960	3.920	5.880
4	0.0	0.0	10.9	3.815	7.630	11.445
5	0.0	0.0	6.0	2.100	4.200	6.300
6	1.5	1.3	1.5	1.309	2.618	3.927
7	5.9	1.7	0.0	2.128	4.256	6.384
8	10.7	0.0	0.0	2.996	5.992	8.988
9	7.6	7.6	7.6	6.916	13.832	20.748
Existing	5.0	5.0	0.0	2.800	5.600	8.400

3.3 Watermain Routes

See attached map for proposed watermain routes to service development lands.

4.0 Model Results

Below is a list summarizing the WaterCAD junctions and their corresponding service area (refer also to the attached map).

Junction	Service Area	Avg. Day (L/s)	Max. Day (L/s)	Peak Day (L/s)
J-15	6	1.309	2.618	3.927
J-20	5	1.050	2.100	3.150
J-25	3	1.960	3.920	5.880
J-30	4	1.272	2.543	3.815
J-40	7	2.128	4.256	6.384
J-40	Existing	2.800	5.600	8.400
J-45	5	1.050	2.100	3.150
J-50	4	1.272	2.543	3.815
J-55	8	2.996	5.992	8.988
J-60	4	1.272	2.543	3.815
J-65	1	0.672	1.344	2.016
J-70	2	1.680	3.360	5.040
J-75	9	6.916	13.832	20.748
Total		26.376	52.752	79.128

The average, maximum, and peak day demands listed in Section 3.0 were applied to each of the appropriate junctions. A fire flow of 150 L/s was applied to each junction at maximum day demand. Results of the analysis are summarized in the tables below.

4.1 Supply from Existing System Only

Trial A: Supply from Existing System, All new pipes at 300 mm dia.

Junction	P at Static (kPa)	P at Q _{AVG} (kPa)	P at Q _{MAX} (kPa)	P at Q _{PEAK} (kPa)	Available Fire Flow at 140 kPa (L/s)
J-15	320	289	254	217	37
J-20	305	274	239	202	37
J-25	327	296	261	223	37
J-30	309	278	243	206	37
J-40	386	355	322	289	41
J-45	310	279	244	207	37
J-50	353	322	287	250	37
J-55	314	283	249	212	37
J-60	316	285	250	212	37
J-65	412	381	346	308	37
J-70	392	361	326	289	37
J-75	259	228	193	156	33
Min	259	228	193	156	33
Max	412	381	346	308	41

Notes:

	denotes operating pressure less than 275 kPa
	denotes operating pressure above 275 kPa but less than 350 kPa
	denotes operating pressure greater than 480 kPa
	denotes fire flow of less than 150 L/s at 140 kPa minimum system pressure

As observed in the results above, a single connection to the existing system at Durham Street & Millenium Way will not provide adequate pressures at many junctions under various demands, nor will available fire flows be close to the target range. This confirms previous analysis work & the conclusion that booster pumping will be required.

4.2 Add Booster Pump

See attached map for booster pump location. Below is a summary of pump curves assumed for the analysis; assume that:

- for model simplicity, boosting is from a reservoir (i.e. from atmosphere; not boosting a pressurized supply)
- under static or average day demands, one booster pump is operational
- under maximum day or peak day demands, two booster pumps are operational
- under maximum day plus fire flow conditions, one booster plus the fire pump are operational

Booster Pump		Fire Pump	
Q (L/s)	P (kPa)	Q (L/s)	P (kPa)
0	450	0	450
50	375	150	375
100	200	225	200

Trial B: Add Booster Pump, All new pipes at 300 mm dia.

Junction	P at Static (kPa)	P at Q _{AVG} (kPa)	P at Q _{MAX} (kPa)	P at Q _{PEAK} (kPa)	Available Fire Flow at 140 kPa (L/s)
J-15	385	359	357	328	194
J-20	370	344	342	313	179
J-25	391	366	363	335	192
J-30	374	348	346	317	177
J-40	450	425	425	400	232
J-45	375	349	347	318	189
J-50	418	392	390	361	181
J-55	379	353	351	323	194
J-60	381	355	353	324	186
J-65	477	451	448	419	175
J-70	457	431	429	400	180
J-75	324	298	296	267	148
Min	324	298	296	267	148
Max	477	451	448	419	232

Notes:

	denotes operating pressure less than 275 kPa
	denotes operating pressure above 275 kPa but less than 350 kPa
	denotes operating pressure greater than 480 kPa
	denotes fire flow of less than 150 L/s at 140 kPa minimum system pressure

Based on the above results, with a suitable booster pumping configuration it will be possible to generally achieve reasonable pressures and fire flows at all junctions. At the time of detailed design of the development and booster pumping station, more analysis should be completed to determine:

- if pipe diameters can be reduced in certain areas
- actual booster & fire pump design points/curves

4.3 Storage

From the results of the hydrant flow testing mentioned in Section 2.0, it is assumed that the new pressure zone can be continually fed by the existing municipal system at a rate of at least 70 L/s. This is sufficient to meet design average and maximum day demands, and nearly sufficient to meet design peak day demands, assuming that adequate booster pumping is provided within the new pressure zone, but in terms of available supply for fire protection probably represents a "worst case" for storage considerations because it corresponds to maintaining a residual pressure of 300 kPa in the existing system, which is significantly higher than the 140 kPa minimum allowable under fire conditions. The "best case" for minimizing storage requirements corresponds to having 190 L/s available from the existing system, and also includes removing Service Area 9 from the design areas.

It is understood that at present, no specific fire storage requirements have been determined for the industrial land. From the 2008 MOE Design Guidelines for Drinking-Water Systems Table 8.1, at a design fire flow of 150 L/s, the storage requirement is based on a duration of between 2 and 3 hours. For the purposes of this analysis, assume 2.5 hours.

"Worst Case" Storage Requirements (i.e. maximum storage)

Design maximum day demand		52.752 L/s
Design fire flow		150 L/s
<hr/>		
Design total; maximum day + Fire		202.752 L/s
Deduct available supply from	-	70 L/s
<hr/>		
Total required flow from storage		132.752 L/s
Fire duration, assumed		2.5 hrs
Storage requirement		1194768 L
	=	1194.768 m ³
Say		1200 m ³

"Best Case" Storage Requirements (i.e. minimum storage)

Design maximum day demand		38.920 L/s
Design fire flow		150 L/s
<hr/>		
Design total; maximum day + Fire		188.920 L/s
Deduct available supply from	-	190 L/s
<hr/>		
Total required flow from storage		-1.080 L/s

No storage required as available supply exceeds demand + fire flow.

Therefore, under minimum storage design conditions, no storage at all would be required. The available storage in the existing municipal distribution system should be reviewed to check that the proposed industrial development would not create a deficit in the available storage.

APPENDIX C

SANITARY MODELLING SHEETS FOR THE VARIOUS DEVELOPMENT SCENARIOS

KINCARDINE BUSINESS PARK - SANITARY COLLECTION SYSTEM REVIEW

DATE June 2016
FILE No. 08055

**SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT ACCEPTED AND POTENTIAL TRIBUTARY AREA**

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 LH/s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA												REVIEW OF HGL										
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION UPPER LOWER	PIPE OBVERT ELEV. UPPER LOWER	FINISHED GROUND AT MH UPPER LOWER	DEPTH TO OBV UPPER LOWER	HGL Slope %	ELEVATION OF HGL UPPER LOWER	DEPTH TO HGL UPPER LOWER	CHANGE IN DEPTH TO SEWAGE UPPER LOWER							
AREA EAST OF HWY. 21 TO MILLENIUM WAY ADDED IN																													
<i>FD1A - Future</i>			<i>Future</i> 0.60	0.60	0.63	0.63																							
<i>FD1B - Under-Construction</i>			<i>Carwash</i> 0.60	1.20	2.00	2.63																							
<i>Temporary Marriott Hotel</i>			<i>Under Const.</i> 0.00	1.20	0.00	2.63																							
Durham	101	102	7.80	9.00	10.53	13.16	PVC	250	0.28	90.00	31.47	0.6	0.6	18.31	203.56	203.31	203.81	203.56											
Durham	102	103	0.00	9.00	0.00	13.16	PVC	250	0.28	120.00	31.47	0.6	0.6	18.31	203.31	202.97	203.56	203.22											
Durham	103	104	1.03	10.03	1.39	14.55	PVC	250	0.28	79.50	31.47	0.6	0.6	16.92	202.97	202.75	203.22	203.00											
Durham	104	105	0.00	10.03	0.00	14.55	PVC	200	1.15	50.00	35.17	1.1	1.1	20.62	202.72	202.31	202.92	202.51											
Durham	105	106	0.93	10.96	1.26	15.81	PVC	200	1.46	66.80	39.63	1.3	1.2	23.82	202.28	201.30	202.48	201.50											
Durham	106	107	0.39	11.35	0.53	16.33	PVC	200	0.66	67.10	26.65	0.9	0.9	10.32	201.27	200.83	201.47	201.03											
LIQUOR STORE AREA ADDED IN																													
<i>Retail Plaza: LCBO, etc</i>			1.50	1.50	1.58	1.58																							
<i>FD2- Condo Site</i>			1.90	3.40	2.00	3.57																							
Durham	107	108	8.00	22.75	10.80	30.70	PVC	200	0.50	87.50	23.19	0.7	0.8	-7.51	199.47	199.04	199.67	199.24	204.80	202.80	5.1	3.6	0.87	200.03	199.27	4.8	3.5	0.4	0.0
Walsh	108	109	0.89	23.64	1.20	31.90	PVC	250	0.46	71.60	40.33	0.8	0.9	8.43	199.02	198.68	199.27	198.93	202.80	204.90	3.5	6.0	0.29	199.27	198.93	3.5	6.0	0.0	0.0
Walsh	109	110	0.60	24.24	0.81	32.71	PVC	250	0.41	71.00	38.08	0.8	0.9	5.37	198.66	198.37	198.91	198.62	204.90	205.30	6.0	6.7	0.30	198.91	198.62	6.0	6.7	0.0	0.0
Walsh	110	111	0.11	24.35	0.15	32.86	PVC	250	1.19	17.40	64.87	1.3	1.3	32.01	198.37	198.16	198.62	198.41	205.30	205.20	6.7	6.8	0.30	198.62	198.41	6.7	6.8	0.0	0.0
Walsh	111	112	0.43	24.78	0.58	33.44	PVC	250	0.50	54.90	42.05	0.9	1.0	8.61	198.11	197.84	198.36	198.09	205.20	204.40	6.8	6.3	0.32	198.36	198.09	6.8	6.3	0.0	0.0
Walsh	112	113	8.69	33.47	11.73	45.18	PVC	250	0.46	26.50	40.33	0.8	0.9	-4.85	197.02	196.92	197.27	197.17	204.40	203.50	7.1	6.3	0.58	197.53	197.38	6.9	6.1	0.3	0.2
Walsh	113	114	0.19	33.66	0.26	45.43	PVC	250	0.46	53.60	40.33	0.8	0.9	-5.10	196.83	196.60	197.08	196.85	203.50	203.30	6.4	6.5	0.58	197.38	197.07	6.1	6.2	0.3	0.2
Easement	114	115	0.87	34.53	1.17	46.61	PVC	250	0.51	99.70	42.47	0.9	1.0	-4.14	196.52	196.01	196.77	196.26	203.30	200.30	6.5	4.0	0.61	197.07	196.46	6.2	3.8	0.3	0.2
Easement	115	116	0.74	35.27	1.00	47.61	PVC	250	0.46	100.60	40.33	0.8	0.9	-7.28	196.00	195.57	196.25	195.82	200.30	197.90	4.0	2.1	0.64	196.46	195.82	3.8	2.1	0.2	0.0
Mackendrick	116	117	6.44	41.71	8.69	56.30	PVC	250	0.60	83.20	46.06	0.9	1.1	-10.24	194.26	193.85	194.51	194.10	197.90	197.80	3.4	3.7	0.89	194.85	194.11	3.0	3.7	0.3	0.0
AREA COMING INTO STRUCTURE 117																													
<i>Davidson Centre</i>			<i>Existing</i> 7.50	7.50		7.50																							
<i>FD3 - Condos</i>			<i>Future</i> 2.00	9.50	2.10	9.60																							
<i>FD4 - Development</i>			<i>Under Const.</i> 2.50	12.00	2.63	12.23																							
Easement	117	118	14.50	68.21	19.58	88.10	PVC	400	0.69	60.40	172.99	1.4	1.4	84.89	193.71	193.49	194.11	193.89	197.80	197.60	3.7	3.7	0.18	194.11	193.89	3.7	3.7	0.0	0.0

SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT ACCEPTED AND POTENTIAL TRIBUTARY AREA

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/Ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA					SEWER DATA														REVIEW OF HGL									
STREET	FROM	TO	INDIVIDUAL AREA POP	CUMULATIVE AREA POP	PEAK FLOW Q(p)	CUM. FLOW Q(D)	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION		PIPE OBVERT ELEV.		FINISHED GROUND AT MH		DEPTH TO OBV		HGL Slope %	ELEVATION OF HGL		DEPTH TO HGL		CHANGE IN DEPTH TO SEWAGE			
			(ha)	(ha)	L/s	L/s									UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		
FUTURE AREAS FROM BUSINESS PARK																															
Stage 1 - KBP			<i>Future</i>	0.00	0.00	0.00	0.00																								
Stage 2 - KBP			<i>Future</i>	0.00	0.00	0.00	0.00																								
Stage 3 - KBP			<i>Future</i>	0.00	0.00	0.00	0.00																								
Scott	118	119		0.00	68.21	0.00	88.10	PVC	400	0.66	16.20	169.19	1.4	1.4	81.09	193.40	193.30	193.80	193.70	197.60	197.50	3.8	3.8	0.18	193.80	193.70	3.8	3.8	0.0	0.0	
Scott	119	120		0.25	68.46	0.34	88.44	PVC	400	0.48	47.20	144.28	1.2	1.2	55.84	193.18	192.96	193.58	193.36	197.50	197.10	3.9	3.7	0.18	193.58	193.36	3.9	3.7	0.0	0.0	
Scott	120	121		5.02	73.48	6.78	95.21	PVC	400	0.48	35.10	144.28	1.2	1.2	49.07	192.91	192.74	193.31	193.14	197.10	196.40	3.8	3.3	0.21	193.31	193.14	3.8	3.3	0.0	0.0	
Scott	121	14		0.65	74.13	0.88	96.09	PVC	400	0.51	81.70	148.73	1.2	1.2	52.64	192.49	192.08	192.89	192.48	196.40	195.70	3.5	3.2	0.21	192.89	192.48	3.5	3.2	0.0	0.0	
AREA COMING INTO STRUCTURE 113 leading to 114																															
South of Wellington St.			<i>Existing</i>	4.00	4.00	5.40	5.40																								
Area North of Russell St.			<i>Existing</i>	3.10	7.10	4.19	9.59																								
Area South of Russell St.			<i>Existing</i>	11.10	18.20	14.99	24.57																								
Scott	14	15		0.69	93.02	0.93	121.59	PVC	400	0.40	87.20	131.71	1.1	1.2	10.12	191.77	191.43	192.17	191.83	195.70	196.00	3.5	4.2	0.34	192.17	191.83	3.5	4.2	0.0	0.0	
Scott	15	16		0.53	93.55	0.72	122.31	PVC	400	0.40	85.30	131.71	1.1	1.2	9.40	191.38	191.04	191.78	191.44	196.00	196.50	4.2	5.1	0.34	191.78	191.44	4.2	5.1	0.0	0.0	
Scott	16	17		2.40	95.95	3.24	125.55	PVC	400	0.46	68.00	141.25	1.1	1.3	15.70	190.99	190.68	191.39	191.08	196.50	197.10	5.1	6.0	0.36	191.39	191.08	5.1	6.0	0.0	0.0	
Scott	17	18		0.59	96.54	0.80	126.34	PVC	400	0.58	69.80	158.60	1.3	1.4	32.26	190.67	190.26	191.07	190.66	197.10	196.40	6.0	5.7	0.37	191.07	190.66	6.0	5.7	0.0	0.0	
Scott	18	19		1.71	98.25	2.31	128.65	PVC	400	0.43	37.80	136.56	1.1	1.2	7.91	190.20	190.04	190.60	190.44	196.40	196.20	5.8	5.8	0.38	190.60	190.44	5.8	5.8	0.0	0.0	
Scott	19	20		0.63	98.88	0.85	129.50	PVC	400	0.40	77.40	131.71	1.1	1.2	2.21	190.03	189.72	190.43	190.12	196.20	195.70	5.8	5.6	0.39	190.43	190.14	5.8	5.6	0.0	0.0	
Scott	20	21		0.64	99.52	0.86	130.37	PVC	400	0.37	68.20	126.68	1.0	1.1	-3.69	189.72	189.45	190.12	189.85	195.70	196.20	5.6	6.4	0.39	190.14	189.87	5.6	6.3	0.0	0.0	
Scott	21	22		0.58	100.10	0.78	131.15	PVC	400	0.41	86.60	133.35	1.1	1.2	2.20	189.47	189.17	189.87	189.57	196.20	197.10	6.3	7.5	0.40	189.87	189.58	6.3	7.5	0.0	0.0	
Scott	22	23		7.50	107.60	10.13	141.28	PVC	450	0.39	45.11	178.05	1.1	1.3	36.77	189.13	188.95	189.58	189.40	197.10	196.50	7.5	7.1	0.25	189.58	189.40	7.5	7.1	0.0	0.0	
Park Street	23	24		0.00	107.60	0.00	141.28	PVC	450	0.40	42.00	180.32	1.1	1.3	39.04	188.80	188.68	189.25	189.13	196.50	195.40	7.3	6.3	0.25	189.25	189.13	7.3	6.3	0.0	0.0	

KINCARDINE BUSINESS PARK - SANITARY COLLECTION SYSTEM REVIEW

DATE June 2016
FILE No. 08055

**SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 1 BUSINESS PARK**

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 LH/s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA											REVIEW OF HGL													
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION UPPER	SEWER INVERT ELEVATION LOWER	PIPE OBVERT ELEV. UPPER	PIPE OBVERT ELEV. LOWER	FINISHED GROUND AT MH UPPER	FINISHED GROUND AT MH LOWER	DEPTH TO OBV UPPER	DEPTH TO OBV LOWER	HGL Slope %	ELEVATION OF HGL UPPER	ELEVATION OF HGL LOWER	DEPTH TO HGL UPPER	DEPTH TO HGL LOWER	CHANGE IN DEPTH TO SEWAGE UPPER	CHANGE IN DEPTH TO SEWAGE LOWER		
AREA EAST OF HWY. 21 TO MILLENIUM WAY ADDED IN																															
			Future	0.60	0.60	0.63	0.63																								
FD1A - Future			Future	0.60	0.60	0.63	0.63																								
FD1B - Under-Construction			Carwash	0.60	1.20	2.00	2.63																								
Temporary Marriott Hotel			Under Const.	0.00	1.20	0.00	2.63																								
Durham	101	102		7.80	9.00	10.53	13.16	PVC	250	0.28	90.00	31.47	0.6	0.6	18.31	203.56	203.31	203.81	203.56												
Durham	102	103		0.00	9.00	0.00	13.16	PVC	250	0.28	120.00	31.47	0.6	0.6	18.31	203.31	202.97	203.56	203.22												
Durham	103	104		1.03	10.03	1.39	14.55	PVC	250	0.28	79.50	31.47	0.6	0.6	16.92	202.97	202.75	203.22	203.00												
Durham	104	105		0.00	10.03	0.00	14.55	PVC	200	1.15	50.00	35.17	1.1	1.1	20.62	202.72	202.31	202.92	202.51												
Durham	105	106		0.93	10.96	1.26	15.81	PVC	200	1.46	66.80	39.63	1.3	1.2	23.82	202.28	201.30	202.48	201.50												
Durham	106	107		0.39	11.35	0.53	16.33	PVC	200	0.66	67.10	26.65	0.9	0.9	10.32	201.27	200.83	201.47	201.03												
LIQUOR STORE AREA ADDED IN																															
			Retail Plaza: LCBO, etc	1.50	1.50	1.58	1.58																								
			FD2- Condo Site	1.90	3.40	2.00	3.57																								
Durham	107	108		8.00	22.75	10.80	30.70	PVC	200	0.50	87.50	23.19	0.7	0.8	-7.51	199.47	199.04	199.67	199.24	204.80	202.80	5.1	3.6	0.87	200.03	199.27	4.8	3.5	0.4	0.0	
Walsh	108	109		0.89	23.64	1.20	31.90	PVC	250	0.46	71.60	40.33	0.8	0.9	8.43	199.02	198.68	199.27	198.93	202.80	204.90	3.5	6.0	0.29	199.27	198.93	3.5	6.0	0.0	0.0	
Walsh	109	110		0.60	24.24	0.81	32.71	PVC	250	0.41	71.00	38.08	0.8	0.9	5.37	198.66	198.37	198.91	198.62	204.90	205.30	6.0	6.7	0.30	198.91	198.62	6.0	6.7	0.0	0.0	
Walsh	110	111		0.11	24.35	0.15	32.86	PVC	250	1.19	17.40	64.87	1.3	1.3	32.01	198.37	198.16	198.62	198.41	205.30	205.20	6.7	6.8	0.30	198.62	198.41	6.7	6.8	0.0	0.0	
Walsh	111	112		0.43	24.78	0.58	33.44	PVC	250	0.50	54.90	42.05	0.9	1.0	8.61	198.11	197.84	198.36	198.09	205.20	204.40	6.8	6.3	0.32	198.36	198.09	6.8	6.3	0.0	0.0	
Walsh	112	113		8.69	33.47	11.73	45.18	PVC	250	0.46	26.50	40.33	0.8	0.9	-4.85	197.02	196.92	197.27	197.17	204.40	203.50	7.1	6.3	0.58	197.53	197.38	6.9	6.1	0.3	0.2	
Walsh	113	114		0.19	33.66	0.26	45.43	PVC	250	0.46	53.60	40.33	0.8	0.9	-5.10	196.83	196.60	197.08	196.85	203.50	203.30	6.4	6.5	0.58	197.38	197.07	6.1	6.2	0.3	0.2	
Easement	114	115		0.87	34.53	1.17	46.61	PVC	250	0.51	99.70	42.47	0.9	1.0	-4.14	196.52	196.01	196.77	196.26	203.30	200.30	6.5	4.0	0.61	197.07	196.46	6.2	3.8	0.3	0.2	
Easement	115	116		0.74	35.27	1.00	47.61	PVC	250	0.46	100.60	40.33	0.8	0.9	-7.28	196.00	195.57	196.25	195.82	200.30	197.90	4.0	2.1	0.64	196.46	195.82	3.8	2.1	0.2	0.0	
Mackendrick	116	117		6.44	41.71	8.69	56.30	PVC	250	0.60	83.20	46.06	0.9	1.1	-10.24	194.26	193.85	194.51	194.10	197.90	197.80	3.4	3.7	0.89	194.85	194.11	3.0	3.7	0.3	0.0	
AREA COMING INTO STRUCTURE 117																															
			Existing	7.50	7.50	7.50	7.50																								
Davidson Centre			Future	2.00	9.50	2.10	9.60																								
FD3 - Condos			Under Const.	2.50	12.00	2.63	12.23																								
FD4 - Development																															
Easement	117	118		14.50	68.21	19.58	88.10	PVC	400	0.69	60.40	172.99	1.4	1.4	84.89	193.71	193.49	194.11	193.89	197.80	197.60	3.7	3.7	0.18	194.11	193.89	3.7	3.7	0.0	0.0	

**SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 1 BUSINESS PARK**

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/Ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA															REVIEW OF HGL									
STREET	FROM	TO	INDIVIDUAL AREA POP	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION		PIPE OBVERT ELEV.		FINISHED GROUND AT MH		DEPTH TO OBV		HGL Slope %	ELEVATION OF HGL		DEPTH TO HGL		CHANGE IN DEPTH TO SEWAGE			
				(ha)											UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		
FUTURE AREAS FROM BUSINESS PARK																															
Stage 1B - KBP			Future	33.60	33.60	26.00																									
Stage 2 - KBP			Future	0.00	33.60	0.00																									
Stage 3 - KBP			Future	0.00	33.60	0.00																									
Scott	118	119		0.00	101.81	0.00	114.10	PVC	400	0.66	16.20	169.19	1.4	1.4	55.09	193.40	193.30	193.80	193.70	197.60	197.50	3.8	3.8	0.30	193.80	193.70	3.8	3.8	0.0	0.0	
Scott	119	120		0.25	102.06	0.34	114.44	PVC	400	0.48	47.20	144.28	1.2	1.3	29.84	193.18	192.96	193.58	193.36	197.50	197.10	3.9	3.7	0.30	193.58	193.36	3.9	3.7	0.0	0.0	
Scott	120	121		5.02	107.08	6.78	121.21	PVC	400	0.48	35.10	144.28	1.2	1.3	23.07	192.91	192.74	193.31	193.14	197.10	196.40	3.8	3.3	0.34	193.31	193.14	3.8	3.3	0.0	0.0	
Scott	121	14		0.65	107.73	0.88	122.09	PVC	400	0.51	81.70	148.73	1.2	1.3	26.64	192.49	192.08	192.89	192.48	196.40	195.70	3.5	3.2	0.34	192.89	192.48	3.5	3.2	0.0	0.0	
AREA COMING INTO STRUCTURE 113 leading to 114																															
South of Wellington St.			Existing	4.00	4.00	5.40																									
Area North of Russell St.			Existing	3.10	7.10	4.19	9.59																								
Area South of Russell St.			Existing	11.10	18.20	14.99	24.57																								
Scott	14	15		0.69	126.62	0.93	147.59	PVC	400	0.40	87.20	131.71	1.1	1.2	-15.88	191.77	191.43	192.17	191.83	195.70	196.00	3.5	4.2	0.50	192.31	191.87	3.4	4.1	0.1	0.0	
Scott	15	16		0.53	127.15	0.72	148.31	PVC	400	0.40	85.30	131.71	1.1	1.2	-16.60	191.38	191.04	191.78	191.44	196.00	196.50	4.2	5.1	0.51	191.87	191.44	4.1	5.1	0.1	0.0	
Scott	16	17		2.40	129.55	3.24	151.55	PVC	400	0.46	68.00	141.25	1.1	1.3	-10.30	190.99	190.68	191.39	191.08	196.50	197.10	5.1	6.0	0.53	191.44	191.08	5.1	6.0	0.0	0.0	
Scott	17	18		0.59	130.14	0.80	152.34	PVC	400	0.58	69.80	158.60	1.3	1.4	6.26	190.67	190.26	191.07	190.66	197.10	196.40	6.0	5.7	0.53	191.07	191.09	6.0	5.3	0.0	0.4	
Scott	18	19		1.71	131.85	2.31	154.65	PVC	400	0.43	37.80	136.56	1.1	1.2	-18.09	190.20	190.04	190.60	190.44	196.40	196.20	5.8	5.8	0.55	191.09	190.88	5.3	5.3	0.5	0.4	
Scott	19	20		0.63	132.48	0.85	155.50	PVC	400	0.40	77.40	131.71	1.1	1.2	-23.79	190.03	189.72	190.43	190.12	196.20	195.70	5.8	5.6	0.56	190.88	190.45	5.3	5.2	0.5	0.3	
Scott	20	21		0.64	133.12	0.86	156.37	PVC	400	0.37	68.20	126.68	1.0	1.1	-29.69	189.72	189.45	190.12	189.85	195.70	196.20	5.6	6.4	0.56	190.45	190.07	5.2	6.1	0.3	0.2	
Scott	21	22		0.58	133.70	0.78	157.15	PVC	400	0.41	86.60	133.35	1.1	1.2	-23.80	189.47	189.17	189.87	189.57	196.20	197.10	6.3	7.5	0.57	190.07	189.58	6.1	7.5	0.2	0.0	
Scott	22	23		7.50	141.20	10.13	167.28	PVC	450	0.39	45.11	178.05	1.1	1.3	10.77	189.13	188.95	189.58	189.40	197.10	196.50	7.5	7.1	0.34	189.58	189.40	7.5	7.1	0.0	0.0	
Park Street	23	24		0.00	141.20	0.00	167.28	PVC	450	0.40	42.00	180.32	1.1	1.3	13.04	188.80	188.68	189.25	189.13	196.50	195.40	7.3	6.3	0.34	189.25	189.13	7.3	6.3	0.0	0.0	

KINCARDINE BUSINESS PARK - SANITARY COLLECTION SYSTEM REVIEW

DATE June 2016
FILE No. 08055

**SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 2 BUSINESS PARK**

Flow Rate = 1.35L/ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/Ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA												REVIEW OF HGL													
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION UPPER	SEWER INVERT ELEVATION LOWER	PIPE OBVERT ELEV. UPPER	PIPE OBVERT ELEV. LOWER	FINISHED GROUND AT MH UPPER	FINISHED GROUND AT MH LOWER	DEPTH TO OBV UPPER	DEPTH TO OBV LOWER	HGL Slope %	ELEVATION OF HGL UPPER	ELEVATION OF HGL LOWER	DEPTH TO HGL UPPER	DEPTH TO HGL LOWER	CHANGE IN DEPTH TO SEWAGE UPPER	CHANGE IN DEPTH TO SEWAGE LOWER			
AREA EAST OF HWY. 21 TO MILLENIUM WAY ADDED IN																																
FD1A - Future			<i>Future</i>	0.60	0.60	0.63	0.63																									
FD1B - Under-Construction			<i>Carwash</i>	0.60	1.20	2.00	2.63																									
Temporary Marriott Hotel			<i>Under Const.</i>	0.00	1.20	0.00	2.63																									
Durham	101	102		7.80	9.00	10.53	13.16	PVC	250	0.28	90.00	31.47	0.6	0.6	18.31	203.56	203.31	203.81	203.56													
Durham	102	103		0.00	9.00	0.00	13.16	PVC	250	0.28	120.00	31.47	0.6	0.6	18.31	203.31	202.97	203.56	203.22													
Durham	103	104		1.03	10.03	1.39	14.55	PVC	250	0.28	79.50	31.47	0.6	0.6	16.92	202.97	202.75	203.22	203.00													
Durham	104	105		0.00	10.03	0.00	14.55	PVC	200	1.15	50.00	35.17	1.1	1.1	20.62	202.72	202.31	202.92	202.51													
Durham	105	106		0.93	10.96	1.26	15.81	PVC	200	1.46	66.80	39.63	1.3	1.2	23.82	202.28	201.30	202.48	201.50													
Durham	106	107		0.39	11.35	0.53	16.33	PVC	200	0.66	67.10	26.65	0.9	0.9	10.32	201.27	200.83	201.47	201.03													
LIQUOR STORE AREA ADDED IN																																
Retail Plaza: LCBO, etc				1.50	1.50	1.58	1.58																									
FD2- Condo Site				1.90	3.40	2.00	3.57																									
Durham	107	108		8.00	22.75	10.80	30.70	PVC	200	0.50	87.50	23.19	0.7	0.8	-7.51	199.47	199.04	199.67	199.24	204.80	202.80	5.1	3.6	0.87	200.03	199.27	4.8	3.5	0.4	0.0		
Walsh	108	109		0.89	23.64	1.20	31.90	PVC	250	0.46	71.60	40.33	0.8	0.9	8.43	199.02	198.68	199.27	198.93	202.80	204.90	3.5	6.0	0.29	199.27	198.93	3.5	6.0	0.0	0.0		
Walsh	109	110		0.60	24.24	0.81	32.71	PVC	250	0.41	71.00	38.08	0.8	0.9	5.37	198.66	198.37	198.91	198.62	204.90	205.30	6.0	6.7	0.30	198.91	198.62	6.0	6.7	0.0	0.0		
Walsh	110	111		0.11	24.35	0.15	32.86	PVC	250	1.19	17.40	64.87	1.3	1.3	32.01	198.37	198.16	198.62	198.41	205.30	205.20	6.7	6.8	0.30	198.62	198.41	6.7	6.8	0.0	0.0		
Walsh	111	112		0.43	24.78	0.58	33.44	PVC	250	0.50	54.90	42.05	0.9	1.0	8.61	198.11	197.84	198.36	198.09	205.20	204.40	6.8	6.3	0.32	198.36	198.09	6.8	6.3	0.0	0.0		
Walsh	112	113		8.69	33.47	11.73	45.18	PVC	250	0.46	26.50	40.33	0.8	0.9	-4.85	197.02	196.92	197.27	197.17	204.40	203.50	7.1	6.3	0.58	197.53	197.38	6.9	6.1	0.3	0.2		
Walsh	113	114		0.19	33.66	0.26	45.43	PVC	250	0.46	53.60	40.33	0.8	0.9	-5.10	196.83	196.60	197.08	196.85	203.50	203.30	6.4	6.5	0.58	197.38	197.07	6.1	6.2	0.3	0.2		
Easement	114	115		0.87	34.53	1.17	46.61	PVC	250	0.51	99.70	42.47	0.9	1.0	-4.14	196.52	196.01	196.77	196.26	203.30	200.30	6.5	4.0	0.61	197.07	196.46	6.2	3.8	0.3	0.2		
Easement	115	116		0.74	35.27	1.00	47.61	PVC	250	0.46	100.60	40.33	0.8	0.9	-7.28	196.00	195.57	196.25	195.82	200.30	197.90	4.0	2.1	0.64	196.46	195.82	3.8	2.1	0.2	0.0		
Mackendrick	116	117		6.44	41.71	8.69	56.30	PVC	250	0.60	83.20	46.06	0.9	1.1	-10.24	194.26	193.85	194.51	194.10	197.90	197.80	3.4	3.7	0.89	194.85	194.11	3.0	3.7	0.3	0.0		
AREA COMING INTO STRUCTURE 117																																
Davidson Centre			<i>Existing</i>	7.50	7.50	7.50	7.50																									
FD3 - Condos			<i>Future</i>	2.00	9.50	2.10	9.60																									
FD4 - Development			<i>Under Const.</i>	2.50	12.00	2.63	12.23																									
Easement	117	118		14.50	68.21	19.58	88.10	PVC	400	0.69	60.40	172.99	1.4	1.4	84.89	193.71	193.49	194.11	193.89	197.80	197.60	3.7	3.7	0.18	194.11	193.89	3.7	3.7	0.0	0.0		

**SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 2 BUSINESS PARK**

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/Ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA																REVIEW OF HGL								
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION		PIPE OBVERT ELEV.		FINISHED GROUND AT MH		DEPTH TO OBV		HGL Slope %	ELEVATION OF HGL		DEPTH TO HGL		CHANGE IN DEPTH TO SEWAGE			
															UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER
FUTURE AREAS FROM BUSINESS PARK																															
Stage 1B - KBP			Future	33.60	33.60	26.00	26.00																								
Stage 2 - KBP			Future	32.70	66.30	31.00	57.00																								
Stage 3 - KBP			Future	0.00	66.30	0.00	57.00																								
Scott	118	119	0.00	134.51	0.00	145.10	PVC	400	0.66	16.20	169.19	1.4	1.5	24.09	193.40	193.30	193.80	193.70	197.60	197.50	3.8	3.8	0.48	193.80	194.99	3.8	2.5	0.0	1.3		
Scott	119	120	0.25	134.76	0.34	145.44	PVC	400	0.48	47.20	144.28	1.2	1.3	-1.16	193.18	192.96	193.58	193.36	197.50	197.10	3.9	3.7	0.49	194.99	194.76	2.5	2.3	1.4	1.4		
Scott	120	121	5.02	139.78	6.78	152.21	PVC	400	0.48	35.10	144.28	1.2	1.3	-7.93	192.91	192.74	193.31	193.14	197.10	196.40	3.8	3.3	0.53	194.76	194.57	2.3	1.8	1.4	1.4		
Scott	121	14	0.65	140.43	0.88	153.09	PVC	400	0.51	81.70	148.73	1.2	1.3	-4.36	192.49	192.08	192.89	192.48	196.40	195.70	3.5	3.2	0.54	194.57	194.13	1.8	1.6	1.7	1.6		
AREA COMING INTO STRUCTURE 113 leading to 114																															
South of Wellington St.			Existing	4.00	4.00	5.40	5.40																								
Area North of Russell St.			Existing	3.10	7.10	4.19	9.59																								
Area South of Russell St.			Existing	11.10	18.20	14.99	24.57																								
Scott	14	15	0.69	159.32	0.93	178.59	PVC	400	0.40	87.20	131.71	1.1	1.2	-46.88	191.77	191.43	192.17	191.83	195.70	196.00	3.5	4.2	0.73	194.13	193.49	1.6	2.5	2.0	1.7		
Scott	15	16	0.53	159.85	0.72	179.31	PVC	400	0.40	85.30	131.71	1.1	1.2	-47.60	191.38	191.04	191.78	191.44	196.00	196.50	4.2	5.1	0.74	193.49	192.86	2.5	3.6	1.7	1.4		
Scott	16	17	2.40	162.25	3.24	182.55	PVC	400	0.46	68.00	141.25	1.1	1.3	-41.30	190.99	190.68	191.39	191.08	196.50	197.10	5.1	6.0	0.77	192.86	192.34	3.6	4.8	1.5	1.3		
Scott	17	18	0.59	162.84	0.80	183.34	PVC	400	0.58	69.80	158.60	1.3	1.4	-24.74	190.67	190.26	191.07	190.66	197.10	196.40	6.0	5.7	0.77	192.34	191.80	4.8	4.6	1.3	1.1		
Scott	18	19	1.71	164.55	2.31	185.65	PVC	400	0.43	37.80	136.56	1.1	1.2	-49.09	190.20	190.04	190.60	190.44	196.40	196.20	5.8	5.8	0.79	191.80	191.50	4.6	4.7	1.2	1.1		
Scott	19	20	0.63	165.18	0.85	186.50	PVC	400	0.40	77.40	131.71	1.1	1.2	-54.79	190.03	189.72	190.43	190.12	196.20	195.70	5.8	5.6	0.80	191.50	190.88	4.7	4.8	1.1	0.8		
Scott	20	21	0.64	165.82	0.86	187.37	PVC	400	0.37	68.20	126.68	1.0	1.1	-60.69	189.72	189.45	190.12	189.85	195.70	196.20	5.6	6.4	0.81	190.88	190.33	4.8	5.9	0.8	0.5		
Scott	21	22	0.58	166.40	0.78	188.15	PVC	400	0.41	86.60	133.35	1.1	1.2	-54.80	189.47	189.17	189.87	189.57	196.20	197.10	6.3	7.5	0.81	190.33	189.62	5.9	7.5	0.5	0.0		
Scott	22	23	7.50	173.90	10.13	198.28	PVC	450	0.39	45.11	178.05	1.1	1.3	-20.23	189.13	188.95	189.58	189.40	197.10	196.50	7.5	7.1	0.48	189.62	189.40	7.5	7.1	0.0	0.0		
Park Street	23	24	0.00	173.90	0.00	198.28	PVC	450	0.40	42.00	180.32	1.1	1.3	-17.96	188.80	188.68	189.25	189.13	196.50	195.40	7.3	6.3	0.48	189.33	189.13	7.2	6.3	0.1	0.0		

KINCARDINE BUSINESS PARK - SANITARY COLLECTION SYSTEM REVIEW

SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 3 (Area North of Hwy. 9)

Flow Rate = 1.35L/ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA				SEWER DATA											REVIEW OF HGL												
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION		PIPE OBVERT ELEV.		FINISHED GROUND AT MH		DEPTH TO OBV		HGL Slope %	ELEVATION OF HGL		DEPTH TO HGL		CHANGE IN DEPTH TO SEWAGE		
															UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	
AREA EAST OF HWY. 21 TO MILLENIUM WAY ADDED IN																														
<i>FD1A - Future</i>			<i>Future</i>	0.60	0.60	0.63	0.63																							
<i>FD1B - Under-Construction</i>			<i>Carwash</i>	0.60	1.20	2.00	2.63																							
<i>Temporary Marriott Hotel</i>			<i>Under Const.</i>	0.00	1.20	0.00	2.63																							
Durham	101	102		7.80	9.00	10.53	13.16	PVC	250	0.28	90.00	31.47	0.6	0.6	18.31	203.56	203.31	203.81	203.56											
Durham	102	103		0.00	9.00	0.00	13.16	PVC	250	0.28	120.00	31.47	0.6	0.6	18.31	203.31	202.97	203.56	203.22											
Durham	103	104		1.03	10.03	1.39	14.55	PVC	250	0.28	79.50	31.47	0.6	0.6	16.92	202.97	202.75	203.22	203.00											
Durham	104	105		0.00	10.03	0.00	14.55	PVC	200	1.15	50.00	35.17	1.1	1.1	20.62	202.72	202.31	202.92	202.51											
Durham	105	106		0.93	10.96	1.26	15.81	PVC	200	1.46	66.80	39.63	1.3	1.2	23.82	202.28	201.30	202.48	201.50											
Durham	106	107		0.39	11.35	0.53	16.33	PVC	200	0.66	67.10	26.65	0.9	0.9	10.32	201.27	200.83	201.47	201.03											
LIQUOR STORE AREA ADDED IN																														
<i>Retail Plaza: LCBO, etc</i>				1.50	1.50	1.58	1.58																							
<i>FD2- Condo Site</i>				1.90	3.40	2.00	3.57																							
Durham	107	108		8.00	22.75	10.80	30.70	PVC	200	0.50	87.50	23.19	0.7	0.8	-7.51	199.47	199.04	199.67	199.24	204.80	202.80	5.1	3.6	0.87	200.03	199.27	4.8	3.5	0.4	0.0
Walsh	108	109		0.89	23.64	1.20	31.90	PVC	250	0.46	71.60	40.33	0.8	0.9	8.43	199.02	198.68	199.27	198.93	202.80	204.90	3.5	6.0	0.29	199.27	198.93	3.5	6.0	0.0	0.0
Walsh	109	110		0.60	24.24	0.81	32.71	PVC	250	0.41	71.00	38.08	0.8	0.9	5.37	198.66	198.37	198.91	198.62	204.90	205.30	6.0	6.7	0.30	198.91	198.62	6.0	6.7	0.0	0.0
Walsh	110	111		0.11	24.35	0.15	32.86	PVC	250	1.19	17.40	64.87	1.3	1.3	32.01	198.37	198.16	198.62	198.41	205.30	205.20	6.7	6.8	0.30	198.62	198.41	6.7	6.8	0.0	0.0
Walsh	111	112		0.43	24.78	0.58	33.44	PVC	250	0.50	54.90	42.05	0.9	1.0	8.61	198.11	197.84	198.36	198.09	205.20	204.40	6.8	6.3	0.32	198.36	198.09	6.8	6.3	0.0	0.0
Walsh	112	113		8.69	33.47	11.73	45.18	PVC	250	0.46	26.50	40.33	0.8	0.9	-4.85	197.02	196.92	197.27	197.17	204.40	203.50	7.1	6.3	0.58	197.53	197.38	6.9	6.1	0.3	0.2
Walsh	113	114		0.19	33.66	0.26	45.43	PVC	250	0.46	53.60	40.33	0.8	0.9	-5.10	196.83	196.60	197.08	196.85	203.50	203.30	6.4	6.5	0.58	197.38	197.07	6.1	6.2	0.3	0.2
Easement	114	115		0.87	34.53	1.17	46.61	PVC	250	0.51	99.70	42.47	0.9	1.0	-4.14	196.52	196.01	196.77	196.26	203.30	200.30	6.5	4.0	0.61	197.07	196.46	6.2	3.8	0.3	0.2
Easement	115	116		0.74	35.27	1.00	47.61	PVC	250	0.46	100.60	40.33	0.8	0.9	-7.28	196.00	195.57	196.25	195.82	200.30	197.90	4.0	2.1	0.64	196.46	195.82	3.8	2.1	0.2	0.0
Mackendrick	116	117		6.44	41.71	8.69	56.30	PVC	250	0.60	83.20	46.06	0.9	1.1	-10.24	194.26	193.85	194.51	194.10	197.90	197.80	3.4	3.7	0.89	194.85	194.11	3.0	3.7	0.3	0.0
AREA COMING INTO STRUCTURE 117																														
<i>Davidson Centre</i>			<i>Existing</i>	7.50	7.50		7.50																							
<i>FD3 - Condos</i>			<i>Future</i>	2.00	9.50	2.10	9.60																							
<i>FD4 - Development</i>			<i>Under Const.</i>	2.50	12.00	2.63	12.23																							
Easement	117	118		14.50	68.21	19.58	88.10	PVC	400	0.69	60.40	172.99	1.4	1.4	84.89	193.71	193.49	194.11	193.89	197.80	197.60	3.7	3.7	0.18	194.11	193.89	3.7	3.7	0.0	0.0

SEWER CAPACITY REVIEW AND HYDRAULIC GRADE LINE EVALUATION
CURRENT TRIBUTARY AREA + STAGE 3 (Area North of Hwy. 9)

Flow Rate = 1.35L/Ha.s (Including Infiltration), refer to sewage flow evaluation.

Peak Flow Per Hectare 1.35 L/Ha.s

DRAINAGE AREA			SANITARY DRAINAGE AREA DATA					SEWER DATA													REVIEW OF HGL									
STREET	FROM	TO	INDIVIDUAL AREA POP (ha)	CUMULATIVE AREA POP (ha)	PEAK FLOW Q(p) L/s	CUM. FLOW Q(D) L/s	TYPE OF PIPE	DIA. (mm)	SLOPE (%)	LENGTH (m)	CAPACITY (L/s) n=0.013	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY Q(d)	REMAINING CAPACITY	SEWER INVERT ELEVATION		PIPE OBVERT ELEV.		FINISHED GROUND AT MH		DEPTH TO OBV		HGL Slope %	ELEVATION OF HGL		DEPTH TO HGL		CHANGE IN DEPTH TO SEWAGE		
															UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER		UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	
FUTURE AREAS FROM BUSINESS PARK																														
Stage 1 - KBP			Future	33.60	33.60	26.00																								
Stage 2 - KBP			Future	32.70	66.30	31.00																								
Stage 3 - KBP			Future	22.90	89.20	20.00																								
Scott	118	119		0.00	157.41	0.00	165.10	PVC	400	0.66	16.20	169.19	1.4	1.5	4.09	193.40	193.30	193.80	193.70	197.60	197.50	3.8	3.8	0.63	193.80	201.48	3.8	-4.0	0.0	7.8
Scott	119	120		0.25	157.66	0.34	165.44	PVC	400	0.48	47.20	144.28	1.2	1.3	-21.16	193.18	192.96	193.58	193.36	197.50	197.10	3.9	3.7	0.63	201.48	201.18	-4.0	-4.1	7.9	7.8
Scott	120	121		5.02	162.68	6.78	172.21	PVC	400	0.48	35.10	144.28	1.2	1.3	-27.93	192.91	192.74	193.31	193.14	197.10	196.40	3.8	3.3	0.68	201.18	200.94	-4.1	-4.5	7.9	7.8
Scott	121	14		0.65	163.33	0.88	173.09	PVC	400	0.51	81.70	148.73	1.2	1.3	-24.36	192.49	192.08	192.89	192.48	196.40	195.70	3.5	3.2	0.69	200.94	200.38	-4.5	-4.7	8.1	7.9
AREA COMING INTO STRUCTURE 113 leading to 114																														
South of Wellington St.			Existing	4.00	4.00	5.40																								
Area North of Russell St.			Existing	3.10	7.10	4.19	9.59																							
Area South of Russell St.			Existing	11.10	18.20	14.99	24.57																							
Scott	14	15		0.69	182.22	0.93	198.59	PVC	400	0.40	87.20	131.71	1.1	1.2	-66.88	191.77	191.43	192.17	191.83	195.70	196.00	3.5	4.2	0.91	200.38	199.59	-4.7	-3.6	8.2	7.8
Scott	15	16		0.53	182.75	0.72	199.31	PVC	400	0.40	85.30	131.71	1.1	1.2	-67.60	191.38	191.04	191.78	191.44	196.00	196.50	4.2	5.1	0.91	199.59	198.81	-3.6	-2.3	7.8	7.4
Scott	16	17		2.40	185.15	3.24	202.55	PVC	400	0.46	68.00	141.25	1.1	1.3	-61.30	190.99	190.68	191.39	191.08	196.50	197.10	5.1	6.0	0.94	198.81	198.17	-2.3	-1.1	7.4	7.1
Scott	17	18		0.59	185.74	0.80	203.34	PVC	400	0.58	69.80	158.60	1.3	1.4	-44.74	190.67	190.26	191.07	190.66	197.10	196.40	6.0	5.7	0.95	198.17	197.50	-1.1	-1.1	7.1	6.8
Scott	18	19		1.71	187.45	2.31	205.65	PVC	400	0.43	37.80	136.56	1.1	1.2	-69.09	190.20	190.04	190.60	190.44	196.40	196.20	5.8	5.8	0.97	197.50	197.13	-1.1	-0.9	6.9	6.7
Scott	19	20		0.63	188.08	0.85	206.50	PVC	400	0.40	77.40	131.71	1.1	1.2	-74.79	190.03	189.72	190.43	190.12	196.20	195.70	5.8	5.6	0.98	197.13	196.38	-0.9	-0.7	6.7	6.3
Scott	20	21		0.64	188.72	0.86	207.37	PVC	400	0.37	68.20	126.68	1.0	1.1	-80.69	189.72	189.45	190.12	189.85	195.70	196.20	5.6	6.4	0.99	196.38	195.70	-0.7	0.5	6.3	5.9
Scott	21	22		0.58	189.30	0.78	208.15	PVC	400	0.41	86.60	133.35	1.1	1.2	-74.80	189.47	189.17	189.87	189.57	196.20	197.10	6.3	7.5	1.00	195.70	194.84	0.5	2.3	5.8	5.3
Scott	22	23		7.50	196.80	10.13	218.28	PVC	450	0.39	45.11	178.05	1.1	1.3	-40.23	189.13	188.95	189.58	189.40	197.10	196.50	7.5	7.1	0.59	194.84	194.57	2.3	1.9	5.3	5.2
Park Street	23	24		0.00	196.80	0.00	218.28	PVC	250	0.40	42.00	37.61	0.8	0.9	-180.67	188.80	188.68	189.05	188.93	196.50	195.40	7.5	6.5	13.44	194.57	188.93	1.9	6.5	5.5	0.0

APPENDIX D

**PARK STREET SPS
CAPACITY AND UPGRADE REVIEW**

**Municipality of Kincardine
Review of Options to Increase Capacity
Park St. Sewage Pumping Station**

Job # :	08055
Date :	Sept. 2011
Revised :	June 2016

1.0 Introduction

The existing sanitary sewer collection system for the Park Street tributary area was constructed in the 1970's to service residential growth in Kincardine. At that time, the service area was not expected to extend east of Highway 21. The sewage pumping station was originally designed by BMROSS and constructed in 1976. The station was sized based on population values provided at the time by the upstream land developer.

The current service area includes residential development, the Davidson Centre, Commercial development along the westerly side of Hwy. 21, Two Schools, One Church, Business Park on east side of Hwy. 21 including Canadian Tire, Sobey's, Tim Horton's, Boston Pizza, a hotel, and a Bank.

2.0 Existing Sewage Pumping Station

Original Design Information:

Drainage Area:	90 Ha.	
Residential Population:	3100 p.	
Per Capita Fow:	455 L/cap/day	(100 lpgd)
P.F.	3.43 (Harmons)	
Peak Res. Sewage:	56.0 L/s	
Infiltration:	10.0 L/s	(Based on pipe length)
Community Centre:	26.5 L/s	
Future School:	5.7 L/s	
Commercial:	0.9 L/s	
Total:	99.1 L/s	(1976 Design Flow)
Req. pump capacity:	66.1 L/s	(Based on 2/3 Calculated Flow)

The station is a drypit/wetwell configuration with 3 pumps in total (2 pumps in parallel providing the required capacity). The station pumps directly to the headworks of the Kincardine sewage treatment plant via. approximately 1,200 metres of 300mm dia. forcemain. A portion of the existing forcemain was installed under the Penetangore River.

Genset:	Detroit Diesel	100 HP 75 kW
Existing Pumps:	Fairbanks Morse Series 5443-32, vertical dry-pit non-clog, 4" suction	
	786.0 Uspgm	49.6 L/s
	81.0 feet	24.7 m
	30.0 HP	22.4 kW

Draw-down testing to determine current pump capacities was completed in April of 2008 with the following results:

Pump	Flow L/s	
1	60	Station Capacity:
2	59	
3	55	
1,2	85	Existing Firm Capacity: 82 L/s (2 Pumps)
2,3	82	Noted CofA Capacity: 99 L/s
1,3	82	

2.0 Historic Sewage Flows

Historic Sewage Flow Data Summary

Year	Pumped Volume m ³	Average Day m ³ /day	Recorded Max. Day m ³ /day
2011 Study Values			
2005	293752	805	3569
2006	350577	960	3177
2007	299313	820	4536
2008	392465	1075	6454
2009	326686	895	5053
2016 Study Update			
2012	322,163	880	2294
2013	345,870	949	9012
2014	344,601	943	3121
2015	293,944	806	2234
Values	328500	900	9000

Based on the above information, a maximum day flow event was observed in 2008 (January thaw/rain event) with a value of 6454 m³/day (75 L/s). As reported by Kincardine operators it was necessary to run 3 pumps during this event to avoid a bypass. Operation staff have noted that similar events have occurred (January 2013) where 3 pumps have not been able to keep up with the peak flow and a "bypass" results. During these "bypass" events, the recorded data does not accurately represent the max. daily flow because the wetwell transducer (during the submerged period) does not accurately record the wetwell volume during the bypass period.

For purposes of being conservative it is suggested that the peak extraneous flow experienced in 2013 be used for peak system flows.

Based on the foregoing, and given the information available related to flows, we can summarize the past data as follows:

Current Service Area:	100 Ha	
Max. Extraneous Flow	9000 m ³ /day	(Based on 2013)
	104.2 L/s	

As noted above, it is very difficult to ascertain the actual peak flow to this facility. We do know, however, through discussions with staff, that the peak flow at times exceeds the capacity of three pumps operating in parallel. Based on the draw-down testing completed in April 2008 it is estimated that 3 pumps in parallel will operate at a rate of about 97 L/s which is somewhat below the estimated peak sewage flow to the station (106 L/s). For estimating purpose it is suggested that the peak flow estimate include a 10% +/- contingency.

Contingency Allowance	10 %
Resulting Flow Allowance	10.4 L/s

Total Est. Peak Sewage 115.0 L/s

3.0 Proposed Development

Kincardine is considering the development of a business park located on over 70 Hectares of property on the east side of Hwy. 21. Some of the proposed development is planned immediately adjacent to the existing commercial developments (i.e., Canadian Tire, Sobeys, Tim Hortons, Holiday Inn Express) while the majority is being proposed to the east of Millenium Way and will require full servicing of the currently vacant property. In addition to the proposed development east of Hwy. 21, there are a few areas of residential development (on the west side of Hwy. 21) which are may possibly be serviced in the future and as such will start contributing flow to the Park St. SPS.

For the purpose of staging infrastructure, the proposed development area has been divided into phases. These phases are for calculation purposes only and are subject to modifications as part of the Master Plan process:

Stage 1 - Remainder of Committed Areas + First Half of Business Park Development Areas

Stage 1A - Flows into Durham St collection system

i. New Development (West of Hwy. 21)	
- Residential - R	6.4 (FD2, FD3, FD4)
- Highway Service Commercial - HSC	1.2
- Large Format Commercial - LFC	0.0
- Light Industrial - LI	0.0

Stage 1B - Flows into Russell St collection system

ii. New Development (East of Hwy. 21 to Millenium Way)	
- Residential - R	0.0
- Highway Service Commercial - HSC	5.2 (Incl. N.E corner of Hwy 9/21)
- Large Format Commercial - LFC	4.3
- Light Industrial - LI	0.0
iii. New Development (East of Hwy. 21 - Business Park)	
- Residential - R	2.2
- Highway Service Commercial - HSC	9.9
- Large Format Commercial - LFC	12.0
- Light Industrial - LI	0.0

Stage 1A - Summary of Areas

- Residential - R	6.4 Ha
- Highway Service Commercial - HSC	1.2 Ha
- Large Format Commercial - LFC	0.0 Ha
- Light Industrial - LI	0.0 Ha
	7.6 Ha

Stage 1B - Summary of Areas

- Residential - R	2.2 Ha
- Highway Service Commercial - HSC	15.1 Ha
- Large Format Commercial - LFC	16.3 Ha
- Light Industrial - LI	0.0 Ha
	33.6 Ha

Stage 1 - Total New Development 41.2 Ha

Stage 2 - Second Half of Business Park Development Areas

i. New Development (East of Hwy. 21 - Business Park)	
- Residential - R	0.0
- Highway Service Commercial - HSC	9.7
- Large Format Commercial - LFC	2.2
- Light Industrial - LI	20.8

Stage 2 - Total New Development 32.7 Ha

Stage 3 - Future Lands North of Hwy 9 - Currently outside the Official Plan area

i New Development (East of Hwy. 21 - North of County Road 9)	
- Residential - R	0.0
- Highway Service Commercial - HSC	7.6 (Not in OP Area)
- Large Format Commercial - LFC	7.6 (Not in OP Area)
- Light Industrial - LI	7.6 (Not in OP Area)

Stage 3 - Total New Development 22.9 Ha

Summary of Development Stages and Associated Land Area

Stage	Development Type (Ha)				Summary
	R	HSC	LFC	LI	
1A	6.4	1.2	0.0	0.0	7.6
1B	2.2	15.1	16.3	0.0	33.6
2	0.0	9.7	2.2	20.8	32.7
3	0.0	7.6	7.6	7.6	22.9
Total	8.6	33.6	26.1	28.4	96.8

4.0 Sewage Flow From New Development Areas

Design Criteria for New Development Areas (Based on MOE Guidelines)

Note: Residential Population Density = 35 ppHa
Residential Sewage Flow = 450 L/cap/day

Land Use	Average Sewage Flow	Peaking Factor	Infiltration Allowance
R	0.18 L/Ha/s	Harmon	0.2 L/Ha/s
HSC	0.28 L/Ha/s	2.0	0.2 L/Ha/s
LFC	0.28 L/Ha/s	2.0	0.2 L/Ha/s
LI	0.35 L/Ha/s	2.5	0.2 L/Ha/s

Stage 1A

Land Use	Area Ha	Population	Peaking Factor	Average Sewage L/s	Peak Sewage L/s	Infiltration Allowance L/s	Total Sewage L/s
R	6.4	224	4.1	1.2	4.7	1.3	6.0
HSC	1.2	N/A	2.0	0.3	0.7	0.2	0.9
LFC	0.0	N/A	2.0	0.0	0.0	0.0	0.0
LI	0.0	N/A	2.5	0.0	0.0	0.0	0.0
Total Avg Sewage Flow						3.0 L/s	
Total Peak Sewage Flow						6.9 L/s	

Stage 1B

Land Use	Area Ha	Population	Peaking Factor	Average Sewage L/s	Peak Sewage L/s	Infiltration Allowance L/s	Total Sewage L/s
R	2.2	77	4.3	0.4	1.7	0.4	2.1
HSC	15.1	N/A	2.0	4.2	8.5	3.0	11.5
LFC	16.3	N/A	2.0	4.6	9.1	3.3	12.4
LI	0.0	N/A	2.5	0.0	0.0	0.0	0.0
Total Avg Sewage Flow						15.9 L/s	
Total Peak Sewage Flow						26.0 L/s	

Stage 2

Land Use	Area Ha	Population	Peaking Factor	Average Sewage L/s	Peak Sewage L/s	Infiltration Allowance L/s	Total Sewage L/s
R	0.0	0	4.5	0.0	0.0	0.0	0.0
HSC	9.7	N/A	2.0	2.7	5.4	1.9	7.4
LFC	2.2	N/A	2.0	0.6	1.2	0.4	1.7
LI	20.8	N/A	2.5	7.3	18.2	4.2	22.4
Total Avg Sewage Flow						17.2 L/s	
Total Peak Sewage Flow						31.4 L/s	

Stage 3 - Currently outside the Official Plan

Land Use	Area Ha	Population	Peaking Factor	Average Sewage L/s	Peak Sewage L/s	Infiltration Allowance L/s	Total Sewage L/s
R	0.0	0	4.5	0.0	0.0	0.0	0.0
HSC	7.6	N/A	2.0	2.1	4.3	1.5	5.8
LFC	7.6	N/A	2.0	2.1	4.3	1.5	5.8
LI	7.6	N/A	2.5	2.7	6.7	1.5	8.2
Total Avg Sewage Flow						11.5 L/s	
Total Peak Sewage Flow						19.8 L/s	

Peak Sewage Flow Summary

	Total Additional Flow to Park St. SPS		Flow Directed to the Russell St. Sanitary	
	Incr. L/s	Cum. L/s	Incr. L/s	Cum. L/s
Stage 1A	7.0	7.0	0.0	0.0
Stage 1B	26.0	33.0	26.0	26.0
Stage 2	31.0	64.0	31.0	57.0
Stage 3	20.0	84.0	20.0	77.0

5.0 Park Street SPS and Peak Sewage Flow

The anticipated cumulative peak sewage flow to the Park Street Station is estimated as follows:

Existing	115.0	L/s
Stage 1A	122.0	L/s
Stage 1B	148.0	L/s
Stage 2	179.0	L/s
Stage 3	199.0	L/s

Note: Stage 3 has been included in the above to review feasibility only.

6.0 Existing Pumping Station Capacity

Check Existing Forcemain and Process Pipe Capacity

From MOE design guidelines, permissible velocities in piping are as noted below:

Station piping	0.8 to 4.0 m/s
Forcemain	0.8 to 2.5 m/s

Existing Forcemain Characteristics:

Forcemain diameter:	300 mm.
Design C factor:	120
Top waterlevel in discharge chamber at STP	201.47 m.
Low waterlevel in SPS wetwell	187.15 m.
Static Head	14.3 m.

Calculate system Curve

Pipe diameter:	250 mm.	(Process Piping)
Pipe length:	3 m.	

250mm Dia. Fitting	Quantity	k" value	Total "k"
90 deg flared elbow	1	0.05	0.05
Gate valve	2	0.06	0.12
250 x 100 reducer	1	0.38	0.38
100 x 250 increaser	1	0.71	0.71
Check Valve	1	2.00	2.00
Branch Tee	1	0.54	0.54
Total "k"			3.80

Pipe ID diameter:	296 mm.	(Forcemain)
Pipe length (scaling from site plan shows 4000'):	1219 m.	

Fitting	Quantity	k" value	Total "k"
90 deg bend	4	0.24	0.96
Gate valve	1	0.05	0.05
Tee (branch)	1	0.51	0.51
Tee (run)	1	0.09	0.09
Exit loss	1	1.00	1.00
Total "k"			2.61

Discharge (L/s)	Velocity in 250mm dia. piping (m/s)	Velocity in 300mm dia. piping (m/s)	Losses in 250mm dia. fittings (m)	Losses in 250mm dia. pipe (m)	Losses in 300mm dia. fittings (m)	Losses in 300mm dia. pipe (m)	Static Head (m)	TDH (m)
0	0.00	0.00	0.00	0.00	0.00	0.00	14.3	14.3
10	0.20	0.15	0.01	0.00	0.00	0.14	14.3	14.5
20	0.41	0.29	0.03	0.00	0.01	0.50	14.3	14.9
30	0.61	0.44	0.07	0.01	0.03	1.05	14.3	15.5
40	0.81	0.58	0.13	0.01	0.04	1.79	14.3	16.3
50	1.02	0.73	0.20	0.02	0.07	2.71	14.3	17.3
60	1.22	0.87	0.29	0.02	0.10	3.80	14.3	18.5
70	1.43	1.02	0.39	0.03	0.14	5.05	14.3	19.9
80	1.63	1.16	0.51	0.04	0.18	6.47	14.3	21.5
90	1.83	1.31	0.65	0.05	0.23	8.04	14.3	23.3
100	2.04	1.45	0.80	0.05	0.28	9.77	14.3	25.2
110	2.24	1.60	0.97	0.07	0.34	11.66	14.3	27.4
120	2.44	1.74	1.16	0.08	0.40	13.69	14.3	29.7
130	2.65	1.89	1.36	0.09	0.47	15.88	14.3	32.1
140	2.85	2.03	1.58	0.10	0.55	18.21	14.3	34.8
150	3.06	2.18	1.81	0.12	0.63	20.69	14.3	37.6
160	3.26	2.33	2.06	0.13	0.72	23.32	14.3	40.5
170	3.46	2.47	2.32	0.15	0.81	26.08	14.3	43.7
180	3.67	2.62	2.60	0.16	0.91	28.99	14.3	47.0
190	3.87	2.76	2.90	0.18	1.01	32.04	14.3	50.5
200	4.07	2.91	3.22	0.20	1.12	35.23	14.3	54.1
210	4.28	3.05	3.54	0.22	1.24	38.56	14.3	57.9
220	4.48	3.20	3.89	0.24	1.36	42.03	14.3	61.8

Maximum Capacity with Existing Forcemain

For velocities to remain close to the range recommended in the MOE Guidelines, the maximum discharge through the existing piping should be kept below around 175 L/s. This flow will result in forcemain velocities at the high end of the range provided by the MOE (i.e., 2.54 m/s).

Consider that the maximum sized pumps to be connected to the existing forcemain should not have a combined pumping rate of greater than 175 L/s @ 45.3 m TDH.

Existing Wetwell Volume

Wetwell length	6.20 m	75056B - Sht4
Wetwell width	2.44 m	75056B - Sht4
Plan area of wetwell	15.13 m ²	
Pump stop elevation	187.45 m	75056B - Sht3
Pump start elevation	188.52 m	75056B - Sht3
Operating range	1.07 m	
Operating volume	16.19 m ³	
Suggested Maximum Pump Capacity	180 L/s	
Resulting inflow resulting in minimum pump cycle time	90 L/s	
Time to fill or empty	180 seconds	
	= 3.00 minutes	
This will result in:	10.01 cycles/hour	

This is greater than the recommended 4-6 cycles/hour and will probably require a VFD on the new pumps to allow them to match their pump rate to inflow and avoid excessive cycling.

To compare:	4 cycles/hour would limit the max. possible pump flow to	72	L/s
	6 cycles/hour would limit the max. possible pump flow to	108	L/s

7.0 Upgrade Options

There are three basic ways to increase the pumping capacity of the William St sewage pumping station:

- Replace existing pumps with larger capacity units capable of forcing more flow through the existing forcemain.
- Twin the existing forcemain to allow the existing pumps to operate at a greater capacity.
- Twin the existing forcemain and replace the existing pumps with larger capacity units.

The options are examined in greater detail below.

7.1 Option 1: Install Larger Pumps to Provide Capacity for Stage 1, Retain Existing Forcemain

- At the completion of Stage 1 Development, calculations indicate that peak sewage flow should be in the range of 155 L/s. To meet this flow with two pumps running (firm capacity), all three pumps would need to be sized for a pumping rate of about 115 L/s to provide at 29m TDH. TDH at a flow of 155 L/s will be around 39 m.
- Pumps of the required capacity from either Hydromatic (SD4T; 56 kW/75 Hp) or Flygt (NT3301HT; 63 kW/85 Hp) are available and they should fit through the openings of the drywell.
- It is not known if the existing electrical service will be adequate to power the upgraded pumps, and will have to be investigated as part of detailed design. For cost estimating purposes it is assumed that some upgrades will be required to the power supply system.
- The existing standby power system will not be adequate for the larger pumps, and will need to be replaced / upgraded with a larger unit.
- VFD control of the larger pumps will be required to avoid excessive cycling.

Costs:

Item	Total Cost
Three new pumps with a capacity of 115 L/s @ 29 m TDH	\$160,000
Install new pumps, including 2 weeks of wetwell bypass pumping	\$110,000
Modifications to discharge piping, valving, and inlet pipe	\$60,000
New 300 kW diesel generator set	\$120,000
Three new VFDs	\$110,000
Power system upgrades	\$30,000
Control system upgrades	\$55,000
Sub Total	\$645,000
30% Engineering and Contingencies	\$193,500
Total Probable Cost	\$838,500

7.2 Option 2: Install Larger Pumps to Max. Forcemain Capacity, Retain Existing Forcemain

- To keep flow velocities in the existing station piping and forcemain within the range recommended in the MOE design guidelines, the pump capacity should be limited to approximately 175 L/s. However, the pumping rate could be increased to meet the theoretical sewage flow requirement (at the end of Stage 2) to about 190 L/s. This would result in forcemain velocities in the range of about 2.8 m/s which is not significantly beyond the maximum velocity suggested by the MOE. Under normal operating conditions the pumping rate could be controlled through a VFD (which is advisable given the existing wetwell and new pump size) to maintain forcemain velocities within the MOE suggested maximum rate. All three pumps would need to be replaced with two units in operation having at least the required capacity. Each pump would need to be sized for about 145 L/s @ 36 m TDH. Two pumps running in parallel would result in a flow rate of about 190 L/s @ 49 m TDH.
- Pumps of the required capacity from Flygt (C3300HT; 78 kW/105 Hp) are available and they should fit through the openings of the drywell.
- It is not known if the existing electrical service will be adequate to power the upgraded pumps, and will have to be investigated as part of detailed design. For cost estimating purposes it is assumed that some upgrades will be required to the power supply system.
- The existing standby power system will not be adequate for the larger pumps, and will need to be replaced / upgraded with a larger unit.
- As noted, VFD control of the larger pumps will be required to avoid excessive cycling and to maintain forcemain velocities to within the range suggested by the MOE in their guidelines.

Costs:

Item	Total Cost
Three new pumps with a capacity of 145 L/s @ 36 m TDH	\$190,000
Install new pumps, including 2 weeks of wetwell bypass pumping	\$110,000
Modifications to discharge piping, valving, and inlet pipe	\$60,000
New 350 kW diesel generator set	\$130,000
Three new VFDs	\$160,000
Power system upgrades	\$30,000
Control system upgrades	\$55,000
Sub Total	\$735,000
30% Engineering and Contingencies	\$220,500
Total Probable Cost	\$955,500

7.3 Option 3: Retain Existing Pumps and Twin the Forcemain

- This option involves installing a second 300mm diameter forcemain from the existing pumping station to the existing inlet structure at the lagoons. A second forcemain will allow two of the three pumps to pump through it's own forcemain. This should allow each of the pumps to deliver it's full single-pump capacity when operating in parallel. This would then give a station capacity of around 115 L/s. It is noted that twinning the forcemain alone does not provide sufficient capacity to accomodate the future business park development.
- Operation in this manner would mean that there would be no electrical or standby power upgrade requirements under this option.
- Modifications will be required to the existing bypass valve chamber and the lagoon inlet chamber to accommodate the second forcemain.

Costs:

Item	Total Cost
300 mm dia. forcemain (directionally drilled)	\$500,000
Modify lagoon chamber for second inlet	\$70,000
Modify bypass chamber and piping for second forcemain	\$170,000
Sub Total	\$740,000
30% Engineering and Contingencies	\$222,000
Total Probable Cost	\$962,000

7.4 Option 4: Twin Existing 300 mm Diameter Forcemain; Replace Existing Pumps (Maximum Capacity)

- This is a combination of the previous options which will maximize station capacity by replacing the existing pumps with three new pumps, each having a capacity of 115 L/s, and twinning the existing forcemain. This will give a firm station capacity of 230 L/s, with one pump acting as standby.
- It is assumed that a new electrical service will be required to the pumping station, along with a new standby power unit and control system. All three pumps will be equipped with VFDs due to wetwell volume limitations.

Costs:

Item	Total Cost
Three new pumps with a capacity of 145 L/s @ 36 m TDH	\$190,000
Install new pumps, including 2 weeks of wetwell bypass pumping	\$110,000
Modifications to discharge piping, valving, and inlet pipe	\$60,000
New 350 kW diesel generator set	\$130,000
Three new VFDs	\$160,000
Power system upgrades	\$30,000
Control system upgrades	\$55,000
300 mm dia. forcemain (directionally drilled)	\$500,000
Modify lagoon chamber for second inlet	\$70,000
Modify bypass chamber and piping for second forcemain	\$170,000
Sub Total	\$1,475,000
30% Engineering and Contingencies	\$442,500
Total Probable Cost	\$1,917,500

8.0 Discussion

Three basic options were considered to increase the capacity of the existing Park St. sewage pumping station. These were:

- Install larger pumps in the existing wetwell and use existing forcemain
- Retain existing pumps and twin the existing forcemain
- Install larger pumps and twin the existing forcemain to maximize station capacity

These will be discussed in greater detail, below.

As noted above, current firm station capacity is about 82 L/s (two pumps in operation)

8.1 **Install Larger Pumps in the Existing Wetwell and Use Existing Forcemain (Option 1,2)**

Revised station capacity:	155 L/s to 190 L/s
Probable option cost:	\$840,000 to \$955,000

Discussion:

- This option provides about a 90% increase to a 130% increase in the existing station capacity.
- A considerable increase in discharge pressure is required to move the greater flows through the existing forcemain. This means greater power costs for operation and increased risk of forcemain failure.
- Capacity can be doubled again through twinning of forcemain and electrical/control modifications (see Option 4).

8.2 **Retain Existing Pumps and Twin the Existing Forcemain (Options 3)**

Revised station capacity:	115 L/s
Probable option cost:	\$962,000

- This option provides a 40% increase in the existing station capacity.
- Construction of this option can be staged, depending on the degree of security/redundancy required for the pumping capacity.
- Twin forcemains will allow swabbing of the forcemains while maintaining station in operation and increases pumping station security by providing forcemain redundancy. This is important since it has been demonstrated that regular forcemain maintenance is required for this installation to maintain design pumping capacity.
- Lower friction losses in twin forcemains will result in lower energy consumption under two-pump operation when compared to pumping the same flow through a single forcemain.
- Capacity can be increased by a further 100 L/s through pump replacement (see Option 4).

8.3 **Install Larger Pumps and Twin Existing Forcemain to Maximize Station Capacity (Option 4)**

Revised station capacity:	230 L/s
Probable option cost:	\$1,917,500

- This option provides a 180% increase in the existing station capacity.

APPENDIX E

MIDUSS INPUT PARAMETERS

MIDUSS - Input Parameters

KINCARDINE BUSINESS PARK
Municipality of Kincardine
08055

No.	Impervious				Catchment				Catch Area	Flow Length	Overland Slope	% Impervious	Impervious Area	Pervious Area	Channel Length
	n	CN	la/S	in.ab	n	CN	la/S	in.ab							
PRE-DEVELOPMENT MIDUSS MODEL PARAMETERS															
50	0.013	98	0.1	0.518	0.22	81	0.1	5.96	396.0	450	2.5	0.0	0.0	396.0	3000
52	0.013	98	0.1	0.518	0.25	80	0.1	6.35	196.0	250	7.0	0.0	0.0	196.0	1300
54	0.013	98	0.1	0.518	0.28	79	0.1	6.75	39.0	140	11.0	0.0	0.0	39.0	800
56	0.013	98	0.1	0.518	0.21	82	0.1	5.58	345.0	240	3.0	0.0	0.0	345.0	1300
58	0.013	98	0.1	0.518	0.23	81	0.1	5.96	82.0	140	15.0	0.0	0.0	82.0	700
59	0.013	98	0.1	0.518	0.35	76	0.1	8.02	128.0	170	18.0	0.0	0.0	128.0	1500
60	0.013	98	0.1	0.518	0.23	81	0.1	5.96	225.0	270	2.5	0.0	0.0	225.0	1800
62	0.013	98	0.1	0.518	0.25	80	0.1	6.35	95.0	160	2.5	0.0	0.0	95.0	1800
64	0.013	98	0.1	0.518	0.21	82	0.1	5.58	80.0	220	5.5	0.0	0.0	80.0	700
100	0.013	98	0.1	0.518	0.23	81	0.1	5.96	45.0	100	7.0	0.0	0.0	45.0	1500
101	0.013	98	0.1	0.518	0.28	80	0.1	6.35	11.2	50	7.0	0.0	0.0	11.2	700
201	0.013	98	0.1	0.518	0.20	82	0.1	5.58	166.0	250	3.0	0.0	0.0	166.0	1900
202	0.013	98	0.1	0.518	0.20	82	0.1	5.58	8.0	225	4.0	0.0	0.0	8.0	260
203	0.013	98	0.1	0.518	0.20	82	0.1	5.58	13.6	150	3.5	0.0	0.0	13.6	350
204	0.013	98	0.1	0.518	0.20	82	0.1	5.58	6.8	120	2.0	0.0	0.0	6.8	150
301	0.013	98	0.1	0.518	0.20	82	0.1	5.58	16.4	95	2.5	0.0	0.0	16.4	480
302	0.013	98	0.1	0.518	0.20	82	0.1	5.58	5.0	110	3.5	0.0	0.0	5.0	280
303	0.013	98	0.1	0.518	0.20	82	0.1	5.58	11.6	135	4.5	0.0	0.0	11.6	430
304	0.013	98	0.1	0.518	0.20	82	0.1	5.58	6.3	150	2.5	0.0	0.0	6.3	130
401	0.013	98	0.1	0.518	0.20	82	0.1	5.58	5.6	240	3.5	0.0	0.0	5.6	225
402	0.013	98	0.1	0.518	0.20	82	0.1	5.58	4.2	80	4.0	0.0	0.0	4.2	280
403	0.013	98	0.1	0.518	0.20	82	0.1	5.58	6.4	75	4.0	0.0	0.0	6.4	410
404	0.013	98	0.1	0.518	0.20	82	0.1	5.58	2.7	60	2.5	0.0	0.0	2.7	160
501	0.013	98	0.1	0.518	0.20	82	0.1	5.58	2.5	80	3.5	0.0	0.0	2.5	120
502	0.013	98	0.1	0.518	0.20	82	0.1	5.58	0.5	120	3.5	0.0	0.0	0.5	170
503	0.013	98	0.1	0.518	0.20	82	0.1	5.58	8.2	90	5.0	0.0	0.0	8.2	350
504	0.013	98	0.1	0.518	0.20	82	0.1	5.58	3.9	90	2.5	0.0	0.0	3.9	140
603	0.013	98	0.1	0.518	0.20	82	0.1	5.58	5.6	100	2.5	0.0	0.0	5.6	260
605	0.013	98	0.1	0.518	0.20	82	0.1	5.58	3.4	100	2.5	0.0	0.0	3.4	170
TOTAL									1918.9				0.0	1918.9	

No.	Impervious				Catchment				Catch Area	Flow Length	Overland Slope	% Impervious	Impervious Area	Pervious Area	Channel Length
	n	CN	la/S	in.ab	n	CN	la/S	in.ab							
POST-DEVELOPMENT MIDUSS MODEL PARAMETERS															
50	0.013	98	0.1	0.518	0.22	81	0.1	5.96	396.0	450	2.5	0.0	0.0	396.0	3000
52	0.013	98	0.1	0.518	0.25	80	0.1	6.35	196.0	250	7.0	0.0	0.0	196.0	1300
54	0.013	98	0.1	0.518	0.28	79	0.1	6.75	39.0	140	11.0	0.0	0.0	39.0	800
56	0.013	98	0.1	0.518	0.21	82	0.1	5.58	345.0	240	3.0	0.0	0.0	345.0	1300
58	0.013	98	0.1	0.518	0.23	81	0.1	5.96	82.0	140	15.0	0.0	0.0	82.0	700
59	0.013	98	0.1	0.518	0.35	76	0.1	8.02	128.0	170	18.0	0.0	0.0	128.0	1500
60	0.013	98	0.1	0.518	0.23	81	0.1	5.96	225.0	270	2.5	0.0	0.0	225.0	1800
62	0.013	98	0.1	0.518	0.25	80	0.1	6.35	95.0	160	2.5	0.0	0.0	95.0	1800
64	0.013	98	0.1	0.518	0.21	82	0.1	5.58	80.0	220	5.5	0.0	0.0	80.0	700
100	0.013	98	0.1	0.518	0.23	81	0.1	5.96	45.0	100	7.0	0.0	0.0	45.0	1500
101	0.013	98	0.1	0.518	0.28	80	0.1	6.35	11.2	50	7.0	0.0	0.0	11.2	700
201	0.013	98	0.1	0.518	0.20	82	0.1	5.58	166.0	250	3.0	0.0	0.0	166.0	1900
202	0.013	98	0.1	0.518	0.25	80	0.1	6.35	4.0	225	4.0	0.0	0.0	4.0	200
203	0.013	98	0.1	0.518	0.21	82	0.1	5.58	9.1	150	3.5	0.0	0.0	9.1	450
301	0.013	98	0.1	0.518	0.23	81	0.1	5.96	16.4	95	2.5	0.0	0.0	16.4	600
302	0.013	98	0.1	0.518	0.28	80	0.1	6.35	6.0	100	2.0	50.0	3.0	3.0	180
303	0.013	98	0.1	0.518	0.20	82	0.1	5.58	4.8	100	2.0	75.0	3.6	1.2	250
304	0.013	98	0.1	0.518	0.20	82	0.1	5.58	1.6	75	1.0	50.0	0.8	0.8	50
310	0.013	98	0.1	0.518	0.20	82	0.1	5.58	2.4	75	2.0	75.0	1.8	0.6	200
311	0.013	98	0.1	0.518	0.20	82	0.1	5.58	6.6	100	2.0	75.0	5.0	1.6	200
312	0.013	98	0.1	0.518	0.30	83	0.1	5.20	4.4	100	2.0	75.0	3.3	1.1	100
313	0.013	98	0.1	0.518	0.30	83	0.1	5.20	1.8	50	2.0	75.0	1.4	0.4	80
314	0.013	98	0.1	0.518	0.30	83	0.1	5.20	3.3	20	1.0	50.0	1.7	1.6	50
401	0.013	98	0.1	0.518	0.30	83	0.1	5.20	5.6	240	3.5	0.0	0.0	5.6	150
402	0.013	98	0.1	0.518	0.30	83	0.1	5.20	7.4	100	2.0	50.0	3.7	3.7	300
403	0.013	98	0.1	0.518	0.30	83	0.1	5.20	4.7	70	2.0	75.0	3.5	1.2	300
404	0.013	98	0.1	0.518	0.30	83	0.1	5.20	3.2	60	2.0	75.0	2.4	0.8	200
405	0.013	98	0.1	0.518	0.30	83	0.1	5.20	3.2	75	2.0	75.0	2.4	0.8	150
406	0.013	98	0.1	0.518	0.20	82	0.1	5.58	1.3	10	2.0	85.0	1.1	0.2	50
407	0.013	98	0.1	0.518	0.30	83	0.1	5.20	3.0	100	2.0	75.0	2.3	0.7	100
500	0.013	98	0.1	0.518	0.20	81	0.1	5.96	5.8	100	2.0	70.0	4.1	1.7	200
501	0.013	98	0.1	0.518	0.30	83	0.1	5.20	2.5	80	3.5	0.0	0.0	2.5	100
603	0.013	98	0.1	0.518	0.30	83	0.1	5.20	5.6	100	2.5	0.0	0.0	5.6	225
604	0.013	98	0.1	0.518	0.30	83	0.1	5.20	2.7	100	2.5	0.0	0.0	2.7	250
605	0.013	98	0.1	0.518	0.30	83	0.1	5.20	3.9	100	2.5	0.0	0.0	3.9	200
750	0.013	98	0.1	0.518	0.20	81	0.1	5.96	0.5	50	2.0	100.0	0.5	0.0	200
751	0.013	98	0.1	0.518	0.20	81	0.1	5.96	0.2	50	2.0	100.0	0.2	0.0	200
TOTAL									1918.2				40.8	1877.4	

- Indicates Catchment Areas that are Tributary to SWM Facility #1 (CTC Pond Area)
- Indicates Catchment Areas that are Tributary to SWM Facility #2
- Indicates Catchment Areas that are Tributary to SWM Facility #3

Table of Curve Numbers for BC Hydrologic Soil Type

Land Use	CN Value	Mann. 'n'	Description			
Meadow	71	0.40	continuous grass			
Woodlot	73.5	0.40	forests			
Long Grass	79	0.35	natural, not maintained			
Lawns	83	0.30	maintained			
Pasture	76	0.25	farm pasture or range			
Crop	82	0.20	farm land			
Fallow	91	0.10	idle farmland (bare)			

	Area Tributary to Pond	Imp. Area	% Impervious
Pond #2	56.0	20.3	36
Pond #3	17.7	12.2	69

PRE-DEVELOPMENT MIDUSS MODEL PARAMETERS											
Catchment	Meadow	Woodlot	Long Grass	Lawns	Pasture	Crop	Fallow	Total Percent.	Weighted CN	Weighted n	Perv. Area From Above
50	0%	5%	5%	0%	0%	90%	0%	100%	81	0.22	396.0
52	0%	20%	5%	0%	0%	75%	0%	100%	80	0.25	196.0
54	0%	30%	15%	0%	0%	55%	0%	100%	79	0.28	39.0
56	0%	2%	5%	0%	0%	93%	0%	100%	82	0.21	345.0
58	0%	5%	15%	0%	0%	80%	0%	100%	81	0.23	82.0
59	0%	60%	20%	0%	0%	20%	0%	100%	76	0.35	128.0
60	0%	10%	5%	0%	0%	85%	0%	100%	81	0.23	225.0
62	0%	20%	5%	0%	0%	75%	0%	100%	80	0.25	95.0
64	0%	0%	5%	0%	0%	95%	0%	100%	82	0.21	80.0
100	0%	5%	10%	0%	0%	85%	0%	100%	81	0.23	45.0
101	0%	20%	25%	0%	0%	55%	0%	100%	80	0.28	11.2
201	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	166.0
202	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	8.0
203	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	13.6
204	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	6.8
301	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	16.4
302	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	5.0
303	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	11.6
304	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	6.3
401	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	5.6
402	0%	0%	0%	0%	0%	100%	0%	100%	82	0.20	4.2

MIDUSS - Rainfall Intensity - IDF Curve Parameters

KINCARDINE BUSINESS PARK
Municipality of Kincardine
08055

Precipitation Data - Goderich - SCS Type II (6 Hour)

Return Period	Return Period			Volume <i>mm</i>
	<i>a</i>	<i>b</i>	<i>c</i>	
2-Year	1154.572	12.323	0.869	40.400
5-Year	2070.901	20.382	0.904	58.700
10-Year	2924.707	25.799	0.929	70.800
25-Year	4210.292	31.868	0.955	86.100
50-Year	5783.612	37.889	0.984	97.500
100-Year	6928.137	40.974	0.994	108.800
250-Year				285.000

(212mm with AMCIII)

Refer to July 2006 Hydrology Study in Support of Floodplain Mapping Project 2005

APPENDIX F

MIDUSS MODEL OUTPUT FILES

MIDUSS MODEL OUTPUT FILE INDEX

Miduss File	Description
08055-Pre-Existing 2 Year.out	Pre-Existing Drainage Area 2 Yr. Storm
08055-Pre- Existing 5 Year.out	Pre-Existing Drainage Area 5 Yr. Storm
08055-Pre-Existing 10 Year.out	Pre-Existing Drainage Area 10 Yr. Storm
08055-Pre-Exisitng 25 Year.out	Pre-Existing Drainage Area 25 Yr. Storm
08055-Pre-Existing 50 Year.out	Pre-Existing Drainage Area 50 Yr. Storm
08055-Pre-Existing 100 Year.out	Pre-Existing Drainage Area 100 Yr. Storm
08055-Post 2 Year.out	Developed Drainage Area 2 Yr. Storm
08055-Post 5 Year.out	Developed Drainage Area 5 Yr. Storm
08055-Post 10 Year.out	Developed Drainage Area 10 Yr. Storm
08055-Post 25 Year.out	Developed Drainage Area 25 Yr. Storm
08055-Post 50 Year.out	Developed Drainage Area 50 Yr. Storm
08055-Post 100 Year.out	Developed Drainage Area 100 Yr. Storm

- Note: 1. All Miduss modelling files provided digitally on CD.
 2. **Highlighted** modelling provided in hard copy format.

PRE-EXISTING – 5 YEAR

```

" MIDUSS Output ----->"
" MIDUSS version Version 2.25 rev. 465"
" MIDUSS created Tuesday, February 05, 2008"
" 10 Units used: ie METRIC"
" Job folder: C:\Users\derb\Desktop\Kincardine Miduss"
" Output filename: 08055 - Pre-Existing 5 Year.out"
" License name: EliteBook"
" Company BMROSS"
" Date & Time last used: 7/14/2011 at 4:05:31 PM"
" 31 TIME PARAMETERS"
" 5.000 Time Step"
" 360.000 Max. Storm length"
" 1800.000 Max. Hydrograph"
" 32 STORM Mass Curve"
" 3 Mass Curve"
" 58.700 Rainfall depth"
" 360.000 Duration"
" 41 C:\Program Files\MIDUSS\SCS_6hr_Type2.mrd SCS Type II - 6 hour
Distribution - Ontario"
" Maximum intensity 45.786 mm/hr"
" Total depth 58.700 mm"
" 6 005hyd Hydrograph extension used in this file"
" 81 ADD COMMENT-----"
" 1 Lines of comment"
" Start of Penetangore Tributary"
" 33 CATCHMENT 50"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 50 No description"
" 0.000 % Impervious"
" 396.000 Total Area"
" 450.000 Flow length"
" 2.500 Overland Slope"
" 396.000 Pervious Area"
" 450.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 450.000 Impervious length"
" 2.500 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.422 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 10.190 0.000 0.000 0.000 c.m/sec"
" Catchment 50 Pervious Impervious Total Area "
" Surface Area 396.000 0.000 396.000 hectare"
" Time of concentration 95.354 13.283 95.354 minutes"
" Time to Centroid 342.104 218.977 342.104 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 23.2452 0.0000 23.2452 ha-m"
" Rainfall losses 33.937 5.504 33.937 mm"
" Runoff depth 24.763 53.196 24.763 mm"
" Runoff volume 9.8061 0.0000 9.8061 ha-m"
" Runoff coefficient 0.422 0.000 0.422 "
" Maximum flow 10.190 0.000 10.190 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 10.190 10.190 0.000 0.000"
" 52 CHANNEL DESIGN"
" 10.190 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.246 metre"
" Velocity 1.425 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.908 metre"
" 53 ROUTE Channel Route 3000"
" 3000.00 Channel Route 3000 Reach length (metre)"
" 0.406 X-factor <= 0.5"
" 315.804 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 5 No. of sub-reaches"
" Peak outflow 10.190 10.190 10.018 c.m/sec"
" 10.190 10.190 10.018 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 10.190 10.018 10.018 0.000"
" 33 CATCHMENT 52"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 52 No description"
" 0.000 % Impervious"
" 196.000 Total Area"
" 250.000 Flow length"
" 7.000 Overland Slope"
" 196.000 Pervious Area"
" 250.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 250.000 Impervious length"
" 7.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.403 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 7.959 10.018 10.018 0.000 c.m/sec"
" Catchment 52 Pervious Impervious Total Area "
" Surface Area 196.000 0.000 196.000 hectare"
" Time of concentration 49.947 6.855 49.947 minutes"
" Time to Centroid 288.104 211.306 288.104 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 11.5052 0.0000 11.5052 ha-m"
" Rainfall losses 35.049 6.025 35.049 mm"
" Runoff depth 23.651 52.675 23.651 mm"
" Runoff volume 4.6356 0.0000 4.6356 ha-m"
" Runoff coefficient 4.403 0.000 4.403 "
" Maximum flow 7.959 0.000 7.959 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 7.959 12.923 10.018 0.000"
" 52 CHANNEL DESIGN"
" 12.923 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.400 Gradient %"
" Depth of flow 1.456 metre"
" Velocity 1.393 m/sec"
" Channel capacity 249.409 c.m/sec"
" Critical depth 1.021 metre"
" 53 ROUTE Channel Route 1300"
" 1300.00 Channel Route 1300 Reach length (metre)"
" 0.376 X-factor <= 0.5"
" 349.856 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
" Peak outflow 12.836 12.836 12.836 c.m/sec"
" 7.959 12.923 12.836 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 7.959 12.836 12.836 0.000"
" 33 CATCHMENT 54"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 54 No description"
" 0.000 % Impervious"
" 39.000 Total Area"
" 140.000 Flow length"
" 11.000 Overland Slope"
" 39.000 Pervious Area"
" 140.000 Pervious length"
" 11.000 Pervious slope"
" 0.000 Impervious Area"
" 140.000 Impervious length"
" 11.000 Impervious slope"
" 0.210 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.422 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 2.426 12.836 12.836 0.000 c.m/sec"
" Catchment 54 Pervious Impervious Total Area "
" Surface Area 39.000 0.000 39.000 hectare"
" Time of concentration 27.329 4.227 27.329 minutes"
" Time to Centroid 259.963 208.037 259.963 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2.2893 0.0000 2.2893 ha-m"
" Rainfall losses 33.953 6.167 33.953 mm"
" Runoff depth 24.747 52.533 24.747 mm"
" Runoff volume 9651.26 0.02 9651.28 c.m"
" Runoff coefficient 0.422 0.000 0.422 "
" Maximum flow 2.426 0.000 2.426 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 2.426 13.266 12.836 0.000"
" 52 CHANNEL DESIGN"
" 13.266 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.400 Gradient %"
" Depth of flow 1.473 metre"
" Velocity 1.403 m/sec"
" Channel capacity 249.409 c.m/sec"
" Critical depth 1.035 metre"
" 53 ROUTE Channel Route 800"
" 800.00 Channel Route 800 Reach length (metre)"
" 0.297 X-factor <= 0.5"
" 213.864 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
" Peak outflow 13.220 13.220 13.220 c.m/sec"
" 2.426 13.266 13.220 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 10"
" 6 Combine "
" 10 Node #"
" Confluence on Penetangore Tributary"
" Maximum flow 13.220 c.m/sec"
" Hydrograph volume 154068.359 c.m"
" 2.426 13.266 13.220 13.220"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 2.426 0.000 13.220 13.220"
" 33 CATCHMENT 60"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 60 No description"
" 0.000 % Impervious"
" 225.000 Total Area"
" 270.000 Flow length"
" 2.500 Overland Slope"
" 225.000 Pervious Area"
" 270.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 270.000 Impervious length"
" 2.500 Impervious slope"

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0.230 Pervious Manning 'n'"
81.000 Pervious SCS Curve No."
0.422 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.958 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
40 7.768 0.000 13.220 13.220 c.m/sec"
Catchment 60 Pervious Impervious Total Area "
Surface Area 225.000 0.000 225.000 hectare"
Time of concentration 66.758 9.777 66.758 minutes"
Time to Centroid 307.583 214.714 307.583 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 13.2075 0.0000 13.2075 ha-m"
Rainfall losses 33.938 5.762 33.938 mm"
Runoff depth 24.762 52.938 24.762 mm"
Runoff volume 5.5715 0.0000 5.5715 ha-m"
Runoff coefficient 0.422 0.000 0.422 "
Maximum flow 7.768 0.000 7.768 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 7.768 13.220 13.220"
52 CHANNEL DESIGN"
7.768 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.400 Gradient %"
Depth of flow 1.159 metre"
Velocity 1.223 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 0.792 metre"
53 ROUTE Channel Route 1800"
1800.00 Channel Route 1800 Reach length (metre)"
0.390 X-factor <= 0.5"
367.870 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
3 No. of sub-reaches"
Peak outflow 7.635 7.635 13.220 c.m/sec"
40 HYDROGRAPH Combine 10"
6 Combine "
10 Node #"
Confluence on Penatangore Tributary"
Maximum flow 19.506 c.m/sec"
Hydrograph volume 209783.594 c.m"
40 HYDROGRAPH Confluence 10"
7 Confluence "
10 Node #"
Confluence on Penatangore Tributary"
Maximum flow 19.506 c.m/sec"
Hydrograph volume 209783.609 c.m"
52 CHANNEL DESIGN"
19.506 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.400 Gradient %"
Depth of flow 1.744 metre"
Velocity 1.547 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 1.248 metre"
53 ROUTE Channel Route 2000"
2000.00 Channel Route 2000 Reach length (metre)"
0.358 X-factor <= 0.5"
323.201 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
3 No. of sub-reaches"
Peak outflow 19.475 19.475 0.000 c.m/sec"
40 HYDROGRAPH Combine 11"
6 Combine "
11 Node #"
Confluence on Penatangore Tributary"
Maximum flow 19.475 c.m/sec"
Hydrograph volume 209783.500 c.m"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary" 7.768 0.000 19.475 19.475"
33 CATCHMENT 62"
1 Triangular SCS"
1 Equal length"
1 SCS method"
62 No description"
0.000 % Impervious"
95.000 Total Area"
160.000 Flow length"
2.500 Overland Slope"
95.000 Pervious Area"
160.000 Pervious length"
2.500 Pervious slope"
0.000 Impervious Area"
160.000 Impervious length"
2.500 Impervious slope"
0.250 Pervious Manning 'n'"
80.000 Pervious SCS Curve No."
0.403 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
6.350 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
3.760 0.000 19.475 19.475 c.m/sec"
Catchment 62 Pervious Impervious Total Area "
Surface Area 95.000 0.000 95.000 hectare"
Time of concentration 52.044 7.142 52.044 minutes"
Time to Centroid 290.632 211.675 290.632 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 5.5765 0.0000 5.5765 ha-m"
Rainfall losses 35.050 5.748 35.050 mm"
Runoff depth 23.650 52.952 23.650 mm"
Runoff volume 2.2467 0.0000 2.2467 ha-m"
Runoff coefficient 0.403 0.000 0.403 "
Maximum flow 3.760 0.000 3.760 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 3.760 3.760 19.475 19.475"
52 CHANNEL DESIGN"
3.760 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.300 Gradient %"
Depth of flow 0.886 metre"
Velocity 0.911 m/sec"
Channel capacity 215.995 c.m/sec"
Critical depth 0.542 metre"
53 ROUTE Channel Route 1800"
1800.00 Channel Route 1800 Reach length (metre)"
0.346 X-factor <= 0.5"
370.426 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
4 No. of sub-reaches"
Peak outflow 3.593 3.593 19.475 c.m/sec"
40 HYDROGRAPH Combine 11"
6 Combine "
11 Node #"
Confluence on Penatangore Tributary"
Maximum flow 22.226 c.m/sec"
Hydrograph volume 232250.453 c.m"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary" 3.760 0.000 3.593 22.226"
33 CATCHMENT 56"
1 Triangular SCS"
1 Equal length"
1 SCS method"
56 No description"
0.000 % Impervious"
345.000 Total Area"
240.000 Flow length"
11.000 Overland Slope"
345.000 Pervious Area"
240.000 Pervious length"
11.000 Pervious slope"
0.000 Impervious Area"
240.000 Impervious length"
15.000 Impervious slope"
0.280 Pervious Manning 'n'"
79.000 Pervious SCS Curve No."
0.385 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
6.752 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
14.138 0.000 3.593 22.226 c.m/sec"
Catchment 56 Pervious Impervious Total Area "
Surface Area 345.000 0.000 345.000 hectare"
Time of concentration 46.250 5.322 46.250 minutes"
Time to Centroid 284.430 209.376 284.430 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 20.2515 0.0000 20.2515 ha-m"
Rainfall losses 36.119 5.390 36.119 mm"
Runoff depth 22.581 53.310 22.581 mm"
Runoff volume 7.7903 0.0000 7.7903 ha-m"
Runoff coefficient 0.385 0.000 0.385 "
Maximum flow 14.138 0.000 14.138 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 14.138 14.138 3.593 22.226"
52 CHANNEL DESIGN"
14.138 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.400 Gradient %"
Depth of flow 1.515 metre"
Velocity 1.426 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 1.067 metre"
53 ROUTE Channel Route 1300"
1300.00 Channel Route 1300 Reach length (metre)"
0.372 X-factor <= 0.5"
341.945 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 13.869 13.869 22.226 c.m/sec"
40 HYDROGRAPH Combine 11"
6 Combine "
11 Node #"
Confluence on Penatangore Tributary"
Maximum flow 30.912 c.m/sec"
Hydrograph volume 310152.906 c.m"
40 HYDROGRAPH Confluence 11"
7 Confluence "
11 Node #"
Confluence on Penatangore Tributary"
Maximum flow 30.912 c.m/sec"
Hydrograph volume 310152.906 c.m"
14.138 14.138 13.869 30.912"
52 CHANNEL DESIGN"
14.138 30.912 13.869 0.000"

"	30.912	Current peak flow	c.m/sec"	"	0.100	Pervious Ia/S coefficient"	"
"	0.040	Manning 'n'"	"	"	5.576	Pervious Initial abstraction"	"
"	0.	Cross-section type: 0=trapezoidal; 1=general"	"	"	0.013	Impervious Manning 'n'"	"
"	2.000	Basewidth	metre"	"	98.000	Impervious SCS Curve No."	"
"	3.000	Left bank slope"	"	"	0.000	Impervious Runoff coefficient"	"
"	3.000	Right bank slope"	"	"	0.100	Impervious Ia/S coefficient"	"
"	5.000	Channel depth	metre"	"	0.518	Impervious Initial abstraction"	"
"	0.500	Gradient	%"	"	3.970	0.000	5.084
"		Depth of flow	2.026 metre"	"			32.000 c.m/sec"
"		Velocity	1.889 m/sec"	"			Catchment 64
"		Channel capacity	278.848 c.m/sec"	"			Surface Area
"		Critical depth	1.552 metre"	"			80.000 0.000 80.000
"	53	ROUTE Channel Route 1300"	"	"			Time of concentration
"	1300.00	Channel Route 1300 Reach length (metre)"	"	"			43.483 6.825 43.483
"	0.367	X-factor <= 0.5"	"	"			Time to Centroid
"	258.058	K-lag (seconds)"	"	"			278.638 211.270 278.638
"	0.000	Default(0) or user spec.(1) values used"	"	"			Rainfall depth
"	0.500	X-factor <= 0.5"	"	"			58.700 58.700 58.700
"	30.000	K-lag (seconds)"	"	"			Rainfall volume
"	0.500	Beta weighting factor"	"	"			4.6960 0.0000 4.6960
"	300.000	Routing time step (seconds)"	"	"			Rainfall losses
"	2	No. of sub-reaches"	"	"			32.787 6.061 32.787
"		Peak outflow	30.822 c.m/sec"	"			Runoff depth
"		14.138 30.912 30.822 0.000 c.m/sec"	"	"			25.913 52.639 25.913
"	40	HYDROGRAPH Combine 12"	"	"			Runoff volume
"	6	Combine "	"	"			2.0730 0.0000 2.0730
"	12	Node #"	"	"			Runoff coefficient
"		Confluence on Penatangore Tributary"	"	"			0.441 0.000 0.441
"		Maximum flow	30.822 c.m/sec"	"			Maximum flow
"		Hydrograph volume	310153.156 c.m"	"			3.970 0.000 3.970
"		14.138 30.912 30.822 30.822"	"	"			HYDROGRAPH Add Runoff "
"	40	HYDROGRAPH Start - New Tributary"	"	"	40	4	Add Runoff "
"	2	Start - New Tributary"	"	"			3.970 3.970 5.084 32.000"
"		14.138 0.000 30.822 30.822"	"	"			CHANNEL DESIGN"
"	33	CATCHMENT 58"	"	"	52		3.970 Current peak flow c.m/sec"
"	1	Triangular SCS"	"	"			0.040 Manning 'n'"
"	1	Equal length"	"	"			0. Cross-section type: 0=trapezoidal; 1=general"
"	1	SCS method"	"	"			2.000 Basewidth metre"
"	0.000	% Impervious"	"	"			3.000 Left bank slope"
"	82.000	Total Area"	"	"			3.000 Right bank slope"
"	140.000	Flow length"	"	"			5.000 Channel depth metre"
"	15.000	Overland Slope"	"	"			0.500 Gradient %"
"	82.000	Pervious Area"	"	"			Depth of flow
"	140.000	Pervious length"	"	"			0.806 metre"
"	15.000	Pervious slope"	"	"			Velocity
"	0.000	Impervious Area"	"	"			1.116 m/sec"
"	140.000	Impervious length"	"	"			Channel capacity
"	15.000	Impervious slope"	"	"			278.848 c.m/sec"
"	0.230	Pervious Manning 'n'"	"	"			Critical depth
"	81.000	Pervious SCS Curve No."	"	"			0.558 metre"
"	0.422	Pervious Runoff coefficient"	"	"			ROUTE Channel Route 700"
"	0.100	Pervious Ia/S coefficient"	"	"			700.00 Channel Route 700 Reach length (metre)"
"	5.958	Pervious Initial abstraction"	"	"			0.390 X-factor <= 0.5"
"	0.013	Impervious Manning 'n'"	"	"			235.253 K-lag (seconds)"
"	98.000	Impervious SCS Curve No."	"	"			0.000 Default(0) or user spec.(1) values used"
"	0.000	Impervious Runoff coefficient"	"	"			0.500 X-factor <= 0.5"
"	0.100	Impervious Ia/S coefficient"	"	"			30.000 K-lag (seconds)"
"	0.518	Impervious Initial abstraction"	"	"			0.500 Beta weighting factor"
"	5.207	0.000 30.822 30.822 c.m/sec"	"	"			300.000 Routing time step (seconds)"
"		Catchment 58	"	"			2
"		Surface Area	82.000	"			No. of sub-reaches"
"		Pervious	0.000	"			Peak outflow
"		Impervious Total Area	82.000	"			3.952 c.m/sec"
"		Flow length	140.000	"			3.970 3.970 3.952 32.000 c.m/sec"
"		Overland Slope	15.000	"			HYDROGRAPH Combine 12"
"		Pervious Area	82.000	"			6
"		Pervious length	140.000	"			Combine "
"		Pervious slope	15.000	"			12
"		Impervious Area	0.000	"			Node #"
"		Impervious length	140.000	"			Confluence on Penatangore Tributary"
"		Impervious slope	15.000	"			Maximum flow
"		Pervious Manning 'n'"	0.230	"			33.877 c.m/sec"
"		Pervious SCS Curve No."	81.000	"			Hydrograph volume
"		Pervious Runoff coefficient"	0.422	"			351176.438 c.m"
"		Pervious Ia/S coefficient"	0.100	"			3.970 3.970 3.952 33.877"
"		Pervious Initial abstraction"	5.958	"			HYDROGRAPH Confluence 12"
"		Impervious Manning 'n'"	0.013	"			7
"		Impervious SCS Curve No."	98.000	"			Confluence "
"		Impervious Runoff coefficient"	0.000	"			12
"		Impervious Ia/S coefficient"	0.100	"			Node #"
"		Impervious Initial abstraction"	0.518	"			Confluence on Penatangore Tributary"
"		5.207 0.000 30.822 30.822 c.m/sec"	"	"			Maximum flow
"		Catchment 58	"	"			33.877 c.m/sec"
"		Surface Area	82.000	"			Hydrograph volume
"		Pervious	0.000	"			351176.406 c.m"
"		Impervious Total Area	82.000	"			3.970 3.970 3.952 0.000"
"		Flow length	140.000	"			CHANNEL DESIGN"
"		Overland Slope	15.000	"			33.877 Current peak flow c.m/sec"
"		Pervious Area	82.000	"			0.040 Manning 'n'"
"		Pervious length	140.000	"			0. Cross-section type: 0=trapezoidal; 1=general"
"		Pervious slope	15.000	"			2.000 Basewidth metre"
"		Impervious Area	0.000	"			3.000 Left bank slope"
"		Impervious length	140.000	"			3.000 Right bank slope"
"		Impervious slope	15.000	"			5.000 Channel depth metre"
"		Pervious Manning 'n'"	0.230	"			0.300 Gradient %"
"		Pervious SCS Curve No."	81.000	"			Depth of flow
"		Pervious Runoff coefficient"	0.422	"			2.347 metre"
"		Pervious Ia/S coefficient"	0.100	"			Velocity
"		Pervious Initial abstraction"	5.958	"			1.597 m/sec"
"		Impervious Manning 'n'"	0.013	"			Channel capacity
"		Impervious SCS Curve No."	98.000	"			215.995 c.m/sec"
"		Impervious Runoff coefficient"	0.000	"			Critical depth
"		Impervious Ia/S coefficient"	0.100	"			1.620 metre"
"		Impervious Initial abstraction"	0.518	"			ROUTE Channel Route 2500"
"		5.207 0.000 30.822 30.822 c.m/sec"	"	"			2500.00 Channel Route 2500 Reach length (metre)"
"		Catchment 58	"	"			0.303 X-factor <= 0.5"
"		Surface Area	82.000	"			391.350 K-lag (seconds)"
"		Pervious	0.000	"			0.000 Default(0) or user spec.(1) values used"
"		Impervious Total Area	82.000	"			0.500 X-factor <= 0.5"
"		Flow length	140.000	"			30.000 K-lag (seconds)"
"		Overland Slope	15.000	"			0.500 Beta weighting factor"
"		Pervious Area	82.000	"			300.000 Routing time step (seconds)"
"		Pervious length	140.000	"			2
"		Pervious slope	15.000	"			No. of sub-reaches"
"		Impervious Area	0.000	"			Peak outflow
"		Impervious length	140.000	"			3.970 3.970 3.952 32.000 c.m/sec"
"		Impervious slope	15.000	"			HYDROGRAPH Combine 12"
"		Pervious Manning 'n'"	0.230	"			6
"		Pervious SCS Curve No."	81.000	"			Combine "
"		Pervious Runoff coefficient"	0.422	"			1000
"		Pervious Ia/S coefficient"	0.100	"			Node #"
"		Pervious Initial abstraction"	5.958	"			Node upstream of Penatangore Culvert"
"		Impervious Manning 'n'"	0.013	"			Maximum flow
"		Impervious SCS Curve No."	98.000	"			33.438 c.m/sec"
"		Impervious Runoff coefficient"	0.000	"			Hydrograph volume
"		Impervious Ia/S coefficient"	0.100	"			351176.469 c.m"
"		Impervious Initial abstraction"	0.518	"			3.970 33.877 33.438 33.438"
"		5.207 0.000 30.822 30.822 c.m/sec"	"	"			HYDROGRAPH Start - New Tributary"
"		Catchment 58	"	"			2
"		Surface Area	82.000	"			Start - New Tributary"
"		Pervious	0.000	"			3.970 0.000 33.438 33.438"
"		Impervious Total Area	82.000	"			33
"		Flow length	140.000	"			CATCHMENT 59"
"		Overland Slope	15.000	"			1
"		Pervious Area	82.000	"			Triangular SCS"
"		Pervious length	140.000	"			1
"		Pervious slope	15.000	"			Equal length"
"		Impervious Area	0.000	"			1
"		Impervious length	140.000	"			SCS method"
"		Impervious slope	15.000	"			59
"		Pervious Manning 'n'"	0.230	"			No description"
"		Pervious SCS Curve No."	81.000	"			% Impervious"
"		Pervious Runoff coefficient"	0.422	"			0.000
"		Pervious Ia/S coefficient"	0.100	"			128.000 Total Area"
"		Pervious Initial abstraction"	5.958	"			170.000 Flow length"
"		Impervious Manning 'n'"	0.013	"			18.000 Overland Slope"
"		Impervious SCS Curve No."	98.000	"			128.000 Pervious Area"
"		Impervious Runoff coefficient"	0.000	"			18.000 Pervious length"
"		Impervious Ia/S coefficient"	0.100	"			18.000 Pervious slope"
"		Impervious Initial abstraction"	0.518	"			0.000 Impervious Area"
"		5.037 0.000 33.438 33.438 c.m/sec"	"	"			170.000 Impervious length"
"		Catchment 59	"	"			18.000 Impervious slope"
"		Surface Area	128.000	"			0.350 Pervious Manning 'n'"
"		Pervious	0.000	"			76.000 Pervious SCS Curve No."
"		Impervious Total Area	128.000	"			0.334 Pervious Runoff coefficient"
"		Flow length	170.000	"			0.100 Pervious Ia/S coefficient"
"		Overland Slope	18.000	"			8.021 Pervious Initial abstraction"
"		Pervious Area	128.000	"			0.013 Pervious Manning 'n'"
"		Pervious length	170.000	"			98.000 Impervious SCS Curve No."
"		Pervious slope	18.000	"			0.000 Impervious Runoff coefficient"
"		Impervious Area	0.000	"			0.100 Impervious Ia/S coefficient"
"		Impervious length	170.000	"			0.518 Impervious Initial abstraction"
"		Impervious slope	18.000	"			5.037 0.000 33.438 33.438 c.m/sec"
"		Pervious Manning 'n'"	0.210	"			Catchment 59
"		Pervious SCS Curve No."	82.000	"			Surface Area
"		Pervious Runoff coefficient"	0.441	"			128.000 0.000 128.000
"				"			Time of concentration
"				"			38.873 4.097 38.873
"				"			Time to Centroid
"				"			277.849 207.770 277.849
"				"			Rainfall depth
"				"			58.700 58.700 58.700


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" 33 CATCHMENT 204"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 204 No description"
" 0.000 % Impervious"
" 6.800 Total Area"
" 120.000 Flow length"
" 2.000 Overland Slope"
" 6.800 Pervious Area"
" 120.000 Pervious length"
" 2.000 Pervious slope"
" 0.000 Impervious Area"
" 120.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.441 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.359 7.647 7.647 35.159 c.m/sec"
" Catchment 204 Pervious Impervious Total Area "
" Surface Area 6.800 0.000 6.800 hectare"
" Time of concentration 39.762 6.426 39.761 minutes"
" Time to Centroid 274.146 210.764 274.146 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 3991.60 0.00 3991.60 c.m"
" Rainfall losses 32.788 5.970 32.788 mm"
" Runoff depth 25.912 52.730 25.912 mm"
" Runoff volume 1762.00 0.00 1762.00 c.m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 0.359 0.000 0.359 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.359 7.869 7.647 35.159"
" 52 CHANNEL DESIGN"
" 7.869 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.944 metre"
" Velocity 1.724 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.797 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length ( metre)"
" 0.353 X-factor <= 0.5"
" 65.265 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.359 7.869 7.812 35.159 c.m/sec"
" 40 HYDROGRAPH Combine 1100"
" 6 Combine "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 7.812 c.m/sec"
" Hydrograph volume 50378.371 c.m"
" 0.359 7.869 7.812 7.812"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" End of Area North of Holtby Drain"
" 40 HYDROGRAPH Confluence 1100"
" 7 Confluence "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 7.812 c.m/sec"
" Hydrograph volume 50378.367 c.m"
" 0.359 7.812 7.812 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Holtby Drain"
" 52 CHANNEL DESIGN"
" 7.812 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.105 metre"
" Velocity 1.331 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.794 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length ( metre)"
" 0.248 X-factor <= 0.5"
" 112.711 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.359 7.812 7.807 c.m/sec"
" 0.359 7.812 7.807 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node #"
" Node at Holtby Drain"
" Maximum flow 7.807 c.m/sec"
" Hydrograph volume 50378.371 c.m"
" 0.359 7.812 7.807 7.807"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.359 0.000 7.807 7.807"
" 33 CATCHMENT 100"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 100 No description"
" 0.000 % Impervious"
" 45.000 Total Area"
" 100.000 Flow length"
" 7.000 Overland Slope"
" 45.000 Pervious Area"
" 100.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 7.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.441 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 3.058 0.000 7.807 7.807 c.m/sec"
" Catchment 100 Pervious Impervious Total Area "
" Surface Area 45.000 0.000 45.000 hectare"
" Time of concentration 24.476 3.956 24.476 minutes"
" Time to Centroid 255.680 207.565 255.680 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2.6415 0.0000 2.6415 ha-m"
" Rainfall losses 32.802 6.485 32.802 mm"
" Runoff depth 25.898 52.215 25.898 mm"
" Runoff volume 1.1654 0.0000 1.1654 ha-m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 3.058 0.000 3.058 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 3.058 3.058 7.807 7.807"
" 52 CHANNEL DESIGN"
" 3.058 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.600 metre"
" Velocity 1.342 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.484 metre"
" 53 ROUTE Channel Route 1500"
" 1500.00 Channel Route 1500 Reach length ( metre)"
" 0.470 X-factor <= 0.5"
" 279.420 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 3 No. of sub-reaches"
" Peak outflow 3.058 3.058 3.022 7.807 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 3.058 3.022 3.022 7.807"
" 33 CATCHMENT 101"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 101 No description"
" 0.000 % Impervious"
" 11.200 Total Area"
" 50.000 Flow length"
" 7.000 Overland Slope"
" 11.200 Pervious Area"
" 50.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 50.000 Impervious length"
" 7.000 Impervious slope"
" 0.280 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.403 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.751 3.022 3.022 7.807 c.m/sec"
" Catchment 101 Pervious Impervious Total Area "
" Surface Area 11.200 0.000 11.200 hectare"
" Time of concentration 20.355 2.610 20.355 minutes"
" Time to Centroid 252.367 206.029 252.367 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 6574.39 0.01 6574.40 c.m"
" Rainfall losses 35.069 6.188 35.069 mm"
" Runoff depth 23.631 52.512 23.631 mm"
" Runoff volume 2646.69 0.01 2646.70 c.m"
" Runoff coefficient 0.403 0.000 0.403 "
" Maximum flow 0.751 0.000 0.751 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.751 3.456 3.022 7.807"
" 52 CHANNEL DESIGN"
" 3.456 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.637 metre"
" Velocity 1.387 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.518 metre"
" 53 ROUTE Channel Route 700"
" 700.00 Channel Route 700 Reach length ( metre)"
" 0.455 X-factor <= 0.5"
" 189.250 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
" Peak outflow 0.751 3.456 3.428 7.807 c.m/sec"
" 0.751 3.456 3.428 7.807 c.m/sec"
" 40 HYDROGRAPH Combine 1200"

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"      6 Combine "
" 1200 Node #"
"      Node taking 100 series for Holtby Drain"
"      Maximum flow      3.428 c.m/sec"
"      Hydrograph volume 14300.893 c.m"
"      0.751 3.456 3.428 3.428"
" 40 HYDROGRAPH Confluence 1200"
" 7 Confluence "
" 1200 Node #"
"      Node taking 100 series for Holtby Drain"
"      Maximum flow      3.428 c.m/sec"
"      Hydrograph volume 14300.893 c.m"
"      0.751 3.428 3.428 0.000"
" 52 CHANNEL DESIGN"
" 3.428 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow      0.751 metre"
"      Velocity           1.073 m/sec"
"      Channel capacity   278.848 c.m/sec"
"      Critical depth     0.515 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 34.935 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.603 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
"      Peak outflow      3.403 c.m/sec"
"      0.751 3.428 3.403 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node #"
"      Node at Holtby Drain"
"      Maximum flow      9.945 c.m/sec"
"      Hydrograph volume 64679.262 c.m"
"      0.751 3.428 3.403 9.945"
" 40 HYDROGRAPH Confluence 1300"
" 7 Confluence "
" 1300 Node #"
"      Node at Holtby Drain"
"      Maximum flow      9.945 c.m/sec"
"      Hydrograph volume 64679.254 c.m"
"      0.751 9.945 3.403 0.000"
" 52 CHANNEL DESIGN"
" 9.945 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow      1.233 metre"
"      Velocity           1.416 m/sec"
"      Channel capacity   278.848 c.m/sec"
"      Critical depth     0.897 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 26.482 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.716 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
"      Peak outflow      9.927 c.m/sec"
"      0.751 9.945 9.927 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1000"
" 6 Combine "
" 1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow      41.655 c.m/sec"
"      Hydrograph volume 440965.406 c.m"
"      0.751 9.945 9.927 41.655"
" 81 ADD COMMENT=====
" 2 Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 40 HYDROGRAPH Confluence 1000"
" 7 Confluence "
" 1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow      41.655 c.m/sec"
"      Hydrograph volume 440965.406 c.m"
"      0.751 41.655 9.927 0.000"
" 81 ADD COMMENT=====
" 2 Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 52 CHANNEL DESIGN"
" 41.655 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow      2.299 metre"
"      Velocity           2.037 m/sec"
"      Channel capacity   278.848 c.m/sec"
"      Critical depth     1.782 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 18.413 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.853 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
"      Peak outflow      41.653 c.m/sec"
"      0.751 41.655 41.653 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
"      Node Combining All Flow"
"      Maximum flow      41.653 c.m/sec"
"      Hydrograph volume 440965.500 c.m"
"      0.751 41.655 41.653 41.653"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
"      0.751 0.000 41.653 41.653"
" 33 CATCHMENT 301"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 301 No description"
" 0.000 % Impervious"
" 16.400 Total Area"
" 95.000 Flow length"
" 2.500 Overland Slope"
" 16.400 Pervious Area"
" 95.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 95.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.441 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
"      0.982 0.000 41.653 41.653 c.m/sec"
" Catchment 301 Pervious Impervious Total Area "
" Surface Area 16.400 0.000 16.400 hectare"
" Time of concentration 32.323 5.692 32.323 minutes"
" Time to Centroid 265.155 209.787 265.154 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 9626.79 0.01 9626.80 c.m"
" Rainfall losses 32.792 5.526 32.792 mm"
" Runoff depth 25.908 53.174 25.908 mm"
" Runoff volume 4248.94 0.01 4248.95 c.m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 0.982 0.000 0.982 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      0.982 0.982 41.653 41.653"
" 52 CHANNEL DESIGN"
" 0.982 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
"      Depth of flow      0.319 metre"
"      Velocity           1.042 m/sec"
"      Channel capacity   431.989 c.m/sec"
"      Critical depth     0.254 metre"
" 53 ROUTE Channel Route 480"
" 480.00 Channel Route 480 Reach length (metre)"
" 0.470 X-factor <= 0.5"
" 172.758 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
"      Peak outflow      0.975 c.m/sec"
"      0.982 0.982 0.975 41.653 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
"      0.982 0.975 0.975 41.653"
" 33 CATCHMENT 302"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 302 No description"
" 0.000 % Impervious"
" 5.000 Total Area"
" 110.000 Flow length"
" 3.500 Overland Slope"
" 5.000 Pervious Area"
" 110.000 Pervious length"
" 3.500 Pervious slope"
" 0.000 Impervious Area"
" 110.000 Impervious length"
" 3.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.441 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
"      0.301 0.975 0.975 41.653 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 5.000 0.000 5.000 hectare"
" Time of concentration 31.906 5.619 31.906 minutes"
" Time to Centroid 264.653 209.706 264.653 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2935.00 0.00 2935.00 c.m"
" Rainfall losses 32.798 5.476 32.798 mm"
" Runoff depth 25.902 53.224 25.902 mm"
" Runoff volume 1295.11 0.00 1295.12 c.m"
" Runoff coefficient 0.441 0.000 0.441 c.m"
" Maximum flow 0.301 0.000 0.301 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
"      0.301 1.260 0.975 41.653"
" 52 CHANNEL DESIGN"
" 1.260 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
"      Depth of flow      0.364 metre"
"      Velocity           1.120 m/sec"
"      Channel capacity   431.989 c.m/sec"

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"	Critical depth	0.294	metre"	"	0.	Cross-section type: 0=trapezoidal; 1=general"
"	ROUTE Channel Route 280"			"	2.000	Basewidth metre"
"	280.00 Channel Route 280 Reach length (metre)"			"	3.000	Left bank slope"
"	0.471 X-factor <= 0.5"			"	3.000	Right bank slope"
"	187.498 K-lag (seconds)"			"	5.000	Channel depth metre"
"	0.000 Default(0) or user spec.(1) values used"			"	1.200	Gradient %"
"	0.500 X-factor <= 0.5"			"		Depth of flow 0.485 metre"
"	30.000 K-lag (seconds)"			"		Velocity 1.309 m/sec"
"	0.500 Beta weighting factor"			"		Channel capacity 431.989 c.m/sec"
"	150.000 Routing time step (seconds)"			"		Critical depth 0.403 metre"
"	1 No. of sub-reaches"			"	53	ROUTE Channel Route 130"
"	Peak outflow 1.247 c.m/sec"			"	130.00	Channel Route 130 Reach length (metre)"
"	0.301 1.260 1.247 41.653 c.m/sec"			"	0.421	X-factor <= 0.5"
"	HYDROGRAPH Next link "			"	74.474	K-lag (seconds)"
"	5 Next link "			"	0.000	Default(0) or user spec.(1) values used"
"	0.301 1.247 1.247 41.653"			"	0.500	X-factor <= 0.5"
"	CATCHMENT 303"			"	30.000	K-lag (seconds)"
"	1 Triangular SCS"			"	0.500	Beta weighting factor"
"	1 Equal length"			"	75.000	Routing time step (seconds)"
"	1 SCS method"			"	1	No. of sub-reaches"
"	303 No description"			"		Peak outflow 2.186 c.m/sec"
"	0.000 % Impervious"			"	0.318	2.192 2.186 41.653 c.m/sec"
"	11.600 Total Area"			"	40	HYDROGRAPH Combine 2000"
"	135.000 Flow length"			"	6	Combine "
"	4.500 Overland Slope"			"	2000	Node #"
"	11.600 Pervious Area "			"		Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
"	135.000 Pervious length"			"		Maximum flow 2.186 c.m/sec"
"	4.500 Pervious slope"			"		Hydrograph volume 10181.607 c.m"
"	0.000 Impervious Area "			"	0.318	2.192 2.186 2.186"
"	135.000 Impervious length"			"	40	HYDROGRAPH Start - New Tributary"
"	4.500 Impervious slope"			"	2	Start - New Tributary"
"	0.200 Pervious Manning 'n'"			"	0.318	0.000 2.186 2.186"
"	82.000 Pervious SCS Curve No."			"	33	CATCHMENT 401"
"	0.441 Pervious Runoff coefficient"			"	1	Triangular SCS"
"	0.100 Pervious Ia/S coefficient"			"	1	Equal length"
"	5.576 Pervious Initial abstraction"			"	1	SCS method"
"	0.015 Impervious Manning 'n'"			"	401	No description"
"	98.000 Impervious SCS Curve No."			"	0.000	% Impervious"
"	0.000 Impervious Runoff coefficient"			"	5.600	Total Area"
"	0.100 Impervious Ia/S coefficient"			"	240.000	Flow length"
"	0.518 Impervious Initial abstraction"			"	3.500	Overland Slope"
"	0.680 1.247 1.247 41.653 c.m/sec"			"	5.600	Pervious Area "
"	Catchment 303 Pervious Impervious Total Area "			"	240.000	Pervious length"
"	Surface Area 11.600 0.000 11.600 hectare"			"	3.500	Pervious slope"
"	Time of concentration 33.458 5.892 33.458 minutes"			"	0.000	Impervious Area "
"	Time to Centroid 266.517 210.046 266.517 minutes"			"	240.000	Impervious length"
"	Rainfall depth 58.700 58.700 58.700 mm"			"	3.500	Impervious slope"
"	Rainfall volume 6809.19 0.01 6809.20 c.m"			"	0.200	Pervious Manning 'n'"
"	Rainfall losses 32.794 5.656 32.794 mm"			"	82.000	Pervious SCS Curve No."
"	Runoff depth 25.906 53.044 25.906 mm"			"	0.441	Pervious Runoff coefficient"
"	Runoff volume 3005.05 0.01 3005.05 c.m"			"	0.100	Pervious Ia/S coefficient"
"	Runoff coefficient 0.441 0.000 0.441 "			"	5.576	Pervious Initial abstraction"
"	Maximum flow 0.680 0.000 0.680 c.m/sec"			"	0.015	Impervious Manning 'n'"
"	HYDROGRAPH Add Runoff "			"	98.000	Impervious SCS Curve No."
"	4 Add Runoff "			"	0.000	Impervious Runoff coefficient"
"	0.680 1.902 1.247 41.653"			"	0.100	Impervious Ia/S coefficient"
"	CHANNEL DESIGN"			"	0.518	Impervious Initial abstraction"
"	1.902 Current peak flow c.m/sec"			"	0.249	0.000 2.186 2.186 c.m/sec"
"	0.040 Manning 'n'"			"		Catchment 401 Pervious Impervious Total Area "
"	0. Cross-section type: 0=trapezoidal; 1=general"			"		Surface Area 5.600 0.000 5.600 hectare"
"	2.000 Basewidth metre"			"		Time of concentration 50.953 8.973 50.953 minutes"
"	3.000 Left bank slope"			"		Time to Centroid 287.659 213.763 287.659 minutes"
"	3.000 Right bank slope"			"		Rainfall depth 58.700 58.700 58.700 mm"
"	5.000 Channel depth metre"			"		Rainfall volume 3287.20 0.00 3287.20 c.m"
"	1.200 Gradient %"			"		Rainfall losses 32.786 5.470 32.786 mm"
"	Depth of flow 0.451 metre"			"		Runoff depth 25.914 53.230 25.914 mm"
"	Velocity 1.259 m/sec"			"		Runoff volume 1451.19 0.00 1451.20 c.m"
"	Channel capacity 431.989 c.m/sec"			"		Runoff coefficient 0.441 0.000 0.441 "
"	Critical depth 0.372 metre"			"		Maximum flow 0.249 0.000 0.249 c.m/sec"
"	ROUTE Channel Route 430"			"	40	HYDROGRAPH Add Runoff "
"	430.00 Channel Route 430 Reach length (metre)"			"	4	Add Runoff "
"	0.478 X-factor <= 0.5"			"	0.249	0.249 2.186 2.186"
"	256.250 K-lag (seconds)"			"	52	CHANNEL DESIGN"
"	0.000 Default(0) or user spec.(1) values used"			"	0.040	Current peak flow c.m/sec"
"	0.500 X-factor <= 0.5"			"		0.040 Manning 'n'"
"	30.000 K-lag (seconds)"			"		0. Cross-section type: 0=trapezoidal; 1=general"
"	0.500 Beta weighting factor"			"	2.000	Basewidth metre"
"	150.000 Routing time step (seconds)"			"	3.000	Left bank slope"
"	1 No. of sub-reaches"			"	3.000	Right bank slope"
"	Peak outflow 1.880 c.m/sec"			"	5.000	Channel depth metre"
"	0.680 1.902 1.880 41.653 c.m/sec"			"	1.200	Gradient %"
"	HYDROGRAPH Next link "			"		Depth of flow 0.149 metre"
"	5 Next link "			"		Velocity 0.681 m/sec"
"	0.680 1.880 1.880 41.653"			"		Channel capacity 431.989 c.m/sec"
"	CATCHMENT 304"			"		Critical depth 0.110 metre"
"	1 Triangular SCS"			"	53	ROUTE Channel Route 225"
"	1 Equal length"			"	225.00	Channel Route 225 Reach length (metre)"
"	1 SCS method"			"	0.484	X-factor <= 0.5"
"	304 No description"			"	247.644	K-lag (seconds)"
"	0.000 % Impervious"			"	0.000	Default(0) or user spec.(1) values used"
"	6.300 Total Area"			"	0.500	X-factor <= 0.5"
"	150.000 Flow length"			"	30.000	K-lag (seconds)"
"	2.500 Overland Slope"			"	0.500	Beta weighting factor"
"	6.300 Pervious Area "			"	150.000	Routing time step (seconds)"
"	150.000 Pervious length"			"	1	No. of sub-reaches"
"	2.500 Pervious slope"			"		Peak outflow 0.249 0.248 2.186 c.m/sec"
"	0.000 Impervious Area "			"		HYDROGRAPH Next link "
"	150.000 Impervious length"			"	5	Next link "
"	2.500 Impervious slope"			"	0.249	0.248 0.248 2.186"
"	0.200 Pervious Manning 'n'"			"	33	CATCHMENT 402"
"	82.000 Pervious SCS Curve No."			"	1	Triangular SCS"
"	0.441 Pervious Runoff coefficient"			"	1	Equal length"
"	0.100 Pervious Ia/S coefficient"			"	1	SCS method"
"	5.576 Pervious Initial abstraction"			"	402	No description"
"	0.015 Impervious Manning 'n'"			"	0.000	% Impervious"
"	98.000 Impervious SCS Curve No."			"	4.200	Total Area"
"	0.000 Impervious Runoff coefficient"			"	80.000	Flow length"
"	0.100 Impervious Ia/S coefficient"			"	4.000	Overland Slope"
"	0.518 Impervious Initial abstraction"			"	4.200	Pervious Area "
"	0.318 1.880 1.880 41.653 c.m/sec"			"	80.000	Pervious length"
"	Catchment 304 Pervious Impervious Total Area "			"	4.000	Pervious slope"
"	Surface Area 6.300 0.000 6.300 hectare"			"	0.000	Impervious Area "
"	Time of concentration 42.514 7.487 42.514 minutes"			"	80.000	Impervious length"
"	Time to Centroid 277.466 212.080 277.465 minutes"			"	4.000	Impervious slope"
"	Rainfall depth 58.700 58.700 58.700 mm"			"	0.200	Pervious Manning 'n'"
"	Rainfall volume 3698.10 0.00 3698.10 c.m"			"	82.000	Pervious SCS Curve No."
"	Rainfall losses 32.788 5.527 32.788 mm"			"	0.441	Pervious Runoff coefficient"
"	Runoff depth 25.912 53.173 25.912 mm"			"	0.100	Pervious Ia/S coefficient"
"	Runoff volume 1632.48 0.00 1632.48 c.m"			"	5.576	Pervious Initial abstraction"
"	Runoff coefficient 0.441 0.000 0.441 "			"	0.015	Impervious Manning 'n'"
"	Maximum flow 0.318 0.000 0.318 c.m/sec"			"	98.000	Impervious SCS Curve No."
"	HYDROGRAPH Add Runoff "			"	0.000	Impervious Runoff coefficient"
"	4 Add Runoff "			"	0.100	Impervious Ia/S coefficient"
"	0.318 2.192 1.880 41.653"			"	0.518	Impervious Initial abstraction"
"	CHANNEL DESIGN"			"	0.285	0.248 0.248 2.186 c.m/sec"
"	2.192 Current peak flow c.m/sec"			"		Catchment 402 Pervious Impervious Total Area "
"	0.040 Manning 'n'"			"		


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" Rainfall volume 1467.50 0.00 1467.50 c.m"
" Rainfall losses 32.796 5.719 32.796 mm"
" Runoff depth 25.904 52.981 25.904 mm"
" Runoff volume 647.59 0.00 647.59 c.m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 0.166 0.000 0.166 c.m/sec"
" HYDROGRAPH Add Runoff "
40 4 Add Runoff " 0.166 0.166 0.991 3.123"
" CHANNEL DESIGN"
52 0.166 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
" Depth of flow 0.118 metre"
" Velocity 0.596 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.085 metre"
53 ROUTE Channel Route 120"
120.00 Channel Route 120 Reach length (metre)"
0.476 X-factor <= 0.5"
151.120 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
150.000 Routing time step (seconds)"
1 No. of sub-reaches"
" Peak outflow 0.163 c.m/sec"
" 0.166 0.166 0.163 3.123 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 0.166 0.163 0.163 3.123"
33 CATCHMENT 502"
1 Triangular SCS"
1 Equal length"
1 SCS method"
502 No description"
0.000 % Impervious"
0.500 Total Area"
120.000 Flow length"
3.500 Overland Slope"
0.500 Pervious Area"
120.000 Pervious length"
3.500 Pervious slope"
0.000 Impervious Area"
120.000 Impervious length"
3.500 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.441 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
" 0.029 0.163 0.163 3.123 c.m/sec"
" Catchment 502 Pervious Impervious Total Area "
" Surface Area 0.500 0.000 0.500 hectare"
" Time of concentration 33.616 5.920 33.616 minutes"
" Time to Centroid 266.712 210.082 266.712 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 293.50 0.00 293.50 c.m"
" Rainfall losses 32.794 5.672 32.794 mm"
" Runoff depth 25.906 53.028 25.906 mm"
" Runoff volume 129.53 0.00 129.53 c.m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 0.029 0.000 0.029 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.029 0.192 0.163 3.123"
52 CHANNEL DESIGN"
0.192 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
" Depth of flow 0.129 metre"
" Velocity 0.625 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.093 metre"
53 ROUTE Channel Route 170"
170.00 Channel Route 170 Reach length (metre)"
0.482 X-factor <= 0.5"
203.887 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
150.000 Routing time step (seconds)"
1 No. of sub-reaches"
" Peak outflow 0.191 c.m/sec"
" 0.029 0.192 0.191 3.123 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 0.029 0.191 0.191 3.123"
33 CATCHMENT 503"
1 Triangular SCS"
1 Equal length"
1 SCS method"
503 No description"
0.000 % Impervious"
8.200 Total Area"
90.000 Flow length"
5.000 Overland Slope"
8.200 Pervious Area"
90.000 Pervious length"
5.000 Pervious slope"
0.000 Impervious Area"
90.000 Impervious length"
5.000 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.441 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
" 0.237 0.724 0.724 3.123 c.m/sec"
" Catchment 504 Pervious Impervious Total Area "
" Surface Area 3.900 0.000 3.900 hectare"
" Time of concentration 31.292 5.511 31.291 minutes"
" Time to Centroid 263.911 209.620 263.911 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2289.30 0.00 2289.30 c.m"
" Rainfall losses 32.798 5.421 32.798 mm"
" Runoff depth 25.902 53.279 25.902 mm"
" Runoff volume 1010.18 0.00 1010.18 c.m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 0.237 0.000 0.237 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.237 0.962 0.724 3.123"
52 CHANNEL DESIGN"
0.962 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
" Depth of flow 0.315 metre"
" Velocity 1.036 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.251 metre"
53 ROUTE Channel Route 140"
140.00 Channel Route 140 Reach length (metre)"
0.450 X-factor <= 0.5"
101.385 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
100.000 Routing time step (seconds)"
1 No. of sub-reaches"
" Peak outflow 0.946 c.m/sec"
" 0.237 0.962 0.946 3.123 c.m/sec"
40 HYDROGRAPH Combine 2200"
6 Combine "
2200 Node #
" Node taking 500 series - dumps into Hwy 21 Ditch"
" Maximum flow 0.946 c.m/sec"
" Hydrograph volume 3910.304 c.m"
" 0.237 0.962 0.946 0.946"
40 HYDROGRAPH Confluence 2200"
7 Confluence "
2200 Node #
" Node taking 500 series - dumps into Hwy 21 Ditch"
" Maximum flow 0.946 c.m/sec"
" Hydrograph volume 3910.304 c.m"
" 0.237 0.946 0.946 0.000"
52 CHANNEL DESIGN"
0.946 Current peak flow c.m/sec"

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"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.394 metre"
"      Velocity 0.755 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.249 metre"
" 53 ROUTE Channel Route 300"
"      300.00 Channel Route 300 Reach length (metre)"
"      0.431 X-factor <= 0.5"
" 298.067 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.941 c.m/sec"
"      0.237 0.946 0.941 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
"      6 Combine "
"      2000 Node #"
"      Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
"      Maximum flow 4.052 c.m/sec"
"      Hydrograph volume 18987.176 c.m"
"      0.237 0.946 0.941 4.052"
" 40 HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.237 0.000 0.941 4.052"
" 33 CATCHMENT 603"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      603 No description"
"      0.000 % Impervious"
"      5.600 Total Area"
"      100.000 Flow length"
"      2.500 Overland Slope"
"      5.600 Pervious Area"
"      100.000 Pervious length"
"      2.500 Pervious slope"
"      0.000 Impervious Area"
"      100.000 Impervious length"
"      2.500 Impervious slope"
"      0.200 Pervious Manning 'n'"
"      82.000 Pervious SCS Curve No."
"      0.441 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.576 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.000 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.329 0.000 0.941 4.052 c.m/sec"
"      Catchment 603 Pervious Impervious Total Area "
"      Surface Area 5.600 0.000 5.600 hectare"
"      Time of concentration 33.334 5.870 33.333 minutes"
"      Time to Centroid 266.365 210.016 266.365 minutes"
"      Rainfall depth 58.700 58.700 58.700 mm"
"      Rainfall volume 3287.20 0.00 3287.20 c.m"
"      Rainfall losses 32.795 5.642 32.795 mm"
"      Runoff depth 25.905 53.058 25.905 mm"
"      Runoff volume 1450.69 0.00 1450.69 c.m"
"      Runoff coefficient 0.441 0.000 0.441 "
"      Maximum flow 0.329 0.000 0.329 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.329 0.329 0.941 4.052"
" 52 CHANNEL DESIGN"
"      0.329 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      1.200 Gradient %"
"      Depth of flow 0.175 metre"
"      Velocity 0.746 m/sec"
"      Channel capacity 431.989 c.m/sec"
"      Critical depth 0.131 metre"
" 53 ROUTE Channel Route 260"
"      260.00 Channel Route 260 Reach length (metre)"
"      0.484 X-factor <= 0.5"
" 261.509 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.326 c.m/sec"
"      0.329 0.329 0.326 4.052 c.m/sec"
" 40 HYDROGRAPH Next link "
"      5 Next link "
"      0.329 0.326 0.326 4.052"
" 33 CATCHMENT 605"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      605 No description"
"      0.000 % Impervious"
"      3.400 Total Area"
"      100.000 Flow length"
"      2.500 Overland Slope"
"      3.400 Pervious Area"
"      100.000 Pervious length"
"      2.500 Pervious slope"
"      0.000 Impervious Area"
"      100.000 Impervious length"
"      2.500 Impervious slope"
"      0.200 Pervious Manning 'n'"
"      82.000 Pervious SCS Curve No."
"      0.441 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.576 Pervious Initial abstraction"
"      0.015 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.000 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.200 0.326 0.326 4.052 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
"      Surface Area 3.400 0.000 3.400 hectare"
"      Time of concentration 33.334 5.870 33.333 minutes"
"      Time to Centroid 266.365 210.016 266.365 minutes"
"      Rainfall depth 58.700 58.700 58.700 mm"
"      Rainfall volume 1995.80 0.00 1995.80 c.m"
"      Rainfall losses 32.795 5.642 32.795 mm"
"      Runoff depth 25.905 53.058 25.905 mm"
"      Runoff volume 880.77 0.00 880.78 c.m"
"      Runoff coefficient 0.441 0.000 0.441 "
"      Maximum flow 0.200 0.000 0.200 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.200 0.518 0.326 4.052"
" CHANNEL DESIGN"
"      0.518 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      1.200 Gradient %"
"      Depth of flow 0.225 metre"
"      Velocity 0.860 m/sec"
"      Channel capacity 431.989 c.m/sec"
"      Critical depth 0.173 metre"
" 53 ROUTE Channel Route 170"
"      170.00 Channel Route 170 Reach length (metre)"
"      0.470 X-factor <= 0.5"
" 148.278 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.517 c.m/sec"
"      0.200 0.518 0.517 4.052 c.m/sec"
" 40 HYDROGRAPH Combine 2300"
"      6 Combine "
"      2300 Node #"
"      Node taking 600 series - dumps into Hwy 21 Ditch"
"      Maximum flow 0.517 c.m/sec"
"      Hydrograph volume 2331.466 c.m"
"      0.200 0.518 0.517 0.517"
" 40 HYDROGRAPH Confluence 2300"
"      7 Confluence "
"      2300 Node #"
"      Node taking 600 series - dumps into Hwy 21 Ditch"
"      Maximum flow 0.517 c.m/sec"
"      Hydrograph volume 2331.466 c.m"
"      0.200 0.517 0.517 0.000"
" 52 CHANNEL DESIGN"
"      0.517 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.286 metre"
"      Velocity 0.633 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.173 metre"
" 53 ROUTE Channel Route 650"
"      650.00 Channel Route 650 Reach length (metre)"
"      0.429 X-factor <= 0.5"
" 256.589 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
"      3 No. of sub-reaches"
"      Peak outflow 0.509 c.m/sec"
"      0.200 0.517 0.509 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
"      6 Combine "
"      2000 Node #"
"      Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
"      Maximum flow 4.518 c.m/sec"
"      Hydrograph volume 21318.639 c.m"
"      0.200 0.517 0.509 4.518"
" 81 ADD COMMENT"
"      1 Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
"      HYDROGRAPH Confluence 2000"
"      7 Confluence "
"      2000 Node #"
"      Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
"      Maximum flow 4.518 c.m/sec"
"      Hydrograph volume 21318.639 c.m"
"      0.200 4.518 0.509 0.000"
" 81 ADD COMMENT"
"      1 Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
" 52 CHANNEL DESIGN"
"      4.518 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.857 metre"
"      Velocity 1.154 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.597 metre"
" 53 ROUTE Channel Route 50"
"      50.00 Channel Route 50 Reach length (metre)"
"      0.000 X-factor <= 0.5"
" 32.486 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.634 Beta weighting factor"
" 75.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 4.510 c.m/sec"
"      0.200 4.518 4.510 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
"      6 Combine "
"      3000 Node #"
"      Node Combining All Flow"

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```

"      Maximum flow           43.024   c.m/sec"
"      Hydrograph volume      462284.031 c.m"
"      0.200   4.518   4.510   43.024"
" 81  ADD COMMENT=====
"      1  Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40  HYDROGRAPH Confluence 3000"
"      7  Confluence "
"      3000 Node #"
"      Node Combining All Flow"
"      Maximum flow           43.024   c.m/sec"
"      Hydrograph volume      462284.063 c.m"
"      0.200   43.024   4.510   0.000"
" 81  ADD COMMENT=====
"      1  Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 38  START/RE-START TOTALS 3000"
"      1  Runoff Totals turned OFF"
"      Catchment area to node 3000           1918.900  hectare"
"      Impervious area to node 3000           0.002  hectare"
"      % impervious to node 3000             0.000"
"      Peak runoff to node 3000              0.000  c.m/sec"
"      Total volume to node 3000             0.0  c.m"

```

PRE-EXISTING 25 YEAR

MIDUSS Output ----->
MIDUSS version Version 2.25 rev. 465
MIDUSS created Tuesday, February 05, 2008
Units used: ie METRIC
Job folder: C:\Users\derb\Desktop\Kincardine Miduss\
Output filename: 08055 - Pre-Existing 25 Year.out
Licensee name: EliteBook
Company: BMROSS
Date & Time last used: 7/19/2011 at 4:10:16 PM
TIME PARAMETERS
5.000 Time Step
360.000 Max. Storm length
1800.000 Max. Hydrograph
STORM Mass Curve
3 Mass Curve
86.100 Rainfall depth
360.000 Duration
C:\Program Files\MIDUSS\SCS_6hr_Type2.mrd SCS Type II - 6 hour
Distribution - Ontario
Maximum intensity 67.158 mm/hr
Total depth 86.100 mm
6 025hyd Hydrograph extension used in this file
ADD COMMENT
1 Lines of comment
Start of Penetangore Tributary
CATCHMENT 50
1 Triangular SCS
1 Equal length
1 SCS method
50 No description
0.000 % Impervious
396.000 Total Area
450.000 Flow length
2.500 Overland Slope
396.000 Pervious Area
450.000 Pervious length
2.500 Pervious slope
0.000 Impervious Area
450.000 Impervious length
2.500 Impervious slope
0.250 Pervious Manning 'n'
81.000 Pervious SCS Curve No.
0.534 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.958 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
23.637 0.000 0.000 0.000 c.m/sec
Catchment 50 Pervious Impervious Total Area
Surface Area 396.000 0.000 396.000 hectare
Time of concentration 75.983 11.366 75.983 minutes
Time to Centroid 314.049 214.390 314.049 minutes
Rainfall depth 86.100 86.100 86.100 mm
Rainfall volume 34.0956 0.0000 34.0956 ha-m
Rainfall losses 40.137 5.520 40.137 mm
Runoff depth 45.963 80.580 45.963 mm
Runoff volume 18.2015 0.0000 18.2015 ha-m
Runoff coefficient 0.534 0.000 0.534
Maximum flow 23.637 0.000 23.637 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
23.637 23.637 0.000 0.000
CHANNEL DESIGN
23.637 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.500 Gradient %
Depth of flow 1.805 metre
Velocity 1.765 m/sec
Channel capacity 278.848 c.m/sec
Critical depth 1.368 metre
ROUTE Channel Route 3000
3000.00 Channel Route 3000 Reach length (metre)
0.396 X-factor <= 0.5
318.652 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
4 No. of sub-reaches
Peak outflow 23.348 c.m/sec
23.637 23.637 23.348 0.000 c.m/sec
HYDROGRAPH Next link
5 Next link
23.637 23.348 23.348 0.000
CATCHMENT 52
1 Triangular SCS
1 Equal length
1 SCS method
52 No description
0.000 % Impervious
196.000 Total Area
250.000 Flow length
7.000 Overland Slope
196.000 Pervious Area
250.000 Pervious length
7.000 Pervious slope
0.000 Impervious Area
250.000 Impervious length
7.000 Impervious slope
0.250 Pervious Manning 'n'
80.000 Pervious SCS Curve No.
0.515 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
6.350 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
18.017 23.348 23.348 0.000 c.m/sec
Catchment 52 Pervious Impervious Total Area
Surface Area 196.000 0.000 196.000 hectare
Time of concentration 39.626 5.865 39.626 minutes
Time to Centroid 270.855 207.757 270.855 minutes

Rainfall depth 86.100 86.100 86.100 mm
Rainfall volume 16.8756 0.0000 16.8756 ha-m
Rainfall losses 41.715 5.922 41.715 mm
Runoff depth 44.385 80.178 44.385 mm
Runoff volume 8.6994 0.0000 8.6994 ha-m
Runoff coefficient 0.515 0.000 0.516
Maximum flow 18.017 0.000 18.017 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
18.017 29.299 23.348 0.000
CHANNEL DESIGN
29.299 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.400 Gradient %
Depth of flow 2.076 metre
Velocity 1.715 m/sec
Channel capacity 249.409 c.m/sec
Critical depth 1.513 metre
ROUTE Channel Route 1300
1300.00 Channel Route 1300 Reach length (metre)
0.330 X-factor <= 0.5
284.328 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
2 No. of sub-reaches
Peak outflow 29.196 c.m/sec
18.017 29.299 29.196 0.000 c.m/sec
HYDROGRAPH Next link
5 Next link
18.017 29.196 29.196 0.000
CATCHMENT 54
1 Triangular SCS
1 Equal length
1 SCS method
54 No description
0.000 % Impervious
39.000 Total Area
140.000 Flow length
11.000 Overland Slope
39.000 Pervious Area
140.000 Pervious length
11.000 Pervious slope
0.000 Impervious Area
140.000 Impervious length
11.000 Impervious slope
0.210 Pervious Manning 'n'
81.000 Pervious SCS Curve No.
0.533 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.958 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
4.989 29.196 29.196 0.000 c.m/sec
Catchment 54 Pervious Impervious Total Area
Surface Area 39.000 0.000 39.000 hectare
Time of concentration 21.777 3.617 21.777 minutes
Time to Centroid 248.526 204.957 248.526 minutes
Rainfall depth 86.100 86.100 86.100 mm
Rainfall volume 3.3579 0.0000 3.3579 ha-m
Rainfall losses 40.195 7.671 40.195 mm
Runoff depth 45.905 78.429 45.905 mm
Runoff volume 1.7903 0.0000 1.7903 ha-m
Runoff coefficient 0.533 0.000 0.533
Maximum flow 4.989 0.000 4.989 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
4.989 30.131 29.196 0.000
CHANNEL DESIGN
30.131 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.400 Gradient %
Depth of flow 2.101 metre
Velocity 1.727 m/sec
Channel capacity 249.409 c.m/sec
Critical depth 1.533 metre
ROUTE Channel Route 800
800.00 Channel Route 800 Reach length (metre)
0.360 X-factor <= 0.5
347.479 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
1 No. of sub-reaches
Peak outflow 30.050 c.m/sec
4.989 30.131 30.050 0.000 c.m/sec
HYDROGRAPH Combine
6 Combine
10 Node #
Confluence on Penetangore Tributary
Maximum flow 30.050 c.m/sec
Hydrograph volume 286911.781 c.m
4.989 30.131 30.050 30.050
HYDROGRAPH Start - New Tributary
2 Start - New Tributary
4.989 0.000 30.050 30.050
CATCHMENT 60
1 Triangular SCS
1 Equal length
1 SCS method
60 No description
0.000 % Impervious
225.000 Total Area
270.000 Flow length
2.500 Overland Slope
225.000 Pervious Area
270.000 Pervious length
2.500 Pervious slope
0.000 Impervious Area
270.000 Impervious length

2.500	Impervious slope"				Surface Area	95.000	0.000	95.000	hectare"
0.230	Pervious Manning 'n'"				Time of concentration	41.289	6.112	41.289	minutes"
81.000	Pervious SCS Curve No."				Time to Centroid	272.861	208.104	272.861	minutes"
0.534	Pervious Runoff coefficient"				Rainfall depth	86.100	86.100	86.100	mm"
0.100	Pervious Ia/S coefficient"				Rainfall volume	8.1795	0.0000	8.1795	ha-m"
5.958	Pervious Initial abstraction"				Rainfall losses	41.720	6.094	41.720	mm"
0.013	Impervious Manning 'n'"				Runoff depth	44.380	80.006	44.380	mm"
98.000	Impervious SCS Curve No."				Runoff volume	4.2161	0.0000	4.2161	ha-m"
0.000	Impervious Runoff coefficient"				Runoff coefficient	0.515	0.000	0.515	"
0.100	Impervious Ia/S coefficient"				Maximum flow	8.472	0.000	8.472	c.m/sec"
0.518	Impervious Initial abstraction"				HYDROGRAPH Add Runoff "				
	17.615	0.000	30.050	30.050 c.m/sec"	4 Add Runoff "				
	Catchment 60	Pervious	Impervious Total Area "			8.472	44.774	44.774"	
	Surface Area	225.000	0.000	225.000	hectare"				
	Time of concentration	53.196	8.366	53.196	minutes"	52			CHANNEL DESIGN"
	Time to Centroid	286.501	210.824	286.501	minutes"		8.472		Current peak flow
	Rainfall depth	86.100	86.100	86.100	mm"				c.m/sec"
	Rainfall volume	19.3725	0.0000	19.3725	ha-m"		0.040		Manning 'n'"
	Rainfall losses	40.141	5.535	40.141	mm"				0. Cross-section type: 0=trapezoidal; 1=general"
	Runoff depth	45.959	80.565	45.959	mm"		2.000		Basewidth
	Runoff volume	10.3407	0.0000	10.3407	ha-m"				Left bank slope"
	Runoff coefficient	0.534	0.000	0.534	"				Right bank slope"
	Maximum flow	17.615	0.000	17.615	c.m/sec"				Channel depth
	HYDROGRAPH Add Runoff "						5.000		metre"
	4 Add Runoff "								0.300
		17.615	17.615	30.050	c.m/sec"				Gradient
	CHANNEL DESIGN"								%"
	17.615	Current peak flow	c.m/sec"						Depth of flow
	0.040	Manning 'n'"							Velocity
	0. Cross-section type: 0=trapezoidal; 1=general"								Channel capacity
	2.000	Basewidth	metre"						Channel capacity
	3.000	Left bank slope"							249.409
	3.000	Right bank slope"							c.m/sec"
	5.000	Channel depth	metre"						Critical depth
	0.400	Gradient	%"						1.188
		Depth of flow	1.668	metre"					metre"
		Velocity	1.508	m/sec"					m/sec"
		Channel capacity	249.409	c.m/sec"					c.m/sec"
		Critical depth	1.188	metre"					metre"
	53	ROUTE	Channel Route 1800"						
	1800.00	Channel Route 1800	Reach length	(metre)"					
	0.349	X-factor <= 0.5"							
	298.497	K-lag	(seconds)"						
	0.000	Default(0) or user spec.(1) values used"							
	0.500	X-factor <= 0.5"							
	30.000	K-lag	(seconds)"						
	0.500	Beta weighting factor"							
	300.000	Routing time step	(seconds)"						
	3	No. of sub-reaches"							
		Peak outflow	17.265	c.m/sec"					
			17.615	17.615	17.265	30.050 c.m/sec"			
	40	HYDROGRAPH	Combine	10"					
		6	Combine	"					
		10	Node	#"					
			Confluence on Penatangore Tributary"						
			Maximum flow	45.035	c.m/sec"				
			Hydrograph volume	390319.781	c.m"				
				17.615	17.615	17.265	45.035"		
		40	HYDROGRAPH	Confluence	10"				
			7	Confluence	"				
			10	Node	#"				
			Confluence on Penatangore Tributary"						
			Maximum flow	45.035	c.m/sec"				
			Hydrograph volume	390319.781	c.m"				
				17.615	45.035	17.265	0.000"		
		52	CHANNEL DESIGN"						
			45.035	Current peak flow	c.m/sec"				
			0.040	Manning 'n'"					
			0. Cross-section type: 0=trapezoidal; 1=general"						
			2.000	Basewidth	metre"				
			3.000	Left bank slope"					
			3.000	Right bank slope"					
			5.000	Channel depth	metre"				
			0.400	Gradient	%"				
				Depth of flow	2.489	metre"			
				Velocity	1.911	m/sec"			
				Channel capacity	249.409	c.m/sec"			
				Critical depth	1.847	metre"			
		53	ROUTE	Channel Route 2000"					
			2000.00	Channel Route 2000	Reach length	(metre)"			
			0.370	X-factor <= 0.5"					
			392.542	K-lag	(seconds)"				
			0.000	Default(0) or user spec.(1) values used"					
			0.500	X-factor <= 0.5"					
			30.000	K-lag	(seconds)"				
			0.500	Beta weighting factor"					
			300.000	Routing time step	(seconds)"				
			2	No. of sub-reaches"					
				Peak outflow	44.774	c.m/sec"			
					17.615	45.035	44.774	0.000 c.m/sec"	
		40	HYDROGRAPH	Combine	11"				
			6	Combine	"				
			11	Node	#"				
			Confluence on Penatangore Tributary"						
			Maximum flow	44.774	c.m/sec"				
			Hydrograph volume	390319.656	c.m"				
				17.615	45.035	44.774	44.774"		
		40	HYDROGRAPH	Start - New Tributary"					
			2	Start - New Tributary"					
					17.615	0.000	44.774	44.774"	
		33	CATCHMENT 62"						
			1	Triangular SCS"					
			1	Equal length"					
			1	SCS method"					
			62	No description"					
			0.000	% Impervious"					
			95.000	Total Area"					
			160.000	Flow length"					
			2.500	Overland Slope"					
			95.000	Pervious Area"					
			160.000	Pervious length"					
			2.500	Pervious slope"					
			0.000	Impervious Area"					
			160.000	Impervious length"					
			2.500	Impervious slope"					
			0.250	Pervious Manning 'n'"					
			80.000	Pervious SCS Curve No."					
			0.515	Pervious Runoff coefficient"					
			0.100	Pervious Ia/S coefficient"					
			6.350	Pervious Initial abstraction"					
			0.013	Impervious Manning 'n'"					
			98.000	Impervious SCS Curve No."					
			0.000	Impervious Runoff coefficient"					
			0.100	Impervious Ia/S coefficient"					
			0.518	Impervious Initial abstraction"					
					8.472	0.000	44.774	44.774 c.m/sec"	
			Catchment 62	Pervious	Impervious Total Area "				

```

" 52 CHANNEL DESIGN "
70.381 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 2.862 metre"
Velocity 2.324 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 2.263 metre"
" 53 ROUTE Channel Route 1300"
1300.00 Channel Route 1300 Reach length ( metre)"
0.318 X-factor <= 0.5"
209.797 K-lag ( seconds)"
0.000 Default (0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
2 No. of sub-reaches"
Peak outflow 70.253 c.m/sec"
32.068 70.381 70.253 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penetangore Tributary"
Maximum flow 70.253 c.m/sec"
Hydrograph volume 580320.063 c.m"
32.068 70.381 70.253 70.253"
" 40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
32.068 0.000 70.253 70.253"
" 33 CATCHMENT 58"
1 Triangular SCS"
1 Equal length"
1 SCS method"
58 No description"
0.000 % Impervious"
82.000 Total Area"
140.000 Flow length"
15.000 Overland Slope"
82.000 Pervious Area"
140.000 Pervious length"
15.000 Pervious slope"
0.000 Impervious Area"
140.000 Impervious length"
15.000 Impervious slope"
0.230 Pervious Manning 'n'"
81.000 Pervious SCS Curve No."
0.533 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.958 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
10.634 0.000 70.253 70.253 c.m/sec"
Catchment 58 Pervious Impervious Total Area "
Surface Area 82.000 0.000 82.000 hectare"
Time of concentration 20.955 3.295 20.955 minutes"
Time to Centroid 247.521 204.757 247.521 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 7.0602 0.0000 7.0602 ha-m"
Rainfall losses 40.178 7.017 40.178 mm"
Runoff depth 45.922 79.083 45.922 mm"
Runoff volume 3.7656 0.0000 3.7656 ha-m"
Runoff coefficient 0.533 0.000 0.533 "
Maximum flow 10.634 0.000 10.634 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
4 Add Runoff "
10.634 10.634 70.253 70.253"
" 52 CHANNEL DESIGN"
10.634 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.270 metre"
Velocity 1.441 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.927 metre"
" 53 ROUTE Channel Route 700"
700.00 Channel Route 700 Reach length ( metre)"
0.337 X-factor <= 0.5"
182.217 K-lag ( seconds)"
0.000 Default (0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
2 No. of sub-reaches"
Peak outflow 10.392 c.m/sec"
10.634 10.634 10.392 70.253 c.m/sec"
" 40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penetangore Tributary"
Maximum flow 72.784 c.m/sec"
Hydrograph volume 617975.438 c.m"
10.634 10.634 10.392 72.784"
" 40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
10.634 0.000 10.392 72.784"
" 33 CATCHMENT 64"
1 Triangular SCS"
1 Equal length"
1 SCS method"
64 No description"
0.000 % Impervious"
80.000 Total Area"
220.000 Flow length"
5.500 Overland Slope"
80.000 Pervious Area"
220.000 Pervious length"
5.500 Pervious slope"
0.000 Impervious Area"
220.000 Impervious length"
5.500 Impervious slope"
0.210 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 8.580 0.000 10.392 72.784 c.m/sec"
" Catchment 64 Pervious Impervious Total Area "
" Surface Area 80.000 0.000 80.000 hectare"
" Time of concentration 34.803 5.840 34.803 minutes"
" Time to Centroid 263.478 207.720 263.478 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 6.8880 0.0000 6.8880 ha-m"
" Rainfall losses 38.551 5.897 38.551 mm"
" Runoff depth 47.549 80.203 47.549 mm"
" Runoff volume 3.8039 0.0000 3.8039 ha-m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 8.580 0.000 8.580 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 8.580 8.580 10.392 72.784"
" 52 CHANNEL DESIGN"
8.580 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.153 metre"
Velocity 1.363 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.833 metre"
" 53 ROUTE Channel Route 700"
700.00 Channel Route 700 Reach length ( metre)"
0.350 X-factor <= 0.5"
192.537 K-lag ( seconds)"
0.000 Default (0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
2 No. of sub-reaches"
Peak outflow 8.497 c.m/sec"
8.580 8.580 8.497 72.784 c.m/sec"
" 40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penetangore Tributary"
Maximum flow 76.961 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 8.580 8.497 76.961"
" 40 HYDROGRAPH Confluence 12"
7 Confluence "
12 Node #"
Confluence on Penetangore Tributary"
Maximum flow 76.961 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 8.497 8.497 0.000"
" 52 CHANNEL DESIGN"
76.961 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.300 Gradient %"
Depth of flow 3.297 metre"
Velocity 1.963 m/sec"
Channel capacity 215.995 c.m/sec"
Critical depth 2.356 metre"
" 53 ROUTE Channel Route 2500"
2500.00 Channel Route 2500 Reach length ( metre)"
0.230 X-factor <= 0.5"
318.467 K-lag ( seconds)"
0.000 Default (0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
3 No. of sub-reaches"
Peak outflow 75.678 c.m/sec"
8.580 76.961 75.678 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1000"
6 Combine "
1000 Node #"
Node upstream of Penetangore Culvert"
Maximum flow 75.678 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 76.961 75.678 75.678"
" 40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
8.580 0.000 75.678 75.678"
" 33 CATCHMENT 59"
1 Triangular SCS"
1 Equal length"
1 SCS method"
59 No description"
0.000 % Impervious"
128.000 Total Area"
170.000 Flow length"
18.000 Overland Slope"
128.000 Pervious Area"
170.000 Pervious length"
18.000 Pervious slope"
0.000 Impervious Area"
170.000 Impervious length"
18.000 Impervious slope"
0.350 Pervious Manning 'n'"
76.000 Pervious SCS Curve No."
0.447 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
8.021 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
11.726 0.000 75.678 75.678 c.m/sec"
Catchment 59 Pervious Impervious Total Area "
Surface Area 128.000 0.000 128.000 hectare"
Time of concentration 30.299 3.505 30.299 minutes"
Time to Centroid 262.475 204.855 262.475 minutes"

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"	Rainfall depth	86.100	86.100	86.100	mm"	"	4.000	Overland Slope"	"					
"	Rainfall volume	11.0208	0.0000	11.0208	ha-m"	"	8.000	Pervious Area"	"					
"	Rainfall losses	47.606	7.396	47.606	mm"	"	225.000	Pervious length"	"					
"	Runoff depth	38.494	78.704	38.494	mm"	"	4.000	Pervious slope"	"					
"	Runoff volume	4.9273	0.0000	4.9273	ha-m"	"	0.000	Impervious Area"	"					
"	Runoff coefficient	0.447	0.000	0.447	"	"	225.000	Impervious length"	"					
"	Maximum flow	11.726	0.000	11.726	c.m/sec"	"	4.000	Impervious slope"	"					
"	HYDROGRAPH Add Runoff "					"	0.206	Pervious Manning 'n'"	"					
"	4 Add Runoff "					"	82.000	Pervious SCS Curve No."	"					
"	11.726	11.726	75.678	75.678"		"	0.552	Pervious Runoff coefficient"	"					
"	52 CHANNEL DESIGN"					"	0.100	Pervious Ia/S coefficient"	"					
"	11.726	Current peak flow	c.m/sec"			"	5.576	Pervious Initial abstraction"	"					
"	0.040	Manning 'n'"				"	0.013	Impervious Manning 'n'"	"					
"	0.	Cross-section type: 0=trapezoidal; 1=general"				"	98.000	Impervious SCS Curve No."	"					
"	2.000	Basewidth	metre"			"	0.000	Impervious Runoff coefficient"	"					
"	3.000	Left bank slope"				"	0.100	Impervious Ia/S coefficient"	"					
"	3.000	Right bank slope"				"	0.518	Impervious Initial abstraction"	"					
"	5.000	Channel depth	metre"			"	0.817	15.353	15.353	79.914	c.m/sec"			
"	0.300	Gradient	%"			"					Impervious Total Area "			
"		Depth of flow	1.487	metre"		"		8.000	0.000	8.000	hectare"			
"		Velocity	1.221	m/sec"		"		37.692	6.513	37.692	minutes"			
"		Channel capacity	215.995	c.m/sec"		"		266.978	208.591	266.978	minutes"			
"		Critical depth	0.973	metre"		"		86.100	86.100	86.100	mm"			
"	53 ROUTE Channel Route 1500"					"		6887.99	0.01	6888.00	c.m"			
"	1500.00	Channel Route 1500 Reach length	(metre)"			"		38.542	6.520	38.542	mm"			
"	0.281	X-factor <= 0.5"				"		47.558	79.580	47.558	mm"			
"	307.084	K-lag (seconds)"				"		3804.65	0.01	3804.66	c.m"			
"	0.000	Default(0) or user spec.(1) values used"				"		0.552	0.000	0.552	"			
"	0.500	X-factor <= 0.5"				"		0.817	0.000	0.817	c.m/sec"			
"	30.000	K-lag (seconds)"				"	40	HYDROGRAPH Add Runoff "			"			
"	0.500	Beta weighting factor"				"	4	Add Runoff "			"			
"	300.000	Routing time step (seconds)"				"		0.817	16.018	15.353	79.914"			
"	3	No. of sub-reaches"				"	52	CHANNEL DESIGN"			"			
"		Peak outflow	11.131	c.m/sec"		"	16.018	Current peak flow	c.m/sec"		"			
"		11.726	11.726	11.131	75.678 c.m/sec"		0.040	Manning 'n'"			"			
"	40 HYDROGRAPH Combine 1000"					"	0.	Cross-section type: 0=trapezoidal; 1=general"			"			
"	1000	Combine "				"	2.000	Basewidth	metre"		"			
"		Node #"				"	3.000	Left bank slope"			"			
"		Node upstream of Penatangore Culvert"				"	3.000	Right bank slope"			"			
"		Maximum flow	79.914	c.m/sec"		"	5.000	Channel depth	metre"		"			
"		Hydrograph volume	705287.563	c.m"		"	1.000	Gradient	%"		"			
"		11.726	11.726	11.131	79.914"						Depth of flow	1.307	metre"	
"	81	ADD COMMENT-----				"					Velocity	2.070	m/sec"	
"	1	Lines of comment"				"					Channel capacity	394.351	c.m/sec"	
"		End of Penatangore Tributary"				"					Critical depth	1.134	metre"	
"	81	ADD COMMENT-----				"	53	ROUTE Channel Route 260"			"			
"	1	Lines of comment"				"	260.00	Channel Route 260 Reach length	(metre)"					
"		Start of Area North of Holtby Drain"				"	0.387	X-factor <= 0.5"						
"	40 HYDROGRAPH Start - New Tributary"					"	94.181	K-lag (seconds)"						
"	2	Start - New Tributary"				"	0.000	Default(0) or user spec.(1) values used"						
"		11.726	0.000	11.131	79.914"		0.500	X-factor <= 0.5"						
"	33	CATCHMENT 201"				"	30.000	K-lag (seconds)"						
"	1	Triangular SCS"				"	0.500	Beta weighting factor"						
"	1	Equal length"				"	100.000	Routing time step (seconds)"						
"	1	SCS method"				"	1	No. of sub-reaches"						
"	201	No description"				"		Peak outflow	15.936	c.m/sec"				
"	0.000	% Impervious"				"		0.817	16.018	15.936	79.914	c.m/sec"		
"	166.000	Total Area"				"	40	HYDROGRAPH Next link "						
"	250.000	Flow length"				"	5	Next link "						
"	3.000	Overland Slope"				"		0.817	15.936	15.936	79.914"			
"	166.000	Pervious Area"				"	33	CATCHMENT 203"						
"	250.000	Pervious length"				"	1	Triangular SCS"						
"	3.000	Pervious slope"				"	1	Equal length"						
"	0.000	Impervious Area"				"	1	SCS method"						
"	250.000	Impervious length"				"		203	No description"					
"	3.000	Impervious slope"				"		0.000	% Impervious"					
"	0.200	Pervious Manning 'n'"				"		13.600	Total Area"					
"	82.000	Pervious SCS Curve No."				"		150.000	Flow length"					
"	0.552	Pervious Runoff coefficient"				"		3.500	Overland Slope"					
"	0.100	Pervious Ia/S coefficient"				"		13.600	Pervious Area"					
"	5.576	Pervious Initial abstraction"				"		150.000	Pervious length"					
"	0.013	Impervious Manning 'n'"				"		3.500	Pervious slope"					
"	98.000	Impervious SCS Curve No."				"		0.000	Impervious Area"					
"	0.000	Impervious Runoff coefficient"				"		150.000	Impervious length"					
"	0.100	Impervious Ia/S coefficient"				"		3.500	Impervious slope"					
"	0.518	Impervious Initial abstraction"				"		0.200	Pervious Manning 'n'"					
"		15.489	0.000	11.131	79.914 c.m/sec"			82.000	Pervious SCS Curve No."					
"		Catchment 201	Pervious	Impervious Total Area "		"		0.552	Pervious Runoff coefficient"					
"		Surface Area	166.000	0.000	166.000	hectare"		0.100	Pervious Ia/S coefficient"					
"		Time of concentration	43.771	7.563	43.771	minutes"		5.576	Pervious Initial abstraction"					
"		Time to Centroid	274.325	209.915	274.325	minutes"		0.013	Impervious Manning 'n'"					
"		Rainfall depth	86.100	86.100	86.100	mm"		98.000	Impervious SCS Curve No."					
"		Rainfall volume	14.2926	0.0000	14.2926	ha-m"		0.000	Impervious Runoff coefficient"					
"		Rainfall losses	38.537	5.756	38.537	mm"		0.100	Impervious Ia/S coefficient"					
"		Runoff depth	47.563	80.344	47.563	mm"		0.518	Impervious Initial abstraction"					
"		Runoff volume	7.8955	0.0000	7.8955	ha-m"		1.552	15.936	15.936	79.914	c.m/sec"		
"		Runoff coefficient	0.552	0.000	0.552	"								
"		Maximum flow	15.489	0.000	15.489	c.m/sec"								
"	40	HYDROGRAPH Add Runoff "				"		Catchment 203	Pervious	Impervious Total Area "				
"	4	Add Runoff "				"		Surface Area	13.600	0.000	13.600	hectare"		
"		15.489	15.489	11.131	79.914"			Time of concentration	30.761	5.315	30.761	minutes"		
"	52	CHANNEL DESIGN"				"		Time to Centroid	258.597	207.148	258.597	minutes"		
"	15.489	Current peak flow	c.m/sec"			"		Rainfall depth	86.100	86.100	86.100	mm"		
"	0.040	Manning 'n'"				"		Rainfall volume	1.1710	0.0000	1.1710	ha-m"		
"	0.	Cross-section type: 0=trapezoidal; 1=general"				"		Rainfall losses	38.557	5.592	38.557	mm"		
"	2.000	Basewidth	metre"			"		Runoff depth	47.543	80.508	47.543	mm"		
"	3.000	Left bank slope"				"		Runoff volume	6465.87	0.01	6465.88	c.m"		
"	3.000	Right bank slope"				"		Runoff coefficient	0.552	0.000	0.552	"		
"	5.000	Channel depth	metre"			"		Maximum flow	1.552	0.000	1.552	c.m/sec"		
"	1.000	Gradient	%"			"	40	HYDROGRAPH Add Runoff "						
"		Depth of flow	1.287	metre"		"		4	Add Runoff "					
"		Velocity	2.053	m/sec"		"	52	CHANNEL DESIGN"						
"		Channel capacity	394.351	c.m/sec"		"	16.794	Current peak flow	c.m/sec"					
"		Critical depth	1.116	metre"		"	0.040	Manning 'n'"						
"	53	ROUTE Channel Route 1900"				"	0.	Cross-section type: 0=trapezoidal; 1=general"						
"	1900.00	Channel Route 1900 Reach length	(metre)"			"	2.000	Basewidth	metre"					
"	0.454	X-factor <= 0.5"				"	3.000	Left bank slope"						
"	231.397	K-lag (seconds)"				"	3.000	Right bank slope"						
"	0.000	Default(0) or user spec.(1) values used"				"	5.000	Channel depth	metre"					
"	0.500	X-factor <= 0.5"				"	1.000	Gradient	%"					
"	30.000	K-lag (seconds)"				"		Depth of flow	1.335	metre"				
"	0.500	Beta weighting factor"				"		Velocity	2.096	m/sec"				
"	300.000	Routing time step (seconds)"				"		Channel capacity	394.351	c.m/sec"				
"	3	No. of sub-reaches"				"		Critical depth	1.161	metre"				
"		Peak outflow	15.489	15.489	15.353	79.914 c.m/sec"		53	ROUTE Channel Route 350"					
"	40	HYDROGRAPH Next link "				"		350.00	Channel Route 350 Reach length	(metre)"				
"	5	Next link "				"		0.415	X-factor <= 0.5"					
"		15.489	15.353	15.353	79.914"			125.258	K-lag (seconds)"					
"	33	CATCHMENT 202"				"		0.000	Default(0) or user spec.(1) values used"					
"	1	Triangular SCS"				"		0.500	X-factor <= 0.5"					
"	1	Equal length"				"		30.000	K-lag (seconds)"					
"	1	SCS method"				"		0.500	Beta weighting factor"					
"	202	No description"				"		100.000	Routing time step (seconds)"					
"	0.000	% Impervious"				"		1	No. of sub-reaches"					
"	8.000	Total Area"				"			Peak outflow	16.755	c.m/sec"			
"	225.000	Flow length"				"			1.552	16.794	16.755	79.914	c.m/sec"	
"						"	40	HYDROGRAPH Next link "						
"						"	5	Next link "						

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"      1.552 16.755 16.755 79.914"
" 33 CATCHMENT 204"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 204 No description"
" 0.000 % Impervious"
" 6.800 Total Area"
" 120.000 Flow length"
" 2.000 Overland Slope"
" 6.800 Pervious Area"
" 120.000 Pervious length"
" 2.000 Pervious slope"
" 0.000 Impervious Area"
" 120.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 6.134 0.000 17.045 17.045 c.m/sec"
" Catchment 100 Pervious Impervious Total Area "
" Surface Area 45.000 0.000 45.000 hectare"
" Time of concentration 19.590 3.385 19.590 minutes"
" Time to Centroid 245.074 204.792 245.074 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 38.595 0.000 38.595 ha-m"
" Rainfall losses 38.595 7.147 38.595 mm"
" Runoff depth 47.505 78.953 47.505 mm"
" Runoff volume 2.1377 0.0000 2.1377 ha-m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 6.134 0.000 6.134 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff " 6.134 17.045 17.045"
" 52 CHANNEL DESIGN"
" 6.134 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 1.348 metre"
" Velocity 2.108 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 1.173 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length ( metre)"
" 0.300 X-factor <= 0.5"
" 53.375 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 17.144 c.m/sec"
" 0.761 17.175 17.144 79.914 c.m/sec"
" 40 HYDROGRAPH Combine 1100"
" 6 Combine "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 17.144 c.m/sec"
" Hydrograph volume 92458.828 c.m"
" 0.761 17.175 17.144 17.144"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" End of Area North of Holtby Drain"
" 40 HYDROGRAPH Confluence 1100"
" 7 Confluence "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 17.144 c.m/sec"
" Hydrograph volume 92458.828 c.m"
" 0.761 17.144 17.144 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Holtby Drain"
" 52 CHANNEL DESIGN"
" 17.144 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.570 metre"
" Velocity 1.627 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 1.172 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length ( metre)"
" 0.156 X-factor <= 0.5"
" 92.183 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 17.045 c.m/sec"
" 0.761 17.144 17.045 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node #"
" Node at Holtby Drain"
" Maximum flow 17.045 c.m/sec"
" Hydrograph volume 92458.789 c.m"
" 0.761 17.144 17.045 17.045"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.761 0.000 17.045 17.045"
" 33 CATCHMENT 100"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 100 No description"
" 0.000 % Impervious"
" 45.000 Total Area"
" 100.000 Flow length"
" 7.000 Overland Slope"
" 45.000 Pervious Area"
" 100.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 7.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 1.446 6.034 6.034 17.045 c.m/sec"
" Catchment 101 Pervious Impervious Total Area "
" Surface Area 11.200 0.000 11.200 hectare"
" Time of concentration 16.148 2.233 16.148 minutes"
" Time to Centroid 242.477 203.345 242.477 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 9643.19 0.01 9643.20 c.m"
" Rainfall losses 41.808 6.646 41.808 mm"
" Runoff depth 44.292 79.454 44.292 c.m"
" Runoff volume 4960.69 0.01 4960.70 c.m"
" Runoff coefficient 0.514 0.000 0.514 "
" Maximum flow 1.446 0.000 1.446 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff " 1.446 6.859 6.034 17.045"
" 52 CHANNEL DESIGN"
" 6.859 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.886 metre"
" Velocity 1.663 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.743 metre"
" 53 ROUTE Channel Route 700"
" 700.00 Channel Route 700 Reach length ( metre)"
" 0.470 X-factor <= 0.5"
" 315.677 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 6.850 c.m/sec"
" 1.446 6.859 6.850 17.045 c.m/sec"

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" 40      HYDROGRAPH      Combine      1200"
"          6      Combine      "
"          1200      Node # "
"          Node taking 100 series for Holtby Drain"
"          Maximum flow      6.850      c.m./sec"
"          Hydrograph volume      26338.104      c.m"
"          1.446      6.859      6.850      6.850"
" 40      HYDROGRAPH      Confluence      1200"
"          7      Confluence      "
"          1200      Node # "
"          Node taking 100 series for Holtby Drain"
"          Maximum flow      6.850      c.m./sec"
"          Hydrograph volume      26338.104      c.m"
"          1.446      6.850      6.850      0.000"
" 52      CHANNEL DESIGN"
"          6.850      Current peak flow      c.m./sec"
"          0.040      Manning 'n'"
"          0.      Cross-section type: 0=trapezoidal; 1=general"
"          2.000      Basewidth      metre"
"          3.000      Left bank slope"
"          3.000      Right bank slope"
"          5.000      Channel depth      metre"
"          0.500      Gradient      %"
"          Depth of flow      1.040      metre"
"          Velocity      1.286      m/sec"
"          Channel capacity      278.848      c.m./sec"
"          Critical depth      0.742      metre"
" 53      ROUTE      Channel Route 50"
"          50.00      Channel Route 50 Reach length ( metre)"
"          0.000      X-factor <= 0.5"
"          29.150      K-lag ( seconds)"
"          0.000      Default(0) or user spec.(1) values used"
"          0.500      X-factor <= 0.5"
"          30.000      K-lag ( seconds)"
"          0.678      Beta weighting factor"
"          75.000      Routing time step ( seconds)"
"          1      No. of sub-reaches"
"          Peak outflow      6.839      c.m./sec"
"          1.446      6.850      6.839      0.000 c.m./sec"
" 40      HYDROGRAPH      Combine      1300"
"          6      Combine      "
"          1300      Node # "
"          Node at Holtby Drain"
"          Maximum flow      21.877      c.m./sec"
"          Hydrograph volume      118796.961      c.m"
"          1.446      6.850      6.839      21.877"
" 40      HYDROGRAPH      Confluence      1300"
"          7      Confluence      "
"          1300      Node # "
"          Node at Holtby Drain"
"          Maximum flow      21.877      c.m./sec"
"          Hydrograph volume      118796.961      c.m"
"          1.446      21.877      6.839      0.000"
" 52      CHANNEL DESIGN"
"          21.877      Current peak flow      c.m./sec"
"          0.040      Manning 'n'"
"          0.      Cross-section type: 0=trapezoidal; 1=general"
"          2.000      Basewidth      metre"
"          3.000      Left bank slope"
"          3.000      Right bank slope"
"          5.000      Channel depth      metre"
"          0.500      Gradient      %"
"          Depth of flow      1.746      metre"
"          Velocity      1.731      m/sec"
"          Channel capacity      278.848      c.m./sec"
"          Critical depth      1.318      metre"
" 53      ROUTE      Channel Route 50"
"          50.00      Channel Route 50 Reach length ( metre)"
"          0.000      X-factor <= 0.5"
"          21.664      K-lag ( seconds)"
"          0.000      Default(0) or user spec.(1) values used"
"          0.500      X-factor <= 0.5"
"          30.000      K-lag ( seconds)"
"          0.793      Beta weighting factor"
"          75.000      Routing time step ( seconds)"
"          1      No. of sub-reaches"
"          Peak outflow      21.856      c.m./sec"
"          1.446      21.877      21.856      0.000 c.m./sec"
" 40      HYDROGRAPH      Combine      1000"
"          6      Combine      "
"          1000      Node # "
"          Node upstream of Penetangore Culvert"
"          Maximum flow      94.559      c.m./sec"
"          Hydrograph volume      824085.063      c.m"
"          1.446      21.877      21.856      94.559"
" 81      ADD COMMENT"
"          2      Lines of comment"
"          Total discharge to Pipe Arch under Hwy. 21 on the "
"          Pentangore Tributary"
" 40      HYDROGRAPH      Confluence      1000"
"          7      Confluence      "
"          1000      Node # "
"          Node upstream of Penetangore Culvert"
"          Maximum flow      94.559      c.m./sec"
"          Hydrograph volume      824085.063      c.m"
"          1.446      94.559      21.856      0.000"
" 81      ADD COMMENT"
"          2      Lines of comment"
"          Total discharge to Pipe Arch under Hwy. 21 on the "
"          Pentangore Tributary"
" 52      CHANNEL DESIGN"
"          94.559      Current peak flow      c.m./sec"
"          0.040      Manning 'n'"
"          0.      Cross-section type: 0=trapezoidal; 1=general"
"          2.000      Basewidth      metre"
"          3.000      Left bank slope"
"          3.000      Right bank slope"
"          5.000      Channel depth      metre"
"          0.500      Gradient      %"
"          Depth of flow      3.231      metre"
"          Velocity      2.502      m/sec"
"          Channel capacity      278.848      c.m./sec"
"          Critical depth      2.582      metre"
" 53      ROUTE      Channel Route 50"
"          50.00      Channel Route 50 Reach length ( metre)"
"          0.000      X-factor <= 0.5"
"          14.986      K-lag ( seconds)"
"          0.000      Default(0) or user spec.(1) values used"
"          0.500      X-factor <= 0.5"
"          30.000      K-lag ( seconds)"
"          0.929      Beta weighting factor"
"          75.000      Routing time step ( seconds)"
"          1      No. of sub-reaches"
"          Peak outflow      94.556      c.m./sec"
"          1.446      94.559      94.556      0.000 c.m./sec"
" 40      HYDROGRAPH      Combine      3000"
"          6      Combine      "

```


Channel capacity 431.989 c.m/sec
Critical depth 0.443 metre
ROUTE Channel Route 280"
280.00 Channel Route 280 Reach length (metre)
0.460 X-factor <= 0.5"
153.104 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)
0.500 Beta weighting factor"
150.000 Routing time step (seconds)
1 No. of sub-reaches"
Peak outflow 2.588 c.m/sec"
0.623 2.596 2.588 94.556 c.m/sec"
HYDROGRAPH Next link "
5 Next link "
0.623 2.588 2.588 94.556"
CATCHMENT 303"
1 Triangular SCS"
1 Equal length"
1 SCS method"
303 No description"
0.000 % Impervious"
11.600 Total Area"
135.000 Flow length"
4.500 Overland Slope"
11.600 Pervious Area"
135.000 Pervious length"
4.500 Pervious slope"
0.000 Impervious Area"
135.000 Impervious length"
4.500 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
1.421 2.588 2.588 94.556 c.m/sec"
Catchment 303 Pervious Impervious Total Area "
Surface Area 11.600 0.000 11.600 hectare"
Time of concentration 26.779 5.042 26.779 minutes"
Time to Centroid 253.773 206.873 253.772 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 9987.59 0.01 9987.60 c.m"
Rainfall losses 38.548 5.609 38.548 mm"
Runoff depth 47.552 80.491 47.552 mm"
Runoff volume 5516.08 0.01 5516.09 c.m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 1.421 0.000 1.421 c.m/sec"
HYDROGRAPH Add Runoff "
4 Add Runoff "
1.421 3.928 2.588 94.556"
CHANNEL DESIGN"
3.928 Current peak flow c.m/sec"
0.040 Manning 'n'"
0 Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.649 metre"
Velocity 1.535 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.554 metre"
ROUTE Channel Route 430"
430.00 Channel Route 430 Reach length (metre)
0.469 X-factor <= 0.5"
210.160 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)
0.500 Beta weighting factor"
150.000 Routing time step (seconds)
1 No. of sub-reaches"
Peak outflow 3.904 c.m/sec"
1.421 3.928 3.904 94.556 c.m/sec"
HYDROGRAPH Next link "
5 Next link "
1.421 3.904 3.904 94.556"
CATCHMENT 304"
1 Triangular SCS"
1 Equal length"
1 SCS method"
304 No description"
0.000 % Impervious"
6.300 Total Area"
150.000 Flow length"
2.500 Overland Slope"
6.300 Pervious Area"
150.000 Pervious length"
2.500 Pervious slope"
0.000 Impervious Area"
150.000 Impervious length"
2.500 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.684 3.904 3.904 94.556 c.m/sec"
Catchment 304 Pervious Impervious Total Area "
Surface Area 6.300 0.000 6.300 hectare"
Time of concentration 34.028 6.407 34.028 minutes"
Time to Centroid 262.535 208.467 262.535 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 5424.29 0.01 5424.30 c.m"
Rainfall losses 38.545 6.373 38.545 mm"
Runoff depth 47.555 79.727 47.555 mm"
Runoff volume 2995.95 0.01 2995.96 c.m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 0.684 0.000 0.684 c.m/sec"
HYDROGRAPH Add Runoff "
4 Add Runoff "
0.684 4.588 3.904 94.556"
CHANNEL DESIGN"
4.588 Current peak flow c.m/sec"

0.040 Manning 'n'"
0 Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.700 metre"
Velocity 1.600 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.602 metre"
ROUTE Channel Route 130"
130.00 Channel Route 130 Reach length (metre)
0.391 X-factor <= 0.5"
60.953 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)
0.500 Beta weighting factor"
60.000 Routing time step (seconds)
1 No. of sub-reaches"
Peak outflow 4.535 c.m/sec"
0.684 4.588 4.535 94.556 c.m/sec"
HYDROGRAPH Combine 2000"
6 Combine "
2000 Node #"
Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
Maximum flow 4.535 c.m/sec"
Hydrograph volume 18685.695 c.m"
0.684 4.588 4.535 4.535"
HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
0.684 0.000 4.535 4.535"
CATCHMENT 401"
1 Triangular SCS"
1 Equal length"
1 SCS method"
401 No description"
0.000 % Impervious"
5.600 Total Area"
240.000 Flow length"
5.600 Overland Slope"
240.000 Pervious Area"
3.500 Pervious length"
2.000 Pervious slope"
0.000 Impervious Area"
240.000 Impervious length"
3.500 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.546 0.000 4.535 4.535 c.m/sec"
Catchment 401 Pervious Impervious Total Area "
Surface Area 5.600 0.000 5.600 hectare"
Time of concentration 40.782 7.678 40.782 minutes"
Time to Centroid 270.706 210.019 270.706 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 4821.59 0.00 4821.60 c.m"
Rainfall losses 38.542 5.716 38.542 mm"
Runoff depth 47.558 80.384 47.558 mm"
Runoff volume 2663.27 0.00 2663.27 c.m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 0.546 0.000 0.546 c.m/sec"
HYDROGRAPH Add Runoff "
4 Add Runoff "
0.546 0.546 4.535 4.535"
CHANNEL DESIGN"
0.546 Current peak flow c.m/sec"
0.040 Manning 'n'"
0 Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.232 metre"
Velocity 0.874 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.179 metre"
ROUTE Channel Route 225"
225.00 Channel Route 225 Reach length (metre)
0.476 X-factor <= 0.5"
193.099 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)
0.500 Beta weighting factor"
150.000 Routing time step (seconds)
1 No. of sub-reaches"
Peak outflow 0.539 c.m/sec"
0.546 0.546 0.539 4.535 c.m/sec"
HYDROGRAPH Next link "
5 Next link "
0.546 0.539 0.539 4.535"
CATCHMENT 402"
1 Triangular SCS"
1 Equal length"
1 SCS method"
402 No description"
0.000 % Impervious"
4.200 Total Area"
80.000 Flow length"
4.000 Overland Slope"
4.200 Pervious Area"
80.000 Pervious length"
4.000 Pervious slope"
0.000 Impervious Area"
80.000 Impervious length"
4.000 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.568 0.539 0.539 4.535 c.m/sec"

" Catchment 402 Pervious Impervious Total Area " " 0.552 Pervious Runoff coefficient"
Surface Area 4.200 0.000 4.200 hectare" " 0.100 Pervious Ia/S coefficient"
Time of concentration 20.267 3.816 20.267 minutes" " 5.576 Pervious Initial abstraction"
Time to Centroid 245.913 205.154 245.913 minutes" " 0.015 Impervious Manning 'n'"
Rainfall depth 86.100 86.100 86.100 mm" " 98.000 Impervious SCS Curve No."
Rainfall volume 3616.20 0.00 3616.20 c.m" " 0.000 Impervious Runoff coefficient"
Rainfall losses 38.558 7.348 38.558 mm" " 0.100 Impervious Ia/S coefficient"
Runoff depth 47.542 78.752 47.542 mm" " 0.518 Impervious Initial abstraction"
Runoff volume 1996.78 0.00 1996.78 c.m" " 0.368 1.724 4.535 c.m/sec"
Runoff coefficient 0.552 0.000 0.552 " "
Maximum flow 0.568 0.000 0.568 c.m/sec" "
HYDROGRAPH Add Runoff " "
40 4 Add Runoff " "
0.568 0.989 0.539 4.535" "
52 CHANNEL DESIGN" "
0.989 Current peak flow c.m/sec" "
0.040 Manning 'n'" "
0. Cross-section type: 0=trapezoidal; 1=general" "
2.000 Basewidth metre" "
3.000 Left bank slope" "
3.000 Right bank slope" "
5.000 Channel depth metre" " 40
1.200 Gradient %" "
4 Add Runoff " "
0.368 2.063 1.724 4.535" "
Depth of flow 0.320 metre" " 52
Velocity 1.044 m/sec" "
Channel capacity 431.989 c.m/sec" "
Critical depth 0.255 metre" "
53 ROUTE Channel Route 280" "
280.00 Channel Route 280 Reach length (metre)" "
0.475 X-factor <= 0.5" "
201.133 K-lag (seconds)" "
0.000 Default(0) or user spec.(1) values used" "
0.500 X-factor <= 0.5" "
30.000 K-lag (seconds)" "
0.500 Beta weighting factor" "
150.000 Routing time step (seconds)" "
1 No. of sub-reaches" "
Peak outflow 0.969 0.969 c.m/sec" "
0.568 0.989 0.969 4.535 c.m/sec" "
40 HYDROGRAPH Next link " "
5 Next link " "
0.568 0.969 0.969 4.535" "
33 CATCHMENT 403" "
1 Triangular SCS" "
1 Equal length" "
1 SCS method" "
403 No description" "
0.000 % Impervious" "
6.400 Total Area" "
75.000 Flow length" "
4.000 Overland Slope" "
6.400 Pervious Area" "
75.000 Pervious length" "
4.000 Pervious slope" "
0.000 Impervious Area" "
75.000 Impervious length" "
4.000 Impervious slope" "
0.200 Pervious Manning 'n'" "
82.000 Pervious SCS Curve No." "
0.552 Pervious Runoff coefficient" "
0.100 Pervious Ia/S coefficient" "
5.576 Pervious Initial abstraction" "
0.015 Impervious Manning 'n'" "
98.000 Impervious SCS Curve No." "
0.000 Impervious Runoff coefficient" "
0.100 Impervious Ia/S coefficient" "
0.518 Impervious Initial abstraction" "
0.873 0.969 0.969 4.535 c.m/sec" "
Catchment 403 Pervious Impervious Total Area " "
Surface Area 6.400 0.000 6.400 hectare" "
Time of concentration 19.498 3.671 19.498 minutes" "
Time to Centroid 244.966 204.999 244.966 minutes" "
Rainfall depth 86.100 86.100 86.100 mm" "
Rainfall volume 5510.39 0.01 5510.40 c.m" "
Rainfall losses 38.598 7.640 38.598 mm" "
Runoff depth 47.502 78.460 47.502 mm" "
Runoff volume 3040.13 0.01 3040.14 c.m" "
Runoff coefficient 0.552 0.000 0.552 " "
Maximum flow 0.873 0.000 0.873 c.m/sec" "
40 HYDROGRAPH Add Runoff " "
4 Add Runoff " "
0.873 1.757 0.969 4.535" "
52 CHANNEL DESIGN" "
1.757 Current peak flow c.m/sec" "
0.040 Manning 'n'" "
0. Cross-section type: 0=trapezoidal; 1=general" "
2.000 Basewidth metre" "
3.000 Left bank slope" "
3.000 Right bank slope" "
5.000 Channel depth metre" "
1.200 Gradient %" "
Depth of flow 0.433 metre" "
Velocity 1.231 m/sec" "
Channel capacity 431.989 c.m/sec" "
Critical depth 0.356 metre" "
53 ROUTE Channel Route 410" "
410.00 Channel Route 410 Reach length (metre)" "
0.477 X-factor <= 0.5" "
249.817 K-lag (seconds)" "
0.000 Default(0) or user spec.(1) values used" "
0.500 X-factor <= 0.5" "
30.000 K-lag (seconds)" "
0.500 Beta weighting factor" "
150.000 Routing time step (seconds)" "
1 No. of sub-reaches" "
Peak outflow 1.724 1.724 c.m/sec" "
0.873 1.757 1.724 4.535 c.m/sec" "
40 HYDROGRAPH Next link " "
5 Next link " "
0.873 1.724 1.724 4.535" "
33 CATCHMENT 404" "
1 Triangular SCS" "
1 Equal length" "
1 SCS method" "
404 No description" "
0.000 % Impervious" "
2.500 Total Area" "
60.000 Flow length" "
2.500 Overland Slope" "
2.700 Pervious Area" "
60.000 Pervious length" "
2.500 Pervious slope" "
0.000 Impervious Area" "
60.000 Impervious length" "
2.500 Impervious slope" "
0.200 Pervious Manning 'n'" "
82.000 Pervious SCS Curve No." "
0.552 Pervious Runoff coefficient" "
0.100 Pervious Ia/S coefficient" "
5.576 Pervious Initial abstraction" "
0.015 Impervious Manning 'n'" "
98.000 Impervious SCS Curve No." "
0.000 Impervious Runoff coefficient" "
0.100 Impervious Ia/S coefficient" "
0.518 Impervious Initial abstraction" "
0.335 0.000 2.004 6.539 c.m/sec" "
Catchment 501 Pervious Impervious Total Area " "
Surface Area 2.500 0.000 2.500 hectare" "
Time of concentration 21.096 3.972 21.096 minutes" "
Time to Centroid 246.891 205.283 246.891 minutes" "
0.552 Pervious Runoff coefficient" "
0.100 Pervious Ia/S coefficient" "
5.576 Pervious Initial abstraction" "
0.015 Impervious Manning 'n'" "
98.000 Impervious SCS Curve No." "
0.000 Impervious Runoff coefficient" "
0.100 Impervious Ia/S coefficient" "
0.518 Impervious Initial abstraction" "
0.368 2.063 2.022 4.535 c.m/sec" "
HYDROGRAPH Combine 2100" "
6 Combine " "
2100 Node #" "
Node taking 400 series - dumps into Hwy 21 Ditch" "
Maximum flow 2.022 c.m/sec" "
Hydrograph volume 8982.868 c.m" "
0.368 2.063 2.022 2.022" "
40 HYDROGRAPH Confluence 2100" "
7 Confluence " "
2100 Node #" "
Node taking 400 series - dumps into Hwy 21 Ditch" "
Maximum flow 2.022 c.m/sec" "
Hydrograph volume 8982.867 c.m" "
0.368 2.022 2.022 0.000" "
52 CHANNEL DESIGN" "
2.022 Current peak flow c.m/sec" "
0.040 Manning 'n'" "
0. Cross-section type: 0=trapezoidal; 1=general" "
2.000 Basewidth metre" "
3.000 Left bank slope" "
3.000 Right bank slope" "
5.000 Channel depth metre" "
0.500 Gradient %" "
Depth of flow 0.580 metre" "
Velocity 0.932 m/sec" "
Channel capacity 278.848 c.m/sec" "
Critical depth 0.385 metre" "
53 ROUTE Channel Route 50" "
50.00 Channel Route 50 Reach length (metre)" "
0.000 X-factor <= 0.5" "
40.241 K-lag (seconds)" "
0.000 Default(0) or user spec.(1) values used" "
0.500 X-factor <= 0.5" "
30.000 K-lag (seconds)" "
0.541 Beta weighting factor" "
75.000 Routing time step (seconds)" "
1 No. of sub-reaches" "
Peak outflow 2.004 2.004 c.m/sec" "
0.368 2.022 2.004 0.000 c.m/sec" "
40 HYDROGRAPH Combine 2000" "
6 Combine " "
2000 Node #" "
Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch" "
Maximum flow 6.539 c.m/sec" "
Hydrograph volume 27668.563 c.m" "
0.368 2.022 2.004 6.539" "
40 HYDROGRAPH Start - New Tributary" "
2 Start - New Tributary" "
0.368 0.000 2.004 6.539" "
33 CATCHMENT 501" "
1 Triangular SCS" "
1 Equal length" "
1 SCS method" "
501 No description" "
0.000 % Impervious" "
2.500 Total Area" "
80.000 Flow length" "
3.500 Overland Slope" "
2.500 Pervious Area" "
80.000 Pervious length" "
3.500 Pervious slope" "
0.000 Impervious Area" "
80.000 Impervious length" "
3.500 Impervious slope" "
0.200 Pervious Manning 'n'" "
82.000 Pervious SCS Curve No." "
0.552 Pervious Runoff coefficient" "
0.100 Pervious Ia/S coefficient" "
5.576 Pervious Initial abstraction" "
0.015 Impervious Manning 'n'" "
98.000 Impervious SCS Curve No." "
0.000 Impervious Runoff coefficient" "
0.100 Impervious Ia/S coefficient" "
0.518 Impervious Initial abstraction" "
0.335 0.000 2.004 6.539 c.m/sec" "
Catchment 501 Pervious Impervious Total Area " "
Surface Area 2.500 0.000 2.500 hectare" "
Time of concentration 21.096 3.972 21.096 minutes" "
Time to Centroid 246.891 205.283 246.891 minutes" "

" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 2152.50 0.00 2152.50 c.m"
" Rainfall losses 38.580 7.179 38.580 mm"
" Runoff depth 47.520 78.921 47.520 mm"
" Runoff volume 1187.99 0.00 1187.99 c.m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 0.335 0.000 0.335 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.335 0.335 2.004 6.539"
52 CHANNEL DESIGN"
0.335 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.177 metre"
Velocity 0.750 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.132 metre"
53 ROUTE Channel Route 120"
120.00 Channel Route 120 Reach length (metre)"
0.465 X-factor <= 0.5"
120.001 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
100.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.325 0.325 c.m/sec"
0.335 0.335 0.325 6.539 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 0.335 0.325 0.325 6.539"
33 CATCHMENT 502"
1 Triangular SCS"
1 Equal length"
1 SCS method"
502 No description"
0.000 % Impervious"
0.500 Total Area"
120.000 Flow length"
3.500 Overland Slope"
0.500 Pervious Area"
120.000 Pervious length"
3.500 Pervious slope"
0.000 Impervious Area"
120.000 Impervious length"
3.500 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.061 0.325 0.325 6.539 c.m/sec"
Catchment 502 Pervious Impervious Total Area "
Surface Area 0.500 0.000 0.500 hectare"
Time of concentration 26.906 5.066 26.906 minutes"
Time to Centroid 253.923 206.894 253.923 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 430.50 0.00 430.50 c.m"
Rainfall losses 38.553 5.600 38.553 mm"
Runoff depth 47.547 80.500 47.547 mm"
Runoff volume 237.74 0.00 237.74 c.m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 0.061 0.000 0.061 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.061 0.386 0.325 6.539"
52 CHANNEL DESIGN"
0.386 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.191 metre"
Velocity 0.785 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.145 metre"
53 ROUTE Channel Route 170"
170.00 Channel Route 170 Reach length (metre)"
0.474 X-factor <= 0.5"
162.523 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
150.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.385 0.385 c.m/sec"
0.061 0.386 0.385 6.539 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 0.061 0.385 0.385 6.539"
33 CATCHMENT 503"
1 Triangular SCS"
1 Equal length"
1 SCS method"
503 No description"
0.000 % Impervious"
8.200 Total Area"
90.000 Flow length"
5.000 Overland Slope"
8.200 Pervious Area"
90.000 Pervious length"
5.000 Pervious slope"
0.000 Impervious Area"
90.000 Impervious length"
5.000 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.015 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.489 1.453 1.453 6.539 c.m/sec"
Catchment 504 Pervious Impervious Total Area "
Surface Area 3.900 0.000 3.900 hectare"
Time of concentration 25.045 4.715 25.045 minutes"
Time to Centroid 251.669 206.556 251.669 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 3357.90 0.00 3357.90 c.m"
Rainfall losses 38.582 5.982 38.582 mm"
Runoff depth 47.518 80.118 47.518 mm"
Runoff volume 1853.18 0.00 1853.18 c.m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 0.489 0.000 0.489 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.489 1.942 1.453 6.539"
52 CHANNEL DESIGN"
1.942 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.456 metre"
Velocity 1.266 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.377 metre"
53 ROUTE Channel Route 140"
140.00 Channel Route 140 Reach length (metre)"
0.430 X-factor <= 0.5"
82.947 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
75.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 1.920 1.920 c.m/sec"
0.489 1.942 1.920 6.539 c.m/sec"
40 HYDROGRAPH Combine 2200"
6 Combine " 2200 "
Node # "
Node taking 500 series - dumps into Hwy 21 Ditch"
Maximum flow 1.920 c.m/sec"
Hydrograph volume 7177.571 c.m"
0.489 1.942 1.920 1.920"
40 HYDROGRAPH Confluence 2200"
7 Confluence " 2200 "
Node # "
Node taking 500 series - dumps into Hwy 21 Ditch"
Maximum flow 1.920 c.m/sec"
Hydrograph volume 7177.571 c.m"
0.489 1.920 1.920 0.000"
52 CHANNEL DESIGN"

```

" 1.920 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.565 metre"
" Velocity 0.919 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.374 metre"
" 53 ROUTE Channel Route 300"
" 300.00 Channel Route 300 Reach length (metre)"
" 0.406 X-factor <= 0.5"
" 244.861 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.489 1.920 1.887 c.m/sec"
" 0.489 1.920 1.887 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 8.427 c.m/sec"
" Hydrograph volume 34846.121 c.m"
" 0.489 1.920 1.887 8.427"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.489 0.000 1.887 8.427"
" 33 CATCHMENT 603"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 603 No description"
" 0.000 % Impervious"
" 5.600 Total Area"
" 100.000 Flow length"
" 2.500 Overland slope"
" 5.600 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.687 0.000 1.887 8.427 c.m/sec"
" Catchment 603 Pervious Impervious Total Area "
" Surface Area 5.600 0.000 5.600 hectare"
" Time of concentration 26.680 5.023 26.680 minutes"
" Time to Centroid 253.653 206.895 253.653 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 4821.59 0.00 4821.60 c.m"
" Rainfall losses 38.545 5.617 38.545 mm"
" Runoff depth 47.555 80.483 47.555 mm"
" Runoff volume 2663.09 0.00 2663.10 c.m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 0.687 0.000 0.687 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.687 0.687 1.887 8.427"
" 52 CHANNEL DESIGN"
" 0.687 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.263 metre"
" Velocity 0.937 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.206 metre"
" 53 ROUTE Channel Route 260"
" 260.00 Channel Route 260 Reach length (metre)"
" 0.477 X-factor <= 0.5"
" 208.091 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.687 0.687 0.673 c.m/sec"
" 0.687 0.687 0.673 8.427 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.687 0.673 0.673 8.427"
" 33 CATCHMENT 605"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 605 No description"
" 0.000 % Impervious"
" 3.400 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 3.400 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.417 0.673 0.673 8.427 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
" Surface Area 3.400 0.000 3.400 hectare"
" Time of concentration 26.680 5.023 26.680 minutes"
" Time to Centroid 253.653 206.895 253.653 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 2927.40 0.00 2927.40 c.m"
" Rainfall losses 38.545 5.617 38.545 mm"
" Runoff depth 47.555 80.483 47.555 mm"
" Runoff volume 1616.88 0.00 1616.88 c.m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 0.417 0.000 0.417 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.417 1.088 0.673 8.427"
" 52 CHANNEL DESIGN"
" 1.088 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.337 metre"
" Velocity 1.074 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.270 metre"
" 53 ROUTE Channel Route 170"
" 170.00 Channel Route 170 Reach length (metre)"
" 0.456 X-factor <= 0.5"
" 118.767 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.417 1.088 1.074 c.m/sec"
" 0.417 1.088 1.074 8.427 c.m/sec"
" 40 HYDROGRAPH Combine 2300"
" 6 Combine "
" 2300 Node #"
" Node taking 600 series - dumps into Hwy 21 Ditch"
" Maximum flow 1.074 c.m/sec"
" Hydrograph volume 4279.979 c.m"
" 0.417 1.088 1.074 1.074"
" 40 HYDROGRAPH Confluence 2300"
" 7 Confluence "
" 2300 Node #"
" Node taking 600 series - dumps into Hwy 21 Ditch"
" Maximum flow 1.074 c.m/sec"
" Hydrograph volume 4279.979 c.m"
" 0.417 1.074 1.074 0.000"
" 52 CHANNEL DESIGN"
" 1.074 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.421 metre"
" Velocity 0.782 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.268 metre"
" 53 ROUTE Channel Route 650"
" 650.00 Channel Route 650 Reach length (metre)"
" 0.433 X-factor <= 0.5"
" 311.517 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
" Peak outflow 0.417 1.074 1.063 c.m/sec"
" 0.417 1.074 1.063 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 9.364 c.m/sec"
" Hydrograph volume 39126.063 c.m"
" 0.417 1.074 1.063 9.364"
" 81 ADD COMMENT"
" 1 Lines of comment"
" Total discharge to Hwy. 21 Ditch"
" 40 HYDROGRAPH Confluence 2000"
" 7 Confluence "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 9.364 c.m/sec"
" Hydrograph volume 39126.063 c.m"
" 0.417 9.364 1.063 0.000"
" 81 ADD COMMENT"
" 1 Lines of comment"
" Total discharge to Hwy. 21 Ditch"
" 52 CHANNEL DESIGN"
" 9.364 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.200 metre"
" Velocity 1.394 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.870 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 26.894 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.710 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.417 9.364 9.312 c.m/sec"
" 0.417 9.364 9.312 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"

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"      Node Combining All Flow"
"      Maximum flow      97.611  c.m/sec"
"      Hydrograph volume 863211.063 c.m"
"      0.417  9.364  9.312  97.611"
" 81  ADD COMMENT=====
"      1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40  HYDROGRAPH Confluence 3000"
"      7 Confluence "
"      3000 Node #"
"      Node Combining All Flow"
"      Maximum flow      97.611  c.m/sec"
"      Hydrograph volume 863211.063 c.m"
"      0.417  97.611  9.312  0.000"
" 81  ADD COMMENT=====
"      1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"

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PRE-EXISTING 100 YEAR

MIDUSS Output ----->
MIDUSS version Version 2.25 rev. 465
MIDUSS created Tuesday, February 05, 2008
Units used: ie METRIC
Job folder: C:\Users\derb\Desktop\Kincardine Miduss\
Output filename: 08055 - Pre-Existing 100 Year.out
Licensee name: EliteBook
Company: BMROSS
Date & Time last used: 7/19/2011 at 4:29:06 PM
TIME PARAMETERS
5.000 Time Step
360.000 Max. Storm length
1800.000 Max. Hydrograph
STORM Mass Curve
3 Mass Curve
108.800 Rainfall depth
360.000 Duration
41 C:\Program Files\MIDUSS\SCS_6hr_Type2.mrd SCS Type II - 6 hour
Distribution - Ontario
Maximum intensity 84.864 mm/hr
Total depth 108.800 mm
6 100hyd Hydrograph extension used in this file
ADD COMMENT-----
1 Lines of comment
Start of Penetangore Tributary
CATCHMENT 50
1 Triangular SCS
1 Equal length
1 SCS method
50 No description
0.000 % Impervious
396.000 Total Area
450.000 Flow length
2.500 Overland Slope
396.000 Pervious Area
450.000 Pervious length
2.500 Pervious slope
0.000 Impervious Area
450.000 Impervious length
2.500 Pervious slope
0.250 Pervious Manning 'n'
81.000 Pervious SCS Curve No.
0.598 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.958 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
37.770 0.000 0.000 0.000 c.m/sec
Catchment 50 Pervious Impervious Total Area
Surface Area 396.000 0.000 396.000 hectare
Time of concentration 66.924 10.341 66.924 minutes
Time to Centroid 300.389 212.009 300.389 minutes
Rainfall depth 108.800 108.800 108.800 mm
Rainfall volume 43.0848 0.0000 43.0848 ha-m
Rainfall losses 43.692 5.981 43.692 mm
Runoff depth 65.108 102.819 65.108 mm
Runoff volume 25.7828 0.0000 25.7828 ha-m
Runoff coefficient 0.598 0.000 0.598
Maximum flow 37.770 0.000 37.770 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
37.770 37.770 0.000 0.000
CHANNEL DESIGN
37.770 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.500 Gradient %
Depth of flow 2.206 metre
Velocity 1.987 m/sec
Channel capacity 278.848 c.m/sec
Critical depth 1.704 metre
ROUTE Channel Route 3000
3000.00 Channel Route 3000 Reach length (metre)
0.376 X-factor <= 0.5
283.088 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
4 No. of sub-reaches
Peak outflow 37.185 c.m/sec
37.770 37.770 37.185 0.000 c.m/sec
HYDROGRAPH Next link
5 Next link
37.770 37.185 37.185 0.000
CATCHMENT 52
1 Triangular SCS
1 Equal length
1 SCS method
52 No description
0.000 % Impervious
196.000 Total Area
250.000 Flow length
7.000 Overland Slope
196.000 Pervious Area
250.000 Pervious length
7.000 Pervious slope
0.000 Impervious Area
250.000 Impervious length
7.000 Impervious slope
0.250 Pervious Manning 'n'
80.000 Pervious SCS Curve No.
0.581 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
6.350 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
28.020 37.185 37.185 0.000 c.m/sec
Catchment 52 Pervious Impervious Total Area
Surface Area 196.000 0.000 196.000 hectare
Time of concentration 34.824 5.336 34.824 minutes
Time to Centroid 262.294 206.023 262.293 minutes

Rainfall depth 108.800 108.800 108.800 mm
Rainfall volume 21.3248 0.0000 21.3248 ha-m
Rainfall losses 45.592 5.703 45.592 mm
Runoff depth 63.208 103.097 63.208 mm
Runoff volume 12.3888 0.0000 12.3888 ha-m
Runoff coefficient 0.581 0.000 0.581
Maximum flow 28.020 0.000 28.020 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
28.020 46.374 37.185 0.000
CHANNEL DESIGN
46.374 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.400 Gradient %
Depth of flow 2.520 metre
Velocity 1.925 m/sec
Channel capacity 249.409 c.m/sec
Critical depth 1.872 metre
ROUTE Channel Route 1300
1300.00 Channel Route 1300 Reach length (metre)
0.297 X-factor <= 0.5
253.279 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
2 No. of sub-reaches
Peak outflow 46.162 c.m/sec
28.020 46.374 46.162 0.000 c.m/sec
HYDROGRAPH Next link
5 Next link
28.020 46.162 46.162 0.000
CATCHMENT 54
1 Triangular SCS
1 Equal length
1 SCS method
54 No description
0.000 % Impervious
39.000 Total Area
140.000 Flow length
11.000 Overland Slope
39.000 Pervious Area
140.000 Pervious length
11.000 Pervious slope
0.000 Impervious Area
140.000 Impervious length
11.000 Impervious slope
0.210 Pervious Manning 'n'
81.000 Pervious SCS Curve No.
0.597 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.958 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
7.223 46.162 46.162 0.000 c.m/sec
Catchment 54 Pervious Impervious Total Area
Surface Area 39.000 0.000 39.000 hectare
Time of concentration 19.181 3.291 19.181 minutes
Time to Centroid 242.650 203.605 242.650 minutes
Rainfall depth 108.800 108.800 108.800 mm
Rainfall volume 4.2432 0.0000 4.2432 ha-m
Rainfall losses 43.802 7.543 43.802 mm
Runoff depth 64.998 101.257 64.998 mm
Runoff volume 2.5349 0.0000 2.5349 ha-m
Runoff coefficient 0.597 0.000 0.597
Maximum flow 7.223 0.000 7.223 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
7.223 47.717 46.162 0.000
CHANNEL DESIGN
47.717 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.400 Gradient %
Depth of flow 2.550 metre
Velocity 1.939 m/sec
Channel capacity 249.409 c.m/sec
Critical depth 1.897 metre
ROUTE Channel Route 800
800.00 Channel Route 800 Reach length (metre)
0.334 X-factor <= 0.5
309.499 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
1 No. of sub-reaches
Peak outflow 47.596 c.m/sec
7.223 47.717 47.596 0.000 c.m/sec
HYDROGRAPH Combine
6 Combine
10 Node #
Confluence on Penetangore Tributary
Maximum flow 47.596 c.m/sec
Hydrograph volume 407065.875 c.m
7.223 47.717 47.596 47.596
HYDROGRAPH Start - New Tributary
2 Start - New Tributary
7.223 0.000 47.596 47.596
CATCHMENT 60
1 Triangular SCS
1 Equal length
1 SCS method
60 No description
0.000 % Impervious
225.000 Total Area
270.000 Flow length
2.500 Overland Slope
225.000 Pervious Area
270.000 Pervious length
2.500 Pervious slope
0.000 Impervious Area
270.000 Impervious length

2.500	Impervious slope"	"	Surface Area	95.000	0.000	95.000	hectare"
0.230	Pervious Manning 'n'"	"	Time of concentration	36.285	5.560	36.285	minutes"
81.000	Pervious SCS Curve No."	"	Time to Centroid	264.065	206.307	264.065	minutes"
0.598	Pervious Runoff coefficient"	"	Rainfall depth	108.800	108.800	108.800	mm"
0.100	Pervious Ia/S coefficient"	"	Rainfall volume	10.3360	0.0000	10.3360	ha-m"
5.958	Pervious Initial abstraction"	"	Rainfall losses	45.578	5.794	45.578	mm"
0.013	Impervious Manning 'n'"	"	Runoff depth	63.222	103.006	63.222	mm"
98.000	Impervious SCS Curve No."	"	Runoff volume	6.0061	0.0000	6.0061	ha-m"
0.000	Impervious Runoff coefficient"	"	Runoff coefficient	0.581	0.000	0.581	"
0.100	Impervious Ia/S coefficient"	"	Maximum flow	13.275	0.000	13.275	c.m/sec"
0.518	Impervious Initial abstraction"	"	HYDROGRAPH Add Runoff "				
	27.615 0.000 47.596	47.596 c.m/sec"	4 Add Runoff "	13.275	13.275	71.140	71.140"
	Catchment 60 Pervious	Impervious Total Area "	52 CHANNEL DESIGN"				
	Surface Area	225.000 0.000 225.000	13.275 Current peak flow	c.m/sec"			
	Time of concentration	46.854 7.611 46.854	0.040 Manning 'n'"				
	Time to Centroid	276.114 208.803 276.113	0. Cross-section type: 0=trapezoidal; 1=general"				
	Rainfall depth	108.800 108.800 108.800	2.000 Basewidth	metre"			
	Rainfall volume	24.4800 0.0000 24.4800	3.000 Left bank slope"				
	Rainfall losses	43.706 5.897 43.706	3.000 Right bank slope"				
	Runoff depth	65.094 102.903 65.094	5.000 Channel depth	metre"			
	Runoff volume	14.6461 0.0000 14.6461	0.300 Gradient	%"			
	Runoff coefficient	0.598 0.000 0.598					
	Maximum flow	27.615 0.000 27.615					
40	HYDROGRAPH Add Runoff "						
	4 Add Runoff "						
	27.615 27.615 47.596 47.596"						
52	CHANNEL DESIGN"						
27.615	Current peak flow	c.m/sec"	53 ROUTE Channel Route 1800"				
0.040	Manning 'n'"		1800.00 Channel Route 1800 Reach length (metre)"				
0. Cross-section type: 0=trapezoidal; 1=general"			0.309 X-factor <= 0.5"				
2.000 Basewidth	metre"		357.055 K-lag (seconds)"				
3.000 Left bank slope"			0.000 Default(0) or user spec.(1) values used"				
3.000 Right bank slope"			0.500 X-factor <= 0.5"				
5.000 Channel depth	metre"		30.000 K-lag (seconds)"				
0.400 Gradient	%"		0.500 Beta weighting factor"				
Depth of flow	2.025	metre"	300.000 Routing time step (seconds)"				
Velocity	1.689	m/sec"	3 No. of sub-reaches"				
Channel capacity	249.409	c.m/sec"	Peak outflow	13.275	13.275	12.594	71.140 c.m/sec"
Critical depth	1.472	metre"	40 HYDROGRAPH Combine 11"				
53 ROUTE Channel Route 1800"			6 Combine "				
1800.00 Channel Route 1800 Reach length (metre)"			11 Node #"				
0.320 X-factor <= 0.5"							
266.406 K-lag (seconds)"							
0.000 Default(0) or user spec.(1) values used"							
0.500 X-factor <= 0.5"							
30.000 K-lag (seconds)"							
0.500 Beta weighting factor"							
300.000 Routing time step (seconds)"							
3 No. of sub-reaches"							
Peak outflow	27.176	c.m/sec"					
27.615 27.615 27.176 47.596 c.m/sec"							
40 HYDROGRAPH Combine 10"							
6 Combine "							
10 Node #"							
Confluence on Penetangore Tributary"							
Maximum flow	71.637	c.m/sec"					
Hydrograph volume	553527.000	c.m"					
27.615 27.615 27.176 71.637"							
40 HYDROGRAPH Confluence 10"							
7 Confluence "							
10 Node #"							
Confluence on Penetangore Tributary"							
Maximum flow	71.637	c.m/sec"					
Hydrograph volume	553527.000	c.m"					
27.615 71.637 27.176 0.000"							
52 CHANNEL DESIGN"							
71.637 Current peak flow	c.m/sec"						
0.040 Manning 'n'"							
0. Cross-section type: 0=trapezoidal; 1=general"							
2.000 Basewidth	metre"						
3.000 Left bank slope"							
3.000 Right bank slope"							
5.000 Channel depth	metre"						
0.400 Gradient	%"						
Depth of flow	3.018	metre"					
Velocity	2.147	m/sec"					
Channel capacity	249.409	c.m/sec"					
Critical depth	2.281	metre"					
53 ROUTE Channel Route 2000"							
2000.00 Channel Route 2000 Reach length (metre)"							
0.345 X-factor <= 0.5"							
349.343 K-lag (seconds)"							
0.000 Default(0) or user spec.(1) values used"							
0.500 X-factor <= 0.5"							
30.000 K-lag (seconds)"							
0.500 Beta weighting factor"							
300.000 Routing time step (seconds)"							
2 No. of sub-reaches"							
Peak outflow	71.140	c.m/sec"					
27.615 71.637 71.140 0.000 c.m/sec"							
40 HYDROGRAPH Combine 11"							
6 Combine "							
11 Node #"							
Confluence on Penetangore Tributary"							
Maximum flow	71.140	c.m/sec"					
Hydrograph volume	553527.188	c.m"					
27.615 71.637 71.140 71.140"							
40 HYDROGRAPH Start - New Tributary"							
2 Start - New Tributary"							
27.615 0.000 71.140 71.140"							
33 CATCHMENT 62"							
1 Triangular SCS"							
1 Equal length"							
1 SCS method"							
62 No description"							
0.000 % Impervious"							
95.000 Total Area"							
160.000 Flow length"							
2.500 Overland Slope"							
95.000 Pervious Area"							
160.000 Pervious length"							
2.500 Pervious slope"							
0.000 Impervious Area"							
160.000 Impervious length"							
2.500 Impervious slope"							
0.250 Pervious Manning 'n'"							
80.000 Pervious SCS Curve No."							
0.581 Pervious Runoff coefficient"							
0.100 Pervious Ia/S coefficient"							
6.350 Pervious Initial abstraction"							
0.013 Impervious Manning 'n'"							
98.000 Impervious SCS Curve No."							
0.000 Impervious Runoff coefficient"							
0.100 Impervious Ia/S coefficient"							
0.518 Impervious Initial abstraction"							
13.275 0.000 71.140 71.140 c.m/sec"							
Catchment 62 Pervious	Impervious Total Area "						


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"      2.332 25.625 25.625 125.579"
" 33 CATCHMENT 204"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 204 No description"
" 0.000 % Impervious"
" 6.800 Total Area"
" 120.000 Flow length"
" 2.000 Overland Slope"
" 6.800 Pervious Area"
" 120.000 Pervious length"
" 2.000 Pervious slope"
" 0.000 Impervious Area"
" 120.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 1.151 25.625 25.625 125.579 c.m/sec"
" Catchment 204 Pervious Impervious Total Area "
" Surface Area 6.800 0.000 6.800 hectare"
" Time of concentration 28.092 5.003 28.092 minutes"
" Time to Centroid 252.678 205.712 252.678 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 7398.39 0.01 7398.40 c.m"
" Rainfall losses 41.833 5.758 41.833 mm"
" Runoff depth 66.967 103.042 66.967 mm"
" Runoff volume 4553.77 0.01 4553.78 c.m"
" Runoff coefficient 0.616 0.000 0.616 "
" Maximum flow 1.151 0.000 1.151 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.151 26.217 25.625 125.579"
" 52 CHANNEL DESIGN"
" 26.217 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 1.625 metre"
" Velocity 2.347 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 1.436 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length ( metre)"
" 0.264 X-factor <= 0.5"
" 47.926 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 26.213 c.m/sec"
" 1.151 26.217 26.213 125.579 c.m/sec"
" 40 HYDROGRAPH Combine 1100"
" 6 Combine "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 26.213 c.m/sec"
" Hydrograph volume 130240.461 c.m"
" 1.151 26.217 26.213 26.213"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" End of Area North of Holtby Drain"
" 40 HYDROGRAPH Confluence 1100"
" 7 Confluence "
" 1100 Node #"
" Node taking 200 series - dumps into Holtby Drain"
" Maximum flow 26.213 c.m/sec"
" Hydrograph volume 130240.461 c.m"
" 1.151 26.213 26.213 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Holtby Drain"
" 52 CHANNEL DESIGN"
" 26.213 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.888 metre"
" Velocity 1.812 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 1.436 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length ( metre)"
" 0.094 X-factor <= 0.5"
" 82.779 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 26.144 c.m/sec"
" 1.151 26.213 26.144 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node #"
" Node at Holtby Drain"
" Maximum flow 26.144 c.m/sec"
" Hydrograph volume 130240.414 c.m"
" 1.151 26.213 26.144 26.144"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 1.151 0.000 26.144 26.144"
" 33 CATCHMENT 100"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 100 No description"
" 0.000 % Impervious"
" 45.000 Total Area"
" 100.000 Flow length"
" 7.000 Overland Slope"
" 45.000 Pervious Area"
" 100.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 7.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 8.520 0.000 26.144 26.144 c.m/sec"
" Catchment 100 Pervious Impervious Total Area "
" Surface Area 45.000 0.000 45.000 hectare"
" Time of concentration 17.293 3.080 17.293 minutes"
" Time to Centroid 239.597 203.358 239.597 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 41.868 0.000 41.868 ha-m"
" Rainfall losses 66.932 101.450 66.932 mm"
" Runoff depth 3.0119 0.0000 3.0120 ha-m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 8.520 0.000 8.520 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 8.520 8.520 26.144 26.144"
" 52 CHANNEL DESIGN"
" 8.520 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.980 metre"
" Velocity 1.760 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.830 metre"
" 53 ROUTE Channel Route 1500"
" 1500.00 Channel Route 1500 Reach length ( metre)"
" 0.455 X-factor <= 0.5"
" 213.100 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 3 No. of sub-reaches"
" Peak outflow 8.436 c.m/sec"
" 8.520 8.520 8.436 26.144 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 8.520 8.436 8.436 26.144"
" 33 CATCHMENT 101"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 101 No description"
" 0.000 % Impervious"
" 11.200 Total Area"
" 50.000 Flow length"
" 7.000 Overland Slope"
" 11.200 Pervious Area"
" 50.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 50.000 Impervious length"
" 7.000 Impervious slope"
" 0.280 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.580 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 2.047 8.436 8.436 26.144 c.m/sec"
" Catchment 101 Pervious Impervious Total Area "
" Surface Area 11.200 0.000 11.200 hectare"
" Time of concentration 14.191 2.032 14.191 minutes"
" Time to Centroid 237.365 202.020 237.365 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 1.2186 0.0000 1.2186 ha-m"
" Rainfall losses 45.642 6.687 45.642 mm"
" Runoff depth 63.158 102.113 63.158 mm"
" Runoff volume 7073.64 0.01 7073.65 c.m"
" Runoff coefficient 0.580 0.000 0.580 "
" Maximum flow 2.047 0.000 2.047 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 2.047 9.854 8.436 26.144"
" 52 CHANNEL DESIGN"
" 9.854 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 1.048 metre"
" Velocity 1.827 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.893 metre"
" 53 ROUTE Channel Route 700"
" 700.00 Channel Route 700 Reach length ( metre)"
" 0.466 X-factor <= 0.5"
" 287.304 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 9.826 c.m/sec"
" 2.047 9.854 9.826 26.144 c.m/sec"

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" 40 HYDROGRAPH Combine 1200"
" 6 Combine "
" 1200 Node #"
" Node taking 100 series for Holtby Drain"
" Maximum flow 9.826 c.m/sec"
" Hydrograph volume 37193.148 c.m"
" 2.047 9.826 9.826"
" 40 HYDROGRAPH Confluence 1200"
" 7 Confluence "
" 1200 Node #"
" Node taking 100 series for Holtby Drain"
" Maximum flow 9.826 c.m/sec"
" Hydrograph volume 37193.148 c.m"
" 2.047 9.826 9.826 0.000"
" 52 CHANNEL DESIGN"
" 9.826 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.226 metre"
" Velocity 1.412 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.891 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 26.564 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.715 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 9.795 c.m/sec"
" 2.047 9.826 9.795 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node #"
" Node at Holtby Drain"
" Maximum flow 33.593 c.m/sec"
" Hydrograph volume 167433.547 c.m"
" 2.047 9.826 9.795 33.593"
" 40 HYDROGRAPH Confluence 1300"
" 7 Confluence "
" 1300 Node #"
" Node at Holtby Drain"
" Maximum flow 33.593 c.m/sec"
" Hydrograph volume 167433.547 c.m"
" 2.047 33.593 9.795 0.000"
" 52 CHANNEL DESIGN"
" 33.593 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 2.099 metre"
" Velocity 1.929 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 1.613 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 19.438 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.833 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 33.550 c.m/sec"
" 2.047 33.593 33.550 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1000"
" 6 Combine "
" 1000 Node #"
" Node upstream of Penetangore Culvert"
" Maximum flow 148.982 c.m/sec"
" Hydrograph volume 1171464.37 c.m"
" 2.047 33.593 33.550 148.982"
" 81 ADD COMMENT"
" Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 40 HYDROGRAPH Confluence 1000"
" 7 Confluence "
" 1000 Node #"
" Node upstream of Penetangore Culvert"
" Maximum flow 148.982 c.m/sec"
" Hydrograph volume 1171464.50 c.m"
" 2.047 148.982 33.550 0.000"
" 81 ADD COMMENT"
" Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 52 CHANNEL DESIGN"
" 148.982 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 3.888 metre"
" Velocity 2.804 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 3.155 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 13.372 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.972 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 148.964 c.m/sec"
" 2.047 148.982 148.964 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
" Node Combining All Flow"
" Maximum flow 148.964 c.m/sec"
" Hydrograph volume 1171464.50 c.m"
" 2.047 148.982 148.964 148.964"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 2.047 0.000 148.964 148.964"
" 33 CATCHMENT 301"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 301 No description"
" 0.000 % Impervious"
" 16.400 Total Area"
" 95.000 Flow length"
" 2.500 Overland Slope"
" 16.400 Pervious Area"
" 95.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 95.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 2.999 0.000 148.964 148.964 c.m/sec"
" Catchment 301 Pervious Impervious Total Area "
" Surface Area 16.400 0.000 16.400 hectare"
" Time of concentration 22.837 4.432 22.837 minutes"
" Time to Centroid 246.332 205.003 246.332 mmn"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 1.7843 0.0000 1.7843 ha-m"
" Rainfall losses 41.842 6.787 41.842 mm"
" Runoff depth 66.958 102.013 66.958 mm"
" Runoff volume 1.0981 0.0000 1.0981 ha-m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 2.999 0.000 2.999 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 2.999 2.999 148.964 148.964"
" 52 CHANNEL DESIGN"
" 2.999 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.568 metre"
" Velocity 1.427 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.479 metre"
" 53 ROUTE Channel Route 480"
" 480.00 Channel Route 480 Reach length (metre)"
" 0.475 X-factor <= 0.5"
" 252.327 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.963 c.m/sec"
" 2.999 2.999 2.963 148.964 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 2.999 2.963 2.963 148.964"
" 33 CATCHMENT 302"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 302 No description"
" 0.000 % Impervious"
" 5.000 Total Area"
" 110.000 Flow length"
" 3.500 Overland Slope"
" 5.000 Pervious Area"
" 110.000 Pervious length"
" 3.500 Pervious slope"
" 0.000 Impervious Area"
" 110.000 Impervious length"
" 3.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.918 2.963 2.963 148.964 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 5.000 0.000 5.000 hectare"
" Time of concentration 22.543 4.374 22.543 minutes"
" Time to Centroid 245.975 204.895 245.974 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 5440.00 0.01 5440.00 c.m"
" Rainfall losses 41.852 6.892 41.852 mm"
" Runoff depth 66.948 101.908 66.948 mm"
" Runoff volume 3347.42 0.01 3347.43 c.m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 0.918 0.000 0.918 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.918 3.849 2.963 148.964"
" 52 CHANNEL DESIGN"
" 3.849 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.642 metre"
" Velocity 1.526 m/sec"

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"      Catchment 402      Pervious      Impervious      Total Area "
"      Surface Area      4.200      0.000      4.200      hectare"
"      Time of concentration 17.891      3.472      17.891      minutes"
"      Time to Centroid 240.348      203.675      240.348      minutes"
"      Rainfall depth 108.800      108.800      108.800      mm"
"      Rainfall volume 4569.60      0.00      4569.60      c.m"
"      Rainfall losses 41.869      7.906      41.869      mm"
"      Runoff depth 66.931      100.894      66.931      mm"
"      Runoff volume 2811.09      0.00      2811.10      c.m"
"      Runoff coefficient 0.615      0.000      0.615      "
"      Maximum flow 0.794      0.000      0.794      c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.794 1.467 0.824 6.720"
" 52 CHANNEL DESIGN"
" 1.467 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.394 metre"
" Velocity 1.170 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.321 metre"
" 53 ROUTE Channel Route 280"
" 280.00 Channel Route 280 Reach length ( metre)"
" 0.469 X-factor <= 0.5"
" 179.524 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.461 c.m/sec"
" 0.794 1.467 1.461 6.720 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.794 1.461 1.461 6.720"
" 33 CATCHMENT 403"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 403 No description"
" 0.000 % Impervious"
" 6.400 Total Area"
" 75.000 Flow length"
" 4.000 Overland Slope"
" 6.400 Pervious Area"
" 75.000 Pervious length"
" 4.000 Pervious slope"
" 0.000 Impervious Area"
" 75.000 Impervious length"
" 4.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 1.213 1.461 1.461 6.720 c.m/sec"
" Catchment 403 Pervious Impervious Total Area "
" Surface Area 6.400 0.000 6.400 hectare"
" Time of concentration 17.211 3.340 17.211 minutes"
" Time to Centroid 239.495 203.637 239.494 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 6963.19 0.01 6963.20 c.m"
" Rainfall losses 41.865 7.618 41.865 mm"
" Runoff depth 66.935 101.182 66.935 mm"
" Runoff volume 4283.85 0.01 4283.85 c.m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 1.213 0.000 1.213 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.213 2.585 1.461 6.720"
" 52 CHANNEL DESIGN"
" 2.585 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.527 metre"
" Velocity 1.370 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.442 metre"
" 53 ROUTE Channel Route 410"
" 410.00 Channel Route 410 Reach length ( metre)"
" 0.473 X-factor <= 0.5"
" 224.449 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.546 c.m/sec"
" 1.213 2.585 2.546 6.720 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 1.213 2.546 2.546 6.720"
" 33 CATCHMENT 404"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 404 No description"
" 0.000 % Impervious"
" 2.700 Total Area"
" 60.000 Flow length"
" 2.500 Overland Slope"
" 2.700 Pervious Area"
" 60.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 60.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.474 0.000 2.956 9.579 c.m/sec"
" Catchment 501 Pervious Impervious Total Area "
" Surface Area 2.500 0.000 2.500 hectare"
" Time of concentration 18.622 3.614 18.622 minutes"
" Time to Centroid 241.214 203.761 241.214 minutes"
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Pervious Initial abstraction"
" 0.511 2.974 2.968 6.720 c.m/sec"
" Catchment 404 Pervious Impervious Total Area "
" Surface Area 2.700 0.000 2.700 hectare"
" Time of concentration 17.334 3.364 17.334 minutes"
" Time to Centroid 239.648 203.622 239.648 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 2937.60 0.00 2937.60 c.m"
" Rainfall losses 41.870 7.660 41.870 mm"
" Runoff depth 66.930 101.140 66.930 mm"
" Runoff volume 1807.10 0.00 1807.10 c.m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 0.511 0.000 0.511 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.511 2.974 2.968 6.720"
" 52 CHANNEL DESIGN"
" 2.974 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.565 metre"
" Velocity 1.423 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.477 metre"
" 53 ROUTE Channel Route 160"
" 160.00 Channel Route 160 Reach length ( metre)"
" 0.427 X-factor <= 0.5"
" 84.301 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.968 c.m/sec"
" 0.511 2.974 2.968 6.720 c.m/sec"
" 40 HYDROGRAPH Combine 2100"
" 6 Combine "
" 2100 Node #"
" Node taking 400 series - dumps into Hwy 21 Ditch"
" Maximum flow 2.968 c.m/sec"
" Hydrograph volume 12654.184 c.m"
" 0.511 2.974 2.968 2.968"
" 40 HYDROGRAPH Confluence 2100"
" 7 Confluence "
" 2100 Node #"
" Node taking 400 series - dumps into Hwy 21 Ditch"
" Maximum flow 2.968 c.m/sec"
" Hydrograph volume 12654.184 c.m"
" 0.511 2.968 2.968 0.000"
" 52 CHANNEL DESIGN"
" 2.968 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.700 metre"
" Velocity 1.033 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.476 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 36.298 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.587 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.956 c.m/sec"
" 0.511 2.968 2.956 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 9.579 c.m/sec"
" Hydrograph volume 38972.008 c.m"
" 0.511 2.968 2.956 9.579"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.511 0.000 2.956 9.579"
" 33 CATCHMENT 501"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 501 No description"
" 0.000 % Impervious"
" 2.500 Total Area"
" 80.000 Flow length"
" 3.500 Overland Slope"
" 2.500 Pervious Area"
" 80.000 Pervious length"
" 3.500 Pervious slope"
" 0.000 Impervious Area"
" 80.000 Impervious length"
" 3.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.474 0.000 2.956 9.579 c.m/sec"
" Catchment 501 Pervious Impervious Total Area "
" Surface Area 2.500 0.000 2.500 hectare"
" Time of concentration 18.622 3.614 18.622 minutes"
" Time to Centroid 241.214 203.761 241.214 minutes"

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" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 2720.00 0.00 2720.00 c.m"
" Rainfall losses 41.907 8.322 41.907 mm"
" Runoff depth 66.893 100.478 66.893 mm"
" Runoff volume 1672.33 0.00 1672.33 c.m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 0.474 0.000 0.474 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff " 0.474 0.474 2.956 9.579"
52 CHANNEL DESIGN"
" 0.474 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.214 metre"
" Velocity 0.837 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.164 metre"
53 ROUTE Channel Route 120"
" 120.00 Channel Route 120 Reach length (metre)"
" 0.459 X-factor <= 0.5"
" 107.579 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.471 0.471 0.471 9.579 c.m/sec"
" 0.474 0.474 0.471 9.579 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link " 0.474 0.471 0.471 9.579"
33 CATCHMENT 502"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 502 No description"
" 0.000 % Impervious"
" 0.500 Total Area"
" 120.000 Flow length"
" 3.500 Overland Slope"
" 0.500 Pervious Area"
" 120.000 Pervious length"
" 3.500 Pervious slope"
" 0.000 Impervious Area"
" 120.000 Impervious length"
" 3.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.090 0.471 0.471 9.579 c.m/sec"
" Catchment 502 Pervious Impervious Total Area "
" Surface Area 0.500 0.000 0.500 hectare"
" Time of concentration 23.751 4.609 23.751 minutes"
" Time to Centroid 247.440 205.288 247.440 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 544.00 0.00 544.00 c.m"
" Rainfall losses 41.826 6.530 41.826 mm"
" Runoff depth 66.974 102.270 66.974 mm"
" Runoff volume 334.87 0.00 334.87 c.m"
" Runoff coefficient 0.616 0.000 0.616 "
" Maximum flow 0.090 0.000 0.090 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff " 0.090 0.561 0.471 9.579"
52 CHANNEL DESIGN"
" 0.561 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.235 metre"
" Velocity 0.881 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.182 metre"
53 ROUTE Channel Route 170"
" 170.00 Channel Route 170 Reach length (metre)"
" 0.468 X-factor <= 0.5"
" 144.690 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.546 0.546 0.546 9.579 c.m/sec"
" 0.090 0.561 0.546 9.579 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link " 0.090 0.546 0.546 9.579"
33 CATCHMENT 503"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 503 No description"
" 0.000 % Impervious"
" 8.200 Total Area"
" 90.000 Flow length"
" 5.000 Overland Slope"
" 8.200 Pervious Area"
" 90.000 Pervious length"
" 5.000 Pervious slope"
" 0.000 Impervious Area"
" 90.000 Impervious length"
" 5.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.615 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" Catchment 503 Pervious Impervious Total Area "
" Surface Area 8.200 0.000 8.200 hectare"
" Time of concentration 22.108 4.290 22.108 minutes"
" Time to Centroid 245.439 204.751 245.439 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 4243.20 0.00 4243.20 c.m"
" Rainfall losses 41.873 7.045 41.873 mm"
" Runoff depth 66.927 101.755 66.927 mm"
" Runoff volume 2610.15 0.00 2610.16 c.m"
" Runoff coefficient 0.615 0.000 0.615 "
" Maximum flow 0.721 0.000 0.721 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff " 0.721 2.773 2.052 9.579"
52 CHANNEL DESIGN"
" 2.773 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.546 metre"
" Velocity 1.397 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.459 metre"
53 ROUTE Channel Route 140"
" 140.00 Channel Route 140 Reach length (metre)"
" 0.419 X-factor <= 0.5"
" 75.183 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.721 2.773 2.726 c.m/sec"
" 0.721 2.773 2.726 9.579 c.m/sec"
40 HYDROGRAPH Combine 2200"
" 6 Combine " 2200
" 2200 Node #"
" Node taking 500 series - dumps into Hwy 21 Ditch"
" Maximum flow 2.726 c.m/sec"
" Hydrograph volume 10105.276 c.m"
" 0.721 2.773 2.726 2.726"
40 HYDROGRAPH Confluence 2200"
" 7 Confluence " 2200
" 2200 Node #"
" Node taking 500 series - dumps into Hwy 21 Ditch"
" Maximum flow 2.726 c.m/sec"
" Hydrograph volume 10105.276 c.m"
" 0.721 2.726 2.726 0.000"
52 CHANNEL DESIGN"

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" 2.726 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.672 metre"
" Velocity 1.010 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.455 metre"
53 ROUTE Channel Route 300"
" 300.00 Channel Route 300 Reach length (metre)"
" 0.391 X-factor <= 0.5"
" 222.784 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.702 c.m/sec"
" 0.721 2.702 0.000 c.m/sec"
40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 12.281 c.m/sec"
" Hydrograph volume 49077.281 c.m"
" 0.721 2.702 12.281"
40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.721 0.000 2.702 12.281"
33 CATCHMENT 603"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 603 No description"
" 0.000 % Impervious"
" 5.600 Total Area"
" 100.000 Flow length"
" 2.500 Overland slope"
" 5.600 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 1.012 0.000 2.702 12.281 c.m/sec"
" Catchment 603 Pervious Impervious Total Area "
" Surface Area 5.600 0.000 5.600 hectare"
" Time of concentration 23.551 4.570 23.551 minutes"
" Time to Centroid 247.186 205.245 247.186 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 6092.79 0.01 6092.80 c.m"
" Rainfall losses 41.829 6.620 41.829 mm"
" Runoff depth 66.971 102.180 66.971 mm"
" Runoff volume 3750.39 0.01 3750.40 c.m"
" Runoff coefficient 0.616 0.000 0.616 "
" Maximum flow 1.012 0.000 1.012 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.012 1.012 2.702 12.281"
52 CHANNEL DESIGN"
" 1.012 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.324 metre"
" Velocity 1.051 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.259 metre"
53 ROUTE Channel Route 260"
" 260.00 Channel Route 260 Reach length (metre)"
" 0.472 X-factor <= 0.5"
" 185.515 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.003 c.m/sec"
" 1.012 1.012 1.003 12.281 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
" 1.012 1.003 1.003 12.281"
33 CATCHMENT 605"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 605 No description"
" 0.000 % Impervious"
" 3.400 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 3.400 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.015 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.614 1.003 1.003 12.281 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
" Surface Area 3.400 0.000 3.400 hectare"
" Time of concentration 23.551 4.570 23.551 minutes"
" Time to Centroid 247.186 205.245 247.186 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 3699.20 0.00 3699.20 c.m"
" Rainfall losses 41.829 6.620 41.829 mm"
" Runoff depth 66.971 102.180 66.971 mm"
" Runoff volume 2277.02 0.00 2277.03 c.m"
" Runoff coefficient 0.616 0.000 0.616 "
" Maximum flow 0.614 0.000 0.614 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.614 1.605 1.003 12.281"
52 CHANNEL DESIGN"
" 1.605 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.200 Gradient %"
" Depth of flow 0.413 metre"
" Velocity 1.200 m/sec"
" Channel capacity 431.989 c.m/sec"
" Critical depth 0.338 metre"
53 ROUTE Channel Route 170"
" 170.00 Channel Route 170 Reach length (metre)"
" 0.447 X-factor <= 0.5"
" 106.256 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.595 c.m/sec"
" 0.614 1.605 1.595 12.281 c.m/sec"
40 HYDROGRAPH Combine 2300"
" 6 Combine "
" 2300 Node #"
" Node taking 600 series - dumps into Hwy 21 Ditch"
" Maximum flow 1.595 c.m/sec"
" Hydrograph volume 6027.422 c.m"
" 0.614 1.605 1.595 1.595"
40 HYDROGRAPH Confluence 2300"
" 7 Confluence "
" 2300 Node #"
" Node taking 600 series - dumps into Hwy 21 Ditch"
" Maximum flow 1.595 c.m/sec"
" Hydrograph volume 6027.422 c.m"
" 0.614 1.595 1.595 0.000"
52 CHANNEL DESIGN"
" 1.595 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.515 metre"
" Velocity 0.873 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.337 metre"
53 ROUTE Channel Route 650"
" 650.00 Channel Route 650 Reach length (metre)"
" 0.420 X-factor <= 0.5"
" 279.063 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
" Peak outflow 1.572 c.m/sec"
" 0.614 1.595 1.572 0.000 c.m/sec"
40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 13.643 c.m/sec"
" Hydrograph volume 55104.695 c.m"
" 0.614 1.595 1.572 13.643"
81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Hwy. 21 Ditch"
40 HYDROGRAPH Confluence 2000"
" 7 Confluence "
" 2000 Node #"
" Node taking 300/400/500/600 series - dumps into Hwy 21 Ditch"
" Maximum flow 13.643 c.m/sec"
" Hydrograph volume 55104.703 c.m"
" 0.614 13.643 1.572 0.000"
81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Hwy. 21 Ditch"
52 CHANNEL DESIGN"
" 13.643 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.420 metre"
" Velocity 1.535 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 1.049 metre"
53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.000 X-factor <= 0.5"
" 24.425 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.747 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 13.641 c.m/sec"
" 0.614 13.643 13.641 0.000 c.m/sec"
40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"

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"      Node Combining All Flow"
"      Maximum flow      153.596  c.m/sec"
"      Hydrograph volume 1226569.12 c.m"
"      0.614  13.643  13.641  153.596"
" 81  ADD COMMENT=====
"      1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40  HYDROGRAPH Confluence 3000"
"      7 Confluence "
" 3000 Node #"
"      Node Combining All Flow"
"      Maximum flow      153.596  c.m/sec"
"      Hydrograph volume 1226569.12 c.m"
"      0.614  153.596  13.641  0.000"
" 81  ADD COMMENT=====
"      1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"

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POST-DEVELOPMENT 5 YEAR

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" MIDUSS Output ----->"
" MIDUSS version Version 2.25 rev. 473"
" MIDUSS created Sunday, February 7, 2010"
" 10 UNITS used: ie METRIC"
" Job folder: C:\Users\derb\Desktop\KBP - Report\"
" 2016 Work\Appendix F - Miduss Modelling\Future"
" Output filename: 08055 - Post 5 Year.out"
" Licensee name: BMROSS - DLE"
" Company: BMROSS"
" Date & Time last used: 6/25/2016 at 10:38:23 AM"
31 TIME PARAMETERS"
" 5.000 Time Step"
" 360.000 Max. Storm length"
" 1800.000 Max. Hydrograph"
32 STORM Mass Curve"
" 3 Mass Curve"
" 58.700 Rainfall depth"
" 360.000 Duration"
" 47 C:\Program Files (x86)\MIDUSS\SCS_6hr_Type2.mrd SCS Type II - 6
hour Distribution - Ontario"
" Maximum intensity 45.786 mm/hr"
" Total depth 58.700 mm"
" 6 005hyd Hydrograph extension used in this file"
81 ADD COMMENT-----"
" 1 Lines of comment"
" Start of Penetangore Tributary"
33 CATCHMENT 50"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 50 No description"
" 0.000 % Impervious"
" 396.000 Total Area"
" 450.000 Flow length"
" 2.500 Overland Slope"
" 396.000 Pervious Area"
" 450.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 450.000 Impervious length"
" 2.500 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.422 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 10.190 0.000 0.000 0.000 c.m/sec"
" Catchment 50 Pervious Impervious Total Area "
" Surface Area 396.000 0.000 396.000 hectare"
" Time of concentration 95.354 13.283 95.354 minutes"
" Time to Centroid 342.104 218.977 342.104 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 23.2452 0.0000 23.2452 ha-m"
" Rainfall losses 33.937 5.504 33.937 mm"
" Runoff depth 24.763 53.196 24.763 mm"
" Runoff volume 9.8061 0.0000 9.8061 ha-m"
" Runoff coefficient 0.422 0.000 0.422 "
" Maximum flow 10.190 0.000 10.190 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 10.190 10.190 0.000 0.000"
52 CHANNEL DESIGN"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.246 metre"
" Velocity 1.425 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.908 metre"
53 ROUTE Channel Route 3000"
" 3000.00 Channel Route 3000 Reach length ( metre)"
" 0.406 X-factor <= 0.5"
" 315.804 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 5 No. of sub-reaches"
" Peak outflow 10.190 10.190 10.018 c.m/sec"
" 10.190 10.190 10.018 0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
" 10.190 10.018 10.018 0.000"
33 CATCHMENT 52"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 52 No description"
" 0.000 % Impervious"
" 196.000 Total Area"
" 250.000 Flow length"
" 7.000 Overland Slope"
" 196.000 Pervious Area"
" 250.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 250.000 Impervious length"
" 7.000 Impervious slope"
" 0.250 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.403 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 7.959 10.018 10.018 0.000 c.m/sec"
" Catchment 52 Pervious Impervious Total Area "
" Surface Area 196.000 0.000 196.000 hectare"
" Time of concentration 49.947 6.855 49.947 minutes"
" Time to Centroid 288.104 211.306 288.104 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 11.5052 0.0000 11.5052 ha-m"
" Rainfall losses 35.049 6.025 35.049 mm"
" Runoff depth 23.651 52.675 23.651 mm"
" Runoff volume 4.6356 0.0000 4.6356 ha-m"
" Runoff coefficient 0.403 0.000 0.403 "
" Maximum flow 7.959 0.000 7.959 c.m/sec"
HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 7.959 12.923 10.018 0.000"
52 CHANNEL DESIGN"
" 12.923 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.400 Gradient %"
" Depth of flow 1.456 metre"
" Velocity 1.393 m/sec"
" Channel capacity 249.409 c.m/sec"
" Critical depth 1.021 metre"
53 ROUTE Channel Route 1300"
" 1300.00 Channel Route 1300 Reach length ( metre)"
" 0.376 X-factor <= 0.5"
" 349.856 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
" Peak outflow 12.836 12.836 12.836 c.m/sec"
" 7.959 12.923 12.836 0.000 c.m/sec"
40 HYDROGRAPH Next link "
" 5 Next link "
" 7.959 12.836 12.836 0.000"
33 CATCHMENT 54"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 54 No description"
" 0.000 % Impervious"
" 39.000 Total Area"
" 140.000 Flow length"
" 11.000 Overland Slope"
" 39.000 Pervious Area"
" 140.000 Pervious length"
" 11.000 Pervious slope"
" 0.000 Impervious Area"
" 140.000 Impervious length"
" 11.000 Impervious slope"
" 0.210 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.422 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 2.426 12.836 12.836 0.000 c.m/sec"
" Catchment 54 Pervious Impervious Total Area "
" Surface Area 39.000 0.000 39.000 hectare"
" Time of concentration 27.329 4.227 27.329 minutes"
" Time to Centroid 259.963 208.037 259.963 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2.2893 0.0000 2.2893 ha-m"
" Rainfall losses 33.953 6.167 33.953 mm"
" Runoff depth 24.747 52.533 24.747 mm"
" Runoff volume 9651.26 0.02 9651.28 c.m"
" Runoff coefficient 0.422 0.000 0.422 "
" Maximum flow 2.426 0.000 2.426 c.m/sec"
40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 2.426 13.266 12.836 0.000"
52 CHANNEL DESIGN"
" 13.266 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.400 Gradient %"
" Depth of flow 1.473 metre"
" Velocity 1.403 m/sec"
" Channel capacity 249.409 c.m/sec"
" Critical depth 1.035 metre"
53 ROUTE Channel Route 800"
" 800.00 Channel Route 800 Reach length ( metre)"
" 0.297 X-factor <= 0.5"
" 213.864 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
" Peak outflow 13.220 13.220 13.220 c.m/sec"
" 2.426 13.266 13.220 0.000 c.m/sec"
40 HYDROGRAPH Combine 10"
" 6 Combine "
" 10 Node #"
" Confluence on Penetangore Tributary"
" Maximum flow 13.220 c.m/sec"
" Hydrograph volume 154068.359 c.m"
" 2.426 13.266 13.220 13.220"
40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 2.426 0.000 13.220 13.220"
33 CATCHMENT 60"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 60 No description"
" 0.000 % Impervious"
" 225.000 Total Area"
" 270.000 Flow length"
" 2.500 Overland Slope"
" 225.000 Pervious Area"
" 270.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"

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52 CHANNEL DESIGN 14.138 30.912 13.869 0.000
30.912 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.500 Gradient %
Depth of flow 2.026 metre
Velocity 1.889 m/sec
Channel capacity 278.848 c.m/sec
Critical depth 1.552 metre
53 ROUTE Channel Route 1300
1300.00 Channel Route 1300 Reach length (metre)
0.367 X-factor <= 0.5
258.058 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
2 No. of sub-reaches
Peak outflow 14.138 30.912 30.822 c.m/sec
HYDROGRAPH Combine 12
6 Combine
12 Node #
Confluence on Penatangore Tributary
Maximum flow 30.822 c.m/sec
Hydrograph volume 310153.156 c.m
HYDROGRAPH Start - New Tributary
2 Start - New Tributary
14.138 0.000 30.822 30.822
33 CATCHMENT 58
1 Triangular SCS
1 Equal length
1 SCS method
58 No description
0.000 % Impervious
82.000 Total Area
140.000 Flow length
15.000 Overland Slope
82.000 Pervious Area
140.000 Pervious length
15.000 Pervious slope
0.000 Impervious Area
140.000 Impervious length
15.000 Impervious slope
0.230 Pervious Manning 'n'
81.000 Pervious SCS Curve No.
0.422 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.958 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
5.207 0.000 30.822 30.822 c.m/sec
Catchment 58 Pervious Impervious Total Area
Surface Area 82.000 0.000 82.000 hectare
Time of concentration 26.297 3.851 26.297 minutes
Time to Centroid 258.726 207.490 258.726 minutes
Rainfall depth 58.700 58.700 58.700 mm
Rainfall volume 4.8134 0.0000 4.8134 ha-m
Rainfall losses 33.952 6.563 33.952 mm
Runoff depth 24.748 52.137 24.748 mm
Runoff volume 2.0293 0.0000 2.0293 ha-m
Runoff coefficient 0.422 0.000 0.422
Maximum flow 5.207 0.000 5.207 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
5.207 5.207 30.822 30.822
52 CHANNEL DESIGN
5.207 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.500 Gradient %
Depth of flow 0.916 metre
Velocity 1.198 m/sec
Channel capacity 278.848 c.m/sec
Critical depth 0.644 metre
53 ROUTE Channel Route 700
700.00 Channel Route 700 Reach length (metre)
0.377 X-factor <= 0.5
219.117 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
2 No. of sub-reaches
Peak outflow 5.207 5.207 5.084 30.822 c.m/sec
HYDROGRAPH Combine 12
6 Combine
12 Node #
Confluence on Penatangore Tributary
Maximum flow 32.000 c.m/sec
Hydrograph volume 330446.219 c.m
HYDROGRAPH Start - New Tributary
2 Start - New Tributary
5.207 0.000 5.084 32.000
33 CATCHMENT 64
1 Triangular SCS
1 Equal length
1 SCS method
64 No description
0.000 % Impervious
80.000 Total Area
220.000 Flow length
5.500 Overland Slope
80.000 Pervious Area
220.000 Pervious length
5.500 Pervious slope
0.000 Impervious Area
220.000 Impervious length
5.500 Impervious slope
0.210 Pervious Manning 'n'
82.000 Pervious SCS Curve No.
0.441 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
5.576 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
3.970 0.000 5.084 32.000 c.m/sec
Catchment 64 Pervious Impervious Total Area
Surface Area 80.000 0.000 80.000 hectare
Time of concentration 43.483 6.825 43.483 minutes
Time to Centroid 278.638 211.270 278.638 minutes
Rainfall depth 58.700 58.700 58.700 mm
Rainfall volume 4.6960 0.0000 4.6960 ha-m
Rainfall losses 32.787 6.061 32.787 mm
Runoff depth 25.913 52.639 25.913 mm
Runoff volume 2.0730 0.0000 2.0730 ha-m
Runoff coefficient 0.441 0.000 0.441
Maximum flow 3.970 0.000 3.970 c.m/sec
HYDROGRAPH Add Runoff
4 Add Runoff
3.970 3.970 5.084 32.000
52 CHANNEL DESIGN
3.970 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.500 Gradient %
Depth of flow 0.806 metre
Velocity 1.116 m/sec
Channel capacity 278.848 c.m/sec
Critical depth 0.558 metre
53 ROUTE Channel Route 700
700.00 Channel Route 700 Reach length (metre)
0.390 X-factor <= 0.5
235.253 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
2 No. of sub-reaches
Peak outflow 3.970 3.970 3.952 32.000 c.m/sec
HYDROGRAPH Combine 12
6 Combine
12 Node #
Confluence on Penatangore Tributary
Maximum flow 33.877 c.m/sec
Hydrograph volume 351176.438 c.m
HYDROGRAPH Confluence 12
7 Confluence
12 Node #
Confluence on Penatangore Tributary
Maximum flow 33.877 c.m/sec
Hydrograph volume 351176.406 c.m
CHANNEL DESIGN
33.877 Current peak flow c.m/sec
0.040 Manning 'n'
0. Cross-section type: 0=trapezoidal; 1=general
2.000 Basewidth metre
3.000 Left bank slope
3.000 Right bank slope
5.000 Channel depth metre
0.300 Gradient %
Depth of flow 2.347 metre
Velocity 1.597 m/sec
Channel capacity 215.995 c.m/sec
Critical depth 1.620 metre
53 ROUTE Channel Route 2500
2500.00 Channel Route 2500 Reach length (metre)
0.303 X-factor <= 0.5
391.350 K-lag (seconds)
0.000 Default(0) or user spec.(1) values used
0.500 X-factor <= 0.5
30.000 K-lag (seconds)
0.500 Beta weighting factor
300.000 Routing time step (seconds)
3 No. of sub-reaches
Peak outflow 3.970 33.877 33.438 0.000 c.m/sec
HYDROGRAPH Combine 1000
6 Combine
1000 Node #
Node upstream of Penatangore Culvert
Maximum flow 33.438 c.m/sec
Hydrograph volume 351176.469 c.m
HYDROGRAPH Start - New Tributary
2 Start - New Tributary
3.970 0.000 33.438 33.438
33 CATCHMENT 59
1 Triangular SCS
1 Equal length
1 SCS method
59 No description
0.000 % Impervious
128.000 Total Area
170.000 Flow length
18.000 Overland Slope
128.000 Pervious Area
170.000 Pervious length
18.000 Pervious slope
0.000 Impervious Area
170.000 Impervious length
18.000 Impervious slope
0.350 Pervious Manning 'n'
76.000 Pervious SCS Curve No.
0.334 Pervious Runoff coefficient
0.100 Pervious Ia/S coefficient
8.021 Pervious Initial abstraction
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No.
0.000 Impervious Runoff coefficient
0.100 Impervious Ia/S coefficient
0.518 Impervious Initial abstraction
5.037 0.000 33.438 33.438 c.m/sec
Catchment 59 Pervious Impervious Total Area
Surface Area 128.000 0.000 128.000 hectare
Time of concentration 38.873 4.097 38.873 minutes

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"      Time to Centroid      277.849      207.770      277.849      minutes"
"      Rainfall depth        58.700      58.700      58.700      mm"
"      Rainfall volume       7.5136     0.0000     7.5136     ha-m"
"      Rainfall losses       39.083     6.349      39.083     mm"
"      Runoff depth          19.617     52.351     19.617     mm"
"      Runoff volume          2.5109     0.0000     2.5110     ha-m"
"      Runoff coefficient     0.334      0.000      0.334      "
"      Maximum flow           5.037      0.000      5.037      c.m/sec"
40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "        5.037      5.037      33.438     33.438"
52  CHANNEL DESIGN"
"      5.037 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.300 Gradient %"
"      Depth of flow          1.015      metre"
"      Velocity                0.983      m/sec"
"      Channel capacity        215.995    c.m/sec"
"      Critical depth          0.633      metre"
53  ROUTE Channel Route 1500"
"      1500.00 Channel Route 1500 Reach length (metre)"
"      0.344 X-factor <= 0.5"
"      381.434 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      300.000 Routing time step (seconds)"
"      3 No. of sub-reaches"
"      Peak outflow            4.776      c.m/sec"
"      5.037 5.037 4.776 33.438 c.m/sec"
40  HYDROGRAPH Combine 1000"
"      6 Combine "
"      1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow            35.159     c.m/sec"
"      Hydrograph volume       376286.094 c.m"
"      5.037 5.037 4.776 35.159"
81  ADD COMMENT"
"      1 Lines of comment"
"      End of Penetangore Tributary"
"      ADD COMMENT"
"      1 Lines of comment"
"      Start of Area North of Holtby Drain"
40  HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      5.037 0.000 4.776 35.159"
33  CATCHMENT 201"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      201 No description"
"      0.000 % Impervious"
"      166.000 Total Area"
"      250.000 Flow length"
"      3.000 Overland Slope"
"      166.000 Pervious Area"
"      250.000 Pervious length"
"      3.000 Pervious slope"
"      0.000 Impervious Area"
"      250.000 Impervious length"
"      3.000 Impervious slope"
"      0.200 Pervious Manning 'n'"
"      82.000 Pervious SCS Curve No."
"      0.441 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.576 Pervious Initial abstraction"
"      0.013 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.000 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      7.058 0.000 4.776 35.159 c.m/sec"
"      Catchment 201 Pervious Impervious Total Area "
"      Surface Area 166.000 0.000 166.000 hectare"
"      Time of concentration 54.688 8.838 54.688 minutes"
"      Time to Centroid 292.169 213.640 292.169 minutes"
"      Rainfall depth 58.700 58.700 58.700 mm"
"      Rainfall volume 9.7442 0.0000 9.7442 ha-m"
"      Rainfall losses 32.785 5.456 32.785 mm"
"      Runoff depth 25.915 53.244 25.915 mm"
"      Runoff volume 4.3019 0.0000 4.3019 ha-m"
"      Runoff coefficient 0.441 0.000 0.441 "
"      Maximum flow 7.058 0.000 7.058 c.m/sec"
40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "        7.058      7.058      4.776      35.159"
52  CHANNEL DESIGN"
"      7.058 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      1.000 Gradient %"
"      Depth of flow          0.898      metre"
"      Velocity                1.676      m/sec"
"      Channel capacity        394.351    c.m/sec"
"      Critical depth          0.754      metre"
53  ROUTE Channel Route 1900"
"      1900.00 Channel Route 1900 Reach length (metre)"
"      0.467 X-factor <= 0.5"
"      283.487 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      300.000 Routing time step (seconds)"
"      3 No. of sub-reaches"
"      Peak outflow            7.014      c.m/sec"
"      7.058 7.058 7.014 35.159 c.m/sec"
40  HYDROGRAPH Next link "
"      5 Next link "        7.058      7.014      35.159"
33  CATCHMENT 202"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      202 No description"
"      0.000 % Impervious"
"      4.000 Total Area"
"      0.920 0.920 0.920 metre"
"      1.699 1.699 1.699 m/sec"
"      394.351 394.351 c.m/sec"
"      0.774 0.774 metre"
53  ROUTE Channel Route 350"
"      350.00 Channel Route 350 Reach length (metre)"
"      0.438 X-factor <= 0.5"
"      154.502 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow            7.356      c.m/sec"
"      0.304 7.444 7.356 35.159 c.m/sec"
40  HYDROGRAPH Combine 1100"

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"      6 Combine "
1100 Node #
"      Node taking 200 series - Bottom end of Holtby Drain"
"      Maximum flow 7.356 c.m/sec"
"      Hydrograph volume 46414.406 c.m"
"      0.304 7.444 7.356 7.356"
81 ADD COMMENT-----
1 Lines of comment"
" End of Area North of Holtby Drain"
" HYDROGRAPH Start - New Tributary"
40 2 Start - New Tributary"
"      0.304 0.000 7.356 7.356"
81 ADD COMMENT-----
1 Lines of comment"
" Start of Holtby Drain"
33 CATCHMENT 100"
1 Triangular SCS"
1 Equal length"
1 SCS method"
100 No description"
0.000 % Impervious"
45.000 Total Area"
100.000 Flow length"
7.000 Overland Slope"
45.000 Pervious Area"
100.000 Pervious length"
7.000 Pervious slope"
0.000 Impervious Area"
100.000 Impervious length"
7.000 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.441 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
"      3.058 0.000 7.356 7.356 c.m/sec"
" Catchment 100 Pervious Impervious Total Area "
" Surface Area 45.000 0.000 45.000 hectare"
" Time of concentration 24.476 3.956 24.476 minutes"
" Time to Centroid 255.680 207.565 255.680 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2,6415 0.0000 2,6415 ha-m"
" Rainfall losses 32.802 6.485 32.802 mm"
" Runoff depth 25.898 52.215 25.898 mm"
" Runoff volume 1.1654 0.0000 1.1654 ha-m"
" Runoff coefficient 0.441 0.000 0.441 "
" Maximum flow 3.058 0.000 3.058 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
"      3.058 3.058 7.356 7.356"
52 CHANNEL DESIGN"
3.058 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.000 Gradient %"
" Depth of flow 0.600 metre"
" Velocity 1.342 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.484 metre"
53 ROUTE Channel Route 1500"
1500.00 Channel Route 1500 Reach length ( metre)"
0.470 X-factor <= 0.5"
279.420 K-lag ( seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
3 No. of sub-reaches"
" Peak outflow 3.058 3.058 3.022 7.356 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link "
"      3.058 3.022 3.022 7.356"
33 CATCHMENT 101"
1 Triangular SCS"
1 Equal length"
1 SCS method"
101 No description"
0.000 % Impervious"
11.200 Total Area"
50.000 Flow length"
7.000 Overland Slope"
11.200 Pervious Area"
50.000 Pervious length"
7.000 Pervious slope"
0.000 Impervious Area"
50.000 Impervious length"
7.000 Impervious slope"
0.280 Pervious Manning 'n'"
80.000 Pervious SCS Curve No."
0.403 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
6.350 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
"      0.145 0.000 3.403 3.403 c.m/sec"
" Catchment 604 Pervious Impervious Total Area "
" Surface Area 11.200 0.000 11.200 hectare"
" Time of concentration 20.355 2.610 20.355 minutes"
" Time to Centroid 252.367 206.029 252.367 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 6574.39 0.01 6574.40 c.m"
" Rainfall losses 35.069 6.188 35.069 mm"
" Runoff depth 23.631 52.512 23.631 mm"
" Runoff volume 2646.69 0.01 2646.70 c.m"
" Runoff coefficient 0.403 0.000 0.403 "
" Maximum flow 0.751 0.000 0.751 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
"      0.751 3.456 3.022 7.356"
52 CHANNEL DESIGN"
3.456 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
2.000 Gradient %"
" Depth of flow 0.094 metre"
" Velocity 0.673 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.078 metre"
53 ROUTE Channel Route 250"

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" 250.00 Channel Route 250 Reach length ( metre) "
" 0.495 X-factor <= 0.5"
" 278.724 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.145 0.145 0.144 c.m/sec"
" 3.403 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.145 0.144 0.144 3.403"
" 33 CATCHMENT 605"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 605 No description"
" 0.000 % Impervious"
" 3.900 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 3.900 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.462 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.209 0.144 0.144 3.403 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
" Surface Area 3.900 0.000 3.900 hectare"
" Time of concentration 41.904 5.387 41.904 minutes"
" Time to Centroid 275.864 209.467 275.863 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 2289.30 0.00 2289.30 c.m"
" Rainfall losses 31.585 5.391 31.585 mm"
" Runoff depth 27.115 53.309 27.115 mm"
" Runoff volume 1057.47 0.00 1057.47 c.m"
" Runoff coefficient 0.462 0.000 0.462 "
" Maximum flow 0.209 0.000 0.209 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.209 0.349 0.144 3.403"
" 52 CHANNEL DESIGN"
" 0.349 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.156 metre"
" Velocity 0.904 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.136 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length ( metre)"
" 0.489 X-factor <= 0.5"
" 166.002 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.209 0.349 0.348 c.m/sec"
" 3.403 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 0.348 c.m/sec"
" Hydrograph volume 1789.568 c.m"
" 0.209 0.349 0.348 0.348"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.209 0.000 0.348 0.348"
" 33 CATCHMENT 603"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 603 No description"
" 0.000 % Impervious"
" 5.600 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 5.600 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.462 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.300 0.000 0.348 0.348 c.m/sec"
" Catchment 603 Pervious Impervious Total Area "
" Surface Area 5.600 0.000 5.600 hectare"
" Time of concentration 41.904 5.387 41.904 minutes"
" Time to Centroid 275.863 209.467 275.863 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 3287.20 0.00 3287.20 c.m"
" Rainfall losses 31.585 5.391 31.585 mm"
" Runoff depth 27.115 53.309 27.115 mm"
" Runoff volume 1518.42 0.00 1518.42 c.m"
" Runoff coefficient 0.462 0.000 0.462 "
" Maximum flow 0.300 0.000 0.300 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.329 0.329 0.641 0.641"
" 52 CHANNEL DESIGN"
" 0.329 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.063 metre"
" Velocity 0.941 m/sec"
" 4 Add Runoff "
" 0.300 0.300 0.348 0.348"
" 52 CHANNEL DESIGN"
" 0.300 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.144 metre"
" Velocity 0.860 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.124 metre"
" 53 ROUTE Channel Route 225"
" 225.00 Channel Route 225 Reach length ( metre)"
" 0.491 X-factor <= 0.5"
" 196.220 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.300 0.300 0.298 c.m/sec"
" 0.300 0.300 0.298 0.348 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 0.646 c.m/sec"
" Hydrograph volume 3307.991 c.m"
" 0.300 0.300 0.298 0.646"
" 40 HYDROGRAPH Confluence 4000"
" 7 Confluence "
" 4000 Node #"
" Maximum flow 0.646 c.m/sec"
" Hydrograph volume 3307.991 c.m"
" 0.300 0.646 0.298 0.000"
" 52 CHANNEL DESIGN"
" 0.646 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.322 metre"
" Velocity 0.676 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.198 metre"
" 53 ROUTE Channel Route 500"
" 500.00 Channel Route 500 Reach length ( metre)"
" 0.431 X-factor <= 0.5"
" 277.247 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
" Peak outflow 0.300 0.646 0.641 c.m/sec"
" 0.300 0.646 0.641 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 0.641 c.m/sec"
" Hydrograph volume 3307.989 c.m"
" 0.300 0.646 0.641 0.641"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.300 0.000 0.641 0.641"
" 33 CATCHMENT 405"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 405 No description"
" 75.000 % Impervious"
" 3.200 Total Area"
" 75.000 Flow length"
" 2.000 Overland Slope"
" 0.800 Pervious Area"
" 75.000 Pervious length"
" 2.000 Pervious slope"
" 2.400 Impervious Area"
" 75.000 Impervious length"
" 2.000 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.462 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.906 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.329 0.000 0.641 0.641 c.m/sec"
" Catchment 405 Pervious Impervious Total Area "
" Surface Area 0.800 2.400 3.200 hectare"
" Time of concentration 37.702 4.847 9.617 minutes"
" Time to Centroid 270.785 208.951 217.929 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 1408.80 1878.40 3287.20 c.m"
" Rainfall losses 31.589 5.497 37.086 mm"
" Runoff depth 27.111 53.203 46.680 mm"
" Runoff volume 1276.87 1493.76 2770.63 c.m"
" Runoff coefficient 0.462 0.906 0.795 "
" Maximum flow 0.046 0.300 0.329 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.329 0.329 0.641 0.641"
" 52 CHANNEL DESIGN"
" 0.329 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.063 metre"
" Velocity 0.941 m/sec"

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" Hydrograph volume 4708.711 c.m"
" 0.564 1.027 0.558 0.000"
" 52 CHANNEL DESIGN"
" 1.027 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.114 metre"
" Velocity 1.310 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.141 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.471 X-factor <= 0.5"
" 28.626 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 30.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.025 c.m/sec"
" 0.564 1.027 1.025 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.564 1.025 1.025 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" EXISTING POND - DRY POND - CTC SITE"
" 54 POND DESIGN"
" 1.025 Current peak flow c.m/sec"
" 0.635 Target outflow c.m/sec"
" 4708.7 Hydrograph volume c.m"
" 15. Number of stages"
" 0.000 Minimum water level metre"
" 1.400 Maximum water level metre"
" 0.000 Starting water level metre"
" 0 Keep Design Data: 1 = True; 0 = False"
" Level Discharge Volume"
" 0.000 0.000 0.000"
" 0.1000 0.00276 124.985"
" 0.2000 0.00477 256.026"
" 0.3000 0.00616 393.250"
" 0.4000 0.00729 536.786"
" 0.5000 0.00827 686.761"
" 0.6000 0.00914 843.304"
" 0.7000 0.00994 1006.543"
" 0.8000 0.01068 1176.605"
" 0.9000 0.2200 1353.618"
" 1.000 0.6243 1537.711"
" 1.100 1.178 1729.012"
" 1.200 1.871 1927.648"
" 1.300 2.698 2133.748"
" 1.400 3.658 2347.440"
" 1. WEIRS"
" Crest Weir Crest Left Right"
" elevation coefficient breadth sideslope sideslope"
" 0.800 0.980 3.800 2.000 2.000"
" 1. ORIFICES"
" Orifice Orifice Orifice Number of"
" invert coefficient diameter orifices"
" 0.000 0.630 0.0750 1.000"
" 2. LAYERS"
" Bottom Aspect Bottom Top Average"
" area ratio elevation elevation sideslope"
" 1220.000 2.000 0.000 1.400 4.000"
" 2175.299 1.688 1.400 1.400 4.000"
" Peak outflow 0.956 c.m/sec"
" Maximum level 1.060 metre"
" Maximum storage 1652.806 c.m"
" Centroidal lag 10.237 hours"
" 0.564 1.025 0.956 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.564 0.956 0.956 0.000"
" 52 CHANNEL DESIGN"
" 0.956 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.396 metre"
" Velocity 0.757 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.250 metre"
" 53 ROUTE Channel Route 220"
" 220.00 Channel Route 220 Reach length ( metre)"
" 0.406 X-factor <= 0.5"
" 217.931 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.934 c.m/sec"
" 0.564 0.956 0.934 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 1.217 c.m/sec"
" Hydrograph volume 7538.245 c.m"
" 0.564 0.956 0.934 1.217"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.564 0.000 0.934 1.217"
" 33 CATCHMENT 750"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 750 No description"
" 100.000 % Impervious"
" 0.500 Total Area"
" 50.000 Flow length"
" 2.000 Overland Slope"
" 0.000 Pervious Area"
" 50.000 Pervious length"
" 2.000 Pervious slope"
" 0.500 Impervious Area"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.887 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.025 0.000 0.008 1.223 c.m/sec"

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"      Catchment 751      Pervious      Impervious      Total Area "
"      Surface Area      0.000      0.200      0.200      hectare"
"      Time of concentration 23.863      3.800      3.800      minutes"
"      Time to Centroid 255.790      207.443      207.443      minutes"
"      Rainfall depth 58.700      58.700      58.700      mm"
"      Rainfall volume 0.00      117.40      117.40      c.m"
"      Rainfall losses 33.956      6.612      6.612      mm"
"      Runoff depth 24.744      52.088      52.088      mm"
"      Runoff volume 0.00      104.18      104.18      c.m"
"      Runoff coefficient 0.000      0.887      0.887      "
"      Maximum flow 0.000      0.025      0.025      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff " " 53
"      0.025      0.025      0.008      1.223"
" 81  ADD COMMENT=====
" 1 Lines of comment"
"      EXISTING POND - PARKING LOT STORAGE - CTC SITE"
" 54  POND DESIGN"
"      0.025 Current peak flow c.m/sec"
"      0.020 Target outflow c.m/sec"
"      104.2 Hydrograph volume c.m"
"      5. Number of stages"
"      0.000 Minimum water level metre"
"      0.700 Maximum water level metre"
"      0.000 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.000"
"      0.1750 0.01148 16.645"
"      0.3500 0.03242 39.036"
"      0.5250 0.04289 67.860"
"      0.7000 0.05126 103.803"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coeffic diameter orifices"
"      0.000 0.630 0.1750 1.000"
"      1. LAYERS"
"      Bottom Aspect Bottom Top Average"
"      area ratio elevation elevation sideslope"
"      80.000 3.000 0.000 0.700 4.000"
"      Peak outflow 0.019 c.m/sec"
"      Maximum level 0.243 metre"
"      Maximum storage 25.361 c.m"
"      Centrifugal lag 3.848 hours"
"      0.025 0.025 0.019 1.223 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link " " 40
"      0.025 0.019 0.019 1.223"
" 52  CHANNEL DESIGN"
"      0.019 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.043 metre"
"      Velocity 0.208 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.021 metre"
" 53  ROUTE Channel Route 50"
"      50.000 Channel Route 50 Reach length (metre)"
"      0.449 X-factor <= 0.5"
"      180.560 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.019 c.m/sec"
"      0.025 0.019 0.019 1.223 c.m/sec"
" 40  HYDROGRAPH Combine 2000"
"      6 Combine "
"      2000 Node #"
"      Flow in Hwy. 21 Ditch"
"      Maximum flow 1.241 c.m/sec"
"      Hydrograph volume 7866.554 c.m"
"      0.025 0.019 1.241"
" 81  ADD COMMENT=====
" 1 Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
" 40  HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.025 0.000 0.019 1.241"
" 33  CATCHMENT 301"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      301 No description"
"      0.000 % Impervious"
"      16.400 Total Area"
"      95.000 Flow length"
"      2.500 Overland Slope"
"      16.400 Pervious Area"
"      95.000 Pervious length"
"      2.500 Pervious slope"
"      0.000 Impervious Area"
"      95.000 Impervious length"
"      2.500 Impervious slope"
"      0.230 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.422 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.013 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.000 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.877 0.000 0.019 1.241 c.m/sec"
"      Catchment 301 Pervious Impervious Total Area "
"      Surface Area 16.400 0.000 16.400 hectare"
"      Time of concentration 35.671 5.224 35.671 minutes"
"      Time to Centroid 270.049 209.250 270.048 minutes"
"      Rainfall depth 58.700 58.700 58.700 mm"
"      Rainfall volume 9626.79 0.01 9626.80 c.m"
"      Rainfall losses 33.943 5.395 33.943 mm"
"      Runoff depth 24.757 53.305 24.757 mm"
"      Runoff volume 4060.16 0.01 4060.17 c.m"
"      Runoff coefficient 0.422 0.000 0.422 "
"      Maximum flow 0.877 0.000 0.877 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff " " 52
"      0.877 0.877 0.019 1.241"
" 52  CHANNEL DESIGN"
"      1.017 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      1.200 Gradient %"
"      Depth of flow 0.325 metre"
"      Velocity 1.053 m/sec"
"      Channel capacity 431.989 c.m/sec"
"      Critical depth 0.260 metre"
" 53  ROUTE Channel Route 150"
"      150.000 Channel Route 150 Reach length (metre)"
"      0.452 X-factor <= 0.5"
"      106.874 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      100.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 1.004 c.m/sec"
"      0.188 1.017 1.004 1.241 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link " " 33
"      0.188 1.004 1.004 1.241"
" 33  CATCHMENT 402"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      402 No description"
"      50.000 % Impervious"
"      7.400 Total Area"
"      100.000 Flow length"
"      2.000 Overland Slope"
"      3.700 Pervious Area"
"      100.000 Pervious length"
"      2.000 Pervious slope"
"      3.700 Impervious Area"
"      100.000 Impervious length"
"      2.000 Impervious slope"
"      0.300 Pervious Manning 'n'"
"      83.000 Pervious SCS Curve No."
"      0.462 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.202 Pervious Initial abstraction"
"      0.013 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.905 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      0.558 1.004 1.004 1.241 c.m/sec"
"      Catchment 402 Pervious Impervious Total Area "
"      Surface Area 3.700 3.700 7.400 hectare"
"      Time of concentration 44.806 5.760 18.954 minutes"
"      Time to Centroid 279.367 209.866 233.351 minutes"
"      Rainfall depth 58.700 58.700 58.700 mm"
"      Rainfall volume 2171.90 2171.90 4343.80 c.m"

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" Rainfall losses 31.587 5.576 18.581 mm"
" Runoff depth 27.113 53.124 40.119 mm"
" Runoff volume 1003.20 1965.58 2968.78 c.m"
" Runoff coefficient 0.462 0.905 0.683 "
" Maximum flow 0.189 0.474 0.558 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
0.558 1.322 1.004 1.241"
52 CHANNEL DESIGN"
1.322 Current peak flow c.m/sec"
0.020 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
4.000 Basewidth metre"
50.000 Left bank slope"
0.000 Right bank slope"
0.300 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.130 metre"
Velocity 1.405 m/sec"
Channel capacity 7.740 c.m/sec"
Critical depth 0.161 metre"
53 ROUTE Channel Route 200"
200.00 Channel Route 200 Reach length (metre)"
0.492 X-factor <= 0.5"
106.762 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
100.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 1.315 c.m/sec"
0.558 1.322 1.315 1.241 c.m/sec"
40 HYDROGRAPH Combine 6000"
6 Combine "
6000 Node #"
Maximum flow 1.315 c.m/sec"
Hydrograph volume 8547.629 c.m"
0.558 1.322 1.315 1.315"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
0.558 0.000 1.315 1.315"
33 CATCHMENT 501"
1 Triangular SCS"
1 Equal length"
1 SCS method"
501 No description"
0.000 % Impervious"
2.500 Total Area"
80.000 Flow length"
3.500 Overland Slope"
2.500 Pervious Area"
80.000 Pervious length"
3.500 Pervious slope"
0.000 Impervious Area"
80.000 Impervious length"
3.500 Impervious slope"
0.300 Pervious Manning 'n'"
83.000 Pervious SCS Curve No."
0.462 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.202 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.153 0.000 1.315 1.315 c.m/sec"
Catchment 501 Pervious Impervious Total Area "
Surface Area 2.500 0.000 2.500 hectare"
Time of concentration 33.134 4.260 33.134 minutes"
Time to Centroid 265.254 208.101 265.254 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 1467.50 0.00 1467.50 c.m"
Rainfall losses 31.591 6.131 31.591 mm"
Runoff depth 27.109 52.569 27.109 mm"
Runoff volume 677.72 0.00 677.72 c.m"
Runoff coefficient 0.462 0.000 0.462 "
Maximum flow 0.153 0.000 0.153 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
0.153 0.153 1.315 1.315"
52 CHANNEL DESIGN"
0.153 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.113 metre"
Velocity 0.579 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.081 metre"
53 ROUTE Channel Route 100"
100.00 Channel Route 100 Reach length (metre)"
0.473 X-factor <= 0.5"
129.456 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
100.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.152 c.m/sec"
0.153 0.153 0.152 1.315 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link "
0.153 0.152 0.152 1.315"
33 CATCHMENT 403"
1 Triangular SCS"
1 Equal length"
1 SCS method"
403 No description"
75.000 % Impervious"
4.700 Total Area"
70.000 Flow length"
2.000 Overland Slope"
1.175 Pervious Area"
70.000 Pervious length"
2.000 Pervious slope"
3.525 Impervious Area"
70.000 Impervious length"
2.000 Impervious slope"
0.300 Pervious Manning 'n'"
83.000 Pervious SCS Curve No."
0.462 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.202 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.895 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.330 0.000 0.552 1.639 c.m/sec"
Catchment 404 Pervious Impervious Total Area "
Surface Area 0.800 2.400 3.200 hectare"
Time of concentration 32.978 4.240 8.457 minutes"
Time to Centroid 265.070 208.062 216.427 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 469.60 1408.80 1878.40 c.m"
Rainfall losses 31.590 6.152 12.512 mm"
Runoff depth 27.110 52.548 46.188 mm"
Runoff volume 216.88 1261.15 1478.03 c.m"
Runoff coefficient 0.462 0.895 0.787 "
Maximum flow 0.049 0.295 0.330 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
0.330 0.330 0.552 1.639"
52 CHANNEL DESIGN"
0.330 Current peak flow c.m/sec"
0.020 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
4.000 Basewidth metre"
50.000 Left bank slope"
0.000 Right bank slope"
0.300 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.063 metre"
Velocity 0.942 m/sec"
Channel capacity 7.740 c.m/sec"
Critical depth 0.075 metre"
53 ROUTE Channel Route 100"
100.00 Channel Route 100 Reach length (metre)"
0.491 X-factor <= 0.5"
79.631 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
75.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.327 c.m/sec"
0.330 0.330 0.327 1.639 c.m/sec"
40 HYDROGRAPH Combine 6000"
6 Combine "
6000 Node #"

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"
"
" Maximum flow 1.766 c.m/sec"
" Hydrograph volume 12889.928 c.m"
" 0.330 0.330 0.327 1.766"
" 40 HYDROGRAPH Confluence 6000"
" 7 Confluence "
" 6000 Node #"
"
" Maximum flow 1.766 c.m/sec"
" Hydrograph volume 12889.927 c.m"
" 0.330 1.766 0.327 0.000"
" 52 CHANNEL DESIGN"
" 1.766 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.150 metre"
" Velocity 1.521 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.187 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length (metre)"
" 0.491 X-factor <= 0.5"
" 98.647 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.758 c.m/sec"
" 0.330 1.766 1.758 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
" Maximum flow 1.758 c.m/sec"
" Hydrograph volume 12889.932 c.m"
" 0.330 1.766 1.758 1.758"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.330 0.000 1.758 1.758"
" 33 CATCHMENT 302"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 302 No description"
" 50.000 % Impervious"
" 6.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 3.000 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.000 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious Manning 'n'"
" 0.280 Pervious SCS Curve No."
" 80.000 Pervious SCS Curve No."
" 0.403 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.905 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.437 0.000 1.758 1.758 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 3.000 3.000 6.000 hectare"
" Time of concentration 44.926 5.760 17.825 minutes"
" Time to Centroid 282.036 209.866 232.097 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 1761.00 1761.00 3522.00 c.m"
" Rainfall losses 35.051 5.576 20.314 mm"
" Runoff depth 23.649 53.124 38.386 mm"
" Runoff volume 709.46 1593.72 2303.18 c.m"
" Runoff coefficient 0.403 0.905 0.654 "
" Maximum flow 0.131 0.384 0.437 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.437 0.437 1.758 1.758"
" 52 CHANNEL DESIGN"
" 0.437 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.073 metre"
" Velocity 1.025 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.088 metre"
" 53 ROUTE Channel Route 180"
" 180.00 Channel Route 180 Reach length (metre)"
" 0.495 X-factor <= 0.5"
" 131.757 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.428 c.m/sec"
" 0.437 0.437 0.428 1.758 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.437 0.428 0.428 1.758"
" 33 CATCHMENT 303"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 303 No description"
" 75.000 % Impervious"
" 4.800 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 1.200 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.600 Impervious Area"
" 100.000 Impervious length"
" 2.000 Impervious slope"
" 2.000 Impervious Manning 'n'"
" 0.280 Pervious SCS Curve No."
" 80.000 Pervious SCS Curve No."
" 0.403 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.905 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.437 0.000 1.758 1.758 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 3.000 3.000 6.000 hectare"
" Time of concentration 44.926 5.760 17.825 minutes"
" Time to Centroid 282.036 209.866 232.097 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 1761.00 1761.00 3522.00 c.m"
" Rainfall losses 35.051 5.576 20.314 mm"
" Runoff depth 23.649 53.124 38.386 mm"
" Runoff volume 709.46 1593.72 2303.18 c.m"
" Runoff coefficient 0.403 0.905 0.654 "
" Maximum flow 0.131 0.384 0.437 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.437 0.437 1.758 1.758"
" 52 CHANNEL DESIGN"
" 0.437 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.060 metre"
" Velocity 0.915 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.071 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length (metre)"
" 0.492 X-factor <= 0.5"
" 81.975 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.298 c.m/sec"
" 0.300 0.300 0.298 2.594 c.m/sec"
" 100.000 Impervious length"
" 2.000 Impervious slope"
" 0.280 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.441 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.905 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.480 0.428 0.428 1.758 c.m/sec"
" Catchment 303 Pervious Impervious Total Area "
" Surface Area 1.200 3.600 4.800 hectare"
" Time of concentration 43.615 5.760 11.054 minutes"
" Time to Centroid 278.798 209.866 219.505 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 704.40 2113.20 2817.60 c.m"
" Rainfall losses 32.787 5.576 12.379 mm"
" Runoff depth 25.913 53.124 46.321 mm"
" Runoff volume 310.95 1912.46 2223.41 c.m"
" Runoff coefficient 0.441 0.905 0.789 "
" Maximum flow 0.059 0.461 0.480 c.m/sec"
" HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.480 0.480 0.480 1.758"
" 52 CHANNEL DESIGN"
" 0.907 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.107 metre"
" Velocity 1.265 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.132 metre"
" 53 ROUTE Channel Route 250"
" 250.00 Channel Route 250 Reach length (metre)"
" 0.494 X-factor <= 0.5"
" 148.203 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.893 c.m/sec"
" 0.480 0.907 0.893 1.758 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
" Maximum flow 2.594 c.m/sec"
" Hydrograph volume 17416.518 c.m"
" 0.480 0.907 0.893 2.594"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.480 0.000 0.893 2.594"
" 33 CATCHMENT 407"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 407 No description"
" 75.000 % Impervious"
" 3.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 0.750 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 2.250 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.462 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.905 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.300 0.000 0.893 2.594 c.m/sec"
" Catchment 407 Pervious Impervious Total Area "
" Surface Area 0.750 2.250 3.000 hectare"
" Time of concentration 44.806 5.760 11.437 minutes"
" Time to Centroid 279.367 209.866 219.971 minutes"
" Rainfall depth 58.700 58.700 58.700 mm"
" Rainfall volume 440.25 1320.75 1761.00 c.m"
" Rainfall losses 31.587 5.576 12.079 mm"
" Runoff depth 27.113 53.124 46.621 mm"
" Runoff volume 203.35 1195.29 1398.64 c.m"
" Runoff coefficient 0.462 0.905 0.794 "
" Maximum flow 0.038 0.288 0.300 c.m/sec"
" HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.300 0.300 0.893 2.594"
" 52 CHANNEL DESIGN"
" 0.300 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.060 metre"
" Velocity 0.915 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.071 metre"

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" 40 HYDROGRAPH Next link " " 0.3833 0.04383 3662.299"
" 5 Next link " " 0.4792 0.05156 4645.824"
" 0.300 0.298 0.298 2.594" " 0.5750 0.05826 5655.543"
" 33 CATCHMENT 310" " 0.6708 0.06427 6692.645"
" 1 Triangular SCS" " 0.7667 0.06977 7758.431"
" 1 Equal length" " 0.8625 0.07486 8850.853"
" 1 SCS method" " 0.9583 0.07963 9971.185"
" 310 No description" " 1.054 0.08412 11118.39"
" 75.000 % Impervious" " 1.150 0.08840 12297.52"
" 2.400 Total Area" " 1.246 0.2294 13505.21"
" 75.000 Flow length" " 1.342 0.4837 14741.64"
" 2.000 Overland Slope" " 1.438 0.8116 16006.97"
" 0.600 Pervious Area" " 1.533 1.195 17287.76"
" 75.000 Pervious length" " 1.629 1.633 18611.14"
" 2.000 Pervious slope" " 1.725 2.118 19963.96"
" 1.800 Impervious Area" " 1.821 2.644 21346.39"
" 75.000 Impervious length" " 1.917 3.209 22758.63"
" 2.000 Impervious slope" " 2.013 3.811 24200.82"
" 0.200 Pervious Manning 'n'" " 2.108 5.348 25657.67"
" 82.000 Pervious SCS Curve No." " 2.204 7.723 27160.03"
" 0.441 Pervious Runoff coefficient" " 2.300 10.675 28692.88"
" 0.100 Pervious Ia/S coefficient" "
" 5.576 Pervious Initial abstraction" " 2. WEIRS "
" 0.013 Impervious Manning 'n'" " Crest Weir Crest Left Right"
" 98.000 Impervious SCS Curve No." " elevation coefficient breadth sideslope sideslope"
" 0.906 Impervious Runoff coefficient" " 1.150 0.900 3.000 0.000 0.000"
" 0.100 Impervious Ia/S coefficient" " 2.013 0.900 20.000 3.000 3.000"
" 0.518 Impervious Initial abstraction" " 1. ORIFICES "
" 0.253 0.298 0.298 2.594 c.m/sec" " Orifice Orifice Orifice Number of"
" Catchment 310 Pervious Impervious Total Area " invert coefficient diameter orifices"
" Surface Area 0.600 1.800 2.400 hectare" " 0.000 0.630 0.2000 1.000"
" Time of concentration 29.991 4.847 8.359 minutes" " 2. LAYERS "
" Time to Centroid 262.344 208.951 216.407 minutes" " Bottom Aspect Bottom Top Average"
" Rainfall depth 58.700 58.700 58.700 mm" " area ratio elevation elevation sideslope"
" Rainfall volume 352.20 1056.60 1408.80 c.m" " 9000.000 7.000 0.000 2.000 5.000"
" Rainfall losses 32.790 5.497 12.320 mm" " 15137.096 4.852 2.000 2.300 5.000"
" Runoff depth 25.910 53.203 46.380 mm" " Peak outflow 0.540 c.m/sec"
" Runoff volume 155.46 957.65 1113.11 c.m" " Maximum level 1.358 metre"
" Runoff coefficient 0.441 0.906 0.790 " " Maximum storage 14957.616 c.m"
" Maximum flow 0.037 0.225 0.253 c.m/sec" " Centroidal lag 25.115 hours"
" 40 HYDROGRAPH Add Runoff " " 0.253 3.096 0.540 0.000 c.m/sec"
" 4 Add Runoff " " 50 HYDROGRAPH Next link "
" 0.253 0.551 0.298 2.594" " 5 Next link "
" 52 CHANNEL DESIGN" " 52 CHANNEL DESIGN"
" 0.551 Current peak flow c.m/sec" " 0.540 Current peak flow c.m/sec"
" 0.040 Manning 'n'" " 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre" " 2.000 Basewidth metre"
" 3.000 Left bank slope" " 3.000 Left bank slope"
" 3.000 Right bank slope" " 3.000 Right bank slope"
" 5.000 Channel depth metre" " 5.000 Channel depth metre"
" 2.000 Gradient %" " 2.000 Gradient %"
" Depth of flow 0.202 metre" " Depth of flow 0.200 metre"
" Velocity 1.045 m/sec" " Velocity 1.039 m/sec"
" Channel capacity 557.696 c.m/sec" " Channel capacity 557.696 c.m/sec"
" Critical depth 0.180 metre" " Critical depth 0.178 metre"
" 53 ROUTE Channel Route 200" " 53 ROUTE Channel Route 250"
" 200.00 Channel Route 200 Reach length (metre)" " 250.00 Channel Route 250 Reach length (metre)"
" 0.486 X-factor <= 0.5" " 0.489 X-factor <= 0.5"
" 143.500 K-lag (seconds)" " 180.512 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used" " 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5" " 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)" " 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor" " 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)" " 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches" " 1 No. of sub-reaches"
" Peak outflow 0.545 c.m/sec" " Peak outflow 0.539 c.m/sec"
" 0.253 0.551 0.545 2.594 c.m/sec" " 0.253 0.540 0.539 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100" " 40 HYDROGRAPH Combine 2000"
" 6 Combine " " 6 Combine "
" 6100 Node #" " 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 3.096 c.m/sec" " Maximum flow 1.309 c.m/sec"
" Hydrograph volume 19928.240 c.m" " Hydrograph volume 20858.201 c.m"
" 0.253 0.551 0.545 3.096" " 0.253 0.540 0.539 1.309"
" 40 HYDROGRAPH Confluence 6100" " 40 HYDROGRAPH Start - New Tributary"
" 7 Confluence " " 2 Start - New Tributary"
" 6100 Node #" " 0.253 0.000 0.539 1.309"
" Maximum flow 3.096 c.m/sec" " 33 CATCHMENT 311"
" Hydrograph volume 19928.240 c.m" " 1 Triangular SCS"
" 0.253 3.096 0.545 0.000" " 1 Equal length"
" 52 CHANNEL DESIGN" " 1 SCS method"
" 3.096 Current peak flow c.m/sec" " 311 No description"
" 0.040 Manning 'n'" " 75.000 % Impervious"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 6.600 Total Area"
" 2.000 Basewidth metre" " 100.000 Flow length"
" 3.000 Left bank slope" " 2.000 Overland Slope"
" 3.000 Right bank slope" " 1.650 Pervious Area"
" 5.000 Channel depth metre" " 100.000 Pervious length"
" 2.000 Gradient %" " 2.000 Pervious slope"
" Depth of flow 0.507 metre" " 4.950 Impervious Area"
" Velocity 1.733 m/sec" " 100.000 Impervious length"
" Channel capacity 557.696 c.m/sec" " 2.000 Impervious slope"
" Critical depth 0.488 metre" " 0.200 Pervious Manning 'n'"
" 53 ROUTE Channel Route 50" " 82.000 Pervious SCS Curve No."
" 50.00 Channel Route 50 Reach length (metre)" " 0.441 Pervious Runoff coefficient"
" 0.372 X-factor <= 0.5" " 0.100 Pervious Ia/S coefficient"
" 21.644 K-lag (seconds)" " 5.576 Pervious Initial abstraction"
" 0.000 Default(0) or user spec.(1) values used" " 0.013 Impervious Manning 'n'"
" 0.500 X-factor <= 0.5" " 98.000 Impervious SCS Curve No."
" 30.000 K-lag (seconds)" " 0.905 Impervious Runoff coefficient"
" 0.500 Beta weighting factor" " 0.100 Impervious Ia/S coefficient"
" 25.000 Routing time step (seconds)" " 0.518 Impervious Initial abstraction"
" 1 No. of sub-reaches" " 0.677 0.000 0.539 1.309 c.m/sec"
" Peak outflow 3.096 c.m/sec" " Catchment 311 Pervious Impervious Total Area "
" 0.253 3.096 3.096 0.000 c.m/sec" " Surface Area 1.650 4.950 6.600 hectare"
" 40 HYDROGRAPH Next link " " Time of concentration 35.641 5.760 9.939 minutes"
" 5 Next link " " Time to Centroid 269.165 209.866 218.158 minutes"
" 0.253 3.096 3.096 0.000" " Rainfall depth 58.700 58.700 58.700 mm"
" 81 ADD COMMENT" " Rainfall volume 968.55 2905.65 3874.20 c.m"
" 1 Lines of comment" " Rainfall losses 32.788 5.576 12.379 mm"
" PROPOSED POND #2" " Runoff depth 25.912 53.124 46.321 mm"
" 54 POND DESIGN" " Runoff volume 427.55 2629.63 3057.18 c.m"
" 3.096 Current peak flow c.m/sec" " Runoff coefficient 0.441 0.905 0.789 "
" 4.007 Target outflow c.m/sec" " Maximum flow 0.093 0.634 0.677 c.m/sec"
" 19928.2 Hydrograph volume c.m" " 40 HYDROGRAPH Add Runoff "
" 25. Number of stages" " 4 Add Runoff "
" 0.000 Minimum water level metre" " 0.677 0.677 0.539 1.309"
" 2.300 Maximum water level metre" " 52 CHANNEL DESIGN"
" 0.000 Starting water level metre" " 0.677 Current peak flow c.m/sec"
" 0 Keep Design Data: 1 = True; 0 = False" " 0.020 Manning 'n'"
" Level Discharge Volume" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 0.000 0.000 0.000" " 4.000 Basewidth metre"
" 0.09583 0.00452 875.671" " 50.000 Left bank slope"
" 0.1917 0.01493 1778.243" " 0.000 Right bank slope"
" 0.2875 0.03442 2706.844" " 0.300 Channel depth metre"
" 2.000 Gradient %"

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"	Depth of flow	0.092	metre"	"	Runoff depth	25.912	53.124	46.321	mm"
"	Velocity	1.164	m/sec"	"	Runoff volume	285.04	1753.09	2038.12	c.m"
"	Channel capacity	7.740	c.m/sec"	"	Runoff coefficient	0.441	0.905	0.789	"
"	Critical depth	0.112	metre"	"	Maximum flow	0.062	0.423	0.452	c.m/sec"
" 53	ROUTE Channel Route 200"			" 40	HYDROGRAPH Add Runoff "				
"	200.00 Channel Route 200 Reach length (metre)"			"	4 Add Runoff "	0.452	0.452	0.990	
"	0.494 X-factor <= 0.5"			" 52	CHANNEL DESIGN"				
"	128.842 K-lag (seconds)"			"	0.452 Current peak flow c.m/sec"				
"	0.000 Default(0) or user spec.(1) values used"			"	0.020 Manning 'n'"				
"	0.500 X-factor <= 0.5"			"	0. Cross-section type: 0=trapezoidal; 1=general"				
"	30.000 K-lag (seconds)"			"	4.000 Basewidth metre"				
"	0.500 Beta weighting factor"			"	50.000 Left bank slope"				
"	100.000 Routing time step (seconds)"			"	0.000 Right bank slope"				
"	1 No. of sub-reaches"			"	0.300 Channel depth metre"				
"	Peak outflow	0.669	c.m/sec"	"	2.000 Gradient %"				
"	0.677 0.677 0.669 1.309 c.m/sec"			"	Depth of flow		0.074	metre"	
" 40	HYDROGRAPH Next link "			"	Velocity		1.035	m/sec"	
"	5 Next link "			"	Channel capacity		7.740	c.m/sec"	
"	0.677 0.669 0.669 1.309"			"	Critical depth		0.090	metre"	
" 33	CATCHMENT 314"			" 53	ROUTE Channel Route 100"				
"	1 Triangular SCS"			"	100.00 Channel Route 100 Reach length (metre)"				
"	1 Equal length"			"	0.490 X-factor <= 0.5"				
"	1 SCS method"			"	72.470 K-lag (seconds)"				
"	314 No description"			"	0.000 Default(0) or user spec.(1) values used"				
"	50.000 % Impervious"			"	0.500 X-factor <= 0.5"				
"	3.300 Total Area"			"	30.000 K-lag (seconds)"				
"	20.000 Flow length"			"	0.500 Beta weighting factor"				
"	1.000 Overland Slope"			"	60.000 Routing time step (seconds)"				
"	1.650 Pervious Area"			"	1 No. of sub-reaches"				
"	20.000 Pervious length"			"	Peak outflow		0.448	c.m/sec"	
"	1.000 Pervious slope"			"	0.452 0.452 0.448 0.990 c.m/sec"				
"	1.650 Impervious Area"			" 40	HYDROGRAPH Combine 7000"				
"	20.000 Impervious length"			"	6 Combine "				
"	1.000 Impervious slope"			"	7000 Node #"				
"	0.200 Pervious Manning 'n'"			"	Maximum flow		1.439	c.m/sec"	
"	82.000 Pervious SCS Curve No."			"	Hydrograph volume		6388.617	c.m"	
"	0.441 Pervious Runoff coefficient"			"	0.452 0.452 0.448 1.439"				
"	0.100 Pervious Ia/S coefficient"			" 40	HYDROGRAPH Start - New Tributary"				
"	5.576 Pervious Initial abstraction"			"	2 Start - New Tributary"				
"	0.013 Impervious Manning 'n'"			"	0.452 0.000 0.448 1.439"				
"	98.000 Impervious SCS Curve No."			" 33	CATCHMENT 304"				
"	0.894 Impervious Runoff coefficient"			"	1 Triangular SCS"				
"	0.100 Impervious Ia/S coefficient"			"	1 Equal length"				
"	0.518 Impervious Initial abstraction"			"	1 SCS method"				
"	0.669 0.669 1.309 c.m/sec"			"	304 No description"				
"	Catchment 314 Pervious Impervious Total Area "			"	50.000 % Impervious"				
"	Surface Area 1.650 1.650 3.300 hectare"			"	1.600 Total Area"				
"	Time of concentration 16.706 2.700 7.327 minutes"			"	75.000 Flow length"				
"	Time to Centroid 246.295 206.081 219.365 minutes"			"	2.000 Overland Slope"				
"	Rainfall depth 58.700 58.700 58.700 mm"			"	0.800 Pervious Area"				
"	Rainfall volume 968.55 968.55 1937.10 c.m"			"	75.000 Pervious length"				
"	Rainfall losses 32.809 6.209 19.509 mm"			"	2.000 Pervious slope"				
"	Runoff depth 25.891 52.491 39.191 mm"			"	0.800 Impervious Area"				
"	Runoff volume 427.21 866.10 1293.31 c.m"			"	75.000 Impervious length"				
"	Runoff coefficient 0.441 0.894 0.668 "			"	2.000 Impervious slope"				
" 40	Maximum flow 0.127 0.204 0.327 c.m/sec"			"	0.200 Pervious Manning 'n'"				
"	HYDROGRAPH Add Runoff "			"	82.000 Pervious SCS Curve No."				
"	4 Add Runoff "			"	0.441 Pervious Runoff coefficient"				
"	0.327 0.996 0.669 1.309"			"	0.100 Pervious Ia/S coefficient"				
" 52	CHANNEL DESIGN"			"	5.576 Pervious Initial abstraction"				
"	0.996 Current peak flow c.m/sec"			"	0.013 Impervious Manning 'n'"				
"	0.040 Manning 'n'"			"	98.000 Impervious SCS Curve No."				
"	0. Cross-section type: 0=trapezoidal; 1=general"			"	0.906 Impervious Runoff coefficient"				
"	2.000 Basewidth metre"			"	0.100 Impervious Ia/S coefficient"				
"	3.000 Left bank slope"			"	0.518 Impervious Initial abstraction"				
"	3.000 Right bank slope"			"	0.137 0.000 0.448 1.439 c.m/sec"				
"	5.000 Channel depth metre"			"	Catchment 304 Pervious Impervious Total Area "				
"	2.000 Gradient %"			"	Surface Area 0.800 0.800 1.600 hectare"				
"	Depth of flow 0.280 metre"			"	Time of concentration 29.991 4.847 13.082 minutes"				
"	Velocity 1.253 m/sec"			"	Time to Centroid 262.344 208.951 226.437 minutes"				
"	Channel capacity 557.696 c.m/sec"			"	Rainfall depth 58.700 58.700 58.700 mm"				
"	Critical depth 0.256 metre"			"	Rainfall volume 469.60 469.60 939.20 c.m"				
" 53	ROUTE Channel Route 80"			"	Rainfall losses 32.790 5.497 19.144 mm"				
"	80.00 Channel Route 80 Reach length (metre)"			"	Runoff depth 25.910 53.203 39.556 mm"				
"	0.453 X-factor <= 0.5"			"	Runoff volume 207.28 425.62 632.90 c.m"				
"	47.901 K-lag (seconds)"			"	Runoff coefficient 0.441 0.906 0.674 "				
"	0.000 Default(0) or user spec.(1) values used"			" 40	Maximum flow 0.049 0.100 0.137 c.m/sec"				
"	0.500 X-factor <= 0.5"			"	HYDROGRAPH Add Runoff "				
"	30.000 K-lag (seconds)"			"	4 Add Runoff "				
"	0.500 Beta weighting factor"			"	0.137 0.137 0.448 1.439"				
"	50.000 Routing time step (seconds)"			" 52	CHANNEL DESIGN"				
"	1 No. of sub-reaches"			"	0.137 Current peak flow c.m/sec"				
"	Peak outflow	0.990	c.m/sec"	"	0.020 Manning 'n'"				
"	0.327 0.996 0.990 1.309 c.m/sec"			"	0. Cross-section type: 0=trapezoidal; 1=general"				
" 40	HYDROGRAPH Combine 7000"			"	4.000 Basewidth metre"				
"	6 Combine "			"	50.000 Left bank slope"				
"	7000 Node #"			"	0.000 Right bank slope"				
"	Maximum flow 0.990 c.m/sec"			"	0.600 Channel depth metre"				
"	Hydrograph volume 4350.491 c.m"			"	2.000 Gradient %"				
"	0.327 0.996 0.990 0.990"			"	Depth of flow 0.039 metre"				
" 40	HYDROGRAPH Start - New Tributary"			"	Velocity 0.714 m/sec"				
"	2 Start - New Tributary"			"	Channel capacity 38.450 c.m/sec"				
"	0.327 0.000 0.990 0.990"			"	Critical depth 0.045 metre"				
" 33	CATCHMENT 312"			" 53	ROUTE Channel Route 50"				
"	1 Triangular SCS"			"	50.00 Channel Route 50 Reach length (metre)"				
"	1 Equal length"			"	0.489 X-factor <= 0.5"				
"	1 SCS method"			"	52.485 K-lag (seconds)"				
"	312 No description"			"	0.000 Default(0) or user spec.(1) values used"				
"	75.000 % Impervious"			"	0.500 X-factor <= 0.5"				
"	4.400 Total Area"			"	30.000 K-lag (seconds)"				
"	100.000 Flow length"			"	0.500 Beta weighting factor"				
"	2.000 Overland Slope"			"	50.000 Routing time step (seconds)"				
"	1.100 Pervious Area"			"	1 No. of sub-reaches"				
"	100.000 Pervious length"			"	Peak outflow		0.136	c.m/sec"	
"	2.000 Pervious slope"			"	0.137 0.137 0.136 1.439 c.m/sec"				
"	3.300 Impervious Area"			" 40	HYDROGRAPH Next link "				
"	100.000 Impervious length"			"	5 Next link "				
"	2.000 Impervious slope"			"	0.137 0.136 0.136 1.439"				
"	0.200 Pervious Manning 'n'"			" 33	CATCHMENT 313"				
"	82.000 Pervious SCS Curve No."			"	1 Triangular SCS"				
"	0.441 Pervious Runoff coefficient"			"	1 Equal length"				
"	0.100 Pervious Ia/S coefficient"			"	1 SCS method"				
"	5.576 Pervious Initial abstraction"			"	313 No description"				
"	0.013 Impervious Manning 'n'"			"	75.000 % Impervious"				
"	98.000 Impervious SCS Curve No."			"	1.800 Total Area"				
"	0.905 Impervious Runoff coefficient"			"	50.000 Flow length"				
"	0.100 Impervious Ia/S coefficient"			"	2.000 Overland Slope"				
"	0.518 Impervious Initial abstraction"			"	0.450 Pervious Area"				
"	0.452 0.000 0.990 0.990 c.m/sec"			"	50.000 Pervious length"				
"	Catchment 312 Pervious Impervious Total Area "			"	2.000 Pervious slope"				
"	Surface Area 1.100 3.300 4.400 hectare"			"	1.350 Impervious Area"				
"	Time of concentration 35.641 5.760 9.939 minutes"			"	50.000 Impervious length"				
"	Time to Centroid 269.164 209.866 218.158 minutes"			"	2.000 Impervious slope"				
"	Rainfall depth 58.700 58.700 58.700 mm"			"	0.200 Pervious Manning 'n'"				
"	Rainfall volume 645.70 1937.10 2582.80 c.m"			"	82.000 Pervious SCS Curve No."				
"	Rainfall losses 32.788 5.576 12.379 mm"			"					

0.441 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.887 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.188 0.136 0.136 1.439 c.m/sec"
Catchment 313 Pervious Impervious Total Area "
Surface Area 0.450 1.350 1.800 hectare"
Time of concentration 23.515 3.800 6.603 minutes"
Time to Centroid 254.524 207.443 214.135 minutes"
Rainfall depth 58.700 58.700 58.700 mm"
Rainfall volume 264.15 792.45 1056.60 c.m"
Rainfall losses 32.803 6.612 13.160 mm"
Runoff depth 25.897 52.088 45.540 mm"
Runoff volume 116.54 703.19 819.72 c.m"
Runoff coefficient 0.441 0.887 0.776 "
Maximum flow 0.031 0.166 0.188 c.m/sec"
HYDROGRAPH Add Runoff "
4 Add Runoff " 0.188 0.323 0.136 1.439"
CHANNEL DESIGN"
0.323 Current peak flow c.m/sec"
0.020 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
4.000 Basewidth metre"
50.000 Left bank slope"
0.000 Right bank slope"
0.300 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.062 metre"
Velocity 0.936 m/sec"
Channel capacity 7.740 c.m/sec"
Critical depth 0.074 metre"
ROUTE Channel Route 200"
200.00 Channel Route 200 Reach length (metre)"
0.496 X-factor <= 0.5"
160.301 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
150.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.188 0.323 0.315 1.439 c.m/sec"
HYDROGRAPH Combine 7000"
6 Combine " 7000 Node #"
Maximum flow 1.754 c.m/sec"
Hydrograph volume 7841.237 c.m"
HYDROGRAPH Confluence 7000"
7 Confluence " 7000 Node #"
Maximum flow 1.754 c.m/sec"
Hydrograph volume 7841.237 c.m"
HYDROGRAPH Confluence 7000"
0.188 0.323 0.315 1.754"
CHANNEL DESIGN"
1.754 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.379 metre"
Velocity 1.477 m/sec"
Channel capacity 557.696 c.m/sec"
Critical depth 0.356 metre"
ROUTE Channel Route 50"
50.00 Channel Route 50 Reach length (metre)"
0.401 X-factor <= 0.5"
25.381 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
30.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.188 1.754 1.749 0.000 c.m/sec"
HYDROGRAPH Next link "
5 Next link " 0.188 1.749 1.749 0.000"
ADD COMMENT=====
1 Lines of comment"
PROPOSED POND #3"
POND DESIGN"
1.749 Current peak flow c.m/sec"
2.000 Target outflow c.m/sec"
7841.2 Hydrograph volume c.m"
21. Number of stages"
0.000 Minimum water level metre"
2.000 Maximum water level metre"
0.000 Starting water level metre"
0 Keep Design Data: 1 = True; 0 = False"
Level Discharge Volume"
0.000 0.000 0.000"
0.1000 0.00487 607.388"
0.2000 0.01603 1237.688"
0.3000 0.03579 1891.097"
0.4000 0.04527 2567.818"
0.5000 0.05309 3268.049"
0.6000 0.05989 3991.990"
0.7000 0.06599 4739.842"
0.8000 0.07158 5511.804"
0.9000 0.07676 6308.077"
1.000 0.08161 7128.861"
1.100 0.08619 7974.355"
1.200 0.09054 8844.760"
1.300 0.1190 9740.274"
1.400 0.1673 10661.10"
1.500 0.2286 11607.44"
1.600 0.3003 12579.48"
1.700 0.3810 13577.44"
1.800 1.208 14601.51"
1.900 2.686 15651.89"
2.000 4.619 16728.78"
2. WEIRS"
Crest Weir Crest Left Right"
elevation coefficient breadth sideslope sideslope"
1.200 0.900 0.500 0.000 0.000"
1.700 0.900 15.000 3.000 3.000"
1. ORIFICES"
Orifice Orifice Orifice Number of"
invert coefficient diameter orifices"
0.000 0.630 0.2000 1.000"
2. LAYERS"
Bottom Aspect Bottom Top Average"
area ratio elevation elevation sideslope"
5960.000 6.500 0.000 2.000 5.000"
10902.110 4.312 2.000 2.000 4.000"
Peak outflow 0.080 c.m/sec"
Maximum level 0.966 metre"
Maximum storage 6847.172 c.m"
Centroidal lag 21.014 hours"
0.188 1.749 0.080 0.000 c.m/sec"
HYDROGRAPH Next link "
5 Next link " 0.188 0.080 0.080 0.000"
CHANNEL DESIGN"
0.080 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.000 Gradient %"
Depth of flow 0.082 metre"
Velocity 0.436 m/sec"
Channel capacity 394.351 c.m/sec"
Critical depth 0.053 metre"
ROUTE Channel Route 300"
300.00 Channel Route 300 Reach length (metre)"
0.484 X-factor <= 0.5"
257.919 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 0.188 0.080 0.080 0.000 c.m/sec"
HYDROGRAPH Combine 1100"
6 Combine " 1100 Node #"
Node taking 200 series - Bottom end of Holtby Drain"
Maximum flow 7.429 c.m/sec"
Hydrograph volume 52318.445 c.m"
ADD COMMENT=====
1 Lines of comment"
Total to Holtby Drain"
HYDROGRAPH Confluence 1100"
7 Confluence " 1100 Node #"
Node taking 200 series - Bottom end of Holtby Drain"
Maximum flow 7.429 c.m/sec"
Hydrograph volume 52318.445 c.m"
ADD COMMENT=====
1 Lines of comment"
Total to Holtby Drain"
CHANNEL DESIGN"
7.429 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.080 metre"
Velocity 1.314 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.774 metre"
ROUTE Channel Route 200"
200.00 Channel Route 200 Reach length (metre)"
0.253 X-factor <= 0.5"
114.182 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
150.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.188 7.429 7.428 0.000 c.m/sec"
HYDROGRAPH Combine 1300"
6 Combine " 1300 Node #"
Node at Holtby Drain"
Maximum flow 9.510 c.m/sec"
Hydrograph volume 66615.258 c.m"
HYDROGRAPH Confluence 1300"
7 Confluence " 1300 Node #"
Node at Holtby Drain"
Maximum flow 9.510 c.m/sec"
Hydrograph volume 66615.250 c.m"
CHANNEL DESIGN"
9.510 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.208 metre"
Velocity 1.400 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.877 metre"
ROUTE Channel Route 50"
50.00 Channel Route 50 Reach length (metre)"
0.000 X-factor <= 0.5"
26.787 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.711 Beta weighting factor"
75.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 9.485 c.m/sec"

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"      0.188      9.510      9.485      0.000 c.m/sec"
" 40      HYDROGRAPH      Combine      1000"
"      6      Combine      "
"      1000      Node #
"      Node upstream of Penetangore Culvert"
"      Maximum flow      41.475      c.m/sec"
"      Hydrograph volume      442900.500      c.m"
"      0.188      9.510      9.485      41.475"
" 81      ADD COMMENT=====
"      2      Lines of comment"
"      Total discharge to Pipe Arch under Hwy. 21 on the "
"      Pentangore Tributary"
" 40      HYDROGRAPH      Confluence      1000"
"      7      Confluence      "
"      1000      Node #
"      Node upstream of Penetangore Culvert"
"      Maximum flow      41.475      c.m/sec"
"      Hydrograph volume      442900.531      c.m"
"      0.188      41.475      9.485      0.000"
" 81      ADD COMMENT=====
"      2      Lines of comment"
"      Total discharge to Pipe Arch under Hwy. 21 on the "
"      Pentangore Tributary"
" 52      CHANNEL DESIGN"
"      41.475      Current peak flow      c.m/sec"
"      0.040      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; l=general"
"      2.000      Basewidth      metre"
"      3.000      Left bank slope"
"      3.000      Right bank slope"
"      5.000      Channel depth      metre"
"      0.500      Gradient      %"
"      Depth of flow      2.295      metre"
"      Velocity      2.034      m/sec"
"      Channel capacity      278.848      c.m/sec"
"      Critical depth      1.779      metre"
" 53      ROUTE      Channel Route 50"
"      50.00      Channel Route 50 Reach length      ( metre)"
"      0.000      X-factor <= 0.5"
"      18.433      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.853      Beta weighting factor"
"      75.000      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      41.471      c.m/sec"
"      0.188      41.475      41.471      0.000 c.m/sec"
" 40      HYDROGRAPH      Combine      3000"
"      6      Combine      "
"      3000      Node #
"      Node Combining All Flow"
"      Maximum flow      41.471      c.m/sec"
"      Hydrograph volume      442899.656      c.m"
"      0.188      41.475      41.471      41.471"
" 81      ADD COMMENT=====
"      1      Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40      HYDROGRAPH      Start - New Tributary"
"      2      Start - New Tributary"
"      0.188      0.000      41.471      41.471"
" 40      HYDROGRAPH      Confluence      2000"
"      7      Confluence      "
"      2000      Node #
"      Flow in Hwy. 21 Ditch"
"      Maximum flow      1.309      c.m/sec"
"      Hydrograph volume      20858.201      c.m"
"      0.188      1.309      41.471      0.000"
" 81      ADD COMMENT=====
"      1      Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
" 52      CHANNEL DESIGN"
"      1.309      Current peak flow      c.m/sec"
"      0.040      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; l=general"
"      2.000      Basewidth      metre"
"      3.000      Left bank slope"
"      3.000      Right bank slope"
"      5.000      Channel depth      metre"
"      0.500      Gradient      %"
"      Depth of flow      0.466      metre"
"      Velocity      0.827      m/sec"
"      Channel capacity      278.848      c.m/sec"
"      Critical depth      0.301      metre"
" 53      ROUTE      Channel Route 100"
"      100.00      Channel Route 100 Reach length      ( metre)"
"      0.262      X-factor <= 0.5"
"      90.687      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.500      Beta weighting factor"
"      100.000      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      1.303      c.m/sec"
"      0.188      1.309      1.303      0.000 c.m/sec"
" 40      HYDROGRAPH      Combine      3000"
"      6      Combine      "
"      3000      Node #
"      Node Combining All Flow"
"      Maximum flow      42.294      c.m/sec"
"      Hydrograph volume      463751.063      c.m"
"      0.188      1.309      1.303      42.294"
" 40      HYDROGRAPH      Confluence      3000"
"      7      Confluence      "
"      3000      Node #
"      Node Combining All Flow"
"      Maximum flow      42.294      c.m/sec"
"      Hydrograph volume      463751.125      c.m"
"      0.188      42.294      1.303      0.000"
" 81      ADD COMMENT=====
"      1      Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 52      CHANNEL DESIGN"
"      42.294      Current peak flow      c.m/sec"
"      0.040      Manning 'n'"
"      0.      Cross-section type: 0=trapezoidal; l=general"
"      2.000      Basewidth      metre"
"      3.000      Left bank slope"
"      3.000      Right bank slope"
"      5.000      Channel depth      metre"
"      0.500      Gradient      %"
"      Depth of flow      2.314      metre"
"      Velocity      2.044      m/sec"
"      Channel capacity      278.848      c.m/sec"
"      Critical depth      1.795      metre"
" 53      ROUTE      Channel Route 50"
"      50.00      Channel Route 50 Reach length      ( metre)"
"      0.000      X-factor <= 0.5"
"      18.342      K-lag      ( seconds)"
"      0.000      Default(0) or user spec.(1) values used"
"      0.500      X-factor <= 0.5"
"      30.000      K-lag      ( seconds)"
"      0.854      Beta weighting factor"
"      75.000      Routing time step      ( seconds)"
"      1      No. of sub-reaches"
"      Peak outflow      42.290      c.m/sec"
"      0.188      42.294      42.290      0.000 c.m/sec"
" 38      START/RE-START TOTALS 3000"
"      1      Runoff Totals turned OFF"
"      Catchment area to node 3000      1918.200      hectare"
"      Impervious area to node 3000      40.592      hectare"
"      % impervious to node 3000      0.000"
"      Peak runoff to node 3000      0.000      c.m/sec"
"      Total volume to node 3000      0.0      c.m"
" 38      START/RE-START TOTALS 3000"
"      1      Runoff Totals turned ON"
"      Catchment area to node 3000      1918.200      hectare"
"      Impervious area to node 3000      40.592      hectare"
"      % impervious to node 3000      2.116"
"      Peak runoff to node 3000      66.106      c.m/sec"
"      Total volume to node 3000      473152.0      c.m"

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POST DEVELOPMENT 25 YEAR

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"          MIDUSS Output ----->"
"          MIDUSS version              Version 2.25 rev. 473"
"          MIDUSS created              Sunday, February 7, 2010"
"          10  UNITS used:              ie METRIC"
"          Job folder:                 C:\Users\derb\Desktop\KBP - Report\
"          Output filename:            2016 Work\Appendix F - Miduss Modelling\Future"
"          Licensee name:              08055 - Post 25 Year.out"
"          Company                    BMROSS - DLE"
"          Date & Time last used:      6/25/2016 at 10:18:23 AM"
"          TIME PARAMETERS"
"          5.000 Time Step"
"          360.000 Max. Storm length"
"          1800.000 Max. Hydrograph"
"          32  STORM Mass Curve"
"          3 Mass Curve"
"          86.100 Rainfall depth"
"          360.000 Duration"
"          47  C:\Program Files (x86)\MIDUSS\SCS_6hr_Type2.mrd  SCS Type II - 6
hour Distribution - Ontario"
"          Maximum intensity            67.158 mm/hr"
"          Total depth                  86.100 mm"
"          6 025hyd Hydrograph extension used in this file"
"          81  ADD COMMENT-----"
"          1 Lines of comment"
"          Start of Penetangore Tributary"
"          33  CATCHMENT 50"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          50 No description"
"          0.000 % Impervious"
"          396.000 Total Area"
"          450.000 Flow length"
"          2.500 Overland Slope"
"          396.000 Pervious Area"
"          450.000 Pervious length"
"          2.500 Pervious slope"
"          0.000 Impervious Area"
"          450.000 Impervious length"
"          2.500 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.534 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.013 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.000 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          23.637 0.000 0.000 0.000 c.m/sec"
"          Catchment 50 Pervious Impervious Total Area "
"          Surface Area 396.000 0.000 396.000 hectare"
"          Time of concentration 75.983 11.366 75.983 minutes"
"          Time to Centroid 314.049 214.390 314.049 minutes"
"          Rainfall depth 86.100 86.100 86.100 mm"
"          Rainfall volume 34.0956 0.0000 34.0956 ha-m"
"          Rainfall losses 40.137 5.520 40.137 mm"
"          Runoff depth 45.963 80.580 45.963 mm"
"          Runoff volume 18.2015 0.0000 18.2015 ha-m"
"          Runoff coefficient 0.534 0.000 0.534 "
"          Maximum flow 23.637 0.000 23.637 c.m/sec"
"          40  HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          23.637 23.637 0.000 0.000"
"          52  CHANNEL DESIGN"
"          23.637 Current peak flow c.m/sec"
"          0.040 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          2.000 Basewidth metre"
"          3.000 Left bank slope"
"          3.000 Right bank slope"
"          5.000 Channel depth metre"
"          0.500 Gradient %"
"          Depth of flow 1.805 metre"
"          Velocity 1.765 m/sec"
"          Channel capacity 278.848 c.m/sec"
"          Critical depth 1.368 metre"
"          53  ROUTE Channel Route 3000"
"          3000.00 Channel Route 3000 Reach length ( metre)"
"          0.396 X-factor <= 0.5"
"          318.652 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          300.000 Routing time step ( seconds)"
"          4 No. of sub-reaches"
"          Peak outflow 23.637 23.637 23.348 c.m/sec"
"          23.637 23.637 23.348 0.000 c.m/sec"
"          40  HYDROGRAPH Next link "
"          5 Next link "
"          23.637 23.348 23.348 0.000"
"          33  CATCHMENT 52"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          52 No description"
"          0.000 % Impervious"
"          196.000 Total Area"
"          250.000 Flow length"
"          7.000 Overland Slope"
"          196.000 Pervious Area"
"          250.000 Pervious length"
"          7.000 Pervious slope"
"          0.000 Impervious Area"
"          250.000 Impervious length"
"          7.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          80.000 Pervious SCS Curve No."
"          0.515 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          6.350 Pervious Initial abstraction"
"          0.013 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.000 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          18.017 23.348 23.348 0.000 c.m/sec"
"          Catchment 52 Pervious Impervious Total Area "
"          Surface Area 196.000 0.000 196.000 hectare"
"          Time of concentration 39.626 5.865 39.626 minutes"
"          Time to Centroid 270.855 207.757 270.855 minutes"
"          Rainfall depth 86.100 86.100 86.100 mm"
"          Rainfall volume 16.8756 0.0000 16.8756 ha-m"
"          Rainfall losses 41.715 5.922 41.715 mm"
"          Runoff depth 44.385 80.178 44.385 mm"
"          Runoff volume 8.6994 0.0000 8.6994 ha-m"
"          Runoff coefficient 0.515 0.000 0.516 "
"          Maximum flow 18.017 0.000 18.017 c.m/sec"
"          HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          18.017 29.299 23.348 0.000"
"          52  CHANNEL DESIGN"
"          29.299 Current peak flow c.m/sec"
"          0.040 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          2.000 Basewidth metre"
"          3.000 Left bank slope"
"          3.000 Right bank slope"
"          5.000 Channel depth metre"
"          0.400 Gradient %"
"          Depth of flow 2.076 metre"
"          Velocity 1.715 m/sec"
"          Channel capacity 249.409 c.m/sec"
"          Critical depth 1.513 metre"
"          53  ROUTE Channel Route 1300"
"          1300.00 Channel Route 1300 Reach length ( metre)"
"          0.330 X-factor <= 0.5"
"          284.328 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          300.000 Routing time step ( seconds)"
"          2 No. of sub-reaches"
"          Peak outflow 18.017 29.299 29.196 c.m/sec"
"          18.017 29.299 29.196 0.000 c.m/sec"
"          40  HYDROGRAPH Next link "
"          5 Next link "
"          18.017 29.196 29.196 0.000"
"          33  CATCHMENT 54"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          54 No description"
"          0.000 % Impervious"
"          39.000 Total Area"
"          140.000 Flow length"
"          11.000 Overland Slope"
"          39.000 Pervious Area"
"          140.000 Pervious length"
"          11.000 Pervious slope"
"          0.000 Impervious Area"
"          140.000 Impervious length"
"          11.000 Impervious slope"
"          0.210 Pervious Manning 'n'"
"          81.000 Pervious SCS Curve No."
"          0.533 Pervious Runoff coefficient"
"          0.100 Pervious Ia/S coefficient"
"          5.958 Pervious Initial abstraction"
"          0.013 Impervious Manning 'n'"
"          98.000 Impervious SCS Curve No."
"          0.000 Impervious Runoff coefficient"
"          0.100 Impervious Ia/S coefficient"
"          0.518 Impervious Initial abstraction"
"          4.989 29.196 29.196 0.000 c.m/sec"
"          Catchment 54 Pervious Impervious Total Area "
"          Surface Area 39.000 0.000 39.000 hectare"
"          Time of concentration 21.777 3.617 21.777 minutes"
"          Time to Centroid 248.526 204.957 248.526 minutes"
"          Rainfall depth 86.100 86.100 86.100 mm"
"          Rainfall volume 3.3579 0.0000 3.3579 ha-m"
"          Rainfall losses 40.195 7.671 40.195 mm"
"          Runoff depth 45.905 78.429 45.905 mm"
"          Runoff volume 1.7903 0.0000 1.7903 ha-m"
"          Runoff coefficient 0.533 0.000 0.533 "
"          Maximum flow 4.989 0.000 4.989 c.m/sec"
"          40  HYDROGRAPH Add Runoff "
"          4 Add Runoff "
"          4.989 30.131 29.196 0.000"
"          52  CHANNEL DESIGN"
"          30.131 Current peak flow c.m/sec"
"          0.040 Manning 'n'"
"          0. Cross-section type: 0=trapezoidal; 1=general"
"          2.000 Basewidth metre"
"          3.000 Left bank slope"
"          3.000 Right bank slope"
"          5.000 Channel depth metre"
"          0.400 Gradient %"
"          Depth of flow 2.101 metre"
"          Velocity 1.727 m/sec"
"          Channel capacity 249.409 c.m/sec"
"          Critical depth 1.533 metre"
"          53  ROUTE Channel Route 800"
"          800.00 Channel Route 800 Reach length ( metre)"
"          0.360 X-factor <= 0.5"
"          347.479 K-lag ( seconds)"
"          0.000 Default(0) or user spec.(1) values used"
"          0.500 X-factor <= 0.5"
"          30.000 K-lag ( seconds)"
"          0.500 Beta weighting factor"
"          300.000 Routing time step ( seconds)"
"          1 No. of sub-reaches"
"          Peak outflow 4.989 30.131 30.050 c.m/sec"
"          4.989 30.131 30.050 0.000 c.m/sec"
"          40  HYDROGRAPH Combine 10"
"          6 Combine "
"          10 Node #"
"          Confluence on Penetangore Tributary"
"          Maximum flow 30.050 c.m/sec"
"          Hydrograph volume 286911.781 c.m"
"          4.989 30.131 30.050 30.050"
"          40  HYDROGRAPH Start - New Tributary"
"          2 Start - New Tributary"
"          4.989 0.000 30.050 30.050"
"          33  CATCHMENT 60"
"          1 Triangular SCS"
"          1 Equal length"
"          1 SCS method"
"          60 No description"
"          0.000 % Impervious"
"          225.000 Total Area"
"          270.000 Flow length"
"          2.500 Overland Slope"
"          225.000 Pervious Area"
"          270.000 Pervious length"
"          2.500 Pervious slope"
"          0.000 Impervious Area"

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" 270.000 Impervious length" " Catchment 62 Pervious Impervious Total Area "

" 2.500 Impervious slope" " Surface Area 95.000 0.000 95.000 hectare"

" 0.230 Pervious Manning 'n'" " Time of concentration 41.289 6.112 41.289 minutes"

" 81.000 Pervious SCS Curve No." " Time to Centroid 272.861 208.104 272.861 minutes"

" 0.534 Pervious Runoff coefficient" " Rainfall depth 86.100 86.100 86.100 mm"

" 0.100 Pervious Ia/S coefficient" " Rainfall volume 8.1795 0.000 8.1795 ha-m"

" 5.958 Pervious Initial abstraction" " Rainfall losses 41.720 6.094 41.720 mm"

" 0.013 Impervious Manning 'n'" " Runoff depth 44.380 80.006 44.380 mm"

" 98.000 Impervious SCS Curve No." " Runoff volume 4.2161 0.000 4.2161 ha-m"

" 0.000 Impervious Runoff coefficient" " Runoff coefficient 0.515 0.000 0.515 "

" 0.100 Impervious Ia/S coefficient" " Maximum flow 8.472 0.000 8.472 c.m/sec"

" 0.518 Impervious Initial abstraction" " 40 HYDROGRAPH Add Runoff "

" 17.615 0.000 30.050 30.050 c.m/sec" " 4 Add Runoff "

" Catchment 60 Pervious Impervious Total Area " " 8.472 8.472 44.774 44.774"

" Surface Area 225.000 0.000 225.000 hectare" " 52 CHANNEL DESIGN"

" Time of concentration 53.196 8.366 53.196 minutes" " 8.472 Current peak flow c.m/sec"

" Time to Centroid 286.501 210.824 286.501 minutes" " 0.040 Manning 'n'"

" Rainfall depth 86.100 86.100 86.100 mm" " 0. Cross-section type: 0=trapezoidal; 1=general"

" Rainfall volume 19.3725 0.0000 19.3725 ha-m" " 2.000 Basewidth metre"

" Rainfall losses 40.141 5.535 40.141 mm" " 3.000 Left bank slope"

" Runoff depth 45.959 80.565 45.959 mm" " 3.000 Right bank slope"

" Runoff volume 10.3407 0.0000 10.3407 ha-m" " 5.000 Channel depth metre"

" Runoff coefficient 0.534 0.000 0.534 " " 0.300 Gradient %"

" Maximum flow 17.615 0.000 17.615 c.m/sec" " Depth of flow 1.286 metre"

" 40 HYDROGRAPH Add Runoff " " Velocity 1.124 m/sec"

" 4 Add Runoff " " Channel capacity 215.995 c.m/sec"

" 17.615 17.615 30.050 30.050" " Critical depth 0.827 metre"

" 52 CHANNEL DESIGN" " 53 ROUTE Channel Route 1800"

" 17.615 Current peak flow c.m/sec" " 1800.00 Channel Route 1800 Reach length (metre)"

" 0.040 Manning 'n'" " 0.340 X-factor <= 0.5"

" 0. Cross-section type: 0=trapezoidal; 1=general" " 400.376 K-lag (seconds)"

" 2.000 Basewidth metre" " 0.000 Default(0) or user spec.(1) values used"

" 3.000 Left bank slope" " 0.500 X-factor <= 0.5"

" 3.000 Right bank slope" " 30.000 K-lag (seconds)"

" 5.000 Channel depth metre" " 0.500 Beta weighting factor"

" 0.400 Gradient %" " 300.000 Routing time step (seconds)"

" Depth of flow 1.668 metre" " 3 No. of sub-reaches"

" Velocity 1.508 m/sec" " Peak outflow 8.135 c.m/sec"

" Channel capacity 249.409 c.m/sec" " 8.472 8.472 8.135 44.774 c.m/sec"

" Critical depth 1.188 metre" " 40 HYDROGRAPH Combine 11"

" 53 ROUTE Channel Route 1800" " 6 Combine "

" 1800.00 Channel Route 1800 Reach length (metre)" " 11 Node #"

" 0.340 X-factor <= 0.5" " Confluence on Penatangore Tributary"

" 298.497 K-lag (seconds)" " Maximum flow 50.903 c.m/sec"

" 0.000 Default(0) or user spec.(1) values used" " Hydrograph volume 432480.250 c.m"

" 0.500 X-factor <= 0.5" " 8.472 8.472 8.135 50.903"

" 30.000 K-lag (seconds)" " 40 HYDROGRAPH Start - New Tributary"

" 0.500 Beta weighting factor" " 2 Start - New Tributary"

" 300.000 Routing time step (seconds)" " 8.472 0.000 8.135 50.903"

" 3 No. of sub-reaches" " 33 CATCHMENT 56"

" Peak outflow 17.265 c.m/sec" " 1 Triangular SCS"

" 17.615 17.615 17.265 30.050 c.m/sec" " 1 Equal length"

" 40 HYDROGRAPH Combine 10" " 1 SCS method"

" 6 Combine " " 56 No description"

" 10 Node #" " 0.000 % Impervious"

" Confluence on Penatangore Tributary" " 345.000 Total Area"

" Maximum flow 45.035 c.m/sec" " 240.000 Flow length"

" Hydrograph volume 390319.781 c.m" " 11.000 Overland Slope"

" 17.615 17.615 17.265 45.035" " 345.000 Pervious Area"

" 40 HYDROGRAPH Confluence 10" " 240.000 Pervious length"

" 7 Confluence " " 11.000 Pervious slope"

" 10 Node #" " 0.000 Impervious Area"

" Confluence on Penatangore Tributary" " 240.000 Impervious length"

" Maximum flow 45.035 c.m/sec" " 15.000 Impervious slope"

" Hydrograph volume 390319.781 c.m" " 0.280 Pervious Manning 'n'"

" 17.615 45.035 17.265 0.000" " 79.000 Pervious SCS Curve No."

" 52 CHANNEL DESIGN" " 0.498 Pervious Runoff coefficient"

" 45.035 Current peak flow c.m/sec" " 0.100 Pervious Ia/S coefficient"

" 0.040 Manning 'n'" " 6.752 Pervious Initial abstraction"

" 0. Cross-section type: 0=trapezoidal; 1=general" " 0.013 Impervious Manning 'n'"

" 2.000 Basewidth metre" " 98.000 Impervious SCS Curve No."

" 3.000 Left bank slope" " 0.000 Impervious Runoff coefficient"

" 3.000 Right bank slope" " 0.100 Impervious Ia/S coefficient"

" 5.000 Channel depth metre" " 0.518 Impervious Initial abstraction"

" 0.400 Gradient %" " 32.068 0.000 8.135 50.903 c.m/sec"

" Depth of flow 2.489 metre" " Catchment 56 Pervious Impervious Total Area "

" Velocity 1.911 m/sec" " Surface Area 345.000 0.000 345.000 hectare"

" Channel capacity 249.409 c.m/sec" " Time of concentration 36.531 4.554 36.531 minutes"

" Critical depth 1.847 metre" " Time to Centroid 267.854 206.382 267.853 minutes"

" 53 ROUTE Channel Route 2000" " Rainfall depth 86.100 86.100 86.100 mm"

" 2000.00 Channel Route 2000 Reach length (metre)" " Rainfall volume 29.7045 0.0000 29.7045 ha-m"

" 0.370 X-factor <= 0.5" " Rainfall losses 43.248 6.318 43.248 mm"

" 392.542 K-lag (seconds)" " Runoff depth 42.852 79.782 42.852 mm"

" 0.000 Default(0) or user spec.(1) values used" " Runoff volume 14.7839 0.0000 14.7839 ha-m"

" 0.500 X-factor <= 0.5" " Runoff coefficient 0.498 0.000 0.498 "

" 30.000 K-lag (seconds)" " Maximum flow 32.068 0.000 32.068 c.m/sec"

" 0.500 Beta weighting factor" " 40 HYDROGRAPH Add Runoff "

" 300.000 Routing time step (seconds)" " 4 Add Runoff "

" 2 No. of sub-reaches" " 32.068 32.068 8.135 50.903"

" Peak outflow 44.774 c.m/sec" " 52 CHANNEL DESIGN"

" 17.615 45.035 44.774 0.000 c.m/sec" " 32.068 Current peak flow c.m/sec"

" 40 HYDROGRAPH Combine 11" " 0.040 Manning 'n'"

" 6 Combine " " 0. Cross-section type: 0=trapezoidal; 1=general"

" 11 Node #" " 2.000 Basewidth metre"

" Confluence on Penatangore Tributary" " 3.000 Left bank slope"

" Maximum flow 44.774 c.m/sec" " 3.000 Right bank slope"

" Hydrograph volume 390319.656 c.m" " 5.000 Channel depth metre"

" 17.615 45.035 44.774 44.774" " 0.400 Gradient %"

" 40 HYDROGRAPH Start - New Tributary" " Depth of flow 2.158 metre"

" 2 Start - New Tributary" " Velocity 1.754 m/sec"

" 17.615 0.000 44.774 44.774" " Channel capacity 249.409 c.m/sec"

" 33 CATCHMENT 62" " Critical depth 1.579 metre"

" 1 Triangular SCS" " 53 ROUTE Channel Route 1300"

" 1 Equal length" " 1300.00 Channel Route 1300 Reach length (metre)"

" 1 SCS method" " 0.324 X-factor <= 0.5"

" 62 No description" " 277.926 K-lag (seconds)"

" 0.000 % Impervious" " 0.000 Default(0) or user spec.(1) values used"

" 95.000 Total Area" " 0.500 X-factor <= 0.5"

" 160.000 Flow length" " 30.000 K-lag (seconds)"

" 2.500 Overland Slope" " 0.500 Beta weighting factor"

" 95.000 Pervious Area" " 300.000 Routing time step (seconds)"

" 160.000 Pervious length" " 2 No. of sub-reaches"

" 2.500 Pervious slope" " Peak outflow 31.517 c.m/sec"

" 0.000 Impervious Area" " 32.068 32.068 31.517 50.903 c.m/sec"

" 160.000 Impervious length" " 40 HYDROGRAPH Combine 11"

" 160.000 Impervious slope" " 6 Combine "

" 2.500 Pervious Manning 'n'" " 11 Node #"

" 0.250 Pervious Manning 'n'" " Confluence on Penatangore Tributary"

" 80.000 Pervious SCS Curve No." " Maximum flow 70.381 c.m/sec"

" 0.515 Pervious Runoff coefficient" " Hydrograph volume 580319.938 c.m"

" 0.100 Pervious Ia/S coefficient" " 32.068 32.068 31.517 70.381"

" 6.350 Pervious Initial abstraction" " 40 HYDROGRAPH Confluence 11"

" 0.013 Impervious Manning 'n'" " 7 Confluence "

" 98.000 Impervious SCS Curve No." " 11 Node #"

" 0.000 Impervious Runoff coefficient" " Confluence on Penatangore Tributary"

" 0.100 Impervious Ia/S coefficient" " Maximum flow 70.381 c.m/sec"

" 0.518 Impervious Initial abstraction" " Hydrograph volume 580319.875 c.m"

" 8.472 0.000 44.774 44.774 c.m/sec" " "

" 32.068 70.381 31.517 0.000"
52 CHANNEL DESIGN"
70.381 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 2.862 metre"
Velocity 2.324 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 2.263 metre"
53 ROUTE Channel Route 1300"
1300.00 Channel Route 1300 Reach length (metre)"
0.318 X-factor <= 0.5"
209.797 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 70.253 c.m/sec"
32.068 70.381 70.253 0.000 c.m/sec"
40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penatangore Tributary"
Maximum flow 70.253 c.m/sec"
Hydrograph volume 580320.063 c.m"
32.068 70.381 70.253 70.253"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
32.068 0.000 70.253 70.253"
33 CATCHMENT 58"
1 Triangular SCS"
1 Equal length"
1 SCS method"
58 No description"
0.000 % Impervious"
82.000 Total Area"
140.000 Flow length"
15.000 Overland Slope"
82.000 Pervious Area"
140.000 Pervious length"
15.000 Pervious slope"
0.000 Impervious Area"
140.000 Impervious length"
15.000 Impervious slope"
0.230 Pervious Manning 'n'"
81.000 Pervious SCS Curve No."
0.533 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.958 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
10.634 0.000 70.253 70.253 c.m/sec"
Catchment 58 Pervious Impervious Total Area "
Surface Area 82.000 0.000 82.000 hectare"
Time of concentration 20.955 3.295 20.955 minutes"
Time to Centroid 247.521 204.757 247.521 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 7.0602 0.0000 7.0602 ha-m"
Rainfall losses 40.178 7.017 40.178 mm"
Runoff depth 45.922 79.083 45.922 mm"
Runoff volume 3.7656 0.0000 3.7656 ha-m"
Runoff coefficient 0.533 0.000 0.533 "
Maximum flow 10.634 0.000 10.634 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
10.634 10.634 70.253 70.253"
52 CHANNEL DESIGN"
10.634 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.270 metre"
Velocity 1.441 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.927 metre"
53 ROUTE Channel Route 700"
700.00 Channel Route 700 Reach length (metre)"
0.337 X-factor <= 0.5"
182.217 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 10.392 c.m/sec"
10.634 10.634 10.392 70.253 c.m/sec"
40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penatangore Tributary"
Maximum flow 72.784 c.m/sec"
Hydrograph volume 617975.438 c.m"
10.634 10.634 10.392 72.784"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
10.634 0.000 10.392 72.784"
33 CATCHMENT 64"
1 Triangular SCS"
1 Equal length"
1 SCS method"
64 No description"
0.000 % Impervious"
80.000 Total Area"
220.000 Flow length"
5.500 Overland Slope"
80.000 Pervious Area"
220.000 Pervious length"
5.500 Pervious slope"
0.000 Impervious Area"
220.000 Impervious length"
5.500 Impervious slope"
0.210 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.552 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
8.580 0.000 10.392 72.784 c.m/sec"
Catchment 64 Pervious Impervious Total Area "
Surface Area 80.000 0.000 80.000 hectare"
Time of concentration 34.803 5.840 34.803 minutes"
Time to Centroid 263.478 207.720 263.478 minutes"
Rainfall depth 86.100 86.100 86.100 mm"
Rainfall volume 6.8880 0.0000 6.8880 ha-m"
Rainfall losses 38.551 5.897 38.551 mm"
Runoff depth 47.549 80.203 47.549 mm"
Runoff volume 3.8039 0.0000 3.8039 ha-m"
Runoff coefficient 0.552 0.000 0.552 "
Maximum flow 8.580 0.000 8.580 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
8.580 8.580 10.392 72.784"
52 CHANNEL DESIGN"
8.580 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 1.153 metre"
Velocity 1.363 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 0.833 metre"
53 ROUTE Channel Route 700"
700.00 Channel Route 700 Reach length (metre)"
0.350 X-factor <= 0.5"
192.537 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 8.497 c.m/sec"
8.580 8.580 8.497 72.784 c.m/sec"
40 HYDROGRAPH Combine 12"
6 Combine "
12 Node #"
Confluence on Penatangore Tributary"
Maximum flow 76.961 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 8.580 8.497 76.961"
40 HYDROGRAPH Confluence 12"
7 Confluence "
12 Node #"
Confluence on Penatangore Tributary"
Maximum flow 76.961 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 76.961 8.497 0.000"
52 CHANNEL DESIGN"
76.961 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.300 Gradient %"
Depth of flow 3.297 metre"
Velocity 1.963 m/sec"
Channel capacity 215.995 c.m/sec"
Critical depth 2.356 metre"
53 ROUTE Channel Route 2500"
2500.00 Channel Route 2500 Reach length (metre)"
0.230 X-factor <= 0.5"
318.467 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
3 No. of sub-reaches"
Peak outflow 75.678 c.m/sec"
8.580 76.961 75.678 0.000 c.m/sec"
40 HYDROGRAPH Combine 1000"
6 Combine "
1000 Node #"
Node upstream of Penatangore Culvert"
Maximum flow 75.678 c.m/sec"
Hydrograph volume 656014.750 c.m"
8.580 76.961 75.678 75.678"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
8.580 0.000 75.678 75.678"
33 CATCHMENT 59"
1 Triangular SCS"
1 Equal length"
1 SCS method"
59 No description"
0.000 % Impervious"
128.000 Total Area"
170.000 Flow length"
18.000 Overland Slope"
128.000 Pervious Area"
170.000 Pervious length"
18.000 Pervious slope"
0.000 Impervious Area"
170.000 Impervious length"
18.000 Impervious slope"
0.350 Pervious Manning 'n'"
76.000 Pervious SCS Curve No."
0.447 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
8.021 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
11.726 0.000 75.678 75.678 c.m/sec"
Catchment 59 Pervious Impervious Total Area "
Surface Area 128.000 0.000 128.000 hectare"
Time of concentration 30.299 3.505 30.299 minutes"

Time to Centroid	262.475	204.855	262.475	minutes"
Rainfall depth	86.100	86.100	86.100	mm"
Rainfall volume	11.0208	0.0000	11.0208	ha-m"
Rainfall losses	47.606	7.396	47.606	mm"
Runoff depth	38.494	78.704	38.494	mm"
Runoff volume	4.9273	0.0000	4.9273	ha-m"
Runoff coefficient	0.447	0.000	0.447	"
Maximum flow	11.726	0.000	11.726	c.m/sec"
HYDROGRAPH Add Runoff "				
4 Add Runoff "	11.726	11.726	75.678	75.678"
CHANNEL DESIGN"				
11.726 Current peak flow	c.m/sec"			
0.040 Manning 'n'"				
0. Cross-section type: 0=trapezoidal; 1=general"				
2.000 Basewidth	metre"			
3.000 Left bank slope"				
3.000 Right bank slope"				
5.000 Channel depth	metre"			
0.300 Gradient	%"			
Depth of flow	1.487	metre"		
Velocity	1.221	m/sec"		
Channel capacity	215.995	c.m/sec"		
Critical depth	0.973	metre"		
ROUTE Channel Route 1500"				
1500.00 Channel Route 1500 Reach length	(metre)"			
0.281 X-factor <= 0.5"				
307.084 K-lag (seconds)"				
0.000 Default(0) or user spec.(1) values used"				
0.500 X-factor <= 0.5"				
30.000 K-lag (seconds)"				
0.500 Beta weighting factor"				
300.000 Routing time step (seconds)"				
3 No. of sub-reaches"				
Peak outflow	11.131	c.m/sec"		
11.726 11.726 11.131	75.678	c.m/sec"		
HYDROGRAPH Combine 1000"				
6 Combine "				
1000 Node #"				
Node upstream of Penetangore Culvert"				
Maximum flow	79.914	c.m/sec"		
Hydrograph volume	705287.563	c.m"		
11.726 11.726 11.131	79.914"			
ADD COMMENT=====				
1 Lines of comment"				
End of Penetangore Tributary"				
ADD COMMENT=====				
1 Lines of comment"				
Start of Area North of Holtby Drain"				
HYDROGRAPH Start - New Tributary"				
2 Start - New Tributary"				
11.726 0.000 11.131	79.914"			
CATCHMENT 201"				
1 Triangular SCS"				
1 Equal length"				
1 SCS method"				
201 No description"				
0.000 % Impervious"				
166.000 Total Area"				
250.000 Flow length"				
3.000 Overland Slope"				
166.000 Pervious Area"				
250.000 Pervious length"				
3.000 Pervious slope"				
0.000 Impervious Area"				
250.000 Impervious length"				
3.000 Impervious slope"				
0.200 Pervious Manning 'n'"				
82.000 Pervious SCS Curve No."				
0.552 Pervious Runoff coefficient"				
0.100 Pervious Ia/S coefficient"				
5.576 Pervious Initial abstraction"				
0.013 Impervious Manning 'n'"				
98.000 Impervious SCS Curve No."				
0.000 Impervious Runoff coefficient"				
0.100 Impervious Ia/S coefficient"				
0.518 Impervious Initial abstraction"				
15.489 0.000 11.131	79.914 c.m/sec"			
Catchment 201 Pervious	Impervious Total Area "			
Surface Area	166.000 0.000 166.000	hectare"		
Time of concentration	43.771 7.563 43.771	minutes"		
Time to Centroid	274.325 209.915 274.325	minutes"		
Rainfall depth	86.100 86.100 86.100	mm"		
Rainfall volume	14.2926 0.0000 14.2926	ha-m"		
Rainfall losses	38.537 5.756 38.537	mm"		
Runoff depth	47.563 80.344 47.563	mm"		
Runoff volume	7.8955 0.0000 7.8955	ha-m"		
Runoff coefficient	0.552 0.000 0.552	"		
Maximum flow	15.489 0.000 15.489	c.m/sec"		
HYDROGRAPH Add Runoff "				
4 Add Runoff "	15.489 15.489 11.131	79.914"		
CHANNEL DESIGN"				
15.489 Current peak flow	c.m/sec"			
0.040 Manning 'n'"				
0. Cross-section type: 0=trapezoidal; 1=general"				
2.000 Basewidth	metre"			
3.000 Left bank slope"				
3.000 Right bank slope"				
5.000 Channel depth	metre"			
1.000 Gradient	%"			
Depth of flow	1.287	metre"		
Velocity	2.053	m/sec"		
Channel capacity	394.351	c.m/sec"		
Critical depth	1.116	metre"		
ROUTE Channel Route 1900"				
1900.00 Channel Route 1900 Reach length	(metre)"			
0.454 X-factor <= 0.5"				
231.397 K-lag (seconds)"				
0.000 Default(0) or user spec.(1) values used"				
0.500 X-factor <= 0.5"				
30.000 K-lag (seconds)"				
0.500 Beta weighting factor"				
300.000 Routing time step (seconds)"				
3 No. of sub-reaches"				
Peak outflow	15.353	c.m/sec"		
15.489 15.489 15.353	79.914 c.m/sec"			
HYDROGRAPH Next link "				
5 Next link "				
15.489 15.353 15.353	79.914"			
CATCHMENT 202"				
1 Triangular SCS"				
1 Equal length"				
1 SCS method"				
202 No description"				
0.000 % Impervious"				
4.000 Total Area"				
225.000 Flow length"				
4.000 Overland Slope"				
4.000 Pervious Area"				
225.000 Pervious length"				
4.000 Pervious slope"				
0.000 Impervious Area"				
225.000 Impervious length"				
4.000 Pervious Manning 'n'"				
0.200 Pervious SCS Curve No."				
0.552 Pervious Runoff coefficient"				
0.100 Pervious Ia/S coefficient"				
5.576 Pervious Initial abstraction"				
0.013 Impervious Manning 'n'"				
98.000 Impervious SCS Curve No."				
0.000 Impervious Runoff coefficient"				
0.100 Impervious Ia/S coefficient"				
0.518 Impervious Initial abstraction"				
0.409 15.353 15.353	79.914 c.m/sec"			
Catchment 202 Pervious	Impervious Total Area "			
Surface Area	4.000 0.000 4.000	hectare"		
Time of concentration	37.692 6.513 37.692	minutes"		
Time to Centroid	266.978 208.591 266.978	minutes"		
Rainfall depth	86.100 86.100 86.100	mm"		
Rainfall volume	3444.00 0.00 3444.00	c.m"		
Rainfall losses	38.542 6.520 38.542	mm"		
Runoff depth	47.558 79.580 47.558	mm"		
Runoff volume	1902.33 0.00 1902.33	c.m"		
Runoff coefficient	0.552 0.000 0.552	"		
Maximum flow	0.409 0.000 0.409	c.m/sec"		
HYDROGRAPH Add Runoff "				
4 Add Runoff "	0.409 15.685 15.353	79.914"		
CHANNEL DESIGN"				
15.685 Current peak flow	c.m/sec"			
0.040 Manning 'n'"				
0. Cross-section type: 0=trapezoidal; 1=general"				
2.000 Basewidth	metre"			
3.000 Left bank slope"				
3.000 Right bank slope"				
5.000 Channel depth	metre"			
1.000 Gradient	%"			
Depth of flow	1.295	metre"		
Velocity	2.059	m/sec"		
Channel capacity	394.351	c.m/sec"		
Critical depth	1.123	metre"		
ROUTE Channel Route 200"				
200.00 Channel Route 200 Reach length	(metre)"			
0.355 X-factor <= 0.5"				
72.838 K-lag (seconds)"				
0.000 Default(0) or user spec.(1) values used"				
0.500 X-factor <= 0.5"				
30.000 K-lag (seconds)"				
0.500 Beta weighting factor"				
75.000 Routing time step (seconds)"				
1 No. of sub-reaches"				
Peak outflow	15.625	c.m/sec"		
0.409 15.685 15.625	79.914 c.m/sec"			
HYDROGRAPH Next link "				
5 Next link "				
0.409 15.625 15.625	79.914"			
CATCHMENT 203"				
1 Triangular SCS"				
1 Equal length"				
1 SCS method"				
203 No description"				
0.000 % Impervious"				
9.100 Total Area"				
450.000 Flow length"				
3.500 Overland Slope"				
9.100 Pervious Area"				
450.000 Pervious length"				
3.500 Pervious slope"				
0.000 Impervious Area"				
450.000 Impervious length"				
3.500 Impervious slope"				
0.200 Pervious Manning 'n'"				
82.000 Pervious SCS Curve No."				
0.552 Pervious Runoff coefficient"				
0.100 Pervious Ia/S coefficient"				
5.576 Pervious Initial abstraction"				
0.013 Impervious Manning 'n'"				
98.000 Impervious SCS Curve No."				
0.000 Impervious Runoff coefficient"				
0.100 Impervious Ia/S coefficient"				
0.518 Impervious Initial abstraction"				
0.685 15.625 15.625	79.914 c.m/sec"			
Catchment 203 Pervious	Impervious Total Area "			
Surface Area	9.100 0.000 9.100	hectare"		
Time of concentration	59.466 10.275 59.466	minutes"		
Time to Centroid	293.301 213.064 293.301	minutes"		
Rainfall depth	86.100 86.100 86.100	mm"		
Rainfall volume	7835.09 0.01 7835.10	c.m"		
Rainfall losses	38.530 5.863 38.530	mm"		
Runoff depth	47.570 80.237 47.570	mm"		
Runoff volume	4328.86 0.01 4328.86	c.m"		
Runoff coefficient	0.552 0.000 0.552	"		
Maximum flow	0.685 0.000 0.685	c.m/sec"		
HYDROGRAPH Add Runoff "				
4 Add Runoff "	0.685 16.303 15.625	79.914"		
CHANNEL DESIGN"				
16.303 Current peak flow	c.m/sec"			
0.040 Manning 'n'"				
0. Cross-section type: 0=trapezoidal; 1=general"				
2.000 Basewidth	metre"			
3.000 Left bank slope"				
3.000 Right bank slope"				
5.000 Channel depth	metre"			
1.000 Gradient	%"			
Depth of flow	1.317	metre"		
Velocity	2.080	m/sec"		
Channel capacity	394.351	c.m/sec"		
Critical depth	1.144	metre"		
ROUTE Channel Route 350"				
350.00 Channel Route 350 Reach length	(metre)"			
0.416 X-factor <= 0.5"				
126.212 K-lag (seconds)"				
0.000 Default(0) or user spec.(1) values used"				
0.500 X-factor <= 0.5"				
30.000 K-lag (seconds)"				
0.500 Beta weighting factor"				
100.000 Routing time step (seconds)"				
1 No. of sub-reaches"				
Peak outflow	16.254	c.m/sec"		
0.685 16.303 16.254	79.914 c.m/sec"			
HYDROGRAPH Combine 1100"				

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"      6 Combine "
1100 Node # "
"      Node taking 200 series - Bottom end of Holtby Drain"
"      Maximum flow 16.254 c.m/sec"
"      Hydrograph volume 85186.055 c.m"
"      0.685 16.303 16.254 16.254"
" 81 ADD COMMENT-----"
" 1 Lines of comment"
" End of Area North of Holtby Drain"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.685 0.000 16.254 16.254"
" 81 ADD COMMENT-----"
" 1 Lines of comment"
" Start of Holtby Drain"
" 33 CATCHMENT 100"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 100 No description"
" 0.000 % Impervious"
" 45.000 Total Area"
" 100.000 Flow length"
" 7.000 Overland Slope"
" 45.000 Pervious Area"
" 100.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 7.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 6.134 0.000 16.254 16.254 c.m/sec"
" Catchment 100 Pervious Impervious Total Area "
" Surface Area 45.000 0.000 45.000 hectare"
" Time of concentration 19.590 3.385 19.590 minutes"
" Time to Centroid 245.074 204.792 245.074 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 3.8745 0.0000 3.8745 ha-m"
" Rainfall losses 38.595 7.147 38.595 mm"
" Runoff depth 47.505 78.953 47.505 mm"
" Runoff volume 2.1377 0.0000 2.1377 ha-m"
" Runoff coefficient 0.552 0.000 0.552 "
" Maximum flow 6.134 0.000 6.134 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 6.134 6.134 16.254 16.254"
" 52 CHANNEL DESIGN"
" 6.134 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.840 metre"
" Velocity 1.615 m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.701 metre"
" 53 ROUTE Channel Route 1500"
" 1500.00 Channel Route 1500 Reach length ( metre)"
" 0.460 X-factor <= 0.5"
" 232.178 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 3 No. of sub-reaches"
" Peak outflow 6.134 6.134 6.034 16.254 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 6.134 6.034 6.034 16.254"
" 33 CATCHMENT 101"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 101 No description"
" 0.000 % Impervious"
" 11.200 Total Area"
" 50.000 Flow length"
" 7.000 Overland Slope"
" 11.200 Pervious Area"
" 50.000 Pervious length"
" 7.000 Pervious slope"
" 0.000 Impervious Area"
" 50.000 Impervious length"
" 7.000 Impervious slope"
" 0.280 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.514 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.305 0.000 6.839 6.839 c.m/sec"
" Catchment 101 Pervious Impervious Total Area "
" Surface Area 11.200 0.000 11.200 hectare"
" Time of concentration 16.148 2.233 16.148 minutes"
" Time to Centroid 242.477 203.345 242.477 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 9643.19 0.01 9643.20 c.m"
" Rainfall losses 41.808 6.646 41.808 mm"
" Runoff depth 44.292 79.454 44.292 c.m"
" Runoff volume 4960.69 0.01 4960.70 c.m"
" Runoff coefficient 0.514 0.000 0.514 "
" Maximum flow 1.446 0.000 1.446 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.446 6.859 6.034 16.254"
" 52 CHANNEL DESIGN"
" 6.859 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.145 metre"
" Velocity 0.865 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.125 metre"
" 53 ROUTE Channel Route 250"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
" Depth of flow 0.886 metre"
" Velocity 1.663 c.m/sec"
" Channel capacity 394.351 c.m/sec"
" Critical depth 0.743 metre"
" 53 ROUTE Channel Route 700"
" 700.00 Channel Route 700 Reach length ( metre)"
" 0.470 X-factor <= 0.5"
" 315.677 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 6.859 6.850 6.850 c.m/sec"
" 1.446 6.859 6.850 16.254 c.m/sec"
" 40 HYDROGRAPH Combine 1200"
" 6 Combine "
" 1200 Node # "
" Node taking 100 series for Holtby Drain"
" Maximum flow 6.850 c.m/sec"
" Hydrograph volume 26338.104 c.m"
" 1.446 6.859 6.850 6.850"
" 81 ADD COMMENT-----"
" 1 Lines of comment"
" End of Holtby Drain"
" 40 HYDROGRAPH Confluence 1200"
" 7 Confluence "
" 1200 Node # "
" Node taking 100 series for Holtby Drain"
" Maximum flow 6.850 c.m/sec"
" Hydrograph volume 26338.104 c.m"
" 1.446 6.850 6.850 0.000"
" 52 CHANNEL DESIGN"
" 6.850 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 1.040 metre"
" Velocity 1.286 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.742 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 29.150 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.678 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 6.839 6.839 0.000 c.m/sec"
" 1.446 6.850 6.839 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1300"
" 6 Combine "
" 1300 Node # "
" Node at Holtby Drain"
" Maximum flow 6.839 c.m/sec"
" Hydrograph volume 26338.102 c.m"
" 1.446 6.850 6.839 6.839"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 1.446 0.000 6.839 6.839"
" 33 CATCHMENT 604"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 604 No description"
" 0.000 % Impervious"
" 2.700 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 2.700 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.572 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.305 0.000 6.839 6.839 c.m/sec"
" Catchment 604 Pervious Impervious Total Area "
" Surface Area 2.700 0.000 2.700 hectare"
" Time of concentration 33.688 4.610 33.688 minutes"
" Time to Centroid 261.328 206.442 261.328 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 2324.70 0.00 2324.70 c.m"
" Rainfall losses 36.890 6.203 36.890 mm"
" Runoff depth 49.210 79.897 49.210 mm"
" Runoff volume 1328.66 0.00 1328.67 c.m"
" Runoff coefficient 0.572 0.000 0.572 "
" Maximum flow 0.305 0.000 0.305 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.305 0.305 6.839 6.839"
" 52 CHANNEL DESIGN"
" 0.305 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.145 metre"
" Velocity 0.865 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.125 metre"

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" 250.00 Channel Route 250 Reach length (metre)"
" 0.492 X-factor <= 0.5"
" 216.841 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.301 c.m/sec"
" 0.305 0.305 0.301 6.839 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.305 0.301 0.301 6.839"
" 33 CATCHMENT 605"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 605 No description"
" 0.000 % Impervious"
" 3.900 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 3.900 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.572 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.441 0.301 0.301 6.839 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
" Surface Area 3.900 0.000 3.900 hectare"
" Time of concentration 33.688 4.610 33.688 minutes"
" Time to Centroid 261.329 206.442 261.328 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 3357.90 0.00 3357.90 c.m"
" Rainfall losses 36.890 6.203 36.890 mm"
" Runoff depth 49.210 79.897 49.210 mm"
" Runoff volume 1919.18 0.00 1919.18 c.m"
" Runoff coefficient 0.572 0.000 0.572 "
" Maximum flow 0.441 0.000 0.441 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.441 0.742 0.301 6.839"
" 52 CHANNEL DESIGN"
" 0.742 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.238 metre"
" Velocity 1.146 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.215 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length (metre)"
" 0.484 X-factor <= 0.5"
" 130.882 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.730 c.m/sec"
" 0.441 0.742 0.730 6.839 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 0.730 c.m/sec"
" Hydrograph volume 3247.852 c.m"
" 0.441 0.742 0.730 0.730"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.441 0.000 0.730 0.730"
" 33 CATCHMENT 603"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 603 No description"
" 0.000 % Impervious"
" 5.600 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 5.600 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.572 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.633 0.000 0.730 0.730 c.m/sec"
" Catchment 603 Pervious Impervious Total Area "
" Surface Area 5.600 0.000 5.600 hectare"
" Time of concentration 33.688 4.610 33.688 minutes"
" Time to Centroid 261.328 206.442 261.328 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 4821.59 0.00 4821.60 c.m"
" Rainfall losses 36.890 6.203 36.890 mm"
" Runoff depth 49.210 79.897 49.210 mm"
" Runoff volume 2755.75 0.00 2755.75 c.m"
" Runoff coefficient 0.572 0.000 0.572 "
" Maximum flow 0.633 0.000 0.633 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.511 1.353 1.353"
" 52 CHANNEL DESIGN"
" 0.511 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.080 metre"
" Velocity 1.073 m/sec"
" 4 Add Runoff "
" 0.633 0.633 0.730 0.730"
" 52 CHANNEL DESIGN"
" 0.633 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.218 metre"
" Velocity 1.091 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.196 metre"
" 53 ROUTE Channel Route 225"
" 225.00 Channel Route 225 Reach length (metre)"
" 0.487 X-factor <= 0.5"
" 154.614 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.628 c.m/sec"
" 0.633 0.633 0.628 0.730 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 1.358 c.m/sec"
" Hydrograph volume 6003.606 c.m"
" 0.633 0.633 0.628 1.358"
" 40 HYDROGRAPH Confluence 4000"
" 7 Confluence "
" 4000 Node #"
" Maximum flow 1.358 c.m/sec"
" Hydrograph volume 6003.607 c.m"
" 0.633 1.358 0.628 0.000"
" 52 CHANNEL DESIGN"
" 1.358 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.475 metre"
" Velocity 0.836 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.307 metre"
" 53 ROUTE Channel Route 500"
" 500.00 Channel Route 500 Reach length (metre)"
" 0.403 X-factor <= 0.5"
" 224.414 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step (seconds)"
" 2 No. of sub-reaches"
" Peak outflow 1.353 c.m/sec"
" 0.633 1.358 1.353 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 1.353 c.m/sec"
" Hydrograph volume 6003.605 c.m"
" 0.633 1.358 1.353 1.353"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.633 0.000 1.353 1.353"
" 33 CATCHMENT 405"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 405 No description"
" 75.000 % Impervious"
" 3.200 Total Area"
" 75.000 Flow length"
" 2.000 Overland Slope"
" 0.800 Pervious Area"
" 75.000 Pervious length"
" 2.000 Pervious slope"
" 2.400 Impervious Area"
" 75.000 Impervious length"
" 2.000 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.572 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.920 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.511 0.000 1.353 1.353 c.m/sec"
" Catchment 405 Pervious Impervious Total Area "
" Surface Area 0.800 2.400 3.200 hectare"
" Time of concentration 30.310 4.148 8.637 minutes"
" Time to Centroid 257.241 205.640 214.494 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 688.80 2066.40 2755.20 c.m"
" Rainfall losses 36.891 6.902 14.399 mm"
" Runoff depth 49.209 79.198 71.701 mm"
" Runoff volume 393.68 1900.74 2294.42 c.m"
" Runoff coefficient 0.572 0.920 0.833 "
" Maximum flow 0.096 0.435 0.511 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.511 1.353 1.353"
" 52 CHANNEL DESIGN"
" 0.511 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.080 metre"
" Velocity 1.073 m/sec"

" Channel capacity 7.740 c.m/sec"
" Critical depth 0.096 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length (metre)"
" 0.493 X-factor <= 0.5"
" 104.847 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.505 c.m/sec"
" 0.511 0.511 0.505 1.353 c.m/sec"
" 40 HYDROGRAPH Combine 4100"
" 6 Combine "
" 4100 Node #"
" "
" Maximum flow 0.505 c.m/sec"
" Hydrograph volume 2294.417 c.m"
" 0.511 0.511 0.505 0.505"
" 40 HYDROGRAPH Confluence 4100"
" 7 Confluence "
" 4100 Node #"
" "
" Maximum flow 0.505 c.m/sec"
" Hydrograph volume 2294.417 c.m"
" 0.511 0.505 0.000"
" 52 CHANNEL DESIGN"
" 0.505 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.079 metre"
" Velocity 1.069 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.096 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length (metre)"
" 0.490 X-factor <= 0.5"
" 70.141 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.500 c.m/sec"
" 0.511 0.505 0.500 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 4200"
" 6 Combine "
" 4200 Node #"
" "
" Maximum flow 0.500 c.m/sec"
" Hydrograph volume 2294.418 c.m"
" 0.511 0.505 0.500 0.500"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.511 0.000 0.500 0.500"
" 33 CATCHMENT 406"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 406 No description"
" 85.000 % Impervious"
" 1.300 Total Area"
" 10.000 Flow length"
" 2.000 Overland Slope"
" 0.195 Pervious Area"
" 10.000 Pervious length"
" 2.000 Pervious slope"
" 1.105 Impervious Area"
" 10.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.549 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.914 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.223 0.000 0.500 0.500 c.m/sec"
" Catchment 406 Pervious Impervious Total Area "
" Surface Area 0.195 1.105 1.300 hectare"
" Time of concentration 7.166 1.238 1.807 minutes"
" Time to Centroid 230.185 201.886 204.600 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 167.89 951.41 1119.30 c.m"
" Rainfall losses 38.798 7.407 12.116 mm"
" Runoff depth 47.302 78.693 73.984 mm"
" Runoff volume 92.24 869.55 961.79 c.m"
" Runoff coefficient 0.549 0.914 0.859 "
" Maximum flow 0.026 0.197 0.223 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.223 0.223 0.500 0.500"
" 52 CHANNEL DESIGN"
" 0.223 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.051 metre"
" Velocity 0.835 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.060 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.486 X-factor <= 0.5"
" 44.925 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 42.857 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.223 c.m/sec"
" " 0.223 0.223 0.223 0.500 c.m/sec"
" 40 HYDROGRAPH Combine 4200"
" 6 Combine "
" " Node #"
" " Node Upstream of CTC Pond"
" Maximum flow 0.723 c.m/sec"
" Hydrograph volume 3256.206 c.m"
" 0.223 0.223 0.223 0.723"
" 52 CHANNEL DESIGN"
" 0.723 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.095 metre"
" Velocity 1.186 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.117 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length (metre)"
" 0.492 X-factor <= 0.5"
" 94.828 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.717 c.m/sec"
" 0.223 0.723 0.717 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 4300"
" 6 Combine "
" 4300 Node #"
" Node Upstream of CTC Pond"
" Maximum flow 0.717 c.m/sec"
" Hydrograph volume 3256.205 c.m"
" 0.223 0.723 0.717 0.717"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.223 0.000 0.717 0.717"
" 33 CATCHMENT 500"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 500 No description"
" 70.000 % Impervious"
" 5.800 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 1.740 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 4.060 Impervious Area"
" 100.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.533 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.934 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.913 0.000 0.717 0.717 c.m/sec"
" Catchment 500 Pervious Impervious Total Area "
" Surface Area 1.740 4.060 5.800 hectare"
" Time of concentration 28.822 4.929 9.627 minutes"
" Time to Centroid 257.024 206.801 216.677 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 1498.14 3495.66 4993.80 c.m"
" Rainfall losses 40.170 5.681 16.028 mm"
" Runoff depth 45.930 80.419 70.072 mm"
" Runoff volume 799.18 3265.00 4064.18 c.m"
" Runoff coefficient 0.533 0.934 0.814 "
" Maximum flow 0.199 0.757 0.913 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.913 0.913 0.717 0.717"
" 52 CHANNEL DESIGN"
" 0.913 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.108 metre"
" Velocity 1.268 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.132 metre"
" 53 ROUTE Channel Route 150"
" 150.00 Channel Route 150 Reach length (metre)"
" 0.491 X-factor <= 0.5"
" 88.757 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.903 c.m/sec"
" 0.913 0.913 0.903 0.717 c.m/sec"
" 40 HYDROGRAPH Combine 4300"
" 6 Combine "
" 4300 Node #"
" Node Upstream of CTC Pond"
" Maximum flow 1.620 c.m/sec"
" Hydrograph volume 7320.388 c.m"
" 0.913 0.913 0.903 1.620"
" 40 HYDROGRAPH Confluence 4300"
" 7 Confluence "
" 4300 Node #"
" Node Upstream of CTC Pond"
" Maximum flow 1.620 c.m/sec"

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" Hydrograph volume 7320.387 c.m"
" 0.913 1.620 0.903 0.000"
" 52 CHANNEL DESIGN"
" 1.620 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.144 metre"
" Velocity 1.485 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.179 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.465 X-factor <= 0.5"
" 25.246 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 25.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.615 c.m/sec"
" 0.913 1.620 1.615 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.913 1.615 1.615 0.000"
" 81 ADD COMMENT"
" 1 Lines of comment"
" EXISTING POND - DRY POND - CTC SITE"
" 54 POND DESIGN"
" 1.615 Current peak flow c.m/sec"
" 0.635 Target outflow c.m/sec"
" 7320.4 Hydrograph volume c.m"
" 15. Number of stages"
" 0.000 Minimum water level metre"
" 1.400 Maximum water level metre"
" 0.000 Starting water level metre"
" 0 Keep Design Data: 1 = True; 0 = False"
" Level Discharge Volume"
" 0.000 0.000 0.000"
" 0.1000 0.00276 124.985"
" 0.2000 0.00477 256.026"
" 0.3000 0.00616 393.250"
" 0.4000 0.00729 536.786"
" 0.5000 0.00827 686.761"
" 0.6000 0.00914 843.304"
" 0.7000 0.00994 1006.543"
" 0.8000 0.01068 1176.605"
" 0.9000 0.2200 1353.618"
" 1.000 0.6243 1537.711"
" 1.100 1.178 1729.012"
" 1.200 1.871 1927.648"
" 1.300 2.698 2133.748"
" 1.400 3.658 2347.440"
" 1. WEIRS"
" Crest Weir Crest Left Right"
" elevation coefficient breadth sideslope sideslope"
" 0.800 0.980 3.800 2.000 2.000"
" 1. ORIFICES"
" Orifice Orifice Orifice Number of"
" invert coefficient diameter orifices"
" 0.000 0.630 0.0750 1.000"
" 2. LAYERS"
" Bottom Aspect Bottom Top Average"
" area ratio elevation elevation sideslope"
" 1220.000 2.000 0.000 1.400 4.000"
" 2175.299 1.688 1.400 1.400 4.000"
" Peak outflow 1.547 c.m/sec"
" Maximum level 1.154 metre"
" Maximum storage 1837.095 c.m"
" Centroidal lag 7.872 hours"
" 0.913 1.615 1.547 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.913 1.547 1.547 0.000"
" 52 CHANNEL DESIGN"
" 1.547 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.507 metre"
" Velocity 0.866 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.331 metre"
" 53 ROUTE Channel Route 220"
" 220.00 Channel Route 220 Reach length (metre)"
" 0.383 X-factor <= 0.5"
" 190.498 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.533 c.m/sec"
" 0.913 1.547 1.533 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 2.433 c.m/sec"
" Hydrograph volume 12856.608 c.m"
" 0.913 1.547 1.533 2.433"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.913 0.000 1.533 2.433"
" 33 CATCHMENT 750"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 750 No description"
" 100.000 % Impervious"
" 0.500 Total Area"
" 50.000 Flow length"
" 2.000 Overland Slope"
" 0.000 Pervious Area"
" 50.000 Pervious length"
" 2.000 Pervious slope"
" 0.500 Impervious Area"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.919 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.093 0.000 1.533 2.433 c.m/sec"
" Catchment 750 Pervious Impervious Total Area "
" Surface Area 0.000 0.500 0.500 hectare"
" Time of concentration 19.015 3.252 3.252 minutes"
" Time to Centroid 245.172 204.723 204.723 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 0.00 430.50 430.50 c.m"
" Rainfall losses 40.215 6.972 6.972 mm"
" Runoff depth 45.885 79.128 79.128 c.m"
" Runoff volume 0.00 395.64 395.64 c.m"
" Runoff coefficient 0.000 0.919 0.919 "
" Maximum flow 0.000 0.093 0.093 c.m/sec"
" 4 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.093 1.533 2.433"
" 81 ADD COMMENT"
" 1 Lines of comment"
" EXISTING POND - ROOFTOP STORAGE - CTC SITE"
" 54 POND DESIGN"
" 0.093 Current peak flow c.m/sec"
" 0.020 Target outflow c.m/sec"
" 395.6 Hydrograph volume c.m"
" 9. Number of stages"
" 0.000 Minimum water level metre"
" 0.200 Maximum water level metre"
" 0.000 Starting water level metre"
" 0 Keep Design Data: 1 = True; 0 = False"
" Level Discharge Volume"
" 0.000 0.000 0.000"
" 0.02500 0.00112 72.969"
" 0.07500 0.00386 146.876"
" 0.10000 0.01047 221.724"
" 0.1250 0.01422 297.514"
" 0.1500 0.01967 451.931"
" 0.1750 0.02190 530.562"
" 0.2000 0.02391 610.142"
" 1. ORIFICES"
" Orifice Orifice Orifice Number of"
" invert coefficient diameter orifices"
" 0.000 0.630 0.0680 6.000"
" 2. LAYERS"
" Bottom Aspect Bottom Top Average"
" area ratio elevation elevation sideslope"
" 2900.000 10.000 0.000 0.200 4.000"
" 3085.338 1.960 0.200 0.200 4.000"
" Peak outflow 0.013 c.m/sec"
" Maximum level 0.095 metre"
" Maximum storage 282.400 c.m"
" Centroidal lag 12.676 hours"
" 0.093 0.093 0.013 2.433 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.093 0.013 0.013 2.433"
" 52 CHANNEL DESIGN"
" 0.013 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0 Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.034 metre"
" Velocity 0.180 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.116 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.459 X-factor <= 0.5"
" 208.115 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.013 c.m/sec"
" 0.093 0.013 0.013 2.433 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 12.445 c.m/sec"
" Hydrograph volume 13211.491 c.m"
" 0.093 0.013 0.013 2.445"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.093 0.000 0.013 2.445"
" 33 CATCHMENT 751"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 751 No description"
" 100.000 % Impervious"
" 0.200 Total Area"
" 50.000 Flow length"
" 2.000 Overland Slope"
" 0.000 Pervious Area"
" 50.000 Pervious length"
" 2.000 Pervious slope"
" 0.200 Impervious Area"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.919 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.037 0.000 0.013 2.445 c.m/sec"

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"	Catchment 751	Pervious	Impervious	Total Area	"	1.886	Current peak flow	c.m/sec"
"	Surface Area	0.000	0.200	0.200	hectare"	0.040	Manning 'n'"	"
"	Time of concentration	19.015	3.252	3.252	minutes"	0.	Cross-section type: 0=trapezoidal; 1=general"	"
"	Time to Centroid	245.172	204.723	204.723	minutes"	2.000	Basewidth	metre"
"	Rainfall depth	86.100	86.100	86.100	mm"	3.000	Left bank slope"	"
"	Rainfall volume	0.00	172.20	172.20	c.m"	3.000	Right bank slope"	"
"	Rainfall losses	40.215	6.972	6.972	mm"	5.000	Channel depth	metre"
"	Runoff depth	45.885	79.128	79.128	mm"	1.200	Gradient %"	"
"	Runoff volume	0.00	158.26	158.26	c.m"		Depth of flow	0.449 metre"
"	Runoff coefficient	0.000	0.919	0.919	"		Velocity	1.256 m/sec"
"	Maximum flow	0.000	0.037	0.037	c.m/sec"		Channel capacity	431.989 c.m/sec"
"	HYDROGRAPH Add Runoff "						Critical depth	0.370 metre"
"	4 Add Runoff "						ROUTE	Channel Route 600"
"	0.037 0.037 0.013 2.445"						600.00	Channel Route 600 Reach length (metre)"
"	1 Lines of comment"						0.468	X-factor <= 0.5"
"	EXISTING POND - PARKING LOT STORAGE - CTC SITE"						179.202	K-lag (seconds)"
"	POND DESIGN"						0.000	Default(0) or user spec.(1) values used"
"	0.037 Current peak flow c.m/sec"						0.500	X-factor <= 0.5"
"	0.020 Target outflow c.m/sec"						30.000	K-lag (seconds)"
"	158.3 Hydrograph volume c.m"						0.500	Beta weighting factor"
"	5. Number of stages"						300.000	Routing time step (seconds)"
"	0.000 Minimum water level metre"						2	No. of sub-reaches"
"	0.700 Maximum water level metre"							Peak outflow
"	0.000 Starting water level metre"							1.886 1.886 1.876 2.473 c.m/sec"
"	0 Keep Design Data: 1 = True; 0 = False"						40	HYDROGRAPH Next link "
"	Level Discharge Volume"						5	Next link "
"	0.000 0.000 0.000"							1.886 1.876 1.876 2.473"
"	0.1750 0.01148 16.645"						33	CATCHMENT 401"
"	0.3500 0.03242 39.036"						1	Triangular SCS"
"	0.5250 0.04289 67.860"						1	Equal length"
"	0.7000 0.05126 103.803"						1	SCS method"
"	1. ORIFICES"						401	No description"
"	Orifice Orifice Orifice Number of "						0.000	% Impervious"
"	invert coefficic diameter orifices"						5.600	Total Area"
"	0.000 0.630 0.1750 1.000"						340.000	Flow length"
"	1. LAYERS"						3.500	Overland Slope"
"	Bottom Aspect Bottom Top Average"						5.600	Pervious Area"
"	area ratio elevation elevation sideslope"						340.000	Pervious length"
"	80.000 3.000 0.000 0.700 4.000"						3.500	Pervious slope"
"	Peak outflow 0.030 c.m/sec"						0.000	Impervious Area"
"	Maximum level 0.329 metre"						340.000	Impervious length"
"	Maximum storage 36.413 c.m"						3.500	Impervious slope"
"	Centroidal lag 3.789 hours"						0.300	Impervious Manning 'n'"
"	0.037 0.037 0.030 2.445 c.m/sec"						83.000	Pervious SCS Curve No."
"	HYDROGRAPH Next link "						0.572	Pervious Runoff coefficient"
"	5 Next link "						0.100	Pervious Ia/S coefficient"
"	0.037 0.030 0.030 2.445"						5.202	Pervious Initial abstraction"
"	CHANNEL DESIGN"						0.013	Impervious Manning 'n'"
"	0.030 Current peak flow c.m/sec"						98.000	Impervious SCS Curve No."
"	0.040 Manning 'n'"						0.000	Impervious Runoff coefficient"
"	0. Cross-section type: 0=trapezoidal; 1=general"						0.100	Impervious Ia/S coefficient"
"	2.000 Basewidth metre"						0.518	Impervious Initial abstraction"
"	3.000 Left bank slope"							0.418 1.876 1.876 2.473 c.m/sec"
"	3.000 Right bank slope"							Catchment 401 Pervious Impervious Total Area "
"	5.000 Channel depth metre"							Surface Area 5.600 0.000 5.600 hectare"
"	0.500 Gradient %"							Time of concentration 63.464 8.684 63.464 minutes"
"	Depth of flow 0.056 metre"							Time to Centroid 297.336 211.233 297.336 minutes"
"	Velocity 0.246 m/sec"							Rainfall depth 86.100 86.100 86.100 mm"
"	Channel capacity 278.848 c.m/sec"							Rainfall volume 4821.59 0.00 4821.60 c.m"
"	Critical depth 0.028 metre"							Rainfall losses 36.873 5.641 36.873 mm"
"	ROUTE Channel Route 50"							Runoff depth 49.227 80.459 49.227 mm"
"	50.000 Channel Route 50 Reach length (metre)"							Runoff volume 2756.73 0.00 2756.73 c.m"
"	0.434 X-factor <= 0.5"							Runoff coefficient 0.572 0.000 0.572 "
"	152.616 K-lag (seconds)"							Maximum flow 0.418 0.000 0.418 c.m/sec"
"	0.000 Default(0) or user spec.(1) values used"							HYDROGRAPH Add Runoff "
"	0.500 X-factor <= 0.5"							4 Add Runoff "
"	30.000 K-lag (seconds)"							0.418 2.204 1.876 2.473"
"	0.500 Beta weighting factor"							CHANNEL DESIGN"
"	150.000 Routing time step (seconds)"							2.204 Current peak flow c.m/sec"
"	1 No. of sub-reaches"							0.040 Manning 'n'"
"	Peak outflow 0.029 c.m/sec"							0. Cross-section type: 0=trapezoidal; 1=general"
"	0.037 0.030 0.029 2.445 c.m/sec"							2.000 Basewidth metre"
"	HYDROGRAPH Combine 2000"							3.000 Left bank slope"
"	6 Combine "							3.000 Right bank slope"
"	2000 Node #"							5.000 Channel depth metre"
"	Flow in Hwy. 21 Ditch"							1.200 Gradient %"
"	Maximum Flow 2.473 c.m/sec"							Depth of flow 0.486 metre"
"	Hydrograph volume 13369.757 c.m"							Velocity 1.311 m/sec"
"	0.037 0.029 2.473"							Channel capacity 431.989 c.m/sec"
"	1 Lines of comment"							Critical depth 0.404 metre"
"	Total discharge to Hwy. 21 Ditch"							ROUTE Channel Route 150"
"	HYDROGRAPH Start - New Tributary"							150.000 Channel Route 150 Reach length (metre)"
"	2 Start - New Tributary"							0.431 X-factor <= 0.5"
"	0.037 0.000 0.029 2.473"							85.802 K-lag (seconds)"
"	CATCHMENT 301"							0.000 Default(0) or user spec.(1) values used"
"	1 Triangular SCS"							0.500 X-factor <= 0.5"
"	1 Equal length"							30.000 K-lag (seconds)"
"	1 SCS method"							0.500 Beta weighting factor"
"	301 No description"							75.000 Routing time step (seconds)"
"	0.000 % Impervious"							1 No. of sub-reaches"
"	16.400 Total Area"							Peak outflow 0.418 2.204 2.198 2.473 c.m/sec"
"	95.000 Flow length"							40 HYDROGRAPH Next link "
"	2.500 Overland Slope"							5 Next link "
"	16.400 Pervious Area"							0.418 2.198 2.198 2.473"
"	95.000 Pervious length"							CATCHMENT 402"
"	2.500 Pervious slope"							1 Triangular SCS"
"	0.000 Impervious Area"							1 Equal length"
"	95.000 Impervious length"							1 SCS method"
"	2.500 Impervious slope"							402 No description"
"	0.230 Pervious Manning 'n'"							50.000 % Impervious"
"	81.000 Pervious SCS Curve No."							7.400 Total Area"
"	0.533 Pervious Runoff coefficient"							100.000 Flow length"
"	0.100 Pervious Ia/S coefficient"							2.000 Overland Slope"
"	5.958 Pervious Initial abstraction"							3.700 Pervious Area"
"	0.013 Impervious Manning 'n'"							100.000 Pervious length"
"	98.000 Impervious SCS Curve No."							2.000 Pervious slope"
"	0.000 Impervious Runoff coefficient"							3.700 Impervious Area"
"	0.100 Impervious Ia/S coefficient"							100.000 Impervious length"
"	0.518 Impervious Initial abstraction"							2.000 Impervious slope"
"	1.886 0.000 0.029 2.473 c.m/sec"							0.300 Pervious Manning 'n'"
"	Catchment 301 Pervious Impervious Total Area "							83.000 Pervious SCS Curve No."
"	Surface Area 16.400 0.000 16.400 hectare"							0.572 Pervious Runoff coefficient"
"	Time of concentration 28.425 4.470 28.425 minutes"							0.100 Pervious Ia/S coefficient"
"	Time to Centroid 256.550 206.240 256.550 minutes"							5.202 Pervious Initial abstraction"
"	Rainfall depth 86.100 86.100 86.100 mm"							0.013 Impervious Manning 'n'"
"	Rainfall volume 1.4120 0.0000 1.4120 ha-m"							98.000 Impervious SCS Curve No."
"	Rainfall losses 40.168 6.401 40.168 mm"							0.934 Impervious Runoff coefficient"
"	Runoff depth 45.932 79.699 45.932 mm"							0.100 Impervious Ia/S coefficient"
"	Runoff volume 7532.80 0.01 7532.81 c.m"							0.518 Impervious Initial abstraction"
"	Runoff coefficient 0.533 0.000 0.533 c.m/sec"							0.975 2.198 2.198 2.473 c.m/sec"
"	Maximum flow 1.886 0.000 1.886 c.m/sec"							Catchment 402 Pervious Impervious Total Area "
"	HYDROGRAPH Add Runoff "							Surface Area 3.700 3.700 7.400 hectare"
"	4 Add Runoff "							Time of concentration 36.021 4.929 16.733 minutes"
"	1.886 1.886 0.029 2.473"							Time to Centroid 264.150 206.801 228.574 minutes"
"	CHANNEL DESIGN"							Rainfall depth 86.100 86.100 86.100 mm"
"								Rainfall volume 3185.70 3185.70 6371.40 c.m"


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"
"
" Maximum flow 3.679 c.m/sec"
" Hydrograph volume 21951.813 c.m"
" 0.505 0.505 0.501 3.679"
" 40 HYDROGRAPH Confluence 6000"
" 7 Confluence "
" 6000 Node #"
"
"
" Maximum flow 3.679 c.m/sec"
" Hydrograph volume 21951.813 c.m"
" 0.505 3.679 0.501 0.000"
" 52 CHANNEL DESIGN"
" 3.679 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.213 metre"
" Velocity 1.849 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.269 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length (metre)"
" 0.487 X-factor <= 0.5"
" 81.117 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 3.630 c.m/sec"
" 0.505 3.679 3.630 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
"
" Maximum flow 3.630 c.m/sec"
" Hydrograph volume 21951.820 c.m"
" 0.505 3.679 3.630 3.630"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.505 0.000 3.630 3.630"
" 33 CATCHMENT 302"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 302 No description"
" 50.000 % Impervious"
" 6.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 3.000 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.000 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious slope"
" 0.280 Pervious Manning 'n'"
" 80.000 Pervious SCS Curve No."
" 0.515 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.934 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.760 0.000 3.630 3.630 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 3.000 3.000 6.000 hectare"
" Time of concentration 35.642 4.929 15.850 minutes"
" Time to Centroid 266.035 206.801 227.863 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 2583.00 2583.00 5166.00 c.m"
" Rainfall losses 41.724 5.681 23.703 mm"
" Runoff depth 44.376 80.419 62.397 mm"
" Runoff volume 1331.29 2412.56 3743.85 c.m"
" Runoff coefficient 0.515 0.934 0.725 "
" Maximum flow 0.294 0.560 0.760 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.760 0.760 3.630 3.630"
" 52 CHANNEL DESIGN"
" 0.760 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.098 metre"
" Velocity 1.203 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.120 metre"
" 53 ROUTE Channel Route 180"
" 180.00 Channel Route 180 Reach length (metre)"
" 0.493 X-factor <= 0.5"
" 112.185 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.738 c.m/sec"
" 0.760 0.760 0.738 3.630 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.760 0.738 0.738 3.630"
" 33 CATCHMENT 303"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 303 No description"
" 75.000 % Impervious"
" 4.800 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 1.200 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.600 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious slope"
" 0.280 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.552 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.934 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.759 0.738 0.738 3.630 c.m/sec"
" Catchment 303 Pervious Impervious Total Area "
" Surface Area 1.200 3.600 4.800 hectare"
" Time of concentration 34.908 4.929 9.865 minutes"
" Time to Centroid 263.605 206.801 216.153 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 1033.20 3099.60 4132.80 c.m"
" Rainfall losses 38.550 5.681 13.898 mm"
" Runoff depth 47.550 80.419 72.202 mm"
" Runoff volume 570.60 2895.07 3465.67 c.m"
" Runoff coefficient 0.552 0.934 0.839 "
" Maximum flow 0.128 0.671 0.759 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.759 1.497 0.738 3.630"
" 52 CHANNEL DESIGN"
" 1.497 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.138 metre"
" Velocity 1.454 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.172 metre"
" 53 ROUTE Channel Route 250"
" 250.00 Channel Route 250 Reach length (metre)"
" 0.493 X-factor <= 0.5"
" 128.980 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.463 c.m/sec"
" 0.759 1.497 1.463 3.630 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
"
" Maximum flow 5.006 c.m/sec"
" Hydrograph volume 29161.334 c.m"
" 0.759 1.497 1.463 5.006"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.759 0.000 1.463 5.006"
" 33 CATCHMENT 407"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 407 No description"
" 75.000 % Impervious"
" 3.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 0.750 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 2.250 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious slope"
" 2.000 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.572 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.934 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.475 0.000 1.463 5.006 c.m/sec"
" Catchment 407 Pervious Impervious Total Area "
" Surface Area 0.750 2.250 3.000 hectare"
" Time of concentration 36.021 4.929 10.197 minutes"
" Time to Centroid 264.150 206.801 216.518 minutes"
" Rainfall depth 86.100 86.100 86.100 mm"
" Rainfall volume 645.75 1937.25 2583.00 c.m"
" Rainfall losses 36.883 5.681 13.482 mm"
" Runoff depth 49.217 80.419 72.618 mm"
" Runoff volume 369.13 1809.42 2178.55 c.m"
" Runoff coefficient 0.572 0.934 0.843 "
" Maximum flow 0.082 0.420 0.475 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.475 0.475 1.463 5.006"
" 52 CHANNEL DESIGN"
" 0.475 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.076 metre"
" Velocity 1.050 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.092 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length (metre)"
" 0.490 X-factor <= 0.5"
" 71.416 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.471 c.m/sec"
" 0.475 0.475 0.471 5.006 c.m/sec"

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" 40 HYDROGRAPH Next link " " 0.3833 0.04383 3662.299"
" 5 Next link " " 0.4792 0.05156 4645.824"
" 0.475 0.471 0.471 5.006" " 0.5750 0.05826 5655.543"
" 33 CATCHMENT 310" " 0.6708 0.06427 6692.645"
" 1 Triangular SCS" " 0.7667 0.06977 7758.431"
" 1 Equal length" " 0.8625 0.07486 8850.853"
" 1 SCS method" " 0.9583 0.07963 9971.185"
" 310 No description" " 1.054 0.08412 11118.39"
" 75.000 % Impervious" " 1.150 0.08840 12297.52"
" 2.400 Total Area" " 1.246 0.2294 13505.21"
" 75.000 Flow length" " 1.342 0.4837 14741.64"
" 2.000 Overland Slope" " 1.438 0.8116 16006.97"
" 0.600 Pervious Area" " 1.533 1.195 17287.76"
" 75.000 Pervious length" " 1.629 1.633 18611.14"
" 2.000 Pervious slope" " 1.725 2.118 19963.96"
" 1.800 Impervious Area" " 1.821 2.644 21346.39"
" 75.000 Impervious length" " 1.917 3.209 22758.63"
" 2.000 Impervious slope" " 2.013 3.811 24200.82"
" 0.200 Pervious Manning 'n'" " 2.108 5.348 25657.67"
" 82.000 Pervious SCS Curve No." " 2.204 7.723 27160.03"
" 0.552 Pervious Runoff coefficient" " 2.300 10.675 28692.88"
" 0.100 Pervious Ia/S coefficient" "
" 5.576 Pervious Initial abstraction" " 2. WEIRS "
" 0.013 Impervious Manning 'n'" " Crest Weir Crest Left Right"
" 98.000 Impervious SCS Curve No." " elevation coefficient breadth sideslope sideslope"
" 0.920 Impervious Runoff coefficient" " 1.150 0.900 3.000 0.000 0.000"
" 0.100 Impervious Ia/S coefficient" " 2.013 0.900 20.000 3.000 3.000"
" 0.518 Impervious Initial abstraction" " 1. ORIFICES "
" 0.393 0.471 0.471 5.006 c.m/sec" " invert coefficient diameter orifices"
" Catchment 310 Pervious Impervious Total Area " " 0.000 0.630 0.2000 1.000"
" Surface Area 0.600 1.800 2.400 hectare" "
" Time of concentration 24.004 4.148 7.459 minutes" "
" Time to Centroid 250.434 205.640 213.109 minutes" "
" Rainfall depth 86.100 86.100 86.100 mm" "
" Rainfall volume 516.60 1549.80 2066.40 c.m" "
" Rainfall losses 38.555 6.902 14.815 mm" "
" Runoff depth 47.545 79.198 71.285 mm" "
" Runoff volume 285.27 1425.56 1710.83 c.m" "
" Runoff coefficient 0.552 0.920 0.828 " "
" Maximum flow 0.076 0.326 0.393 c.m/sec" "
" 40 HYDROGRAPH Add Runoff " " 40 HYDROGRAPH Next link "
" 4 Add Runoff " " 5 Next link "
" 0.393 0.864 0.471 5.006" " 0.393 2.080 2.080 0.000"
" 52 CHANNEL DESIGN" " 52 CHANNEL DESIGN"
" 0.864 Current peak flow c.m/sec" " 2.080 Current peak flow c.m/sec"
" 0.040 Manning 'n'" " 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; l=general" " 0. Cross-section type: 0=trapezoidal; l=general"
" 2.000 Basewidth metre" " 2.000 Basewidth metre"
" 3.000 Left bank slope" " 3.000 Left bank slope"
" 3.000 Right bank slope" " 3.000 Right bank slope"
" 5.000 Channel depth metre" " 5.000 Channel depth metre"
" 2.000 Gradient %" " 2.000 Gradient %"
" Depth of flow 0.259 metre" " Depth of flow 0.414 metre"
" Velocity 1.200 m/sec" " Velocity 1.551 m/sec"
" Channel capacity 557.696 c.m/sec" " Channel capacity 557.696 c.m/sec"
" Critical depth 0.236 metre" " Critical depth 0.391 metre"
" 53 ROUTE Channel Route 200" " 53 ROUTE Channel Route 250"
" 200.00 Channel Route 200 Reach length (metre)" " 250.00 Channel Route 250 Reach length (metre)"
" 0.482 X-factor <= 0.5" " 0.479 X-factor <= 0.5"
" 124.972 K-lag (seconds)" " 120.906 K-lag (seconds)"
" Default(0) or user spec.(1) values used" " Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5" " 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)" " 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor" " 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)" " 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches" " 1 No. of sub-reaches"
" Peak outflow 0.853 c.m/sec" " Peak outflow 2.073 c.m/sec"
" 0.393 0.864 0.853 5.006 c.m/sec" " 0.393 2.080 2.073 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100" " 40 HYDROGRAPH Combine 2000"
" 6 Combine " " 6 Combine "
" 6100 Node #" " 2000 Node #"
" Flow in Hwy. 21 Ditch" "
" Maximum flow 5.767 c.m/sec" " Maximum flow 3.546 c.m/sec"
" Hydrograph volume 33050.715 c.m" " Hydrograph volume 39391.145 c.m"
" 0.393 0.864 0.853 5.767" " 0.393 2.080 2.073 3.546"
" 40 HYDROGRAPH Confluence 6100" " 40 HYDROGRAPH Start - New Tributary"
" 7 Confluence " " 2 Start - New Tributary"
" 6100 Node #" " 0.393 0.000 2.073 3.546"
" Maximum flow 5.767 c.m/sec" "
" Hydrograph volume 33050.715 c.m" "
" 0.393 5.767 0.853 0.000" "
" 52 CHANNEL DESIGN" "
" 5.767 Current peak flow c.m/sec" "
" 0.040 Manning 'n'" "
" 0. Cross-section type: 0=trapezoidal; l=general" "
" 2.000 Basewidth metre" "
" 3.000 Left bank slope" "
" 3.000 Right bank slope" "
" 5.000 Channel depth metre" "
" 2.000 Gradient %" "
" Depth of flow 0.691 metre" "
" Velocity 2.050 m/sec" "
" Channel capacity 557.696 c.m/sec" "
" Critical depth 0.679 metre" "
" 53 ROUTE Channel Route 50" "
" 50.00 Channel Route 50 Reach length (metre)" "
" 0.332 X-factor <= 0.5" "
" 18.289 K-lag (seconds)" "
" Default(0) or user spec.(1) values used" "
" 0.500 X-factor <= 0.5" "
" 30.000 K-lag (seconds)" "
" 0.500 Beta weighting factor" "
" 23.077 Routing time step (seconds)" "
" 1 No. of sub-reaches" "
" Peak outflow 5.767 c.m/sec" "
" 0.393 5.767 5.762 0.000 c.m/sec" "
" 40 HYDROGRAPH Next link " "
" 5 Next link " "
" 0.393 5.762 5.762 0.000" "
" 81 ADD COMMENT-----" "
" 1 Lines of comment" "
" PROPOSED POND #2" "
" 54 POND DESIGN" "
" 5.762 Current peak flow c.m/sec" "
" 4.007 Target outflow c.m/sec" "
" 33050.7 Hydrograph volume c.m" "
" 25. Number of stages" "
" 0.000 Minimum water level metre" "
" 2.300 Maximum water level metre" "
" 0.000 Starting water level metre" "
" 0 Keep Design Data: 1 = True; 0 = False" "
" Level Discharge Volume" "
" 0.000 0.000 0.000" "
" 0.09583 0.00452 875.671" "
" 0.1917 0.01493 1778.243" "
" 0.2875 0.03442 2706.844" "
" 40 HYDROGRAPH Add Runoff " "
" 4 Add Runoff " "
" 1.079 1.079 2.073 3.546" "
" 52 CHANNEL DESIGN" "
" 1.079 Current peak flow c.m/sec" "
" 0.020 Manning 'n'" "
" 0. Cross-section type: 0=trapezoidal; l=general" "
" 4.000 Basewidth metre" "
" 50.000 Left bank slope" "
" 0.000 Right bank slope" "
" 0.300 Channel depth metre" "
" 2.000 Gradient %" "

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"	Depth of flow	0.117	metre"	"	Runoff depth	47.540	80.419	72.199	mm"
"	Velocity	1.328	m/sec"	"	Runoff volume	522.94	2653.82	3176.75	c.m"
"	Channel capacity	7.740	c.m/sec"	"	Runoff coefficient	0.552	0.934	0.839	"
"	Critical depth	0.145	metre"	"	Maximum flow	0.131	0.615	0.719	c.m/sec"
"	ROUTE Channel Route 200"			"	HYDROGRAPH Add Runoff "				
"	200.00 Channel Route 200 Reach length (metre)"			"	4 Add Runoff "	0.719	1.592	1.592"	
"	0.493 X-factor <= 0.5"			"					
"	112.936 K-lag (seconds)"			"	52 CHANNEL DESIGN"				
"	0.000 Default(0) or user spec.(1) values used"			"	0.719 Current peak flow c.m/sec"				
"	0.500 X-factor <= 0.5"			"	0.020 Manning 'n'"				
"	30.000 K-lag (seconds)"			"	0. Cross-section type: 0=trapezoidal; 1=general"				
"	0.500 Beta weighting factor"			"	4.000 Basewidth metre"				
"	100.000 Routing time step (seconds)"			"	50.000 Left bank slope"				
"	1 No. of sub-reaches"			"	0.000 Right bank slope"				
"	Peak outflow	1.065	c.m/sec"	"	0.300 Channel depth metre"				
"	1.079 1.079 1.065 3.546 c.m/sec"			"	2.000 Gradient %"				
"	40 HYDROGRAPH Next link "			"	Depth of flow	0.095	metre"		
"	5 Next link "			"	Velocity	1.184	m/sec"		
"	1.079 1.065 1.065 3.546"			"	Channel capacity	7.740	c.m/sec"		
"	33 CATCHMENT 314"			"	Critical depth	0.116	metre"		
"	1 Triangular SCS"			"	ROUTE Channel Route 100"				
"	1 Equal length"			"	100.00 Channel Route 100 Reach length (metre)"				
"	1 SCS method"			"	0.488 X-factor <= 0.5"				
"	314 No description"			"	63.319 K-lag (seconds)"				
"	50.000 % Impervious"			"	0.000 Default(0) or user spec.(1) values used"				
"	3.300 Total Area"			"	0.500 X-factor <= 0.5"				
"	20.000 Flow length"			"	30.000 K-lag (seconds)"				
"	1.000 Overland Slope"			"	0.500 Beta weighting factor"				
"	1.650 Pervious Area"			"	60.000 Routing time step (seconds)"				
"	20.000 Pervious length"			"	1 No. of sub-reaches"				
"	1.000 Pervious slope"			"	Peak outflow	0.714	c.m/sec"		
"	1.650 Impervious Area"			"	0.719 0.719 0.714 1.592 c.m/sec"				
"	20.000 Impervious length"			"	40 HYDROGRAPH Combine 7000"				
"	1.000 Impervious slope"			"	6 Combine "				
"	0.200 Pervious Manning 'n'"			"	7000 Node #"				
"	82.000 Pervious SCS Curve No."			"					
"	0.551 Pervious Runoff coefficient"			"	Maximum flow	2.306	c.m/sec"		
"	0.100 Pervious Ia/S coefficient"			"	Hydrograph volume	10035.589	c.m"		
"	5.576 Pervious Initial abstraction"			"	0.719 0.719 0.714 2.306"				
"	0.013 Impervious Manning 'n'"			"	40 HYDROGRAPH Start - New Tributary"				
"	98.000 Impervious SCS Curve No."			"	2 Start - New Tributary"				
"	0.922 Impervious Runoff coefficient"			"	0.719 0.000 0.714 2.306"				
"	0.100 Impervious Ia/S coefficient"			"	33 CATCHMENT 304"				
"	0.518 Impervious Initial abstraction"			"	1 Triangular SCS"				
"	0.533 1.065 1.065 3.546 c.m/sec"			"	1 Equal length"				
"	Catchment 314 Pervious Impervious Total Area "			"	1 SCS method"				
"	Surface Area 1.650 1.650 3.300 hectare"			"	304 No description"				
"	Time of concentration 13.372 2.310 6.448 minutes"			"	50.000 % Impervious"				
"	Time to Centroid 237.551 203.437 216.199 minutes"			"	1.600 Total Area"				
"	Rainfall depth 86.100 86.100 86.100 mm"			"	75.000 Flow length"				
"	Rainfall volume 1420.65 1420.65 2841.30 c.m"			"	2.000 Overland Slope"				
"	Rainfall losses 38.630 6.678 22.654 mm"			"	0.800 Pervious Area"				
"	Runoff depth 47.470 79.422 63.446 mm"			"	75.000 Pervious length"				
"	Runoff volume 783.25 1310.46 2093.71 c.m"			"	2.000 Pervious slope"				
"	Runoff coefficient 0.551 0.922 0.737 "			"	0.800 Impervious Area"				
"	Maximum flow 0.228 0.305 0.533 c.m/sec"			"	75.000 Impervious length"				
"	40 HYDROGRAPH Add Runoff "			"	2.000 Impervious slope"				
"	4 Add Runoff "	0.533	1.599	1.065	3.546"				
"									
"	52 CHANNEL DESIGN"			"	82.000 Pervious SCS Curve No."				
"	1.599 Current peak flow c.m/sec"			"	0.552 Pervious Runoff coefficient"				
"	0.040 Manning 'n'"			"	0.100 Pervious Ia/S coefficient"				
"	0. Cross-section type: 0=trapezoidal; 1=general"			"	5.576 Pervious Initial abstraction"				
"	2.000 Basewidth metre"			"	0.013 Impervious Manning 'n'"				
"	3.000 Left bank slope"			"	98.000 Impervious SCS Curve No."				
"	3.000 Right bank slope"			"	0.920 Impervious Runoff coefficient"				
"	5.000 Channel depth metre"			"	0.100 Impervious Ia/S coefficient"				
"	2.000 Gradient %"			"	0.518 Impervious Initial abstraction"				
"	Depth of flow	0.361	metre"	"	0.235 0.000 0.714 2.306 c.m/sec"				
"	Velocity	1.439	m/sec"	"	Catchment 304 Pervious Impervious Total Area "				
"	Channel capacity	557.696	c.m/sec"	"	Surface Area 0.800 0.800 1.600 hectare"				
"	Critical depth	0.337	metre"	"	Time of concentration 24.004 4.148 11.596 minutes"				
"	53 ROUTE Channel Route 80"			"	Time to Centroid 250.434 205.640 222.444 minutes"				
"	80.00 Channel Route 80 Reach length (metre)"			"	Rainfall depth 86.100 86.100 86.100 mm"				
"	0.441 X-factor <= 0.5"			"	Rainfall volume 688.80 688.80 1377.60 c.m"				
"	41.701 K-lag (seconds)"			"	Rainfall losses 38.555 6.902 22.729 mm"				
"	0.000 Default(0) or user spec.(1) values used"			"	Runoff depth 47.545 79.198 63.371 mm"				
"	0.500 X-factor <= 0.5"			"	Runoff volume 380.36 633.58 1013.94 c.m"				
"	30.000 K-lag (seconds)"			"	Runoff coefficient 0.552 0.920 0.736 "				
"	0.500 Beta weighting factor"			"	Maximum flow 0.101 0.145 0.235 c.m/sec"				
"	42.857 Routing time step (seconds)"			"	40 HYDROGRAPH Add Runoff "				
"	1 No. of sub-reaches"			"	4 Add Runoff "	0.235	0.714	2.306"	
"	Peak outflow	1.592	c.m/sec"	"					
"	0.533 1.599 1.592 3.546 c.m/sec"			"	52 CHANNEL DESIGN"				
"	40 HYDROGRAPH Combine 7000"			"	0.235 Current peak flow c.m/sec"				
"	6 Combine "			"	0.020 Manning 'n'"				
"	7000 Node #"			"	0. Cross-section type: 0=trapezoidal; 1=general"				
"				"	4.000 Basewidth metre"				
"	Maximum flow	1.592	c.m/sec"	"	50.000 Left bank slope"				
"	Hydrograph volume	6858.837	c.m"	"	0.000 Right bank slope"				
"	0.533 1.599 1.592 1.592"			"	0.600 Channel depth metre"				
"	40 HYDROGRAPH Start - New Tributary"			"	2.000 Gradient %"				
"	2 Start - New Tributary"			"	Depth of flow	0.052	metre"		
"	0.533 0.000 1.592 1.592"			"	Velocity	0.848	m/sec"		
"	33 CATCHMENT 312"			"	Channel capacity	38.450	c.m/sec"		
"	1 Triangular SCS"			"	Critical depth	0.062	metre"		
"	1 Equal length"			"	ROUTE Channel Route 50"				
"	1 SCS method"			"	50.00 Channel Route 50 Reach length (metre)"				
"	312 No description"			"	0.486 X-factor <= 0.5"				
"	75.000 % Impervious"			"	44.196 K-lag (seconds)"				
"	4.400 Total Area"			"	0.000 Default(0) or user spec.(1) values used"				
"	100.000 Flow length"			"	0.500 X-factor <= 0.5"				
"	2.000 Overland Slope"			"	30.000 K-lag (seconds)"				
"	1.100 Pervious Area"			"	0.500 Beta weighting factor"				
"	100.000 Pervious length"			"	42.857 Routing time step (seconds)"				
"	2.000 Pervious slope"			"	1 No. of sub-reaches"				
"	3.300 Impervious Area"			"	Peak outflow	0.232	c.m/sec"		
"	100.000 Impervious length"			"	0.235 0.235 0.232 2.306 c.m/sec"				
"	2.000 Impervious slope"			"	40 HYDROGRAPH Next link "				
"	0.200 Pervious Manning 'n'"			"	5 Next link "				
"	82.000 Pervious SCS Curve No."			"	0.235 0.232 0.232 2.306"				
"	0.552 Pervious Runoff coefficient"			"	33 CATCHMENT 313"				
"	0.100 Pervious Ia/S coefficient"			"	1 Triangular SCS"				
"	5.576 Pervious Initial abstraction"			"	1 Equal length"				
"	0.013 Impervious Manning 'n'"			"	1 SCS method"				
"	98.000 Impervious SCS Curve No."			"	313 No description"				
"	0.934 Impervious Runoff coefficient"			"	75.000 % Impervious"				
"	0.100 Impervious Ia/S coefficient"			"	1.800 Total Area"				
"	0.518 Impervious Initial abstraction"			"	50.000 Flow length"				
"	0.719 0.000 1.592 1.592 c.m/sec"			"	2.000 Overland Slope"				
"	Catchment 312 Pervious Impervious Total Area "			"	0.450 Pervious Area"				
"	Surface Area 1.100 3.300 4.400 hectare"			"	50.000 Pervious length"				
"	Time of concentration 28.527 4.929 8.813 minutes"			"	2.000 Pervious slope"				
"	Time to Centroid 255.889 206.801 214.881 minutes"			"	1.350 Impervious Area"				
"	Rainfall depth 86.100 86.100 86.100 mm"			"	50.000 Impervious length"				
"	Rainfall volume 947.10 2841.30 3788.40 c.m"			"	2.000 Impervious slope"				
"	Rainfall losses 38.560 5.681 13.901 mm"			"	0.200 Pervious Manning 'n'"				
"				"	82.000 Pervious SCS Curve No."				

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" 0.552 Pervious Runoff coefficient" " 1.200 0.900 0.500 0.000 0.000"
" 0.100 Pervious Ia/S coefficient" " 1.700 0.900 15.000 3.000 3.000"
" 5.576 Pervious Initial abstraction" " 1. ORIFICES"
" 0.013 Impervious Manning 'n'" " Orifice Orifice Orifice Number of"
" 98.000 Impervious SCS Curve No." " invert coefficient diameter orifices"
" 0.919 Impervious Runoff coefficient" " 0.000 0.630 0.2000 1.000"
" 0.100 Impervious Ia/S coefficient" " 2. LAYERS"
" 0.518 Impervious Initial abstraction" " Bottom Aspect Bottom Top Average"
" 0.299 0.232 2.306 c.m/sec" " area ratio elevation elevation sideslope"
" Catchment 313 Pervious Impervious Total Area " 5960.000 6.500 0.000 2.000 5.000"
" Surface Area 0.450 1.350 1.800 hectare" " 10902.110 4.312 2.000 2.000 4.000"
" Time of concentration 18.821 3.252 5.847 minutes" " Peak outflow 0.168 c.m/sec"
" Time to Centroid 244.145 204.723 211.295 minutes" " Maximum level 1.402 metre"
" Rainfall depth 86.100 86.100 86.100 mm" " Maximum storage 10679.215 c.m"
" Rainfall volume 387.45 1162.35 1549.80 c.m" " Centroidal lag 22.716 hours"
" Rainfall losses 38.606 6.972 14.881 mm" " 0.299 2.819 0.168 0.000 c.m/sec"
" Runoff depth 47.494 79.128 71.219 mm" " 40 HYDROGRAPH Next link "
" Runoff volume 213.73 1068.22 1281.95 c.m" " 5 Next link "
" Runoff coefficient 0.552 0.919 0.827 " " 0.299 0.168 0.168 0.000"
" Maximum flow 0.062 0.251 0.299 c.m/sec" " 52 CHANNEL DESIGN"
" 40 HYDROGRAPH Add Runoff " " 0.168 Current peak flow c.m/sec"
" 4 Add Runoff " " 0.299 0.532 0.232 2.306" " 0.040 Manning 'n'"
" 52 CHANNEL DESIGN" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 0.532 Current peak flow c.m/sec" " 2.000 Basewidth metre"
" 0.020 Manning 'n'" " 3.000 Left bank slope"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 3.000 Right bank slope"
" 4.000 Basewidth metre" " 5.000 Channel depth metre"
" 50.000 Left bank slope" " 1.000 Gradient %"
" 0.000 Right bank slope" " Depth of flow 0.126 metre"
" 0.300 Channel depth metre" " Velocity 0.563 m/sec"
" 2.000 Gradient %" " Channel capacity 394.351 c.m/sec"
" Depth of flow 0.081 metre" " Critical depth 0.086 metre"
" Velocity 1.086 m/sec" " 53 ROUTE Channel Route 300"
" Channel capacity 7.740 c.m/sec" " 300.00 Channel Route 300 Reach length (metre)"
" Critical depth 0.098 metre" " 0.476 X-factor <= 0.5"
" 53 ROUTE Channel Route 200" " 199.882 K-lag (seconds)"
" 200.00 Channel Route 200 Reach length (metre)" " 0.000 Default(0) or user spec.(1) values used"
" 0.495 X-factor <= 0.5" " 0.500 X-factor <= 0.5"
" 138.158 K-lag (seconds)" " 30.000 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used" " 0.500 Beta weighting factor"
" 0.500 X-factor <= 0.5" " 300.000 Routing time step (seconds)"
" 30.000 K-lag (seconds)" " 2 No. of sub-reaches"
" 0.500 Beta weighting factor" " Peak outflow 0.168 0.168 0.000 c.m/sec"
" 100.000 Routing time step (seconds)" " 40 HYDROGRAPH Combine 1100"
" 1 No. of sub-reaches" " 6 Combine "
" Peak outflow 0.521 0.521 2.306 c.m/sec" " 1100 Node #"
" 0.299 0.532 0.521 2.306 c.m/sec" " Node taking 200 series - Bottom end of Holtby Drain"
" 40 HYDROGRAPH Combine 7000" " Maximum flow 16.345 c.m/sec"
" 6 Combine " " Hydrograph volume 93803.180 c.m"
" 7000 Node #" " 0.299 0.168 0.168 16.345"
" Maximum flow 2.827 c.m/sec" " 81 ADD COMMENT=====
" Hydrograph volume 12331.485 c.m" " 1 Lines of comment"
" 0.299 0.532 0.521 2.827" " Total to Holtby Drain"
" 40 HYDROGRAPH Confluence 7000" " 40 HYDROGRAPH Confluence 1100"
" 7 Confluence " " 7 Confluence "
" 7000 Node #" " 1100 Node #"
" Maximum flow 2.827 c.m/sec" " Node taking 200 series - Bottom end of Holtby Drain"
" Hydrograph volume 12331.485 c.m" " Maximum flow 16.345 c.m/sec"
" 0.299 2.827 0.521 0.000" " Hydrograph volume 93803.172 c.m"
" 52 CHANNEL DESIGN" " 0.299 16.345 0.168 0.000"
" 2.827 Current peak flow c.m/sec" " 81 ADD COMMENT=====
" 0.040 Manning 'n'" " 1 Lines of comment"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 52 CHANNEL DESIGN"
" 2.000 Basewidth metre" " 16.345 Current peak flow c.m/sec"
" 3.000 Left bank slope" " 0.040 Manning 'n'"
" 3.000 Right bank slope" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 5.000 Channel depth metre" " 2.000 Basewidth metre"
" 2.000 Gradient %" " 3.000 Left bank slope"
" Depth of flow 0.484 metre" " 3.000 Right bank slope"
" Velocity 1.690 m/sec" " 5.000 Channel depth metre"
" Channel capacity 557.696 c.m/sec" " 0.500 Gradient %"
" Critical depth 0.464 metre" " Depth of flow 1.538 metre"
" 53 ROUTE Channel Route 50" " Velocity 1.608 m/sec"
" 50.00 Channel Route 50 Reach length (metre)" " Channel capacity 278.848 c.m/sec"
" 0.377 X-factor <= 0.5" " Critical depth 1.146 metre"
" 22.194 K-lag (seconds)" " 53 ROUTE Channel Route 200"
" 0.000 Default(0) or user spec.(1) values used" " 200.00 Channel Route 200 Reach length (metre)"
" 0.500 X-factor <= 0.5" " 0.162 X-factor <= 0.5"
" 30.000 K-lag (seconds)" " 93.308 K-lag (seconds)"
" 0.500 Beta weighting factor" " 0.000 Default(0) or user spec.(1) values used"
" 27.273 Routing time step (seconds)" " 0.500 X-factor <= 0.5"
" 1 No. of sub-reaches" " 30.000 K-lag (seconds)"
" Peak outflow 2.819 2.819 0.000 c.m/sec" " 0.500 Beta weighting factor"
" 40 HYDROGRAPH Next link " " 150.000 Routing time step (seconds)"
" 5 Next link " " 1 No. of sub-reaches"
" 0.299 2.819 2.819 0.000" " Peak outflow 16.201 16.201 0.000 c.m/sec"
" 81 ADD COMMENT===== " " 0.299 16.345 16.201 0.000 c.m/sec"
" 1 Lines of comment" " 40 HYDROGRAPH Combine 1300"
" PROPOSED POND #3" " 6 Combine "
" 54 POND DESIGN" " 1300 Node #"
" 2.819 Current peak flow c.m/sec" " Node at Holtby Drain"
" 2.000 Target outflow c.m/sec" " Maximum flow 20.879 c.m/sec"
" 12331.5 Hydrograph volume c.m" " Hydrograph volume 120136.023 c.m"
" 21. Number of stages" " 40 HYDROGRAPH Confluence 1300"
" 0.000 Minimum water level metre" " 7 Confluence "
" 2.000 Maximum water level metre" " 1300 Node #"
" 0.000 Starting water level metre" " Node at Holtby Drain"
" 0 Keep Design Data: 1 = True; 0 = False" " Maximum flow 20.879 c.m/sec"
" Level Discharge Volume" " Hydrograph volume 120136.008 c.m"
" 0.000 0.000 0.000" " 0.299 20.879 16.201 0.000"
" 0.1000 0.00487 607.388" " 52 CHANNEL DESIGN"
" 0.2000 0.01603 1237.688" " 20.879 Current peak flow c.m/sec"
" 0.3000 0.03579 1891.097" " 0.040 Manning 'n'"
" 0.4000 0.04527 2567.818" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 0.5000 0.05309 3268.049" " 2.000 Basewidth metre"
" 0.6000 0.05989 3991.990" " 3.000 Left bank slope"
" 0.7000 0.06599 4739.842" " 3.000 Right bank slope"
" 0.8000 0.07158 5511.804" " 5.000 Channel depth metre"
" 0.9000 0.07676 6308.077" " 0.500 Gradient %"
" 1.000 0.08161 7128.861" " Depth of flow 1.711 metre"
" 1.100 0.08619 7974.355" " Velocity 1.711 m/sec"
" 1.200 0.09054 8844.760" " Channel capacity 278.848 c.m/sec"
" 1.300 0.1190 9740.274" " Critical depth 1.289 metre"
" 1.400 0.1673 10661.10" " 53 ROUTE Channel Route 50"
" 1.500 0.2286 11607.44" " 50.00 Channel Route 50 Reach length (metre)"
" 1.600 0.3003 12579.48" " 0.000 X-factor <= 0.5"
" 1.700 0.3810 13577.44" " 21.922 K-lag (seconds)"
" 1.800 1.208 14601.51" " 0.000 Default(0) or user spec.(1) values used"
" 1.900 2.686 15651.89" " 0.500 X-factor <= 0.5"
" 2.000 4.619 16728.78" " 30.000 K-lag (seconds)"
" 2. WEIRS" " 0.788 Beta weighting factor"
" Crest Weir Crest Left Right" " 75.000 Routing time step (seconds)"
" elevation coefficient breadth sideslope sideslope" " 1 No. of sub-reaches"
" Peak outflow 20.843 c.m/sec"

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```

"      0.299 20.879 20.843 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1000"
" 6 Combine "
" 1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow 94.112 c.m/sec"
"      Hydrograph volume 825422.625 c.m"
" 81 0.299 20.879 20.843 94.112"
" ADD COMMENT=====
" 2 Lines of comment"
"      Total discharge to Pipe Arch under Hwy. 21 on the "
"      Pentangore Tributary"
" 40 HYDROGRAPH Confluence 1000"
" 7 Confluence "
" 1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow 94.112 c.m/sec"
"      Hydrograph volume 825422.625 c.m"
" 81 0.299 94.112 20.843 0.000"
" ADD COMMENT=====
" 2 Lines of comment"
"      Total discharge to Pipe Arch under Hwy. 21 on the "
"      Pentangore Tributary"
" 52 CHANNEL DESIGN"
" 94.112 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow 3.225 metre"
"      Velocity 2.499 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 2.577 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 15.004 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.929 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
"      Peak outflow 94.104 c.m/sec"
"      0.299 94.112 94.104 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
"      Node Combining All Flow"
"      Maximum flow 94.104 c.m/sec"
"      Hydrograph volume 825421.875 c.m"
" 81 0.299 94.112 94.104 94.104"
" ADD COMMENT=====
" 1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.299 0.000 94.104 94.104"
" 40 HYDROGRAPH Confluence 2000"
" 7 Confluence "
" 2000 Node #"
"      Flow in Hwy. 21 Ditch"
"      Maximum flow 3.546 c.m/sec"
"      Hydrograph volume 39391.148 c.m"
" 81 0.299 3.546 94.104 0.000"
" ADD COMMENT=====
" 1 Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
" 52 CHANNEL DESIGN"
" 3.546 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow 0.763 metre"
"      Velocity 1.083 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.525 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length ( metre)"
" 0.134 X-factor <= 0.5"
" 69.248 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
"      Peak outflow 3.530 c.m/sec"
"      0.299 3.546 3.530 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
"      Node Combining All Flow"
"      Maximum flow 97.161 c.m/sec"
"      Hydrograph volume 864808.313 c.m"
" 40 0.299 3.546 3.530 97.161"
" HYDROGRAPH Confluence 3000"
" 7 Confluence "
" 3000 Node #"
"      Node Combining All Flow"
"      Maximum flow 97.161 c.m/sec"
"      Hydrograph volume 864808.250 c.m"
" 81 0.299 97.161 3.530 0.000"
" ADD COMMENT=====
" 1 Lines of comment"
"      Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 52 CHANNEL DESIGN"
" 97.161 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
"      Depth of flow 3.267 metre"
"      Velocity 2.519 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 2.614 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 14.884 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.932 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
"      Peak outflow 97.160 c.m/sec"
"      0.299 97.161 97.160 0.000 c.m/sec"
" 38 START/RE-START TOTALS 3000"
" 1 Runoff Totals turned OFF"
"      Catchment area to node 3000 1918.200 hectare"
"      Impervious area to node 3000 40.592 hectare"
"      % impervious to node 3000 0.000"
"      Peak runoff to node 3000 0.000 c.m/sec"
"      Total volume to node 3000 0.0 c.m"
" 38 START/RE-START TOTALS 3000"
" 1 Runoff Totals turned ON"
"      Catchment area to node 3000 1918.200 hectare"
"      Impervious area to node 3000 40.592 hectare"
"      % impervious to node 3000 2.116"
"      Peak runoff to node 3000 149.139 c.m/sec"
"      Total volume to node 3000 876072.6 c.m"

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POST DEVELOPMENT 100 YEAR

MIDUSS Output ----->
MIDUSS version Version 2.25 rev. 473
MIDUSS created Sunday, February 7, 2010
10 Units used: ie METRIC
Job folder: C:\Users\derb\Desktop\KBP - Report\ 40
Output filename: 2016 Work\Appendix F - Miduss Modelling
Licensee name: 08055 - Post 100 Year.out
Company BMROSS - DLE 52
Date & Time last used: 6/25/2016 at 9:35:43 AM
31 TIME PARAMETERS
5.000 Time Step
360.000 Max. Storm length
1800.000 Max. Hydrograph
32 STORM Mass Curve
3 Mass Curve
108.800 Rainfall depth
360.000 Duration
47 C:\Program Files (x86)\MIDUSS\SCS_6hr_Type2.mrd SCS Type II - 6
hour Distribution - Ontario
Maximum intensity 84.864 mm/hr
Total depth 108.800 mm
6 100% Hydrograph extension used in this file
81 ADD COMMENT-----
1 Lines of comment
Start of Penetangore Tributary
33 CATCHMENT 50
1 Triangular SCS
1 Equal length
1 SCS method
50 No description
0.000 % Impervious
396.000 Total Area
450.000 Flow length
2.500 Overland Slope
396.000 Pervious Area
450.000 Pervious length
2.500 Pervious slope
0.000 Impervious Area
450.000 Impervious length
2.500 Impervious slope
0.250 Pervious Manning 'n'
81.000 Pervious SCS Curve No."
0.598 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.958 Pervious Initial abstraction"
0.013 Impervious Manning 'n'
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
37.770 0.000 0.000 0.000 c.m/sec"
Catchment 50 Pervious Impervious Total Area "
Surface Area 396.000 0.000 396.000 hectare"
Time of concentration 66.924 10.341 66.924 minutes"
Time to Centroid 300.389 212.009 300.389 minutes"
Rainfall depth 108.800 108.800 108.800 mm
Rainfall volume 43.0948 0.0000 43.0948 ha-m"
Rainfall losses 43.692 5.981 43.692 mm
Runoff depth 65.108 102.819 65.108 mm
Runoff volume 25.7828 0.0000 25.7828 ha-m"
Runoff coefficient 0.598 0.000 0.598 "
Maximum flow 37.770 0.000 37.770 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 37.770 37.770 0.000 0.000"
52 CHANNEL DESIGN"
37.770 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
Depth of flow 2.206 metre"
Velocity 1.987 m/sec"
Channel capacity 278.848 c.m/sec"
Critical depth 1.704 metre"
53 ROUTE Channel Route 3000"
3000.00 Channel Route 3000 Reach length (metre)"
0.376 X-factor <= 0.5"
283.088 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
4 No. of sub-reaches"
Peak outflow 37.770 37.770 37.185 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 37.770 37.185 37.185 0.000"
33 CATCHMENT 52
1 Triangular SCS
1 Equal length"
1 SCS method"
52 No description"
0.000 % Impervious"
196.000 Total Area"
250.000 Flow length"
7.000 Overland Slope"
196.000 Pervious Area"
250.000 Pervious length"
7.000 Pervious slope"
0.000 Impervious Area"
250.000 Impervious length"
7.000 Impervious slope"
0.250 Pervious Manning 'n'"
80.000 Pervious SCS Curve No."
0.581 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
6.350 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
28.020 37.185 37.185 0.000 c.m/sec"
Catchment 52 Pervious Impervious Total Area "
Surface Area 196.000 0.000 196.000 hectare"
Time of concentration 34.824 5.336 34.824 minutes"
Time to Centroid 262.294 206.023 262.293 minutes"
Rainfall depth 108.800 108.800 108.800 mm"
Rainfall volume 21.3248 0.0000 21.3248 ha-m"
Rainfall losses 45.592 5.703 45.592 mm"
Runoff depth 63.208 103.097 63.208 mm"
Runoff volume 12.3888 0.0000 12.3888 ha-m"
Runoff coefficient 0.581 0.000 0.581 "
Maximum flow 28.020 0.000 28.020 c.m/sec"
HYDROGRAPH Add Runoff "
4 Add Runoff " 28.020 46.374 37.185 0.000"
52 CHANNEL DESIGN"
46.374 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.400 Gradient %"
Depth of flow 2.520 metre"
Velocity 1.925 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 1.872 metre"
53 ROUTE Channel Route 1300"
1300.00 Channel Route 1300 Reach length (metre)"
0.297 X-factor <= 0.5"
253.279 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
2 No. of sub-reaches"
Peak outflow 46.162 46.162 c.m/sec"
28.020 46.374 46.162 0.000 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 28.020 46.162 46.162 0.000"
33 CATCHMENT 54
1 Triangular SCS
1 Equal length"
1 SCS method"
54 No description"
0.000 % Impervious"
39.000 Total Area"
140.000 Flow length"
11.000 Overland Slope"
39.000 Pervious Area"
140.000 Pervious length"
11.000 Pervious slope"
0.000 Impervious Area"
140.000 Impervious length"
11.000 Impervious slope"
0.210 Pervious Manning 'n'"
81.000 Pervious SCS Curve No."
0.597 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.958 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
7.223 46.162 46.162 0.000 c.m/sec"
Catchment 54 Pervious Impervious Total Area "
Surface Area 39.000 0.000 39.000 hectare"
Time of concentration 19.181 3.291 19.181 minutes"
Time to Centroid 242.650 203.605 242.650 minutes"
Rainfall depth 108.800 108.800 108.800 mm"
Rainfall volume 4.2432 0.0000 4.2432 ha-m"
Rainfall losses 43.802 7.543 43.802 mm"
Runoff depth 64.998 101.257 64.998 mm"
Runoff volume 2.5349 0.0000 2.5349 ha-m"
Runoff coefficient 0.597 0.000 0.597 "
Maximum flow 7.223 0.000 7.223 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 7.223 47.717 46.162 0.000"
52 CHANNEL DESIGN"
47.717 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.400 Gradient %"
Depth of flow 2.550 metre"
Velocity 1.939 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 1.897 metre"
53 ROUTE Channel Route 800"
800.00 Channel Route 800 Reach length (metre)"
0.334 X-factor <= 0.5"
309.499 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 47.596 47.596 c.m/sec"
7.223 47.717 47.596 0.000 c.m/sec"
40 HYDROGRAPH Combine 10"
6 Combine "
10 Node #"
Confluence on Penetangore Tributary"
Maximum flow 47.596 c.m/sec"
Hydrograph volume 407065.875 c.m"
7.223 47.717 47.596 47.596"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
7.223 0.000 47.596 47.596"
33 CATCHMENT 60
1 Triangular SCS"
1 Equal length"
1 SCS method"
60 No description"
0.000 % Impervious"
225.000 Total Area"
270.000 Flow length"
2.500 Overland Slope"
225.000 Pervious Area"
270.000 Pervious length"
2.500 Pervious slope"
0.000 Impervious Area"

270.000 Impervious length" " Catchment 62 Pervious Impervious Total Area "
2.500 Impervious slope" " Surface Area 95.000 0.000 95.000 hectare"
0.230 Pervious Manning 'n'" " Time of concentration 36.285 5.560 36.285 minutes"
81.000 Pervious SCS Curve No." " Time to Centroid 264.065 206.307 264.065 minutes"
0.598 Pervious Runoff coefficient" " Rainfall depth 108.800 108.800 108.800 mm"
0.100 Pervious Ia/S coefficient" " Rainfall volume 10.3360 0.0000 10.3360 ha-m"
5.958 Pervious Initial abstraction" " Rainfall losses 45.578 5.794 45.578 mm"
0.013 Impervious Manning 'n'" " Runoff depth 63.222 103.006 63.222 mm"
98.000 Pervious SCS Curve No." " Runoff volume 6.0061 0.0000 6.0061 ha-m"
0.000 Impervious Runoff coefficient" " Runoff coefficient 0.581 0.000 0.581 "
0.100 Impervious Ia/S coefficient" " Maximum flow 13.275 0.000 13.275 c.m/sec"
0.518 Impervious Initial abstraction" " HYDROGRAPH Add Runoff "
27.615 0.000 47.596 47.596 c.m/sec" 40 4 Add Runoff "
Catchment 60 Pervious Impervious Total Area " 13.275 13.275 71.140 71.140"
Surface Area 225.000 0.000 225.000 hectare" 52 CHANNEL DESIGN"
Time of concentration 46.854 7.611 46.854 minutes" 13.275 Current peak flow c.m/sec"
Time to Centroid 276.114 208.803 276.113 minutes" 0.040 Manning 'n'"
Rainfall depth 108.800 108.800 108.800 mm" 0. Cross-section type: 0=trapezoidal; 1=general"
Rainfall volume 24.4800 0.0000 24.4800 ha-m" 2.000 Basewidth metre"
Rainfall losses 43.706 5.897 43.706 mm" 3.000 Left bank slope"
Runoff depth 65.094 102.903 65.094 mm" 3.000 Right bank slope"
Runoff volume 14.6461 0.0000 14.6461 ha-m" 5.000 Channel depth metre"
Runoff coefficient 0.598 0.000 0.598 " 0.300 Gradient %"
Maximum flow 27.615 0.000 27.615 c.m/sec" Depth of flow 1.570 metre"
HYDROGRAPH Add Runoff " Velocity 1.260 m/sec"
4 Add Runoff " Channel capacity 215.995 c.m/sec"
27.615 27.615 47.596 47.596" Critical depth 1.035 metre"
CHANNEL DESIGN" 53 ROUTE Channel Route 1800"
27.615 Current peak flow c.m/sec" 1800.00 Channel Route 1800 Reach length (metre)"
0.040 Manning 'n'" 0.309 X-factor <= 0.5"
0. Cross-section type: 0=trapezoidal; 1=general" 357.055 K-lag (seconds)"
2.000 Basewidth metre" 0.000 Default(0) or user spec.(1) values used"
3.000 Left bank slope" 0.500 X-factor <= 0.5"
3.000 Right bank slope" 30.000 K-lag (seconds)"
5.000 Channel depth metre" 0.500 Beta weighting factor"
0.400 Gradient %" 300.000 Routing time step (seconds)"
3 No. of sub-reaches"
Depth of flow 2.025 metre" Peak outflow 12.594 c.m/sec"
Velocity 1.689 m/sec" 13.275 13.275 12.594 71.140 c.m/sec"
Channel capacity 249.409 c.m/sec" 40 HYDROGRAPH Combine 11"
Critical depth 1.472 metre" 6 Combine "
ROUTE Channel Route 1800" 11 Node #"
1800.00 Channel Route 1800 Reach length (metre)" Confluence on Penatangore Tributary"
0.320 X-factor <= 0.5" Maximum flow 80.574 c.m/sec"
266.406 K-lag (seconds)" Hydrograph volume 613588.125 c.m"
0.000 Default(0) or user spec.(1) values used" 13.275 13.275 12.594 80.574"
0.500 X-factor <= 0.5" 40 HYDROGRAPH Start - New Tributary"
30.000 K-lag (seconds)" 2 Start - New Tributary"
0.500 Beta weighting factor" 13.275 0.000 12.594 80.574"
300.000 Routing time step (seconds)" 3 No. of sub-reaches"
3 No. of sub-reaches" Peak outflow 27.176 c.m/sec"
27.615 27.615 27.176 47.596 c.m/sec" 33 CATCHMENT 56"
HYDROGRAPH Combine 10" 1 Triangular SCS"
6 Combine " 1 Equal length"
10 Node #" 1 SCS method"
Confluence on Penatangore Tributary" 56 No description"
Maximum flow 71.637 c.m/sec" 0.000 % Impervious"
Hydrograph volume 553527.000 c.m" 345.000 Total Area"
27.615 27.615 27.176 71.637" 240.000 Flow length"
40 HYDROGRAPH Confluence 10" 11.000 Overland Slope"
7 Confluence " 345.000 Pervious Area"
10 Node #" 240.000 Pervious length"
Confluence on Penatangore Tributary" 11.000 Impervious Area"
Maximum flow 71.637 c.m/sec" 240.000 Impervious length"
Hydrograph volume 553527.000 c.m" 15.000 Impervious slope"
27.615 71.637 27.176 0.000" 0.280 Pervious Manning 'n'"
52 CHANNEL DESIGN" 79.000 Pervious SCS Curve No."
71.637 Current peak flow c.m/sec" 0.564 Pervious Runoff coefficient"
0.040 Manning 'n'" 0.100 Pervious Ia/S coefficient"
0. Cross-section type: 0=trapezoidal; 1=general" 6.752 Pervious Initial abstraction"
2.000 Basewidth metre" 0.013 Impervious Manning 'n'"
3.000 Left bank slope" 98.000 Impervious SCS Curve No."
3.000 Right bank slope" 0.000 Impervious Runoff coefficient"
5.000 Channel depth metre" 0.100 Impervious Ia/S coefficient"
0.400 Gradient %" 0.518 Impervious Initial abstraction"
Depth of flow 3.018 metre" 49.743 0.000 12.594 80.574 c.m/sec"
Velocity 2.147 m/sec" Catchment 56 Pervious Impervious Total Area "
Channel capacity 249.409 c.m/sec" Surface Area 345.000 0.000 345.000 hectare"
Critical depth 2.281 metre" Time of concentration 32.032 4.143 32.032 minutes"
53 ROUTE Channel Route 2000" 259.645 204.458 259.645 minutes"
2000.00 Channel Route 2000 Reach length (metre)" Rainfall depth 108.800 108.800 108.800 mm"
0.345 X-factor <= 0.5" Rainfall volume 37.5360 0.0000 37.5360 ha-m"
349.343 K-lag (seconds)" Rainfall losses 47.417 7.379 47.417 mm"
0.000 Default(0) or user spec.(1) values used" Runoff depth 61.383 101.421 61.383 mm"
0.500 X-factor <= 0.5" Runoff volume 21.1772 0.0000 21.1772 ha-m"
30.000 K-lag (seconds)" Runoff coefficient 0.564 0.000 0.564 "
0.500 Beta weighting factor" Maximum flow 49.743 0.000 49.743 c.m/sec"
300.000 Routing time step (seconds)" 40 HYDROGRAPH Add Runoff "
2 No. of sub-reaches" 4 Add Runoff "
Peak outflow 71.140 c.m/sec" 49.743 49.743 12.594 80.574"
27.615 71.637 71.140 0.000 c.m/sec" 52 CHANNEL DESIGN"
HYDROGRAPH Combine 11" 49.743 Current peak flow c.m/sec"
6 Combine " 0.040 Manning 'n'"
11 Node #" 0. Cross-section type: 0=trapezoidal; 1=general"
Confluence on Penatangore Tributary" 2.000 Basewidth metre"
Maximum flow 71.140 c.m/sec" 3.000 Left bank slope"
Hydrograph volume 553527.188 c.m" 3.000 Right bank slope"
27.615 71.637 71.140 71.140" 5.000 Channel depth metre"
40 HYDROGRAPH Start - New Tributary" 0.400 Gradient %"
2 Start - New Tributary" Depth of flow 2.595 metre"
27.615 0.000 71.140 71.140" Velocity 1.959 m/sec"
Channel capacity 249.409 c.m/sec"
Critical depth 1.933 metre"
33 CATCHMENT 62" ROUTE Channel Route 1300"
1 Triangular SCS" 1300.00 Channel Route 1300 Reach length (metre)"
1 Equal length" 0.292 X-factor <= 0.5"
1 SCS method" 248.853 K-lag (seconds)"
62 No description" 0.000 Default(0) or user spec.(1) values used"
0.000 % Impervious" 0.500 X-factor <= 0.5"
95.000 Total Area" 30.000 K-lag (seconds)"
160.000 Flow length" 0.500 Beta weighting factor"
2.500 Overland Slope" 300.000 Routing time step (seconds)"
95.000 Pervious Area" 2 No. of sub-reaches"
160.000 Pervious length" Peak outflow 49.013 c.m/sec"
2.500 Pervious slope" 49.743 49.743 49.013 80.574 c.m/sec"
0.000 Impervious Area" 40 HYDROGRAPH Combine 11"
160.000 Impervious length" 6 Combine "
160.000 Impervious slope" 11 Node #"
2.500 Impervious slope" Confluence on Penatangore Tributary"
0.250 Pervious Manning 'n'" Maximum flow 111.465 c.m/sec"
80.000 Pervious SCS Curve No." Hydrograph volume 825360.125 c.m"
0.581 Pervious Runoff coefficient" 49.743 49.743 49.013 111.465"
0.100 Pervious Ia/S coefficient" 40 HYDROGRAPH Confluence 11"
6.350 Pervious Initial abstraction" 7 Confluence "
0.013 Impervious Manning 'n'" 11 Node #"
98.000 Impervious SCS Curve No." Confluence on Penatangore Tributary"
0.000 Impervious Runoff coefficient" Maximum flow 111.465 c.m/sec"
0.100 Impervious Ia/S coefficient" Hydrograph volume 825360.125 c.m"
0.518 Impervious Initial abstraction" 13.275 0.000 71.140 71.140 c.m/sec"


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"      Time to Centroid      254.845      203.515      254.845      minutes"
"      Rainfall depth        108.800      108.800      108.800      mm"
"      Rainfall volume       13.9264      0.0000      13.9264      ha-m"
"      Rainfall losses       52.712      7.437      52.712      mm"
"      Runoff depth          56.088      101.363      56.088      mm"
"      Runoff volume         7.1792      0.0000      7.1792      ha-m"
"      Runoff coefficient    0.516      0.000      0.516      "
"      Maximum flow         18.574      0.000      18.574      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      18.574      18.574      118.722      118.722"
" 52  CHANNEL DESIGN"
" 18.574 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.300 Gradient %"
"      Depth of flow          1.817      metre"
"      Velocity              1.372      m/sec"
"      Channel capacity      215.995      c.m/sec"
"      Critical depth        1.219      metre"
" 53  ROUTE Channel Route 1500"
" 1500.00 Channel Route 1500 Reach length ( metre)"
" 0.326 X-factor <= 0.5"
" 409.886 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
"      Peak outflow          17.439      c.m/sec"
"      18.574      18.574      17.439      118.722 c.m/sec"
" 40  HYDROGRAPH Combine 1000"
" 6 Combine "
" 1000 Node #"
"      Node upstream of Penetangore Culvert"
"      Maximum flow         125.579      c.m/sec"
"      Hydrograph volume    1004030.56      c.m"
"      18.574      18.574      17.439      125.579"
" 81  ADD COMMENT"
" 1 Lines of comment"
" End of Penetangore Tributary"
" 81  ADD COMMENT"
" 1 Lines of comment"
" Start of Area North of Holtby Drain"
" 40  HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
"      18.574      0.000      17.439      125.579"
" 33  CATCHMENT 201"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 201 No description"
" 0.000 % Impervious"
" 166.000 Total Area"
" 250.000 Flow length"
" 3.000 Overland Slope"
" 166.000 Pervious Area"
" 250.000 Pervious length"
" 3.000 Pervious slope"
" 0.000 Impervious Area"
" 250.000 Impervious length"
" 3.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
"      23.743      0.000      17.439      125.579 c.m/sec"
"      Catchment 201 Pervious Impervious Total Area "
"      Surface Area 166.000 0.000 166.000 hectare"
"      Time of concentration 38.638 6.881 38.638 minutes"
"      Time to Centroid 265.432 207.930 265.432 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 18.0608 0.0000 18.0608 ha-m"
"      Rainfall losses 41.801 6.917 41.801 mm"
"      Runoff depth 66.999 101.883 66.999 mm"
"      Runoff volume 11.1219 0.0000 11.1219 ha-m"
"      Runoff coefficient 0.616 0.000 0.616 "
"      Maximum flow 23.743 0.000 23.743 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      23.743      23.743      17.439      125.579"
" 52  CHANNEL DESIGN"
" 23.743 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
"      Depth of flow          1.556      metre"
"      Velocity              2.289      m/sec"
"      Channel capacity      394.351      c.m/sec"
"      Critical depth        1.370      metre"
" 53  ROUTE Channel Route 1900"
" 1900.00 Channel Route 1900 Reach length ( metre)"
" 0.464 X-factor <= 0.5"
" 311.272 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
"      Peak outflow          23.609      c.m/sec"
"      23.743      23.743      23.609      125.579 c.m/sec"
" 40  HYDROGRAPH Next link "
" 5 Next link "
"      23.743      23.609      23.609      125.579"
" 33  CATCHMENT 202"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 202 No description"
" 0.000 % Impervious"
" 4.000 Total Area"
"      Catchment 202 Pervious Impervious Total Area "
"      Surface Area 9.100 0.000 9.100 hectare"
"      Time of concentration 52.492 9.348 52.492 minutes"
"      Time to Centroid 282.188 210.834 282.187 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 9900.79 0.01 9900.80 c.m"
"      Rainfall losses 41.791 5.994 41.791 mm"
"      Runoff depth 67.009 102.806 67.009 mm"
"      Runoff volume 6097.79 0.01 6097.80 c.m"
"      Runoff coefficient 0.616 0.000 0.616 "
"      Maximum flow 1.072 0.000 1.072 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      1.072      24.991      23.934      125.579"
" 52  CHANNEL DESIGN"
" 24.991 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 1.000 Gradient %"
"      Depth of flow          1.591      metre"
"      Velocity              2.319      m/sec"
"      Channel capacity      394.351      c.m/sec"
"      Critical depth        1.404      metre"
" 53  ROUTE Channel Route 350"
" 350.00 Channel Route 350 Reach length ( metre)"
" 0.401 X-factor <= 0.5"
" 113.196 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
"      Peak outflow          24.977      c.m/sec"
"      1.072      24.991      24.977      125.579 c.m/sec"
" 40  HYDROGRAPH Combine 1100"

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"      6 Combine "
1100 Node #
"      Node taking 200 series - Bottom end of Holtby Drain"
"      Maximum flow      24.977 c.m/sec"
"      Hydrograph volume 119996.328 c.m"
"      1.072 24.991 24.977 24.977"
81 ADD COMMENT-----"
1 Lines of comment"
"      End of Area North of Holtby Drain"
"      HYDROGRAPH Start - New Tributary"
40 2 Start - New Tributary"
"      1.072 0.000 24.977 24.977"
81 ADD COMMENT-----"
1 Lines of comment"
"      Start of Holtby Drain"
33 CATCHMENT 100"
1 Triangular SCS"
1 Equal length"
1 SCS method"
100 No description"
0.000 % Impervious"
45.000 Total Area"
100.000 Flow length"
7.000 Overland Slope"
45.000 Pervious Area"
100.000 Pervious length"
7.000 Pervious slope"
0.000 Impervious Area"
100.000 Impervious length"
7.000 Impervious slope"
0.200 Pervious Manning 'n'"
82.000 Pervious SCS Curve No."
0.615 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.576 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
"      8.520 0.000 24.977 24.977 c.m/sec"
"      Catchment 100 Pervious Impervious Total Area "
"      Surface Area 45.000 0.000 45.000 hectare"
"      Time of concentration 17.293 3.080 17.293 minutes"
"      Time to Centroid 239.597 203.358 239.597 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 4.8960 0.0000 4.8960 ha-m"
"      Rainfall losses 41.868 7.350 41.868 mm"
"      Runoff depth 66.932 101.450 66.932 mm"
"      Runoff volume 3.0119 0.0000 3.0120 ha-m"
"      Runoff coefficient 0.615 0.000 0.615 "
"      Maximum flow 8.520 0.000 8.520 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
"      8.520 8.520 24.977 24.977"
52 CHANNEL DESIGN"
8.520 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.000 Gradient %"
"      Depth of flow 0.980 metre"
"      Velocity 1.760 m/sec"
"      Channel capacity 394.351 c.m/sec"
"      Critical depth 0.830 metre"
53 ROUTE Channel Route 1500"
1500.00 Channel Route 1500 Reach length ( metre)"
0.455 X-factor <= 0.5"
213.100 K-lag ( seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
3 No. of sub-reaches"
"      Peak outflow 8.520 8.520 8.436 24.977 c.m/sec"
"      HYDROGRAPH Next link "
40 5 Next link "
"      8.520 8.436 8.436 24.977"
33 CATCHMENT 101"
1 Triangular SCS"
1 Equal length"
1 SCS method"
101 No description"
0.000 % Impervious"
11.200 Total Area"
50.000 Flow length"
7.000 Overland Slope"
11.200 Pervious Area"
50.000 Pervious length"
7.000 Pervious slope"
0.000 Impervious Area"
50.000 Impervious length"
7.000 Impervious slope"
0.280 Pervious Manning 'n'"
80.000 Pervious SCS Curve No."
0.580 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
6.350 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
"      0.458 0.000 9.795 9.795 c.m/sec"
"      Catchment 101 Pervious Impervious Total Area "
"      Surface Area 11.200 0.000 11.200 hectare"
"      Time of concentration 14.191 2.032 14.191 minutes"
"      Time to Centroid 237.365 202.020 237.365 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 1.2186 0.0000 1.2186 ha-m"
"      Rainfall losses 45.642 6.687 45.642 mm"
"      Runoff depth 63.158 102.113 63.158 mm"
"      Runoff volume 7073.64 0.01 7073.65 c.m"
"      Runoff coefficient 0.580 0.000 0.580 "
"      Maximum flow 2.047 0.000 2.047 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
"      2.047 9.854 8.436 24.977"
52 CHANNEL DESIGN"
9.854 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      2.000 Gradient %"
"      Depth of flow 0.182 metre"
"      Velocity 0.986 m/sec"
"      Channel capacity 557.696 c.m/sec"
"      Critical depth 0.161 metre"
53 ROUTE Channel Route 250"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.000 Gradient %"
"      Depth of flow 1.048 metre"
"      Velocity 1.827 m/sec"
"      Channel capacity 394.351 c.m/sec"
"      Critical depth 0.893 metre"
53 ROUTE Channel Route 700"
700.00 Channel Route 700 Reach length ( metre)"
0.466 X-factor <= 0.5"
287.304 K-lag ( seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.500 Beta weighting factor"
300.000 Routing time step ( seconds)"
1 No. of sub-reaches"
"      Peak outflow 2.047 9.854 9.826 24.977 c.m/sec"
"      HYDROGRAPH Combine 1200"
6 Combine "
1200 Node #
"      Node taking 100 series for Holtby Drain"
"      Maximum flow 9.826 c.m/sec"
"      Hydrograph volume 37193.148 c.m"
"      2.047 9.854 9.826 9.826"
81 ADD COMMENT-----"
1 Lines of comment"
"      End of Holtby Drain"
40 HYDROGRAPH Confluence 1200"
7 Confluence "
1200 Node #
"      Node taking 100 series for Holtby Drain"
"      Maximum flow 9.826 c.m/sec"
"      Hydrograph volume 37193.148 c.m"
"      2.047 9.826 9.826 0.000"
52 CHANNEL DESIGN"
9.826 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
0.500 Gradient %"
"      Depth of flow 1.226 metre"
"      Velocity 1.412 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.891 metre"
53 ROUTE Channel Route 50"
50.00 Channel Route 50 Reach length ( metre)"
0.000 X-factor <= 0.5"
26.564 K-lag ( seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag ( seconds)"
0.715 Beta weighting factor"
75.000 Routing time step ( seconds)"
1 No. of sub-reaches"
"      Peak outflow 2.047 9.826 9.795 0.000 c.m/sec"
"      HYDROGRAPH Combine 1300"
40 6 Combine " Combine 1300"
1300 Node #
"      Node at Holtby Drain"
"      Maximum flow 9.795 c.m/sec"
"      Hydrograph volume 37193.152 c.m"
"      2.047 9.826 9.795 9.795"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
"      2.047 0.000 9.795 9.795"
33 CATCHMENT 604"
1 Triangular SCS"
1 Equal length"
1 SCS method"
604 No description"
0.000 % Impervious"
2.700 Total Area"
100.000 Flow length"
2.500 Overland Slope"
2.700 Pervious Area"
100.000 Pervious length"
2.500 Pervious slope"
0.000 Impervious Area"
100.000 Impervious length"
2.500 Impervious slope"
0.300 Pervious Manning 'n'"
83.000 Pervious SCS Curve No."
0.634 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.202 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
"      0.458 0.000 9.795 9.795 c.m/sec"
"      Catchment 604 Pervious Impervious Total Area "
"      Surface Area 2.700 0.000 2.700 hectare"
"      Time of concentration 29.804 4.194 29.804 minutes"
"      Time to Centroid 253.973 204.572 253.973 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 2937.60 0.00 2937.60 c.m"
"      Rainfall losses 39.869 7.255 39.869 mm"
"      Runoff depth 68.931 101.545 68.931 mm"
"      Runoff volume 1861.15 0.00 1861.15 c.m"
"      Runoff coefficient 0.634 0.000 0.634 "
"      Maximum flow 0.458 0.000 0.458 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff "
"      0.458 0.458 9.795 9.795"
52 CHANNEL DESIGN"
0.458 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
2.000 Gradient %"
"      Depth of flow 0.182 metre"
"      Velocity 0.986 m/sec"
"      Channel capacity 557.696 c.m/sec"
"      Critical depth 0.161 metre"
53 ROUTE Channel Route 250"

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" 250.00 Channel Route 250 Reach length ( metre) "
" 0.490 X-factor <= 0.5"
" 190.146 K-lag ( seconds)"
" 0.000 Default (0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.453 0.453 0.453 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.458 0.458 0.453 9.795 c.m/sec"
" 33 CATCHMENT 605"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 605 No description"
" 0.000 % Impervious"
" 3.900 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 3.900 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.634 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.662 0.453 0.453 9.795 c.m/sec"
" Catchment 605 Pervious Impervious Total Area "
" Surface Area 3.900 0.000 3.900 hectare"
" Time of concentration 29.804 4.194 29.804 minutes"
" Time to Centroid 253.973 204.572 253.973 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 4243.20 0.00 4243.20 c.m"
" Rainfall losses 39.869 7.255 39.869 mm"
" Runoff depth 68.931 101.545 68.931 mm"
" Runoff volume 2688.32 0.00 2688.33 c.m"
" Runoff coefficient 0.634 0.000 0.634 "
" Maximum flow 0.662 0.000 0.662 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.662 1.107 0.453 9.795"
" 52 CHANNEL DESIGN"
" 1.107 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.296 metre"
" Velocity 1.293 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.273 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length ( metre)"
" 0.480 X-factor <= 0.5"
" 116.054 K-lag ( seconds)"
" 0.000 Default (0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.662 1.107 1.099 9.795 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 1.099 c.m/sec"
" Hydrograph volume 4549.473 c.m"
" 0.662 1.107 1.099 1.099"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.662 0.000 1.099 1.099"
" 33 CATCHMENT 603"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 603 No description"
" 0.000 % Impervious"
" 5.600 Total Area"
" 100.000 Flow length"
" 2.500 Overland Slope"
" 5.600 Pervious Area"
" 100.000 Pervious length"
" 2.500 Pervious slope"
" 0.000 Impervious Area"
" 100.000 Impervious length"
" 2.500 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.634 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.000 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.950 0.000 1.099 1.099 c.m/sec"
" Catchment 603 Pervious Impervious Total Area "
" Surface Area 5.600 0.000 5.600 hectare"
" Time of concentration 29.804 4.194 29.804 minutes"
" Time to Centroid 253.973 204.572 253.973 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 6092.79 0.01 6092.80 c.m"
" Rainfall losses 39.869 7.255 39.869 mm"
" Runoff depth 68.931 101.545 68.931 mm"
" Runoff volume 3860.15 0.01 3860.16 c.m"
" Runoff coefficient 0.634 0.000 0.634 "
" Maximum flow 0.950 0.000 0.950 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.659 0.659 2.026 2.026"
" 52 CHANNEL DESIGN"
" 0.659 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.091 metre"
" Velocity 1.155 m/sec"
" 4 Add Runoff "
" 0.950 0.950 1.099 1.099"
" 52 CHANNEL DESIGN"
" 0.950 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.273 metre"
" Velocity 1.235 m/sec"
" Channel capacity 557.696 c.m/sec"
" Critical depth 0.249 metre"
" 53 ROUTE Channel Route 225"
" 225.00 Channel Route 225 Reach length ( metre)"
" 0.484 X-factor <= 0.5"
" 136.640 K-lag ( seconds)"
" 0.000 Default (0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.934 0.950 0.934 c.m/sec"
" 40 HYDROGRAPH Combine 4000"
" 6 Combine "
" 4000 Node #"
" Maximum flow 2.033 c.m/sec"
" Hydrograph volume 8409.629 c.m"
" 0.950 0.950 0.934 2.033"
" 40 HYDROGRAPH Confluence 4000"
" 7 Confluence "
" 4000 Node #"
" Maximum flow 2.033 c.m/sec"
" Hydrograph volume 8409.629 c.m"
" 0.950 2.033 0.934 0.000"
" 52 CHANNEL DESIGN"
" 2.033 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.582 metre"
" Velocity 0.933 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.386 metre"
" 53 ROUTE Channel Route 500"
" 500.00 Channel Route 500 Reach length ( metre)"
" 0.384 X-factor <= 0.5"
" 200.907 K-lag ( seconds)"
" 0.000 Default (0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 300.000 Routing time step ( seconds)"
" 2 No. of sub-reaches"
" Peak outflow 2.026 0.950 2.026 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 2.026 c.m/sec"
" Hydrograph volume 8409.625 c.m"
" 0.950 2.033 2.026 2.026"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.950 0.000 2.026 2.026"
" 33 CATCHMENT 405"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 405 No description"
" 75.000 % Impervious"
" 3.200 Total Area"
" 75.000 Flow length"
" 2.000 Overland Slope"
" 0.800 Pervious Area"
" 75.000 Pervious length"
" 2.000 Pervious slope"
" 2.400 Impervious Area"
" 75.000 Impervious length"
" 2.000 Impervious slope"
" 0.300 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.633 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.926 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.659 0.000 2.026 2.026 c.m/sec"
" Catchment 405 Pervious Impervious Total Area "
" Surface Area 0.800 2.400 3.200 hectare"
" Time of concentration 26.815 3.773 8.050 minutes"
" Time to Centroid 250.348 203.918 212.537 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 870.40 2611.20 3481.60 c.m"
" Rainfall losses 39.886 8.015 15.983 mm"
" Runoff depth 68.914 100.785 92.817 mm"
" Runoff volume 551.31 2418.84 2970.15 c.m"
" Runoff coefficient 0.633 0.926 0.853 "
" Maximum flow 0.142 0.562 0.659 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.659 0.659 2.026 2.026"

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" Hydrograph volume 9484.756 c.m"
" 1.207 2.116 1.195 0.000"
" 52 CHANNEL DESIGN"
" 2.116 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.164 metre"
" Velocity 1.597 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.205 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.460 X-factor <= 0.5"
" 23.488 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 25.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.110 c.m/sec"
" 1.207 2.116 2.110 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 1.207 2.110 2.110 0.000"
" 81 ADD COMMENT"
" 1 Lines of comment"
" EXISTING POND - DRY POND - CTC SITE"
" 54 POND DESIGN"
" 2.110 Current peak flow c.m/sec"
" 0.635 Target outflow c.m/sec"
" 9484.8 Hydrograph volume c.m"
" 15. Number of stages"
" 0.000 Minimum water level metre"
" 1.400 Maximum water level metre"
" 0.000 Starting water level metre"
" 0 Keep Design Data: 1 = True; 0 = False"
" Level Discharge Volume"
" 0.000 0.000 0.000"
" 0.1000 0.00276 124.985"
" 0.2000 0.00477 256.026"
" 0.3000 0.00616 393.250"
" 0.4000 0.00729 536.786"
" 0.5000 0.00827 686.761"
" 0.6000 0.00914 843.304"
" 0.7000 0.00994 1006.543"
" 0.8000 0.01068 1176.605"
" 0.9000 0.2200 1353.618"
" 1.000 0.6243 1537.711"
" 1.100 1.178 1729.012"
" 1.200 1.871 1927.648"
" 1.300 2.698 2133.748"
" 1.400 3.658 2347.440"
" 1. WEIRS"
" Crest Weir Crest Left Right"
" elevation coefficient breadth sideslope sideslope"
" 0.800 0.980 3.800 2.000 2.000"
" 1. ORIFICES"
" Orifice Orifice Orifice Number of"
" invert coefficient diameter orifices"
" 0.000 0.630 0.0750 1.000"
" 2. LAYERS"
" Bottom Aspect Bottom Top Average"
" area ratio elevation elevation sideslope"
" 1220.000 2.000 0.000 1.400 4.000"
" 2175.299 1.688 1.400 1.400 4.000"
" Peak outflow 2.035 c.m/sec"
" Maximum level 1.220 metre"
" Maximum storage 1968.814 c.m"
" Centroidal lag 6.941 hours"
" 1.207 2.110 2.035 0.000 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 1.207 2.035 2.035 0.000"
" 52 CHANNEL DESIGN"
" 2.035 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.582 metre"
" Velocity 0.934 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.387 metre"
" 53 ROUTE Channel Route 220"
" 220.00 Channel Route 220 Reach length (metre)"
" 0.368 X-factor <= 0.5"
" 176.751 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 2.004 c.m/sec"
" 1.207 2.035 2.004 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 3.579 c.m/sec"
" Hydrograph volume 17424.738 c.m"
" 1.207 2.035 2.004 3.579"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 1.207 0.000 2.004 3.579"
" 33 CATCHMENT 750"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 750 No description"
" 100.000 % Impervious"
" 0.500 Total Area"
" 50.000 Flow length"
" 2.000 Overland Slope"
" 0.000 Pervious Area"
" 50.000 Pervious length"
" 2.000 Pervious slope"
" 0.200 Pervious Area"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.933 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.047 0.000 0.017 3.594 c.m/sec"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.933 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.118 0.000 2.004 3.579 c.m/sec"
" Catchment 750 Pervious Impervious Total Area "
" Surface Area 0.000 0.500 0.500 hectare"
" Time of concentration 16.748 2.959 2.959 minutes"
" Time to Centroid 239.708 203.134 203.134 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 0.00 544.00 544.00 c.m"
" Rainfall losses 43.750 7.287 7.288 mm"
" Runoff depth 65.050 101.513 101.512 c.m"
" Runoff volume 0.00 507.56 507.56 c.m"
" Runoff coefficient 0.000 0.933 0.933 "
" Maximum flow 0.000 0.118 0.118 c.m/sec"
" HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.118 2.004 3.579"
" 81 ADD COMMENT"
" 1 Lines of comment"
" EXISTING POND - ROOFTOP STORAGE - CTC SITE"
" 54 POND DESIGN"
" 0.118 Current peak flow c.m/sec"
" 0.020 Target outflow c.m/sec"
" 507.6 Hydrograph volume c.m"
" 9. Number of stages"
" 0.000 Minimum water level metre"
" 0.200 Maximum water level metre"
" 0.000 Starting water level metre"
" 0 Keep Design Data: 1 = True; 0 = False"
" Level Discharge Volume"
" 0.000 0.000 0.000"
" 0.02500 0.00112 72.969"
" 0.05000 0.00386 146.876"
" 0.07500 0.01047 221.724"
" 0.1000 0.01422 297.514"
" 0.1250 0.01716 374.249"
" 0.1500 0.01967 451.931"
" 0.1750 0.02190 530.562"
" 0.2000 0.02391 610.142"
" 1. ORIFICES"
" Orifice Orifice Orifice Number of"
" invert coefficient diameter orifices"
" 0.000 0.630 0.0680 6.000"
" 2. LAYERS"
" Bottom Aspect Bottom Top Average"
" area ratio elevation elevation sideslope"
" 2900.000 10.000 0.000 0.200 4.000"
" 3085.338 1.960 0.200 0.200 4.000"
" Peak outflow 0.017 c.m/sec"
" Maximum level 0.121 metre"
" Maximum storage 362.324 c.m"
" Centroidal lag 11.910 hours"
" 0.118 0.118 0.017 3.579 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 0.118 0.017 0.017 3.579"
" 52 CHANNEL DESIGN"
" 0.017 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.040 metre"
" Velocity 0.199 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.019 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length (metre)"
" 0.452 X-factor <= 0.5"
" 188.197 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 150.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.017 c.m/sec"
" 0.118 0.017 0.017 3.579 c.m/sec"
" 40 HYDROGRAPH Combine 2000"
" 6 Combine "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 3.594 c.m/sec"
" Hydrograph volume 17888.156 c.m"
" 0.118 0.017 0.017 3.594"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.118 0.000 0.017 3.594"
" 33 CATCHMENT 751"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 751 No description"
" 100.000 % Impervious"
" 0.200 Total Area"
" 50.000 Flow length"
" 2.000 Overland Slope"
" 0.000 Pervious Area"
" 50.000 Pervious length"
" 2.000 Pervious slope"
" 0.200 Pervious Area"
" 50.000 Impervious length"
" 2.000 Impervious slope"
" 0.200 Pervious Manning 'n'"
" 81.000 Pervious SCS Curve No."
" 0.000 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.958 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.933 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.047 0.000 0.017 3.594 c.m/sec"

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"      Catchment 751      Pervious      Impervious      Total Area "
"      Surface Area      0.000      0.200      0.200      hectare"
"      Time of concentration 16.748      2.959      2.959      minutes"
"      Time to Centroid 239.708      203.134      203.134      minutes"
"      Rainfall depth 108.800      108.800      108.800      mm"
"      Rainfall volume 0.000      217.60      217.60      c.m"
"      Rainfall losses 43.750      7.287      7.288      mm"
"      Runoff depth 65.050      101.513      101.512      mm"
"      Runoff volume 0.000      203.02      203.03      c.m"
"      Runoff coefficient 0.000      0.933      0.933      "
"      Maximum flow 0.000      0.047      0.047      c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.047      0.047      0.017      3.594"
" 81  ADD COMMENT=====
" 1  Lines of comment"
"      EXISTING POND - PARKING LOT STORAGE - CTC SITE"
" 54  POND DESIGN"
"      0.047 Current peak flow c.m/sec"
"      0.020 Target outflow c.m/sec"
"      203.0 Hydrograph volume c.m"
"      5. Number of stages"
"      0.000 Minimum water level metre"
"      0.700 Maximum water level metre"
"      0.000 Starting water level metre"
"      0 Keep Design Data: 1 = True; 0 = False"
"      Level Discharge Volume"
"      0.000 0.000 0.000"
"      0.1750 0.01148 16.645"
"      0.3500 0.03242 39.036"
"      0.5250 0.04289 67.860"
"      0.7000 0.05126 103.803"
"      1. ORIFICES"
"      Orifice Orifice Orifice Number of"
"      invert coeffic diameter orifices"
"      0.000 0.630 0.1750 1.000"
"      1. LAYERS"
"      Bottom Aspect Bottom Top Average"
"      area ratio elevation elevation sideslope"
"      80.000 3.000 0.000 0.700 4.000"
"      Peak outflow 0.035 c.m/sec"
"      Maximum level 0.401 metre"
"      Maximum storage 47.359 c.m"
"      Centroidal lag 3.760 hours"
"      0.047 0.047 0.035 3.594 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link "
"      0.047 0.035 0.035 3.594"
" 52  CHANNEL DESIGN"
"      0.035 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      0.500 Gradient %"
"      Depth of flow 0.062 metre"
"      Velocity 0.260 m/sec"
"      Channel capacity 278.848 c.m/sec"
"      Critical depth 0.031 metre"
" 53  ROUTE Channel Route 50"
"      50.000 Channel Route 50 Reach length (metre)"
"      0.427 X-factor <= 0.5"
"      144.311 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      150.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.047 0.035 0.035 3.594 c.m/sec"
" 40  HYDROGRAPH Combine 2000"
"      6 Combine "
"      2000 Node #"
"      Flow in Hwy. 21 Ditch"
"      Maximum Flow 3.629 c.m/sec"
"      Hydrograph volume 18091.137 c.m"
"      0.047 0.035 3.629"
" 81  ADD COMMENT=====
" 1  Lines of comment"
"      Total discharge to Hwy. 21 Ditch"
" 40  HYDROGRAPH Start - New Tributary"
"      2 Start - New Tributary"
"      0.047 0.000 0.035 3.629"
" 33  CATCHMENT 301"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      301 No description"
"      0.000 % Impervious"
"      16.400 Total Area"
"      95.000 Flow length"
"      2.500 Overland Slope"
"      16.400 Pervious Area"
"      2.500 Pervious length"
"      2.500 Pervious slope"
"      0.000 Impervious Area"
"      95.000 Impervious length"
"      2.500 Impervious slope"
"      0.230 Pervious Manning 'n'"
"      81.000 Pervious SCS Curve No."
"      0.598 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.958 Pervious Initial abstraction"
"      0.013 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.000 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      2.801 0.000 0.035 3.629 c.m/sec"
"      Catchment 301 Pervious Impervious Total Area "
"      Surface Area 16.400 0.000 16.400 hectare"
"      Time of concentration 25.036 4.067 25.036 minutes"
"      Time to Centroid 249.717 204.274 249.717 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 1.7843 0.0000 1.7843 ha-m"
"      Rainfall losses 43.763 7.558 43.763 mm"
"      Runoff depth 65.037 101.242 65.037 mm"
"      Runoff volume 1.0666 0.0000 1.0666 ha-m"
"      Runoff coefficient 0.598 0.000 0.598 "
"      Maximum flow 2.801 0.000 2.801 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      2.801 2.801 0.035 3.629"
" 52  CHANNEL DESIGN"
"      0.648 2.801 2.801 3.629 c.m/sec"
"      Catchment 401 Pervious Impervious Total Area "
"      Surface Area 5.600 0.000 5.600 hectare"
"      Time of concentration 56.146 7.901 56.146 minutes"
"      Time to Centroid 209.131 209.131 209.131 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 6092.79 0.01 6092.80 c.m"
"      Rainfall losses 39.852 5.770 39.852 mm"
"      Runoff depth 68.948 103.030 68.948 mm"
"      Runoff volume 3861.07 0.01 3861.08 c.m"
"      Runoff coefficient 0.634 0.000 0.634 "
"      Maximum flow 0.648 0.000 0.648 c.m/sec"
" 40  HYDROGRAPH Add Runoff "
"      4 Add Runoff "
"      0.648 3.361 2.801 3.629"
" 52  CHANNEL DESIGN"
"      3.361 Current peak flow c.m/sec"
"      0.040 Manning 'n'"
"      0. Cross-section type: 0=trapezoidal; 1=general"
"      2.000 Basewidth metre"
"      3.000 Left bank slope"
"      3.000 Right bank slope"
"      5.000 Channel depth metre"
"      1.200 Gradient %"
"      Depth of flow 0.601 metre"
"      Velocity 1.471 m/sec"
"      Channel capacity 431.989 c.m/sec"
"      Critical depth 0.510 metre"
" 53  ROUTE Channel Route 150"
"      150.000 Channel Route 150 Reach length (metre)"
"      0.417 X-factor <= 0.5"
"      76.454 K-lag (seconds)"
"      0.000 Default(0) or user spec.(1) values used"
"      0.500 X-factor <= 0.5"
"      30.000 K-lag (seconds)"
"      0.500 Beta weighting factor"
"      75.000 Routing time step (seconds)"
"      1 No. of sub-reaches"
"      Peak outflow 0.648 3.361 3.332 3.629 c.m/sec"
" 40  HYDROGRAPH Next link "
"      5 Next link "
"      0.648 3.332 3.332 3.629"
" 33  CATCHMENT 402"
"      1 Triangular SCS"
"      1 Equal length"
"      1 SCS method"
"      402 No description"
"      50.000 % Impervious"
"      7.400 Total Area"
"      100.000 Flow length"
"      2.000 Overland Slope"
"      3.700 Pervious Area"
"      100.000 Pervious length"
"      2.000 Pervious slope"
"      3.700 Impervious Area"
"      100.000 Impervious length"
"      2.000 Impervious slope"
"      0.300 Pervious Manning 'n'"
"      83.000 Pervious SCS Curve No."
"      0.633 Pervious Runoff coefficient"
"      0.100 Pervious Ia/S coefficient"
"      5.202 Pervious Initial abstraction"
"      0.013 Impervious Manning 'n'"
"      98.000 Impervious SCS Curve No."
"      0.938 Impervious Runoff coefficient"
"      0.100 Impervious Ia/S coefficient"
"      0.518 Impervious Initial abstraction"
"      1.347 3.332 3.332 3.629 c.m/sec"
"      Catchment 402 Pervious Impervious Total Area "
"      Surface Area 3.700 3.700 7.400 hectare"
"      Time of concentration 31.867 4.484 15.520 minutes"
"      Time to Centroid 256.479 205.099 225.808 minutes"
"      Rainfall depth 108.800 108.800 108.800 mm"
"      Rainfall volume 4025.60 4025.60 8051.20 c.m"

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" Rainfall losses 39.877 6.711 23.294 mm"
" Runoff depth 68.923 102.089 85.506 mm"
" Runoff volume 2550.15 3777.31 6327.44 c.m"
" Runoff coefficient 0.633 0.938 0.786 "
" Maximum flow 0.605 0.859 1.347 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 1.347 4.162 3.332 3.629"
52 CHANNEL DESIGN"
4.162 Current peak flow c.m/sec"
0.020 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
4.000 Basewidth metre"
50.000 Left bank slope"
0.000 Right bank slope"
0.300 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.226 metre"
Velocity 1.910 m/sec"
Channel capacity 7.740 c.m/sec"
Critical depth 0.286 metre"
53 ROUTE Channel Route 200"
200.00 Channel Route 200 Reach length (metre)"
0.487 X-factor <= 0.5"
78.534 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
75.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 4.125 c.m/sec"
1.347 4.162 4.125 3.629 c.m/sec"
40 HYDROGRAPH Combine 6000"
6 Combine "
6000 Node #"
Maximum flow 4.125 c.m/sec"
Hydrograph volume 20854.529 c.m"
1.347 4.162 4.125 4.125"
40 HYDROGRAPH Start - New Tributary"
2 Start - New Tributary"
1.347 0.000 4.125 4.125"
33 CATCHMENT 501"
1 Triangular SCS"
1 Equal length"
1 SCS method"
501 No description"
0.000 % Impervious"
2.500 Total Area"
80.000 Flow length"
3.500 Overland Slope"
2.500 Pervious Area"
80.000 Pervious length"
3.500 Pervious slope"
0.000 Impervious Area"
80.000 Impervious length"
3.500 Impervious slope"
0.300 Pervious Manning 'n'"
83.000 Pervious SCS Curve No."
0.633 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.202 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.464 0.000 4.125 4.125 c.m/sec"
Catchment 501 Pervious Impervious Total Area "
Surface Area 2.500 0.000 2.500 hectare"
Time of concentration 23.566 3.316 23.566 minutes"
Time to Centroid 246.432 203.623 246.432 minutes"
Rainfall depth 108.800 108.800 108.800 mm"
Rainfall volume 2720.00 0.00 2720.00 c.m"
Rainfall losses 39.885 7.581 39.885 mm"
Runoff depth 68.915 101.219 68.915 mm"
Runoff volume 1722.88 0.00 1722.88 c.m"
Runoff coefficient 0.633 0.000 0.633 "
Maximum flow 0.464 0.000 0.464 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.464 0.464 4.125 4.125"
52 CHANNEL DESIGN"
0.464 Current peak flow c.m/sec"
0.040 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
2.000 Basewidth metre"
3.000 Left bank slope"
3.000 Right bank slope"
5.000 Channel depth metre"
1.200 Gradient %"
Depth of flow 0.212 metre"
Velocity 0.831 m/sec"
Channel capacity 431.989 c.m/sec"
Critical depth 0.162 metre"
53 ROUTE Channel Route 100"
100.00 Channel Route 100 Reach length (metre)"
0.451 X-factor <= 0.5"
90.245 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
75.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.457 c.m/sec"
0.464 0.464 0.457 4.125 c.m/sec"
40 HYDROGRAPH Next link "
5 Next link " 0.464 0.457 0.457 4.125"
33 CATCHMENT 403"
1 Triangular SCS"
1 Equal length"
1 SCS method"
403 No description"
75.000 % Impervious"
4.700 Total Area"
70.000 Flow length"
2.000 Overland Slope"
1.175 Pervious Area"
70.000 Pervious length"
2.000 Pervious slope"
3.525 Impervious Area"
70.000 Impervious length"
2.000 Impervious slope"
0.300 Pervious Manning 'n'"
83.000 Pervious SCS Curve No."
0.633 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
5.202 Pervious Initial abstraction"
0.013 Impervious Manning 'n'"
98.000 Impervious SCS Curve No."
0.931 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction"
0.677 0.000 1.321 5.086 c.m/sec"
Catchment 404 Pervious Impervious Total Area "
Surface Area 0.800 2.400 3.200 hectare"
Time of concentration 23.455 3.301 7.028 minutes"
Time to Centroid 246.293 203.612 211.505 minutes"
Rainfall depth 108.800 108.800 108.800 mm"
Rainfall volume 870.40 2611.20 3481.60 c.m"
Rainfall losses 39.890 7.558 15.641 mm"
Runoff depth 68.910 101.242 93.159 mm"
Runoff volume 551.28 2429.82 2981.10 c.m"
Runoff coefficient 0.633 0.931 0.856 "
Maximum flow 0.149 0.567 0.677 c.m/sec"
40 HYDROGRAPH Add Runoff "
4 Add Runoff " 0.677 0.677 1.321 5.086"
52 CHANNEL DESIGN"
0.677 Current peak flow c.m/sec"
0.020 Manning 'n'"
0. Cross-section type: 0=trapezoidal; 1=general"
4.000 Basewidth metre"
50.000 Left bank slope"
0.000 Right bank slope"
0.300 Channel depth metre"
2.000 Gradient %"
Depth of flow 0.092 metre"
Velocity 1.164 m/sec"
Channel capacity 7.740 c.m/sec"
Critical depth 0.112 metre"
53 ROUTE Channel Route 100"
100.00 Channel Route 100 Reach length (metre)"
0.488 X-factor <= 0.5"
64.421 K-lag (seconds)"
0.000 Default(0) or user spec.(1) values used"
0.500 X-factor <= 0.5"
30.000 K-lag (seconds)"
0.500 Beta weighting factor"
60.000 Routing time step (seconds)"
1 No. of sub-reaches"
Peak outflow 0.672 c.m/sec"
0.677 0.677 0.672 5.086 c.m/sec"
40 HYDROGRAPH Combine 6000"
6 Combine "
6000 Node #"


```

"
"
" Maximum flow 5.602 c.m/sec"
" Hydrograph volume 29909.250 c.m"
" 0.677 0.677 0.672 5.602"
" 40 HYDROGRAPH Confluence 6000"
" 7 Confluence "
" 6000 Node #"
"
" Maximum flow 5.602 c.m/sec"
" Hydrograph volume 29909.248 c.m"
" 0.677 5.602 0.672 0.000"
" 52 CHANNEL DESIGN"
" 5.602 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.259 metre"
" Velocity 2.064 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.329 metre"
" 53 ROUTE Channel Route 200"
" 200.00 Channel Route 200 Reach length (metre)"
" 0.485 X-factor <= 0.5"
" 72.683 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 5.548 c.m/sec"
" 0.677 5.602 5.548 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
" Maximum flow 5.548 c.m/sec"
" Hydrograph volume 29909.258 c.m"
" 0.677 5.602 5.548 5.548"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.677 0.000 5.548 5.548"
" 33 CATCHMENT 302"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 302 No description"
" 50.000 % Impervious"
" 6.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 3.000 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.000 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious Manning 'n'"
" 0.280 Pervious SCS Curve No."
" 80.000 Pervious SCS Curve No."
" 0.581 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 6.350 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.938 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 1.056 0.000 5.548 5.548 c.m/sec"
" Catchment 302 Pervious Impervious Total Area "
" Surface Area 3.000 3.000 6.000 hectare"
" Time of concentration 31.323 4.484 14.746 minutes"
" Time to Centroid 258.059 205.099 225.349 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 3264.00 3264.00 6528.00 c.m"
" Rainfall losses 45.606 6.711 26.158 mm"
" Runoff depth 63.194 102.089 82.642 mm"
" Runoff volume 1895.82 3062.68 4958.50 c.m"
" Runoff coefficient 0.581 0.938 0.760 "
" Maximum flow 0.452 0.696 1.056 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 1.056 1.056 5.548 5.548"
" 52 CHANNEL DESIGN"
" 1.056 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.116 metre"
" Velocity 1.320 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.143 metre"
" 53 ROUTE Channel Route 180"
" 180.00 Channel Route 180 Reach length (metre)"
" 0.492 X-factor <= 0.5"
" 102.255 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.029 c.m/sec"
" 1.056 1.056 1.029 5.548 c.m/sec"
" 40 HYDROGRAPH Next link "
" 5 Next link "
" 1.056 1.029 1.029 5.548"
" 33 CATCHMENT 303"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 303 No description"
" 75.000 % Impervious"
" 4.800 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 1.200 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 3.600 Impervious Area"
" 100.000 Impervious length"
" 2.000 Impervious slope"
" 2.000 Pervious Manning 'n'"
" 82.000 Pervious SCS Curve No."
" 0.616 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.576 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.938 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.995 1.029 1.029 5.548 c.m/sec"
" Catchment 303 Pervious Impervious Total Area "
" Surface Area 1.200 3.600 4.800 hectare"
" Time of concentration 30.815 4.484 9.209 minutes"
" Time to Centroid 255.972 205.099 214.228 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 1305.60 3916.80 5222.40 c.m"
" Rainfall losses 41.826 6.711 15.490 mm"
" Runoff depth 66.974 102.089 93.310 mm"
" Runoff volume 803.68 3675.22 4478.90 c.m"
" Runoff coefficient 0.616 0.938 0.858 "
" Maximum flow 0.194 0.835 0.995 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.995 2.024 1.029 5.548"
" 52 CHANNEL DESIGN"
" 2.024 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.160 metre"
" Velocity 1.578 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.200 metre"
" 53 ROUTE Channel Route 250"
" 250.00 Channel Route 250 Reach length (metre)"
" 0.492 X-factor <= 0.5"
" 118.851 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 1.979 c.m/sec"
" 0.995 2.024 1.979 5.548 c.m/sec"
" 40 HYDROGRAPH Combine 6100"
" 6 Combine "
" 6100 Node #"
"
" Maximum flow 7.386 c.m/sec"
" Hydrograph volume 39346.617 c.m"
" 0.995 2.024 1.979 7.386"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.995 0.000 1.979 7.386"
" 33 CATCHMENT 407"
" 1 Triangular SCS"
" 1 Equal length"
" 1 SCS method"
" 407 No description"
" 75.000 % Impervious"
" 3.000 Total Area"
" 100.000 Flow length"
" 2.000 Overland Slope"
" 0.750 Pervious Area"
" 100.000 Pervious length"
" 2.000 Pervious slope"
" 2.250 Impervious Area"
" 100.000 Impervious length"
" 2.000 Pervious Manning 'n'"
" 83.000 Pervious SCS Curve No."
" 0.633 Pervious Runoff coefficient"
" 0.100 Pervious Ia/S coefficient"
" 5.202 Pervious Initial abstraction"
" 0.013 Impervious Manning 'n'"
" 98.000 Impervious SCS Curve No."
" 0.938 Impervious Runoff coefficient"
" 0.100 Impervious Ia/S coefficient"
" 0.518 Impervious Initial abstraction"
" 0.621 0.000 1.979 7.386 c.m/sec"
" Catchment 407 Pervious Impervious Total Area "
" Surface Area 0.750 2.250 3.000 hectare"
" Time of concentration 31.867 4.484 9.515 minutes"
" Time to Centroid 256.479 205.099 214.538 minutes"
" Rainfall depth 108.800 108.800 108.800 mm"
" Rainfall volume 816.00 2448.00 3264.00 c.m"
" Rainfall losses 39.877 6.711 15.002 mm"
" Runoff depth 68.923 102.089 93.798 mm"
" Runoff volume 516.92 2297.01 2813.93 c.m"
" Runoff coefficient 0.633 0.938 0.862 "
" Maximum flow 0.123 0.522 0.621 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
" 4 Add Runoff "
" 0.621 0.621 1.979 7.386"
" 52 CHANNEL DESIGN"
" 0.621 Current peak flow c.m/sec"
" 0.020 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general"
" 4.000 Basewidth metre"
" 50.000 Left bank slope"
" 0.000 Right bank slope"
" 0.300 Channel depth metre"
" 2.000 Gradient %"
" Depth of flow 0.088 metre"
" Velocity 1.136 m/sec"
" Channel capacity 7.740 c.m/sec"
" Critical depth 0.107 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length (metre)"
" 0.488 X-factor <= 0.5"
" 66.043 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor"
" 60.000 Routing time step (seconds)"
" 1 No. of sub-reaches"
" Peak outflow 0.617 c.m/sec"
" 0.621 0.621 0.617 7.386 c.m/sec"

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" 40 HYDROGRAPH Next link " " 0.3833 0.04383 3662.299"
" 5 Next link " " 0.4792 0.05156 4645.824"
" 0.621 0.617 0.617 7.386" " 0.5750 0.05826 5655.543"
" 33 CATCHMENT 310" " 0.6708 0.06427 6692.645"
" 1 Triangular SCS" " 0.7667 0.06977 7758.431"
" 1 Equal length" " 0.8625 0.07486 8850.853"
" 1 SCS method" " 0.9583 0.07963 9971.185"
" 310 No description" " 1.054 0.08412 11118.39"
" 75.000 % Impervious" " 1.150 0.08840 12297.52"
" 2.400 Total Area" " 1.246 0.2294 13505.21"
" 75.000 Flow length" " 1.342 0.4837 14741.64"
" 2.000 Overland Slope" " 1.438 0.8116 16006.97"
" 0.600 Pervious Area" " 1.533 1.195 17287.76"
" 75.000 Pervious length" " 1.629 1.633 18611.14"
" 2.000 Pervious slope" " 1.725 2.118 19963.96"
" 1.800 Impervious Area" " 1.821 2.644 21346.39"
" 75.000 Impervious length" " 1.917 3.209 22758.63"
" 2.000 Impervious slope" " 2.013 3.811 24200.82"
" 0.200 Pervious Manning 'n'" " 2.108 5.348 25657.67"
" 82.000 Pervious SCS Curve No." " 2.204 7.723 27160.03"
" 0.615 Pervious Runoff coefficient" " 2.300 10.675 28692.88"
" 0.100 Pervious Ia/S coefficient" " " " " " "
" 5.576 Pervious Initial abstraction" " 2. WEIRS" " " " " "
" 0.013 Impervious Manning 'n'" " Crest Weir Crest Left Right"
" 98.000 Impervious SCS Curve No." " elevation coefficient breadth sideslope sideslope"
" 0.926 Impervious Runoff coefficient" " 1.150 0.900 3.000 0.000 0.000"
" 0.100 Impervious Ia/S coefficient" " 2.013 0.900 20.000 3.000 3.000"
" 0.518 Impervious Initial abstraction" " 1. ORIFICES" " " " " "
" 0.507 0.617 0.617 7.386 c.m/sec" " Orifice Orifice Orifice Number of"
" Catchment 310 Pervious Impervious Total Area " invert coefficient diameter orifices"
" Surface Area 0.600 1.800 2.400 hectare" " 0.000 0.630 0.2000 1.000"
" Time of concentration 21.189 3.773 6.930 minutes" " 2. LAYERS" " " " " "
" Time to Centroid 244.317 203.918 211.240 minutes" " Bottom Aspect Bottom Top Average"
" Rainfall depth 108.800 108.800 108.800 area ratio elevation elevation sideslope"
" Rainfall volume 652.80 1958.40 2611.20 mm" " 9000.000 7.000 0.000 2.000 5.000"
" Rainfall losses 41.871 8.015 16.479 mm" " 15137.096 4.852 2.000 2.300 5.000"
" Runoff depth 66.929 100.785 92.321 mm" " Peak outflow 3.779 c.m/sec"
" Runoff volume 401.57 1814.13 2215.70 c.m" " Maximum level 2.008 metre"
" Runoff coefficient 0.615 0.926 0.849 " " Maximum storage 24124.971 c.m"
" Maximum flow 0.112 0.421 0.507 c.m/sec" " Centroidal lag 14.202 hours"
" 40 HYDROGRAPH Add Runoff " " 0.507 8.351 3.779 0.000 c.m/sec"
" 4 Add Runoff " " 1.223 0.617 7.386" " 50 HYDROGRAPH Next link "
" 0.507 3.779 3.779 0.000" " 52 CHANNEL DESIGN" "
" 1.123 Current peak flow c.m/sec" " 3.779 Current peak flow c.m/sec"
" 0.040 Manning 'n'" " 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 2.000 Basewidth metre" " 2.000 Basewidth metre"
" 3.000 Left bank slope" " 3.000 Left bank slope"
" 3.000 Right bank slope" " 3.000 Right bank slope"
" 5.000 Channel depth metre" " 5.000 Channel depth metre"
" 2.000 Gradient %" " 2.000 Gradient %"
" Depth of flow 0.299 metre" " Depth of flow 0.561 metre"
" Velocity 1.298 m/sec" " Velocity 1.830 m/sec"
" Channel capacity 557.696 c.m/sec" " Channel capacity 557.696 c.m/sec"
" Critical depth 0.275 metre" " Critical depth 0.543 metre"
" 53 ROUTE Channel Route 200" " 53 ROUTE Channel Route 250"
" 200.00 Channel Route 200 Reach length (metre)" " 250.00 Channel Route 250 Reach length (metre)"
" 0.480 X-factor <= 0.5" " 0.472 X-factor <= 0.5"
" 115.562 K-lag (seconds)" " 102.471 K-lag (seconds)"
" 0.000 Default(0) or user spec.(1) values used" " 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5" " 0.500 X-factor <= 0.5"
" 30.000 K-lag (seconds)" " 30.000 K-lag (seconds)"
" 0.500 Beta weighting factor" " 0.500 Beta weighting factor"
" 100.000 Routing time step (seconds)" " 100.000 Routing time step (seconds)"
" 1 No. of sub-reaches" " 1 No. of sub-reaches"
" Peak outflow 1.110 c.m/sec" " Peak outflow 3.765 c.m/sec"
" 0.507 1.123 1.110 7.386 c.m/sec" " 0.507 3.779 3.765 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 6100" " 40 HYDROGRAPH Combine 2000"
" 6 Combine " " 6 Combine "
" 6100 Node #" " 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 8.355 c.m/sec" " Maximum flow 6.137 c.m/sec"
" Hydrograph volume 44376.262 c.m" " Hydrograph volume 55406.535 c.m"
" 0.507 1.123 1.110 8.355" " 0.507 3.779 3.765 6.137"
" 40 HYDROGRAPH Confluence 6100" " 40 HYDROGRAPH Start - New Tributary"
" 7 Confluence " " 2 Start - New Tributary"
" 6100 Node #" " 0.507 0.000 3.765 6.137"
" Maximum flow 8.355 c.m/sec" " 33 CATCHMENT 311"
" Hydrograph volume 44376.266 c.m" " 1 Triangular SCS"
" 0.507 8.355 1.110 0.000" " 1 Equal length"
" 52 CHANNEL DESIGN" " 1 SCS method"
" 8.355 Current peak flow c.m/sec" " 311 No description"
" 0.040 Manning 'n'" " 75.000 % Impervious"
" 0. Cross-section type: 0=trapezoidal; 1=general" " 6.600 Total Area"
" 2.000 Basewidth metre" " 100.000 Flow length"
" 3.000 Left bank slope" " 2.000 Overland Slope"
" 3.000 Right bank slope" " 1.650 Pervious Area"
" 5.000 Channel depth metre" " 100.000 Pervious length"
" 2.000 Gradient %" " 2.000 Pervious slope"
" Depth of flow 0.825 metre" " 4.950 Impervious Area"
" Velocity 2.262 m/sec" " 100.000 Impervious length"
" Channel capacity 557.696 c.m/sec" " 2.000 Impervious slope"
" Critical depth 0.821 metre" " 0.200 Pervious Manning 'n'"
" 53 ROUTE Channel Route 50" " 82.000 Pervious SCS Curve No."
" 50.00 Channel Route 50 Reach length (metre)" " 0.615 Pervious Runoff coefficient"
" 0.304 X-factor <= 0.5" " 0.100 Pervious Ia/S coefficient"
" 16.580 K-lag (seconds)" " 5.576 Pervious Initial abstraction"
" 0.000 Default(0) or user spec.(1) values used" " 0.013 Impervious Manning 'n'"
" 0.500 X-factor <= 0.5" " 98.000 Impervious SCS Curve No."
" 30.000 K-lag (seconds)" " 0.938 Impervious Runoff coefficient"
" 0.500 Beta weighting factor" " 0.100 Impervious Ia/S coefficient"
" 21.429 Routing time step (seconds)" " 0.518 Impervious Initial abstraction"
" 1 No. of sub-reaches" " 1.411 0.000 3.765 6.137 c.m/sec"
" Peak outflow 8.351 c.m/sec" " Catchment 311 Pervious Impervious Total Area "
" 0.507 8.355 8.351 0.000 c.m/sec" " Surface Area 1.650 4.950 6.600 hectare"
" 40 HYDROGRAPH Next link " " Time of concentration 25.181 4.484 8.197 minutes"
" 5 Next link " " Time to Centroid 249.147 205.099 213.000 minutes"
" 0.507 8.351 8.351 0.000" " Rainfall depth 108.800 108.800 108.800 mm"
" 81 ADD COMMENT-----" " Rainfall volume 1795.20 5385.60 7180.80 c.m"
" 1 Lines of comment" " Rainfall losses 41.862 6.711 15.498 mm"
" PROPOSED POND #2" " Runoff depth 66.938 102.089 93.302 mm"
" 54 POND DESIGN" " Runoff volume 1104.48 5053.43 6157.91 c.m"
" 8.351 Current peak flow c.m/sec" " Runoff coefficient 0.615 0.938 0.858 "
" 4.007 Target outflow c.m/sec" " Maximum flow 0.289 1.149 1.411 c.m/sec"
" 44376.3 Hydrograph volume c.m" " 40 HYDROGRAPH Add Runoff "
" 25. Number of stages" " 4 Add Runoff "
" 0.000 Minimum water level metre" " 1.411 1.411 3.765 6.137"
" 2.300 Maximum water level metre" " 52 CHANNEL DESIGN"
" 0.000 Starting water level metre" " 1.411 Current peak flow c.m/sec"
" 0 Keep Design Data: 1 = True; 0 = False" " 0.020 Manning 'n'"
" Level Discharge Volume" " 0. Cross-section type: 0=trapezoidal; 1=general"
" 0.000 0.000 0.000" " 4.000 Basewidth metre"
" 0.09583 0.00452 875.671" " 50.000 Left bank slope"
" 0.1917 0.01493 1778.243" " 0.000 Right bank slope"
" 0.2875 0.03442 2706.844" " 0.300 Channel depth metre"
" 2.000 Gradient %"

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"	Depth of flow	0.134	metre"	"	Runoff depth	66.938	102.089	93.302	mm"
"	Velocity	1.430	m/sec"	"	Runoff volume	736.32	3368.95	4105.27	c.m"
"	Channel capacity	7.740	c.m/sec"	"	Runoff coefficient	0.615	0.938	0.858	"
"	Critical depth	0.166	metre"	"	Maximum flow	0.193	0.766	0.940	c.m/sec"
"	ROUTE Channel Route 200"			"	HYDROGRAPH Add Runoff "				
53	200.00 Channel Route 200 Reach length (metre)"			40	4 Add Runoff "	0.940	2.083	2.083"	
"	0.492 X-factor <= 0.5"			"					
"	104.869 K-lag (seconds)"			52	CHANNEL DESIGN"				
"	0.000 Default(0) or user spec.(1) values used"			"	0.940 Current peak flow c.m/sec"				
"	0.500 X-factor <= 0.5"			"	0.020 Manning 'n'"				
"	30.000 K-lag (seconds)"			"	0. Cross-section type: 0=trapezoidal; 1=general"				
"	0.500 Beta weighting factor"			"	4.000 Basewidth metre"				
"	100.000 Routing time step (seconds)"			"	50.000 Left bank slope"				
"	1 No. of sub-reaches"			"	0.000 Right bank slope"				
"	Peak outflow	1.395	c.m/sec"	"	0.300 Channel depth metre"				
"	1.411 1.411 1.395 6.137 c.m/sec"			"	2.000 Gradient %"				
40	HYDROGRAPH Next link "			"	Depth of flow	0.109	metre"		
"	5 Next link "			"	Velocity	1.278	m/sec"		
"	1.411 1.395 1.395 6.137"			"	Channel capacity	7.740	c.m/sec"		
33	CATCHMENT 314"			"	Critical depth	0.134	metre"		
"	1 Triangular SCS"			53	ROUTE Channel Route 100"				
"	1 Equal length"			"	100.00 Channel Route 100 Reach length (metre)"				
"	1 SCS method"			"	0.486 X-factor <= 0.5"				
"	314 No description"			"	58.688 K-lag (seconds)"				
50.000	% Impervious"			"	0.000 Default(0) or user spec.(1) values used"				
3.300	Total Area"			"	0.500 X-factor <= 0.5"				
20.000	Flow length"			"	30.000 K-lag (seconds)"				
1.000	Overland Slope"			"	0.500 Beta weighting factor"				
1.650	Pervious Area"			"	60.000 Routing time step (seconds)"				
20.000	Pervious length"			"	1 No. of sub-reaches"				
1.000	Pervious slope"			"	Peak outflow	0.935	c.m/sec"		
1.650	Impervious Area"			"	0.940 0.940 0.935 2.083 c.m/sec"				
20.000	Impervious length"			40	HYDROGRAPH Combine 7000"				
1.000	Impervious slope"			"	6 Combine "				
0.200	Pervious Manning 'n'"			"	7000 Node #"				
82.000	Pervious SCS Curve No."			"					
0.614	Pervious Runoff coefficient"			"	Maximum flow	3.017	c.m/sec"		
0.100	Pervious Ia/S coefficient"			"	Hydrograph volume	13047.581	c.m"		
5.576	Pervious Initial abstraction"			"	0.940 0.940 0.935 3.017"				
0.013	Impervious Manning 'n'"			40	HYDROGRAPH Start - New Tributary"				
98.000	Impervious SCS Curve No."			"	2 Start - New Tributary"				
0.937	Impervious Runoff coefficient"			"	0.940 0.000 0.935 3.017"				
0.100	Impervious Ia/S coefficient"			33	CATCHMENT 304"				
0.518	Impervious Initial abstraction"			"	1 Triangular SCS"				
"	1.395 1.395 6.137 c.m/sec"			"	1 Equal length"				
"	Catchment 314 Pervious Impervious Total Area "			"	1 SCS method"				
"	Surface Area 1.650 1.650 3.300 hectare"			"	304 No description"				
"	Time of concentration 11.803 2.102 5.940 minutes"			"	50.000 % Impervious"				
"	Time to Centroid 232.929 202.091 214.292 minutes"			"	1.600 Total Area"				
"	Rainfall depth 108.800 108.800 108.800 mm"			"	75.000 Flow length"				
"	Rainfall volume 1795.20 1795.20 3590.40 c.m"			"	2.000 Overland Slope"				
"	Rainfall losses 42.035 6.813 24.424 mm"			"	0.800 Pervious Area"				
"	Runoff depth 66.765 101.987 84.376 mm"			"	75.000 Pervious length"				
"	Runoff volume 1101.62 1682.79 2784.41 c.m"			"	2.000 Pervious slope"				
"	Runoff coefficient 0.614 0.937 0.776 "			"	0.800 Impervious Area"				
"	Maximum flow 0.306 0.387 0.694 c.m/sec"			"	75.000 Impervious length"				
40	HYDROGRAPH Add Runoff "			"	2.000 Impervious slope"				
"	4 Add Runoff "	0.694	2.089	1.395	0.200 Pervious Manning 'n'"				
"	0.694 2.089 1.395 6.137"			"	82.000 Pervious SCS Curve No."				
52	CHANNEL DESIGN"			"	0.615 Pervious Runoff coefficient"				
"	2.089 Current peak flow c.m/sec"			"	0.100 Pervious Ia/S coefficient"				
"	0.040 Manning 'n'"			"	5.576 Pervious Initial abstraction"				
"	0. Cross-section type: 0=trapezoidal; 1=general"			"	0.013 Impervious Manning 'n'"				
"	2.000 Basewidth metre"			"	98.000 Impervious SCS Curve No."				
"	3.000 Left bank slope"			"	0.926 Impervious Runoff coefficient"				
"	3.000 Right bank slope"			"	0.100 Impervious Ia/S coefficient"				
"	5.000 Channel depth metre"			"	0.518 Impervious Initial abstraction"				
"	2.000 Gradient %"			"	0.319 0.000 0.935 3.017 c.m/sec"				
"	Depth of flow	0.415	metre"	"	Catchment 304 Pervious Impervious Total Area "				
"	Velocity	1.553	m/sec"	"	Surface Area 0.800 0.800 1.600 hectare"				
"	Channel capacity	557.696	c.m/sec"	"	Time of concentration 21.189 3.773 10.724 minutes"				
"	Critical depth	0.392	metre"	"	Time to Centroid 244.317 203.918 220.040 minutes"				
53	ROUTE Channel Route 80"			"	Rainfall depth 108.800 108.800 108.800 mm"				
"	80.00 Channel Route 80 Reach length (metre)"			"	Rainfall volume 870.40 870.40 1740.80 c.m"				
"	0.433 X-factor <= 0.5"			"	Rainfall losses 41.871 8.015 24.943 mm"				
"	38.643 K-lag (seconds)"			"	Runoff depth 66.929 100.785 83.857 mm"				
"	0.000 Default(0) or user spec.(1) values used"			"	Runoff volume 535.43 806.28 1341.71 c.m"				
"	0.500 X-factor <= 0.5"			"	Runoff coefficient 0.615 0.926 0.771 "				
"	30.000 K-lag (seconds)"			"	Maximum flow 0.150 0.187 0.319 c.m/sec"				
"	0.500 Beta weighting factor"			40	HYDROGRAPH Add Runoff "				
"	42.857 Routing time step (seconds)"			"	4 Add Runoff "	0.319	0.935	3.017"	
"	1 No. of sub-reaches"			"					
"	Peak outflow	2.083	c.m/sec"	52	CHANNEL DESIGN"				
"	0.694 2.089 2.083 6.137 c.m/sec"			"	0.319 Current peak flow c.m/sec"				
40	HYDROGRAPH Combine 7000"			"	0.020 Manning 'n'"				
"	6 Combine "			"	0. Cross-section type: 0=trapezoidal; 1=general"				
"	7000 Node #"			"	4.000 Basewidth metre"				
"				"	50.000 Left bank slope"				
"	Maximum flow	2.083	c.m/sec"	"	0.000 Right bank slope"				
"	Hydrograph volume	8942.320	c.m"	"	0.600 Channel depth metre"				
"	0.694 2.089 2.083 2.083"			"	2.000 Gradient %"				
40	HYDROGRAPH Start - New Tributary"			"	Depth of flow	0.062	metre"		
"	2 Start - New Tributary"			"	Velocity	0.932	m/sec"		
"	0.694 0.000 2.083 2.083"			"	Channel capacity	38.450	c.m/sec"		
33	CATCHMENT 312"			"	Critical depth	0.074	metre"		
"	1 Triangular SCS"			53	ROUTE Channel Route 50"				
"	1 Equal length"			"	50.00 Channel Route 50 Reach length (metre)"				
"	1 SCS method"			"	0.483 X-factor <= 0.5"				
"	312 No description"			"	40.227 K-lag (seconds)"				
75.000	% Impervious"			"	0.000 Default(0) or user spec.(1) values used"				
4.400	Total Area"			"	0.500 X-factor <= 0.5"				
100.000	Flow length"			"	30.000 K-lag (seconds)"				
2.000	Overland Slope"			"	0.500 Beta weighting factor"				
1.100	Pervious Area"			"	37.500 Routing time step (seconds)"				
100.000	Pervious length"			"	1 No. of sub-reaches"				
2.000	Pervious slope"			"	Peak outflow	0.317	c.m/sec"		
3.300	Impervious Area"			"	0.319 0.319 0.317 3.017 c.m/sec"				
100.000	Impervious length"			40	HYDROGRAPH Next link "				
"	2.000 Impervious slope"			"	5 Next link "	0.317	0.317	3.017"	
"	0.200 Pervious Manning 'n'"			"	0.319 0.317 0.317 3.017"				
"	82.000 Pervious SCS Curve No."			33	CATCHMENT 313"				
"	0.615 Pervious Runoff coefficient"			"	1 Triangular SCS"				
"	0.100 Pervious Ia/S coefficient"			"	1 Equal length"				
"	5.576 Pervious Initial abstraction"			"	1 SCS method"				
"	0.013 Impervious Manning 'n'"			"	313 No description"				
"	98.000 Impervious SCS Curve No."			"	75.000 % Impervious"				
"	0.938 Impervious Runoff coefficient"			"	1.800 Total Area"				
"	0.100 Impervious Ia/S coefficient"			"	50.000 Flow length"				
"	0.518 Impervious Initial abstraction"			"	2.000 Overland Slope"				
"	0.940 0.000 2.083 2.083 c.m/sec"			"	0.450 Pervious Area"				
"	Catchment 312 Pervious Impervious Total Area "			"	50.000 Pervious length"				
"	Surface Area 1.100 3.300 4.400 hectare"			"	2.000 Pervious slope"				
"	Time of concentration 25.181 4.484 8.197 minutes"			"	1.350 Impervious Area"				
"	Time to Centroid 249.147 205.099 213.000 minutes"			"	50.000 Impervious length"				
"	Rainfall depth 108.800 108.800 108.800 mm"			"	2.000 Impervious slope"				
"	Rainfall volume 1196.80 3590.40 4787.20 c.m"			"	0.200 Pervious Manning 'n'"				
"	Rainfall losses 41.862 6.711 15.498 mm"			"	82.000 Pervious SCS Curve No."				

"	0.615	Pervious Runoff coefficient"	"	1.200	0.900	0.500	0.000	0.000"
"	0.100	Pervious Ia/S coefficient"	"	1.700	0.900	15.000	3.000	3.000"
"	5.576	Pervious Initial abstraction"	"	1.	ORIFICES"			
"	0.013	Impervious Manning 'n'"	"		Orifice	Orifice	Orifice Number of"	
"	98.000	Impervious SCS Curve No."	"		invert	coefficient	diameter	orifices"
"	0.933	Impervious Runoff coefficient"	"		0.000	0.630	0.2000	1.000"
"	0.100	Impervious Ia/S coefficient"	"		2.	LAYERS"		
"	0.518	Impervious Initial abstraction"	"		Bottom	Aspect	Bottom	Top
"	0.395	0.317	3.017 c.m/sec"		area	ratio	elevation	Average
"	Catchment 313	Pervious	Impervious Total Area "		5960.000	6.500	0.000	2.000
"	Surface Area	0.450	1.350	1.800	10902.110	4.312	2.000	2.000
"	Time of concentration	16.614	2.959	5.419	Peak outflow		0.325	c.m/sec"
"	Time to Centroid	238.809	203.134	209.564	Maximum level		1.631	metre"
"	Rainfall depth	108.800	108.800	108.800	Maximum storage		12886.288	c.m"
"	Rainfall volume	489.60	1468.80	1958.40	Centroidal lag		20.543	hours"
"	Rainfall losses	41.851	7.287	15.928		0.395	3.709	0.325
"	Runoff depth	66.949	101.513	92.872	" 40	HYDROGRAPH Next link "		0.000 c.m/sec"
"	Runoff volume	301.27	1370.42	1671.69	"	5	Next link "	
"	Runoff coefficient	0.615	0.933	0.854	"		0.395	0.325
"	Maximum flow	0.086	0.319	0.395	" 52	CHANNEL DESIGN"		
" 40	HYDROGRAPH Add Runoff "				"	0.325	Current peak flow	c.m/sec"
"	4	Add Runoff "	0.395	0.712	0.317	3.017"	0.040	Manning 'n'"
"					"	0.	Cross-section type: 0=trapezoidal; 1=general"	
" 52	CHANNEL DESIGN"				"	2.000	Basewidth	metre"
"	0.712	Current peak flow	c.m/sec"		"	3.000	Left bank slope"	
"	0.020	Manning 'n'"			"	3.000	Right bank slope"	
"	0.	Cross-section type: 0=trapezoidal; 1=general"			"	5.000	Channel depth	metre"
"	4.000	Basewidth	metre"		"	1.000	Gradient	%"
"	50.000	Left bank slope"			"		Depth of flow	0.183
"	0.000	Right bank slope"			"		Velocity	0.698
"	0.300	Channel depth	metre"		"		Channel capacity	394.351
"	2.000	Gradient	%"		"		Critical depth	0.130
"		Depth of flow	0.095	metre"	" 53	ROUTE	Channel Route 300"	
"		Velocity	1.181	m/sec"	"	300.00	Channel Route 300	Reach length (metre)"
"		Channel capacity	7.740	c.m/sec"	"	0.466	X-factor <= 0.5"	
"		Critical depth	0.116	metre"	"	161.164	K-lag (seconds)"	
" 53	ROUTE	Channel Route 200"			"	0.000	Default(0) or user spec.(1) values used"	
"	200.00	Channel Route 200	Reach length (metre)"		"	0.500	X-factor <= 0.5"	
"	0.494	X-factor <= 0.5"			"	30.000	K-lag (seconds)"	
"	126.993	K-lag (seconds)"			"	0.500	Beta weighting factor"	
"	0.000	Default(0) or user spec.(1) values used"			"	300.000	Routing time step (seconds)"	
"	0.500	X-factor <= 0.5"			"	2	No. of sub-reaches"	
"	30.000	K-lag (seconds)"			"		Peak outflow	0.325
"	0.500	Beta weighting factor"			"	0.395	0.325	0.325
"	100.000	Routing time step (seconds)"			" 40	HYDROGRAPH	Combine	1100"
"	1	No. of sub-reaches"			"	6	Combine "	
"		Peak outflow	0.700	c.m/sec"	"	1100	Node #"	
"	0.395	0.712	0.700	3.017 c.m/sec"	"		Node taking 200 series - Bottom end of Holtby Drain"	
" 40	HYDROGRAPH	Combine	7000"		"		Maximum flow	25.184
"	7000	Node #"			"		Hydrograph volume	131820.375
"					"		0.395	0.325
"		Maximum flow	3.717	c.m/sec"	" 81	ADD COMMENT=====		
"		Hydrograph volume	16060.994	c.m"	"	1	Lines of comment"	
"		0.395	0.712	3.717"	" 40	Total to Holtby Drain"		
" 40	HYDROGRAPH	Confluence	7000"		"	HYDROGRAPH	Confluence	1100"
"		7	Confluence "		"	7	Confluence "	
"		7000	Node #"		"	1100	Node #"	
"					"		Node taking 200 series - Bottom end of Holtby Drain"	
"		Maximum flow	3.717	c.m/sec"	"		Maximum flow	25.184
"		Hydrograph volume	16060.994	c.m"	"		Hydrograph volume	131820.375
"		0.395	3.717	0.700	" 81	0.395	25.184	0.325
" 52	CHANNEL DESIGN"				"		0.000"	
"	3.717	Current peak flow	c.m/sec"		" 52	CHANNEL DESIGN"		
"	0.040	Manning 'n'"			"	25.184	Current peak flow	c.m/sec"
"	0.	Cross-section type: 0=trapezoidal; 1=general"			"	0.040	Manning 'n'"	
"	2.000	Basewidth	metre"		"	0.	Cross-section type: 0=trapezoidal; 1=general"	
"	3.000	Left bank slope"			"	2.000	Basewidth	metre"
"	3.000	Right bank slope"			"	3.000	Left bank slope"	
"	5.000	Channel depth	metre"		"	3.000	Right bank slope"	
"	2.000	Gradient	%"		"	5.000	Channel depth	metre"
"		Depth of flow	0.556	metre"	"	0.500	Gradient	%"
"		Velocity	1.822	m/sec"	"		Depth of flow	1.855
"		Channel capacity	557.696	c.m/sec"	"		Velocity	1.794
" 53	ROUTE	Channel Route 50"			"		Channel capacity	278.848
"	50.00	Channel Route 50	Reach length (metre)"		"		Critical depth	1.409
"	0.361	X-factor <= 0.5"			" 53	ROUTE	Channel Route 200"	
"	20.587	K-lag (seconds)"			"	200.00	Channel Route 200	Reach length (metre)"
"	0.000	Default(0) or user spec.(1) values used"			"	0.101	X-factor <= 0.5"	
"	0.500	X-factor <= 0.5"			"	83.622	K-lag - (seconds)"	
"	30.000	K-lag (seconds)"			"	0.000	Default(0) or user spec.(1) values used"	
"	0.500	Beta weighting factor"			"	0.500	X-factor <= 0.5"	
"	25.000	Routing time step (seconds)"			"	30.000	K-lag (seconds)"	
"	1	No. of sub-reaches"			"	0.500	Beta weighting factor"	
"		Peak outflow	3.709	c.m/sec"	"	150.000	Routing time step (seconds)"	
" 40	HYDROGRAPH	Next link "	3.709	0.000 c.m/sec"	"	1	No. of sub-reaches"	
"	5	Next link "			"		Peak outflow	25.025
"		0.395	3.709	3.709	" 40	0.395	25.184	25.025
" 81	ADD COMMENT=====				"	HYDROGRAPH	Combine	1300"
"	1	Lines of comment"			"	6	Combine "	
" 54	PROPOSED POND #3"				"	1300	Node #"	
"		POND DESIGN"			"		Node at Holtby Drain"	
"	3.709	Current peak flow	c.m/sec"		"		Maximum flow	32.131
"	2.000	Target outflow	c.m/sec"		"		Hydrograph volume	169008.359
"	16061.0	Hydrograph volume	c.m"		" 40	0.395	25.184	25.025
"	21.	Number of stages"			"	HYDROGRAPH	Confluence	1300"
"	0.000	Minimum water level	metre"		"	7	Confluence "	
"	2.000	Maximum water level	metre"		"	1300	Node #"	
"	0.000	Starting water level	metre"		"		Node at Holtby Drain"	
"	0	Keep Design Data: 1 = True; 0 = False"			"		Maximum flow	32.131
"		Level Discharge	Volume"		"		Hydrograph volume	169008.328
"	0.000	0.000	0.000"		"	0.395	32.131	25.025
"	0.1000	0.00487	607.388"		" 52	CHANNEL DESIGN"		
"	0.2000	0.01603	1237.688"		"	32.131	Current peak flow	c.m/sec"
"	0.3000	0.03579	1891.097"		"	0.040	Manning 'n'"	
"	0.4000	0.04527	2567.818"		"	0.	Cross-section type: 0=trapezoidal; 1=general"	
"	0.5000	0.05309	3268.049"		"	2.000	Basewidth	metre"
"	0.6000	0.05989	3991.990"		"	3.000	Left bank slope"	
"	0.7000	0.06599	4739.842"		"	3.000	Right bank slope"	
"	0.8000	0.07158	5511.804"		"	5.000	Channel depth	metre"
"	0.9000	0.07676	6308.077"		"	0.500	Gradient	%"
"	1.000	0.08161	7128.861"		"		Depth of flow	2.059
"	1.100	0.08619	7974.355"		"		Velocity	1.908
"	1.200	0.09054	8844.760"		"		Channel capacity	278.848
"	1.300	0.1190	9740.274"		" 53		Critical depth	1.580
"	1.400	0.1673	10661.10"		"	ROUTE	Channel Route 50"	
"	1.500	0.2286	11607.44"		"	50.00	Channel Route 50	Reach length (metre)"
"	1.600	0.3003	12579.48"		"	0.000	X-factor <= 0.5"	
"	1.700	0.3810	13577.44"		"	19.658	K-lag (seconds)"	
"	1.800	1.208	14601.51"		"	0.000	Default(0) or user spec.(1) values used"	
"	1.900	2.686	15651.89"		"	0.500	X-factor <= 0.5"	
"	2.000	4.619	16728.78"		"	30.000	K-lag (seconds)"	
"		2.	WEIRS"		"	0.829	Beta weighting factor"	
"		Crest	Weir	Crest		75.000	Routing time step (seconds)"	
"		elevation	coefficient	breadth	Left	1	No. of sub-reaches"	
"				Right			Peak outflow	32.065
"				sideslope				c.m/sec"

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"      0.395 32.131 32.065 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 1000"
" 6 Combine "
" 1000 Node #"
" Node upstream of Penetangore Culvert"
" Maximum flow 148.381 c.m/sec"
" Hydrograph volume 1173038.00 c.m"
" 0.395 32.131 32.065 148.381"
" 81 ADD COMMENT=====
" 2 Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 40 HYDROGRAPH Confluence 1000"
" 7 Confluence "
" 1000 Node #"
" Node upstream of Penetangore Culvert"
" Maximum flow 148.381 c.m/sec"
" Hydrograph volume 1173038.00 c.m"
" 0.395 148.381 32.065 0.000"
" 81 ADD COMMENT=====
" 2 Lines of comment"
" Total discharge to Pipe Arch under Hwy. 21 on the "
" Pentangore Tributary"
" 52 CHANNEL DESIGN"
" 148.381 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; l=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 3.882 metre"
" Velocity 2.801 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 3.150 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 13.386 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.971 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 148.357 c.m/sec"
" 0.395 148.381 148.357 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
" Node Combining All Flow"
" Maximum flow 148.357 c.m/sec"
" Hydrograph volume 1173036.87 c.m"
" 0.395 148.381 148.357 148.357"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 40 HYDROGRAPH Start - New Tributary"
" 2 Start - New Tributary"
" 0.395 0.000 148.357 148.357"
" 40 HYDROGRAPH Confluence 2000"
" 7 Confluence "
" 2000 Node #"
" Flow in Hwy. 21 Ditch"
" Maximum flow 6.137 c.m/sec"
" Hydrograph volume 55406.535 c.m"
" 0.395 6.137 148.357 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total discharge to Hwy. 21 Ditch"
" 52 CHANNEL DESIGN"
" 6.137 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; l=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 0.988 metre"
" Velocity 1.250 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 0.701 metre"
" 53 ROUTE Channel Route 100"
" 100.00 Channel Route 100 Reach length ( metre)"
" 0.042 X-factor <= 0.5"
" 59.985 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.500 Beta weighting factor"
" 100.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 6.133 c.m/sec"
" 0.395 6.137 6.133 0.000 c.m/sec"
" 40 HYDROGRAPH Combine 3000"
" 6 Combine "
" 3000 Node #"
" Node Combining All Flow"
" Maximum flow 153.706 c.m/sec"
" Hydrograph volume 1228439.12 c.m"
" 0.395 6.137 6.133 153.706"
" 40 HYDROGRAPH Confluence 3000"
" 7 Confluence "
" 3000 Node #"
" Node Combining All Flow"
" Maximum flow 153.706 c.m/sec"
" Hydrograph volume 1228439.12 c.m"
" 0.395 153.706 6.133 0.000"
" 81 ADD COMMENT=====
" 1 Lines of comment"
" Total Off-site Discharge - Hwy. 21 + Penetangore Tributary"
" 52 CHANNEL DESIGN"
" 153.706 Current peak flow c.m/sec"
" 0.040 Manning 'n'"
" 0. Cross-section type: 0=trapezoidal; l=general"
" 2.000 Basewidth metre"
" 3.000 Left bank slope"
" 3.000 Right bank slope"
" 5.000 Channel depth metre"
" 0.500 Gradient %"
" Depth of flow 3.937 metre"
" Velocity 2.826 m/sec"
" Channel capacity 278.848 c.m/sec"
" Critical depth 3.199 metre"
" 53 ROUTE Channel Route 50"
" 50.00 Channel Route 50 Reach length ( metre)"
" 0.000 X-factor <= 0.5"
" 13.268 K-lag ( seconds)"
" 0.000 Default(0) or user spec.(1) values used"
" 0.500 X-factor <= 0.5"
" 30.000 K-lag ( seconds)"
" 0.974 Beta weighting factor"
" 75.000 Routing time step ( seconds)"
" 1 No. of sub-reaches"
" Peak outflow 153.694 c.m/sec"
" 0.395 153.706 153.694 0.000 c.m/sec"
" 38 START/RE-START TOTALS 3000"
" 1 Runoff Totals turned OFF"
" Catchment area to node 3000 1918.200 hectare"
" Impervious area to node 3000 40.592 hectare"
" % impervious to node 3000 0.000"
" Peak runoff to node 3000 0.000 c.m/sec"
" Total volume to node 3000 0.0 c.m"
" 38 START/RE-START TOTALS 3000"
" 1 Runoff Totals turned ON"
" Catchment area to node 3000 1918.200 hectare"
" Impervious area to node 3000 40.592 hectare"
" % impervious to node 3000 2.116"
" Peak runoff to node 3000 231.535 c.m/sec"
" Total volume to node 3000 1240259.9 c.m"

```

APPENDIX G

SURFACE WATER MANAGEMENT FACILITY DESIGN AND RELATED CALCULATIONS

SWM Facility Design Calculations
Wet Pond SWM Facility Configuration and Water Quality Requirements

KINCARDINE BUSINESS PARK
Municipality of Kincardine
08055

Water Quality Volume Requirements for a Wet Pond as per MOE Stormwater Management Planning and Design Manual, Table 3.2.

SWM Facility Requirements

		<u>Pond #2</u>	<u>Pond #3</u>
Protection Level	=	Enhanced (Level 1)	Enhanced (Level 1)
Total Drainage Area	=	56.00 ha	17.70 ha
Total Impervious Area	=	20.30 ha	12.20 ha
% Impervious	=	36.0 %	69.0 %
Required Wet Pond Storage Req. for Impervious Level (MOE Design Manual - Table 3.2)	=	143 m ³ /ha	223 m ³ /ha
Required Water Quality Volume, Wet Pond	=	7,980 m ³	3,941 m ³
Permanent Pool Volume Required	=	5,740 m ³	3,233 m ³
Extended Detention Volume Required	=	2,240 m ³	708 m ³

Table 3.2 - MOE Guidelines

Storage Volume for Percent Impervious - Enhanced					
Imp	35	55	70	85	%
Volume	140	190	225	250	m ³ /Ha
Calculated Storage Volume = Requirements	143 m ³ /Ha			Pond #2	
	223 m ³ /Ha			Pond #3	

Pond Dimensions

				<u>Pond #2</u>		<u>Pond #3</u>	
				Length (m)	Width (m)	Length (m)	Width (m)
- Forebay	Bottom of Pond	=	81.0	25.0	65.0	5.0	
	Top of Permanent Pool	=	90.0	35.0	75.0	12.0	
	Top of Pond	=	100.0	55.0	95.0	32.0	
- Main Pond	Bottom of Pond	=	131.0	30.0	78.0	47.0	
	Top of Permanent Pool	=	141.0	44.0	88.0	57.0	
	Top of Pond	=	160.0	65.0	100.0	77.0	

Length to Width Ratio

- Forebay	=	2.6 :1	6.3 :1
- Overall	=	5.3 :1	2.9 :1

Elevation Details

- Pond Bottom Elevation	=	0.00 m	0.00 m
- Permanent Pool Depth	=	1.00 m	1.00 m
- Top of Permanent Pool Depth	=	1.00 m	1.00 m
- Total Pond Depth	=	3.30 m	3.00 m
- Top of Pond Elevation	=	3.30 m	3.00 m
- Water Quality Extended Detention Depth	=	0.45 m	0.37 m
- Water Quality E.D. Elevation	=	1.45 m	1.37 m
- Permanent Pool Side Slopes	=	5 :1	5 :1
- Extended Detention Side Slopes	=	5 :1	5 :1

Pond Volumes

				Volumes (m³)		Volumes (m³)	
				Actual	Req.d	Actual	Req.d
- Total Pond Volume Available - Water Quality	=	11775	7980	7342	3941.2		
- Total Permanent Pool Volume	=	7450	5740	4900	3233.2		
- Total Extended Detention Volume - Water Quality	=	4325	2240	2442	708		

Surface Areas Provided in the SWM Facility at Various Water Levels

						<u>Pond #2</u>		<u>Pond #3</u>	
						Main	Forebay	Main	Forebay
						m ²	m ²	m ²	m ²
- Bottom						4,100	1,900	3,400	400
- Top Permanent Pool						5,850	3,050	4,650	1,350
- Extended Detention						6,588	3,590	5,168	1,720
- 0.50m height above Permanent Pool						6,670	3,650	5,350	1,850
- 1.0m height above Permanent Pool						7,750	4,250	6,100	2,300
- 1.50m height above Permanent Pool						8,650	4,900	6,800	2,700
- 2.0m height above Permanent Pool						9,750	5,650	7,600	3,200

Ponding Volumes Provided in the SWM Facility at Various Water Levels Above the Permanent Pool
(Active Storage Only - Permanent Pool Volume Not Included)

	<u>Pond #2</u>			
	Main	Forebay	Incr. Total	Cum. Total
	m ³	m ³	m ³	m ³
- Top Permanent Pool	0	0	0	0
- 0.50m height above Permanent Pool	3,130	1,675	4,805	4,805
- 1.0m height above Permanent Pool	3,605	1,975	5,580	10,385
- 1.50m height above Permanent Pool	4,100	2,288	6,388	16,773
- 2.0m height above Permanent Pool	4,600	2,638	7,238	24,010

	<u>Pond #3</u>			
	Main	Forebay	Incr. Total	Cum. Total
	m ³	m ³	m ³	m ³
- Top Permanent Pool	0	0	0	0
- 0.50m height above Permanent Pool	2,500	800	3,300	3,300
- 1.0m height above Permanent Pool	2,863	1,038	3,900	7,200
- 1.50m height above Permanent Pool	3,225	1,250	4,475	11,675
- 2.0m height above Permanent Pool	3,600	1,475	5,075	16,750

SWM Wet Pond Forebay Sizing

KINCARDINE BUSINESS PARK
Municipality of Kincardine
08055

Forebay sizing as per MOE Stormwater Management Planning and Design Manual

Surface Area

Forebay surface area to be < 33% of total pond surface area.

Pond #2

Total pond surface area @ extended detention elevation	=	10178 m ²
Forebay surface area @ extended detention elevation	=	3590 m ²
Forebay area as a % of total pond area	=	35 %

Pond #3

Total pond surface area @ extended detention elevation	=	6888 m ²
Forebay surface area @ extended detention elevation	=	1720 m ²
Forebay area as a % of total pond area	=	25 %

Settling

$$\text{Settling Distance} = (rQ_p/V_s)^{1/2}$$

where:	r	=	L to W ratio average
	Q _p	=	Peak Flow Rate from the pond - 25mm storm
	V _s	=	settling velocity for 0.15m particles (0.003 m/s)

Pond #2

r	=	2.6
Q _p	=	0.08 m ³ /s
V _s	=	0.0003 m/s

Therefore,

$$\text{Settling Distance} = 26.3 \text{ m} \quad \text{Actual} = 35 \text{ m}$$

Pond #3

r	=	6.3
Q _p	=	0.043 m ³ /s
V _s	=	0.0003 m/s

Therefore,

$$\text{Settling Distance} = 30.0 \text{ m} \quad \text{Actual} = 75 \text{ m}$$

Dispersion Length

$$\text{Dispersion Length} = 8Q/DV_f$$

where:	Q	=	inlet flow (m ³ /s) - Quality Storm
	d	=	depth of permanent pool in forebay (m), (Assume min. depth of 0.8m)

Pond #2

$$\begin{aligned} Q &= 0.937 \text{ m}^3/\text{s} \\ d &= 0.8 \text{ m} \\ V_f &= 0.5 \text{ m/s} \end{aligned}$$

Therefore,

$$\text{Dispersion Length} = 18.7 \text{ m} \quad \text{Actual} = 35 \text{ m}$$

Pond #3

$$\begin{aligned} Q &= 0.662 \text{ m}^3/\text{s} \\ d &= 0.8 \text{ m} \\ V_f &= 0.5 \text{ m/s} \end{aligned}$$

Therefore,

$$\text{Dispersion Length} = 13.2 \text{ m} \quad \text{Actual} = 75 \text{ m}$$

Cleanout Frequency

$$\text{Cleanout Frequency} = \text{Vol} / (\text{Load})(A \text{ sed.})(\text{eff.})$$

where:

$$\begin{aligned} \text{Vol} &= \text{Volume of allowable sediment} \\ \text{Load} &= \text{sediment loading (m}^3/\text{ha)} \\ \text{eff.} &= \text{Removal Efficiency (60\%)} \end{aligned}$$

Pond #2

$$\begin{aligned} \text{Allowable Sediment Depth} &= 0.2 \text{ m} \\ \text{Actual Forebay Length} &= 90 \text{ m} \\ \text{Actual Forebay Width} &= 55 \text{ m} \\ \text{Side Slopes} &= 5 \\ \text{Contributing Area} &= 56.00 \text{ ha} \\ \\ \text{Volume of Allowable Sediment} &= 1019 \text{ m}^3 \\ \text{Sediment Loading} &= 1.90 \text{ m}^3/\text{ha} \end{aligned}$$

Therefore,

$$\text{Cleanout Frequency} = 16.0 \text{ years}$$

Pond #3

$$\begin{aligned} \text{Allowable Sediment Depth} &= 0.2 \text{ m} \\ \text{Actual Forebay Length} &= 75 \text{ m} \\ \text{Actual Forebay Width} &= 12 \text{ m} \\ \text{Side Slopes} &= 5 \\ \text{Contributing Area} &= 17.70 \text{ ha} \\ \\ \text{Volume of Allowable Sediment} &= 197 \text{ m}^3 \\ \text{Sediment Loading} &= 2.80 \text{ m}^3/\text{ha} \end{aligned}$$

Therefore,

$$\text{Cleanout Frequency} = 6.6 \text{ years}$$

Detention Time

$$\text{Detention Time} = \frac{2 A_p}{C A_o (2g)^{0.50}} (h_1 - h_2)^{0.50}$$

where: A_o = cross-sectional area of orifice
 A_p = surface area of pond at storage level (permanent pool)
 C = discharge coefficient (0.65)
 h_1 = starting water elevation above orifice
 h_2 = ending water elevation above orifice

Pond #2

A_o = 0.0314 m² 200 mm
 A_p = 8900 m²
 C = 0.65
 h_1 = 0.45 m
 h_2 = 0 m

Therefore, t = 132,079 secs.
= 37 hrs.

Pond #3

A_o = 0.0314 m² 200 mm
 A_p = 6000 m²
 C = 0.65
 h_1 = 0.37 m
 h_2 = 0 m

Therefore, t = 80,740 secs.
= 22 hrs.

Stage Storage Relationship for Proposed Stormwater Management Facilities (Pond #2 and Pond #3)

KINCARDINE BUSINESS PARK
Municipality of Kincardine
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POND #2							
Pond Control Structure (Orifice / Weir) Rating Calculations							
Height Above PP m	Elev m	Pond Volume m ³	Calculated Discharge				Total Miduss Discharge m ³ /s
			Orifice 1 m ³ /s	Control Weir m ³ /s	Overflow Weir m ³ /s	TOTAL m ³ /s	
-1.00	0.00	-	-	-	-	-	-
-0.90	0.10	-	-	-	-	-	-
-0.80	0.20	-	-	-	-	-	-
-0.70	0.30	-	-	-	-	-	-
-0.60	0.40	-	-	-	-	-	-
-0.50	0.50	-	-	-	-	-	-
-0.40	0.60	-	-	-	-	-	-
-0.30	0.70	-	-	-	-	-	-
-0.20	0.80	-	-	-	-	-	-
-0.10	0.90	-	-	-	-	-	-
0.00	1.00	0	0.000	-	-	0.000	0.000
0.10	1.10	876	0.004	-	-	0.004	0.004
0.19	1.19	1778	0.014	-	-	0.014	0.015
0.29	1.29	2707	0.037	-	-	0.037	0.034
0.38	1.38	3662	0.045	-	-	0.045	0.043
0.48	1.48	4645	0.052	-	-	0.052	0.052
0.57	1.57	5655	0.058	-	-	0.058	0.058
0.67	1.67	6692	0.064	-	-	0.064	0.064
0.77	1.77	7758	0.069	-	-	0.069	0.069
0.86	1.86	8850	0.074	-	-	0.074	0.074
0.96	1.96	9971	0.079	-	-	0.079	0.080
1.05	2.05	11118	0.083	-	-	0.083	0.084
1.15	2.15	12297	0.087	0.000	-	0.087	0.088
1.25	2.25	13505	0.091	0.136	-	0.226	0.229
1.34	2.34	14741	0.095	0.380	-	0.475	0.483
1.44	2.44	16006	0.098	0.697	-	0.795	0.811
1.53	2.53	17287	0.102	1.072	-	1.174	1.195
1.63	2.63	18611	0.105	1.497	-	1.602	1.633
1.72	2.72	19963	0.108	1.967	-	2.075	2.118
1.82	2.82	21346	0.111	2.478	-	2.589	2.644
1.92	2.92	22758	0.114	3.026	-	3.141	3.209
2.01	3.01	24200	0.117	3.610	0.042	3.769	3.811
2.11	3.11	25657	0.120	4.228	1.069	5.417	5.348
2.20	3.20	27160	0.123	4.877	2.766	7.766	7.723
2.30	3.30	28692	0.126	5.556	4.928	10.610	10.675
Discharge Structure		Height to Inv. m	Dia/Length mm	Area m ²	Coefficient		
Orifice 1		0.00	200	0.03140	0.61		
Control Weir		1.15	3000	n/a	1.50		
Overflow Weir		2.00	20000	n/a	1.50		

POND #3

Pond Control Structure (Orifice / Weir) Rating Calculations

Height Above PP m	Elev m	Pond Volume m ³	Calculated Discharge				Total Miduss Discharge m ³ /s
			Orifice 1 m ³ /s	Control Weir m ³ /s	Overflow Weir m ³ /s	TOTAL m ³ /s	
-1.00	0.00	-	-	-	-	-	-
-0.90	0.10	-	-	-	-	-	-
-0.80	0.20	-	-	-	-	-	-
-0.70	0.30	-	-	-	-	-	-
-0.60	0.40	-	-	-	-	-	-
-0.50	0.50	-	-	-	-	-	-
-0.40	0.60	-	-	-	-	-	-
-0.30	0.70	-	-	-	-	-	-
-0.20	0.80	-	-	-	-	-	-
-0.10	0.90	-	-	-	-	-	-
0.00	1.00	0	0.000	-	-	0.000	0.000
0.10	1.10	607	0.005	-	-	0.005	0.005
0.20	1.20	1238	0.016	-	-	0.016	0.016
0.30	1.30	1891	0.038	-	-	0.038	0.036
0.40	1.40	2568	0.046	-	-	0.046	0.045
0.50	1.50	3268	0.054	-	-	0.054	0.053
0.60	1.60	3992	0.060	-	-	0.060	0.060
0.70	1.70	4740	0.066	-	-	0.066	0.066
0.80	1.80	5511	0.071	-	-	0.071	0.072
0.90	1.90	6308	0.076	-	-	0.076	0.077
1.00	2.00	7129	0.080	-	-	0.080	0.082
1.10	2.10	7975	0.085	-	-	0.085	0.086
1.20	2.20	8845	0.089	0.000	-	0.089	0.091
1.30	2.30	9740	0.093	0.024	-	0.117	0.119
1.40	2.40	10661	0.097	0.068	-	0.164	0.167
1.50	2.50	11607	0.100	0.124	-	0.224	0.229
1.60	2.60	12580	0.104	0.191	-	0.295	0.300
1.70	2.70	13577	0.107	0.267	0.000	0.374	0.381
1.80	2.80	14602	0.111	0.351	0.762	1.224	1.208
1.90	2.90	15652	0.114	0.442	2.156	2.712	2.686
2.00	3.00	16729	0.117	0.540	3.961	4.618	4.619
Discharge Structure		Height to Inv. m	Dia/Length mm	Area m ²	Coefficient		
Orifice 1		0.00	200	0.03140	0.61		
Control Weir		1.20	500	n/a	1.51		
Overflow Weir		1.70	15000	n/a	1.61		

**Comparison of Pre to Post Flow Results
at Various Locations**

KINCARDINE BUSINESS PARK
Municipality of Kincardine
08055

PRE-EXISTING CONDITIONS				
FLOW SUMMARY (m³/s)				
Storm Event	Holtby Drain at Confluence with Pen. Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	3.3	1.9	16.9	17.4
5	7.8	4.5	41.7	43.0
10	11.6	6.6	63.0	65.0
25	17.1	9.4	94.6	97.6
50	21.5	11.6	120.8	124.7
100	26.2	13.6	149.0	153.6

POST DEVELOPMENT CONDITIONS				
FLOW SUMMARY (m³/s)				
Storm Event	Holtby Drain at Confluence with Pen. Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	3.1	0.6	16.8	17.1
5	7.4	1.3	41.5	42.3
10	11.1	2.0	62.7	64.4
25	16.3	3.6	94.1	97.2
50	20.5	4.8	120.2	124.5
100	25.5	6.1	148.4	153.7

FLOW COMPARISON				
% CHANGE				
Storm Event	Holtby Drain at Confluence with Pen. Tributary (Confluence 1100)	A 1500mm CSP under Hwy. 21 (Confluence 2000)	B Multi-Plate Arch under Hwy. 21 (Confluence 1000)	A+B Combined at Hwy. 21 (Confluence 3000)
2	-4.9	-69.1	-0.3	-2.0
5	-5.3	-71.2	-0.4	-1.7
10	-4.6	-69.7	-0.5	-1.0
25	-4.9	-61.6	-0.5	-0.4
50	-4.8	-58.5	-0.5	-0.2
100	-2.7	-55.3	-0.4	0.1

APPENDIX H

**MAINTENANCE REPORT ON
EROSION PROTECTION**

**MAINTENANCE REPORT ON EROSION PROTECTION
KINCARDINE BUSINESS PARK
STORMWATER MANAGEMENT FACILITIES**

Date	Inspector	Status of Control Measures		Comments	
		Silt Fence	Catchbasin Sumps	Action to be Taken	Action Verified

This report to be kept on file and available for review.
 Completion inspection to be undertaken monthly and after a significant rainfall event.
 Action required on erosion control unit must be relayed to owner of development.

APPENDIX I
PROBABLE COST WORKSHEETS

SUMMARY - PROJECT COSTS

SERVICING COMPONENT	COST			Total
	Items	Engineering	Contingency	
Internal Servicing				
Roads	\$3,077,000	\$462,000	\$462,000	\$4,001,000
Storm Sewer	\$1,491,000	\$224,000	\$224,000	\$1,939,000
Stormwater Management	\$528,000	\$79,000	\$79,000	\$686,000
Sanitary Sewer	\$739,000	\$111,000	\$111,000	\$961,000
Watermain	\$836,000	\$125,000	\$125,000	\$1,086,000
TOTAL - Internal Servicing	\$6,671,000	\$1,001,000	\$1,001,000	\$8,673,000
External / Other Servicing				
Russell Street Sanitary Sewer	\$510,000	\$41,000	\$76,000	\$627,000
Park Street Pumping Station Upgrades	\$730,000	\$110,000	\$110,000	\$950,000
Hwy. 21 Improvements	\$475,000	\$71,000	\$71,000	\$617,000
Water Booster Station	\$615,000	\$92,000	\$92,000	\$799,000
TOTAL - External / Other Servicing	\$2,330,000	\$314,000	\$349,000	\$2,993,000
TOTAL - PROJECT COSTS	\$9,001,000	\$1,315,000	\$1,350,000	\$11,666,000

MUNICIPALITY OF KINCARDINE
BMROSS JOB No. 08055
PHASE 1 SERVICING
PRELIMINARY PROBABLE COST ESTIMATE

08055
 June 2016
 DLE

Item	Description	Qty./Unit	Price	Amount	Rounded
ROADS					
1	a) 8.5m Road Width	320 m	\$1,130	\$361,600	\$362,000
	b) 10.5m Road Width	370 m	\$1,270	\$469,900	\$470,000
	Sub-Total -- Roads			\$831,500	\$832,000
	Engineering	15 %		\$124,725	\$125,000
	Contingency	15 %		\$124,725	\$125,000
	Total -- Roads			\$1,080,950	\$1,082,000

STORM SEWER					
1	a) 300mm Pipe	140 m	\$185	\$25,900	\$26,000
	b) 375mm Pipe	m	\$200	\$0	\$0
	c) 450mm Pipe	235 m	\$240	\$56,400	\$56,000
	d) 525mm Pipe	180 m	\$250	\$45,000	\$45,000
	e) 600mm Pipe	265 m	\$280	\$74,200	\$74,000
	f) 675mm Pipe	170 m	\$430	\$73,100	\$73,000
	g) 750mm Pipe	90 m	\$470	\$42,300	\$42,000
	h) 825mm Pipe	100 m	\$480	\$48,000	\$48,000
	i) 900mm Pipe	100 m	\$500	\$50,000	\$50,000
	j) 975mm Pipe	m	\$600	\$0	\$0
	k) 1050mm Pipe	m	\$750	\$0	\$0
	l) 1200mm Pipe	m	\$800	\$0	\$0
2	a) 1200mm MH	6 Ea.	\$3,600	\$21,600	\$22,000
	b) 1500mm MH	6 Ea.	\$5,500	\$33,000	\$33,000
	c) 1800mm MH	Ea.	\$7,900	\$0	\$0
	d) 2400mm MH	2 Ea.	\$10,000	\$20,000	\$20,000
	e) 3000mm MH	Ea.	\$19,000	\$0	\$0
3	a) Catchbasins	21 Ea.	\$1,800	\$37,800	\$38,000
	b) 300mm Pipe	105 m	\$185	\$19,425	\$19,000
	Sub-Total -- Storm Sewer			\$546,725	\$546,000
	Engineering	15 %		\$82,009	\$82,000
	Contingency	15 %		\$82,009	\$82,000
	Total -- Storm Sewer			\$710,743	\$710,000

STORMWATER MANAGEMENT (SWM)					
1	Clearing and Grubbing	1 LS	\$10,000	\$10,000	\$10,000
2	Stripping	15000 m ³	\$3	\$37,500	\$38,000
3	Earthwork	35000 m ³	\$5	\$157,500	\$158,000
4	Topsoil	20000 m ²	\$1	\$15,000	\$15,000

5	Seed and Mulch	20000 m ³	\$1	\$10,000	\$10,000
6	Discharge Structure and Outlet Pipe	1 LS	\$35,000	\$35,000	\$35,000
7	Pond Subdrain	250 m	\$20	\$5,000	\$5,000
8	Rip-Rap Protection	1 LS	\$15,000	\$15,000	\$15,000
9	Cable Concrete Entry Lane and Granular Forebay Bottom	1 LS	\$10,000	\$10,000	\$10,000
Sub-Total -- Stormwater Management				\$295,000	\$296,000
	Engineering	15 %		\$44,250	\$44,000
	Contingency	15 %		\$44,250	\$44,000
Total -- Stormwater Management				\$383,500	\$384,000

SANITARY

1	a) 200mm Pipe	0 m	\$200	\$0	\$0
	b) 250mm Pipe	140 m	\$200	\$28,000	\$28,000
	c) 300mm Pipe	860 m	\$230	\$197,800	\$198,000
2	1200mm MH	11 Ea.	\$4,400	\$48,400	\$48,000
3	a) Services	11 Ea.	\$1,900	\$20,900	\$21,000
	b) Cleanouts	11 Ea.	\$400	\$4,400	\$4,000
Sub-Total -- Sanitary Sewer				\$299,500	\$299,000
	Engineering	15 %		\$44,925	\$45,000
	Contingency	15 %		\$44,925	\$45,000
Total -- Sanitary Sewer				\$389,350	\$389,000

WATERMAIN

1	a) 150mm Pipe	75 m	\$140	\$10,500	\$11,000
	b) 200mm Pipe	0 m	\$190	\$0	\$0
	c) 250mm Pipe	0 m	\$200	\$0	\$0
	c) 300mm Pipe	1100 m	\$250	\$275,000	\$275,000
2	Highway No. 21 Jack and Bore and Casing Pipe	30 m	\$1,500	\$45,000	\$45,000
3	Hydrant Assemblies	6 Ea.	\$5,000	\$30,000	\$30,000
4	a) Tees	6 Ea.	\$1,500	\$9,000	\$9,000
	b) Valves	6 Ea.	\$2,500	\$15,000	\$15,000
Sub-Total -- Watermain				\$384,500	\$385,000
	Engineering	15 %		\$57,675	\$58,000
	Contingency	15 %		\$57,675	\$58,000
Total -- Watermain				\$499,850	\$501,000

EXTERNAL / OTHER

1	Russell Street Sanitary Sewer	1 LS	\$509,500	\$509,500	\$510,000
	Engineering	8 %		\$40,760	\$41,000
	Contingency	15 %		\$76,425	\$76,000
	Sub-Total -- Russell Street Sanitary			\$626,685	\$627,000
2	Park Street Pumping Station Upgrades	1 LS	\$730,000	\$730,000	\$730,000
	Engineering	15 %		\$109,500	\$110,000
	Contingency	15 %		\$109,500	\$110,000
	Sub-Total -- Park Street Pumping Station			\$949,000	\$950,000
	Total -- External / Other			\$1,575,685	\$1,577,000

SUMMARY - PHASE 1 COSTS

SERVICING COMPONENT	Items	COST		Total
		Engineering	Contingency	
Internal Servicing				
Roads	\$832,000	\$125,000	\$125,000	\$1,082,000
Storm Sewer	\$546,000	\$82,000	\$82,000	\$710,000
Stormwater Management	\$296,000	\$44,000	\$44,000	\$384,000
Sanitary Sewer	\$299,000	\$45,000	\$45,000	\$389,000
Watermain	\$385,000	\$58,000	\$58,000	\$501,000
TOTAL - Internal Servicing	\$2,358,000	\$354,000	\$354,000	\$3,066,000
External / Other Servicing				
Russell Street Sanitary	\$510,000	\$41,000	\$76,000	\$627,000
Park Street Pumping Station	\$730,000	\$110,000	\$110,000	\$950,000
TOTAL - External / Other Servicing	\$1,240,000	\$151,000	\$186,000	\$1,577,000
TOTAL - PHASE 1 COSTS	\$3,598,000	\$505,000	\$540,000	\$4,643,000

MUNICIPALITY OF KINCARDINE
BMROSS JOB No. 08055
PHASE 2 SERVICING
PRELIMINARY PROBABLE COST ESTIMATE

08055
 June 2016
 DLE

Item	Description	Qty./Unit	Price	Amount	Rounded
ROADS					
1	a) 8.5m Road Width	850 m	\$1,130	\$960,500	\$961,000
	b) 10.5m Road Width	300 m	\$1,270	\$381,000	\$381,000
	Sub-Total -- Roads			\$1,341,500	\$1,342,000
	Engineering	15 %		\$201,225	\$201,000
	Contingency	15 %		\$201,225	\$201,000
	Total -- Roads			\$1,743,950	\$1,744,000

STORM SEWER					
1	a) 300mm Pipe	60 m	\$185	\$11,100	\$11,000
	b) 375mm Pipe	75 m	\$200	\$15,000	\$15,000
	c) 450mm Pipe	190 m	\$240	\$45,600	\$46,000
	d) 525mm Pipe	0 m	\$250	\$0	\$0
	e) 600mm Pipe	110 m	\$280	\$30,800	\$31,000
	f) 675mm Pipe	0 m	\$430	\$0	\$0
	g) 750mm Pipe	240 m	\$470	\$112,800	\$113,000
	h) 825mm Pipe	20 m	\$480	\$9,600	\$10,000
	i) 900mm Pipe	70 m	\$500	\$35,000	\$35,000
	j) 975mm Pipe	0 m	\$600	\$0	\$0
	k) 1050mm Pipe	0 m	\$750	\$0	\$0
	l) 1200mm Pipe	300 m	\$800	\$240,000	\$240,000
2	a) 1200mm MH	6 Ea.	\$3,600	\$21,600	\$22,000
	b) 1500mm MH	3 Ea.	\$5,500	\$16,500	\$17,000
	c) 1800mm MH	1 Ea.	\$7,900	\$7,900	\$8,000
	d) 2400mm MH	3 Ea.	\$10,000	\$30,000	\$30,000
	e) 3000mm MH	2 Ea.	\$19,000	\$38,000	\$38,000
					\$0
3	a) Catchbasins	22.5 Ea.	\$1,800	\$40,500	\$41,000
	b) 300mm Pipe	112.5 m	\$185	\$20,813	\$21,000
	Sub-Total -- Storm Sewer			\$675,213	\$678,000
	Engineering	15 %		\$101,282	\$101,000
	Contingency	15 %		\$101,282	\$101,000
	Total -- Storm Sewer			\$877,776	\$880,000

STORMWATER MANAGEMENT (SWM)					
1	Clearing and Grubbing	1 LS	\$10,000	\$10,000	\$10,000
2	Stripping	12000 m ³	\$3	\$30,000	\$30,000
3	Earthwork	24000 m ³	\$5	\$108,000	\$108,000
4	Topsoil	16000 m ²	\$1	\$12,000	\$12,000

5	Seed and Mulch	16000 m ³	\$1	\$8,000	\$8,000
6	Discharge Structure and Outlet Pipe	1 LS	\$35,000	\$35,000	\$35,000
7	Pond Subdrain	200 m	\$20	\$4,000	\$4,000
8	Rip-Rap Protection	1 LS	\$15,000	\$15,000	\$15,000
9	Cable Concrete Entry Lane and Granular Forebay Bottom	1 LS	\$10,000	\$10,000	\$10,000
Sub-Total -- Stormwater Management				\$232,000	\$232,000
	Engineering	15 %		\$34,800	\$35,000
	Contingency	15 %		\$34,800	\$35,000

Total -- Stormwater Management				\$301,600	\$302,000
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SANITARY

1	a) 200mm Pipe	220 m	\$200	\$44,000	\$44,000
	b) 250mm Pipe	590 m	\$200	\$118,000	\$118,000
	c) 300mm Pipe	60 m	\$230	\$13,800	\$14,000
2	1200mm MH	10 Ea.	\$4,400	\$44,000	\$44,000
3	a) Services	10 Ea.	\$1,900	\$19,000	\$19,000
	b) Cleanouts	10 Ea.	\$400	\$4,000	\$4,000
Sub-Total -- Sanitary Sewer				\$242,800	\$243,000
	Engineering	15 %		\$36,420	\$36,000
	Contingency	15 %		\$36,420	\$36,000

Total -- Sanitary Sewer				\$315,640	\$315,000
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WATERMAIN

1	a) 150mm Pipe	130 m	\$140	\$18,200	\$18,000
	b) 200mm Pipe	270 m	\$190	\$51,300	\$51,000
	c) 250mm Pipe	600 m	\$200	\$120,000	\$120,000
	c) 300mm Pipe	100 m	\$250	\$25,000	\$25,000
2	Hydrant Assemblies	6 Ea.	\$5,000	\$30,000	\$30,000
3	a) Tees	6 Ea.	\$1,500	\$9,000	\$9,000
	b) Valves	6 Ea.	\$2,500	\$15,000	\$15,000
Sub-Total -- Watermain				\$268,500	\$268,000
	Engineering	15 %		\$40,275	\$40,000
	Contingency	15 %		\$40,275	\$40,000

Total -- Watermain				\$349,050	\$348,000
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EXTERNAL / OTHER

1	Hwy. 21 Improvements	1 LS	\$475,000	\$475,000	\$475,000
	Engineering	15 %		\$71,250	\$71,000
	Contingency	15 %		\$71,250	\$71,000
	Sub-Total -- Highway 21 Improvements			\$617,500	\$617,000
2	Water Booster Station	1 LS	\$615,000	\$615,000	\$615,000
	Engineering	15 %		\$92,250	\$92,000
	Contingency	15 %		\$92,250	\$92,000
	Sub-Total -- Water Booster Station			\$799,500	\$799,000
	Total -- External / Other			\$1,417,000	\$1,416,000

SUMMARY - PHASE 2 COSTS

SERVICING COMPONENT	Items	COST		Total
		Engineering	Contingency	
Internal Servicing				
Roads	\$1,342,000	\$201,000	\$201,000	\$1,744,000
Storm Sewer	\$678,000	\$101,000	\$101,000	\$880,000
Stormwater Management	\$232,000	\$35,000	\$35,000	\$302,000
Sanitary Sewer	\$243,000	\$36,000	\$36,000	\$315,000
Watermain	\$268,000	\$40,000	\$40,000	\$348,000
TOTAL - Internal Servicing	\$2,763,000	\$413,000	\$413,000	\$3,589,000
External / Other Servicing				
Hwy. 21 Improvements	\$475,000	\$71,000	\$71,000	\$617,000
Water Booster Station	\$615,000	\$92,000	\$92,000	\$799,000
TOTAL - External / Other Servicing	\$1,090,000	\$163,000	\$163,000	\$1,416,000
TOTAL - PHASE 2 COSTS	\$3,853,000	\$576,000	\$576,000	\$5,005,000

MUNICIPALITY OF KINCARDINE
BMROSS JOB No. 08055
PHASE 3 SERVICING
PRELIMINARY PROBABLE COST ESTIMATE

08055
 June 2016
 DLE

Item	Description	Qty./Unit	Price	Amount	Rounded
ROADS					
1	a) 8.5m Road Width	800 m	\$1,130	\$904,000	\$904,000
	b) 10.5m Road Width	0 m	\$1,270	\$0	\$0
	Sub-Total -- Roads			\$904,000	\$904,000
	Engineering	15 %		\$135,600	\$136,000
	Contingency	15 %		\$135,600	\$136,000
	Total -- Roads			\$1,175,200	\$1,176,000

STORM SEWER					
1	a) 300mm Pipe	100 m	\$185	\$18,500	\$19,000
	b) 375mm Pipe	0 m	\$200	\$0	\$0
	c) 450mm Pipe	270 m	\$240	\$64,800	\$65,000
	d) 525mm Pipe	0 m	\$250	\$0	\$0
	e) 600mm Pipe	110 m	\$280	\$30,800	\$31,000
	f) 675mm Pipe	0 m	\$430	\$0	\$0
	g) 750mm Pipe	90 m	\$470	\$42,300	\$42,000
	h) 825mm Pipe	110 m	\$480	\$52,800	\$53,000
	i) 900mm Pipe	0 m	\$500	\$0	\$0
	j) 975mm Pipe	0 m	\$600	\$0	\$0
	k) 1050mm Pipe	0 m	\$750	\$0	\$0
	l) 1200mm Pipe	0 m	\$800	\$0	\$0
2	a) 1200mm MH	5 Ea.	\$3,600	\$18,000	\$18,000
	b) 1500mm MH	1 Ea.	\$5,500	\$5,500	\$6,000
	c) 1800mm MH	1 Ea.	\$7,900	\$7,900	\$8,000
	d) 2400mm MH	0 Ea.	\$10,000	\$0	\$0
	e) 3000mm MH	0 Ea.	\$19,000	\$0	\$0
					\$0
3	a) Catchbasins	11 Ea.	\$1,800	\$19,800	\$20,000
	b) 300mm Pipe	55 m	\$185	\$10,175	\$10,000
	Sub-Total -- Storm Sewer			\$270,575	\$272,000
	Engineering	15 %		\$40,586	\$41,000
	Contingency	15 %		\$40,586	\$41,000
	Total -- Storm Sewer			\$351,748	\$354,000

STORMWATER MANAGEMENT (SWM)					
1	Clearing and Grubbing	0 LS	\$10,000	\$0	\$0
2	Stripping	0 m ³	\$3	\$0	\$0
3	Earthwork	0 m ³	\$5	\$0	\$0
4	Topsoil	0 m ²	\$1	\$0	\$0

5	Seed and Mulch	0 m ³	\$1	\$0	\$0
6	Discharge Structure and Outlet Pipe	0 LS	\$35,000	\$0	\$0
7	Pond Subdrain	0 m	\$20	\$0	\$0
8	Rip-Rap Protection	0 LS	\$15,000	\$0	\$0
9	Cable Concrete Entry Lane and Granular Forebay Bottom	0 LS	\$10,000	\$0	\$0
Sub-Total -- Stormwater Management				\$0	\$0
	Engineering	15 %		\$0	\$0
	Contingency	15 %		\$0	\$0

Total -- Stormwater Management	\$0	\$0
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SANITARY

1	a) 200mm Pipe	650 m	\$200	\$130,000	\$130,000
	b) 250mm Pipe	100 m	\$200	\$20,000	\$20,000
	c) 300mm Pipe	0 m	\$230	\$0	\$0
2	1200mm MH	7 Ea.	\$4,400	\$30,800	\$31,000
3	a) Services	7 Ea.	\$1,900	\$13,300	\$13,000
	b) Cleanouts	7 Ea.	\$400	\$2,800	\$3,000
Sub-Total -- Sanitary Sewer				\$196,900	\$197,000
	Engineering	15 %		\$29,535	\$30,000
	Contingency	15 %		\$29,535	\$30,000

Total -- Sanitary Sewer	\$255,970	\$257,000
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WATERMAIN

1	a) 150mm Pipe	0 m	\$140	\$0	\$0
	b) 200mm Pipe	320 m	\$190	\$60,800	\$61,000
	c) 250mm Pipe	430 m	\$200	\$86,000	\$86,000
	c) 300mm Pipe	0 m	\$250	\$0	\$0
2	Hydrant Assemblies	4 Ea.	\$5,000	\$20,000	\$20,000
3	a) Tees	4 Ea.	\$1,500	\$6,000	\$6,000
	b) Valves	4 Ea.	\$2,500	\$10,000	\$10,000
Sub-Total -- Watermain				\$182,800	\$183,000
	Engineering	15 %		\$27,420	\$27,000
	Contingency	15 %		\$27,420	\$27,000

Total -- Watermain	\$237,640	\$237,000
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EXTERNAL / OTHER

1	Nil	0 LS	\$275,000	\$0	\$0
	Engineering	15 %		\$0	\$0
	Contingency	15 %		\$0	\$0
	Sub-Total --			\$0	\$0
2	Nil	0 LS	\$550,000	\$0	\$0
	Engineering	15 %		\$0	\$0
	Contingency	15 %		\$0	\$0
	Sub-Total --			\$0	\$0
Total -- External / Other				\$0	\$0

SUMMARY - PHASE 3 COSTS

SERVICING COMPONENT	Items	COST		Total
		Engineering	Contingency	
Internal Servicing				
Roads	\$904,000	\$136,000	\$136,000	\$1,176,000
Storm Sewer	\$272,000	\$41,000	\$41,000	\$354,000
Stormwater Management	\$0	\$0	\$0	\$0
Sanitary Sewer	\$197,000	\$30,000	\$30,000	\$257,000
Watermain	\$183,000	\$27,000	\$27,000	\$237,000
TOTAL - Internal Servicing	\$1,556,000	\$234,000	\$234,000	\$2,024,000
External / Other Servicing				
	\$0	\$0	\$0	\$0
	\$0	\$0	\$0	\$0
TOTAL - External / Other Servicing	\$0	\$0	\$0	\$0
TOTAL - PHASE 3 COSTS	\$1,556,000	\$234,000	\$234,000	\$2,024,000

**MUNICIPALITY OF KINCARDINE
BMROSS JOB No. 08055
COMPLETE SERVICING
PRELIMINARY PROBABLE COST ESTIMATE**

08055
June 2016
DLE

Item	Description	Qty./Unit	Price	Amount	Rounded
ROADS					
1	a) 8.5m Road Width	1970 m	\$1,130	\$2,226,100	\$2,226,000
	b) 10.5m Road Width	670 m	\$1,270	\$850,900	\$851,000
	Sub-Total -- Roads			\$3,077,000	\$3,077,000
	Engineering	15 %		\$461,550	\$462,000
	Contingency	15 %		\$461,550	\$462,000
	Total -- Roads			\$4,000,100	\$4,001,000

STORM SEWER					
1	a) 300mm Pipe	300 m	\$185	\$55,500	\$56,000
	b) 375mm Pipe	75 m	\$200	\$15,000	\$15,000
	c) 450mm Pipe	695 m	\$240	\$166,800	\$167,000
	d) 525mm Pipe	180 m	\$250	\$45,000	\$45,000
	e) 600mm Pipe	485 m	\$280	\$135,800	\$136,000
	f) 675mm Pipe	170 m	\$430	\$73,100	\$73,000
	g) 750mm Pipe	420 m	\$470	\$197,400	\$197,000
	h) 825mm Pipe	230 m	\$480	\$110,400	\$110,000
	i) 900mm Pipe	170 m	\$500	\$85,000	\$85,000
	j) 975mm Pipe	0 m	\$600	\$0	\$0
	k) 1050mm Pipe	0 m	\$750	\$0	\$0
	l) 1200mm Pipe	300 m	\$800	\$240,000	\$240,000
2	a) 1200mm MH	17 Ea.	\$3,600	\$61,200	\$61,000
	b) 1500mm MH	10 Ea.	\$5,500	\$55,000	\$55,000
	c) 1800mm MH	2 Ea.	\$7,900	\$15,800	\$16,000
	d) 2400mm MH	5 Ea.	\$10,000	\$50,000	\$50,000
	e) 3000mm MH	2 Ea.	\$19,000	\$38,000	\$38,000
					\$0
3	a) Catchbasins	54 Ea.	\$1,800	\$97,200	\$97,000
	b) 300mm Pipe	270 m	\$185	\$49,950	\$50,000
	Sub-Total -- Storm Sewer			\$1,491,150	\$1,491,000
	Engineering	15 %		\$223,673	\$224,000
	Contingency	15 %		\$223,673	\$224,000
	Total -- Storm Sewer			\$1,938,495	\$1,939,000

STORMWATER MANAGEMENT (SWM)					
1	Clearing and Grubbing	2 LS	\$10,000	\$20,000	\$20,000
2	Stripping	27000 m ³	\$3	\$67,500	\$68,000
3	Earthwork	59000 m ³	\$5	\$265,500	\$266,000
4	Topsoil	36000 m ²	\$1	\$27,000	\$27,000

5	Seed and Mulch	36000 m ³	\$1	\$18,000	\$18,000
6	Discharge Structure and Outlet Pipe	2 LS	\$35,000	\$70,000	\$70,000
7	Pond Subdrain	450 m	\$20	\$9,000	\$9,000
8	Rip-Rap Protection	2 LS	\$15,000	\$30,000	\$30,000
9	Cable Concrete Entry Lane and Granular Forebay Bottom	2 LS	\$10,000	\$20,000	\$20,000
Sub-Total -- Stormwater Management				\$527,000	\$528,000
	Engineering	15 %		\$79,050	\$79,000
	Contingency	15 %		\$79,050	\$79,000
Total -- Stormwater Management				\$685,100	\$686,000

SANITARY

1	a) 200mm Pipe	870 m	\$200	\$174,000	\$174,000
	b) 250mm Pipe	830 m	\$200	\$166,000	\$166,000
	c) 300mm Pipe	920 m	\$230	\$211,600	\$212,000
2	1200mm MH	28 Ea.	\$4,400	\$123,200	\$123,000
3	a) Services	28 Ea.	\$1,900	\$53,200	\$53,000
	b) Cleanouts	28 Ea.	\$400	\$11,200	\$11,000
Sub-Total -- Sanitary Sewer				\$739,200	\$739,000
	Engineering	15 %		\$110,880	\$111,000
	Contingency	15 %		\$110,880	\$111,000
Total -- Sanitary Sewer				\$960,960	\$961,000

WATERMAIN

1	a) 150mm Pipe	205 m	\$140	\$28,700	\$29,000
	b) 200mm Pipe	590 m	\$190	\$112,100	\$112,000
	c) 250mm Pipe	1030 m	\$200	\$206,000	\$206,000
	c) 300mm Pipe	1200 m	\$250	\$300,000	\$300,000
2	Highway No. 21 Jack and Bore and Casing Pipe	30 m	\$1,500	\$45,000	\$45,000
3	Hydrant Assemblies	16 Ea.	\$5,000	\$80,000	\$80,000
4	a) Tees	16 Ea.	\$1,500	\$24,000	\$24,000
	b) Valves	16 Ea.	\$2,500	\$40,000	\$40,000
Sub-Total -- Watermain				\$835,800	\$836,000
	Engineering	15 %		\$125,370	\$125,000
	Contingency	15 %		\$125,370	\$125,000
Total -- Watermain				\$1,086,540	\$1,086,000

EXTERNAL / OTHER

1	Russell Street Sanitary Sewer	1 LS	\$509,500	\$509,500	\$510,000
	Engineering	8 %		\$40,760	\$41,000
	Contingency	15 %		\$76,425	\$76,000
	Sub-Total -- Russell Street Sanitary			\$626,685	\$627,000
2	Park Street Pumping Station Upgrades	1 LS	\$730,000	\$730,000	\$730,000
	Engineering	15 %		\$109,500	\$110,000
	Contingency	15 %		\$109,500	\$110,000
	Sub-Total -- Park Street Pumping Station			\$949,000	\$950,000
3	Hwy. 21 Improvements	1 LS	\$475,000	\$475,000	\$475,000
	Engineering	15 %		\$71,250	\$71,000
	Contingency	15 %		\$71,250	\$71,000
	Sub-Total -- Highway 21 Improvements			\$617,500	\$617,000
4	Water Booster Station	1 LS	\$615,000	\$615,000	\$615,000
	Engineering	15 %		\$92,250	\$92,000
	Contingency	15 %		\$92,250	\$92,000
	Sub-Total -- Water Booster Station			\$799,500	\$799,000
	Total -- External / Other			\$2,992,685	\$2,993,000

APPENDIX 3
CONSULTATION

MUNICIPALITY OF KINCARDINE

KINCARDINE BUSINESS PARK MASTER PLAN

NOTICE OF PUBLIC OPEN HOUSE

NOTICE OF STUDY COMMENCEMENT

THE PROJECT:

The Municipality of Kincardine is undertaking a Master Plan process to identify infrastructure requirements associated with development of the Kincardine Business Park. The study is being conducted in accordance with the requirements of Phases 1 & 2 of the Municipal Class Environmental Assessment process which is an approved planning process under the Environmental Assessment Act.

The Master Plan study process will involve a detailed investigation of the existing roads, water supply, storm drainage and sanitary sewage collection infrastructure components present in the vicinity of the Business Park and identify future infrastructure needs required to service the remainder of the Business Park footprint. Impacts to existing infrastructure will also be assessed. Upon completion, the study will establish a plan to integrate the remainder of the Business Park land base into an expanded municipal service area. The study will also identify strategies to coordinate the construction of roads, watermains, sanitary and storm sewer facilities within the study area with other municipal infrastructure improvement projects.

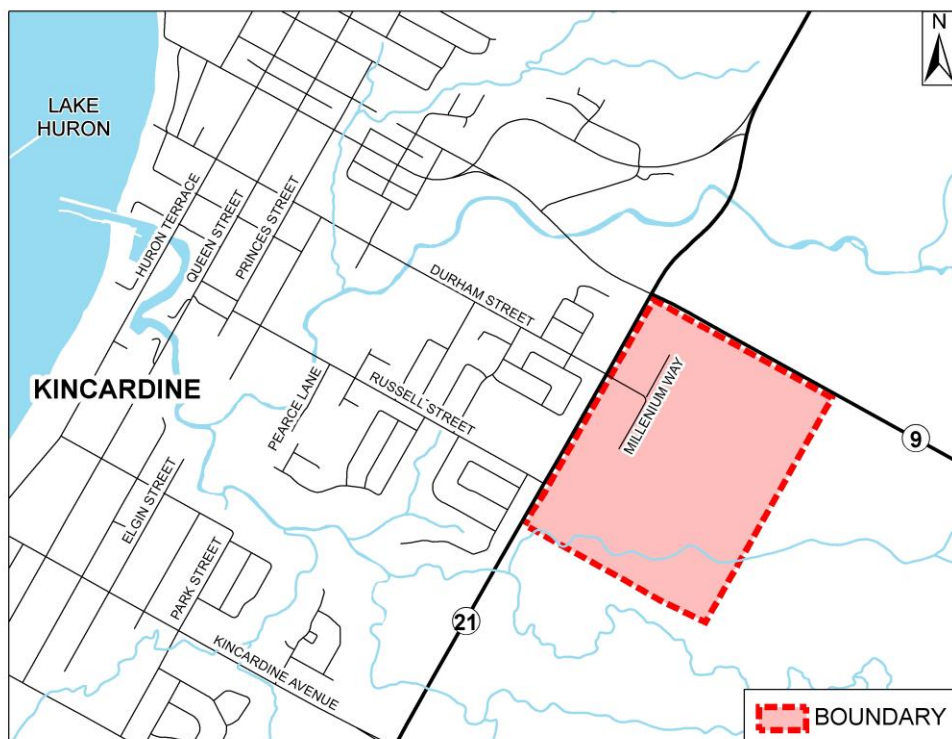
THE ENVIRONMENTAL ASSESSMENT PROCESS:

The investigation is being planned as a Master Plan project under the Municipal Class Environmental Assessment document, dated October 2000, as amended in 2007. Master Plan projects incorporate Phases 1 & 2 of the Class EA process and also include consultation with the general public, government review agencies and affected property owners.

PUBLIC INVOLVEMENT:

Public consultation is a key component of this study. The proposed consultation plan provides for a public open house to be held in the spring of 2011 to review alternative servicing solutions and to give interested parties an opportunity to provide input into the project. Details regarding the date and location of the Public Open House will be announced in a future notice. The study area is shown on the attached key plan.

For further information on this project, or to review the Master Plan process, please contact the consulting engineers: B.M. Ross and Associates: 62 North Street, Goderich, Ontario, N7A 2T4. Telephone: (519) 524-2641. Fax: (519) 524-4403. Lisa Courtney, Environmental Planner (e-mail: lcourtney@bmross.net).



MUNICIPALITY OF KINCARDINE
SERVICING MASTER PLAN
KINCARDINE BUSINESS PARK

REVIEW AGENCY CIRCULATION LIST

REVIEW AGENCY	INVOLVEMENT
Ministry of the Environment (London) - EA Co-ordinator	Mandatory Contact
Ministry of Natural Resources Midhurst	Potential Impact on Natural Features
Ministry of Culture	Toronto
Ministry of Municipal Affairs	General Information (London)
Ministry of Transportation	Planning and Design Review (London)
Ministry of Infrastructure	General Information (Toronto)
OMAFRA	General Information (Guelph)
OPP	General Information (South Bruce Detachment)
County of Bruce - Administration Department - Planning & Development Department - Emergency Medical Services	- General Information - Implications for Long-Term Development
Saugeen Valley Conservation Authority	Potential Impact on Natural Features
Municipality of Kincardine	Proponent
Grey-Bruce Health Unit Owen Sound	General Information
Kincardine Fire Department	General Information

January 26, 2011

Agency

**RE: Municipality of Kincardine
Kincardine Business Park Servicing Master Plan**

The Municipality of Kincardine is undertaking a Master Plan process to identify infrastructure requirements associated with the development of the Kincardine Business Park (refer to Figure No.1, attached) over the next 20 – 25 years. The study is being conducted in accordance with the requirements of Phases 1 and 2 of the Municipal Class Environmental Assessment (EA) process which is an approved planning process under the Environmental Assessment Act.

The Master Plan study process will include a detailed investigation of existing roads, water supply, stormwater drainage and sanitary sewage collection infrastructure present in the vicinity of the Business Park. Additionally, the study will identify future infrastructure needs required to service the remainder of the Business Park. The impacts of future development on existing services will also be assessed. The Master Plan will establish a plan to integrate the remainder of the Business Park into an expanded municipal service area, while identifying appropriate strategies to coordinate construction of roads, watermains, sanitary and storm sewer facilities within the study area with other municipal infrastructure improvement projects.

Historically, lands within the Kincardine Business Park have been subject to a number of individual Class Environmental Assessments related to localized servicing and development issues. To ensure that the remainder of the Business Park is developed in comprehensive and coordinated manner, the Master Plan will examine the following components relating to sanitary and storm water sewers, water servicing and transportation:

Sanitary and Stormwater Collection

- Determine existing and future need for these services over the entire study area;
- Review topography of the study area;
- Identify facilities required to service the entire Business Park, pipe sizing, cost estimates and any additional EA requirements, including the impact on existing infrastructure that would connect the Park to existing municipal facilities;
- Determine possible timing scenarios for development.

Water Services

- Assess the feasibility of servicing the eastern-most portion of the Business Park with regards to topographic challenges;

- Modeling of the existing distribution network to ensure adequate pipe capacity and storage.

Transportation

- Assess the viability of the current transportation network;
- Define the need for additional collector and secondary road construction;
- Establish timing scenarios, coordinating the needs of property owners and the construction of other servicing components.

Public consultation is a key component of the Master Plan process and this study. A public open house, at a date yet to be determined, will provide an opportunity for the public and interested parties to provide input and review alternative solutions for servicing the Business Park. The consultation plan for this study also includes consultation with stakeholders and government review agencies.

Your organization has been identified as possibly having an interest in this project and we are soliciting your input. To facilitate comments, we have enclosed further information regarding the Kincardine Business Park (see list of enclosures). Please forward your response to our office by March 23, 2011. If you have any questions or require further information on this project, please contact the undersigned.

Yours very truly

B. M. ROSS AND ASSOCIATES LIMITED

Per _____
Lisa J. Courtney, M.Sc.
Environmental Planner

LJC:es

Encl: Kincardine Business Park – Major Tasks
Kincardine Business Park – Study Schedule
Kincardine Business Park – Previous Studies
Kincardine Business Park – Figure 1: Preliminary Servicing Network Design
Kincardine Business Park – Figure 2: Kincardine Business Park Study Area

SERVICING MASTER PLAN – KINCARDINE BUSINESS PARK STUDY SCHEDULE

Timing	Task	Task Detail
Fall 2010	Initial Stakeholders Meeting	Property owners and Municipality
Winter 2011	Notice of Study Commencement	Notice published in local papers for two consecutive weeks
	Circulation to Review Agencies for Comment	Agencies include: MOE, MNR, MTO, MOC, OMAFRA, MOI, MOMA, First Nations and Métis, Saugeen Valley Conservation Authority, Local Fire/Police/Emergency Services
	Review Input	Review comments from property owners, review agencies, interested parties and the public
Spring 2011	Inventory of the Environment	Natural, Social and Economic Environment
	Engineering Studies	Review of existing sanitary and stormwater sewer designs, define future sewage and water flows, review water supply and booster pumping needs, review water supply and sewage treatment capacities, conduct traffic study
	Identify Alternative Solutions and Mitigating Measures	Evaluate all reasonable alternatives and identify mitigation methods
	Consult with the Public and Interested Parties	Public Meeting with notice in local papers for two consecutive weeks
Summer 2011	Prepare Draft Master Plan Document	Identify preferred solution
	Review Draft Master Plan Document	Circulate to agencies and interested parties. Make available to the public
Early Fall 2011	Finalize Master Plan Document	Subject to approval by Municipality.

SERVICING MASTER PLAN – KINCARDINE BUSINESS PARK

PREVIOUS STUDIES

A number of studies have been completed relating to the development and expansion of municipal services (roads, water supply, sanitary and storm sewers) in the Kincardine Business Park. A brief summary of each study follows below. The studies are listed by date initiated, in ascending order.

1998 – Durham Street Extension

- ◆ For the extension of Durham Street and servicing of the Canadian Tire Corporation (CTC) site in the Business Park, the Municipality completed a Stormwater Management Design Report that:
 - Outlines stormwater management criteria for development of the CTC site and future lands in the Business Park within the same drainage area.
 - Addresses concerns expressed by the Ministry of Environment (MOE) and Saugeen Valley Conservation Authority and follows the design guidelines of the MOE.
 - Addresses stormwater quality and quality impacts, and sediment and erosion concerns.

2005 – Class Environmental Assessment (EA) for the Extension of Russell Street

- ◆ To investigate the potential impacts of extending Russell Street east of Highway No. 21, extending full municipal servicing within the Russell Street road allowance and an adjacent stormwater management facility, a Class EA was completed.
- ◆ The Class EA included a Traffic Impact Study completed by Paradigm Transportation Solutions Limited that recommended:
 - Upgrades to intersection of Russell Street and Highway No. 21, with design for traffic control signals
 - Provision of sidewalks on both sides of Russell and Durham Street from Highway No. 21
- ◆ The EA review period concluded September 17, 2005; however, the extension of Russell Street has not been constructed.

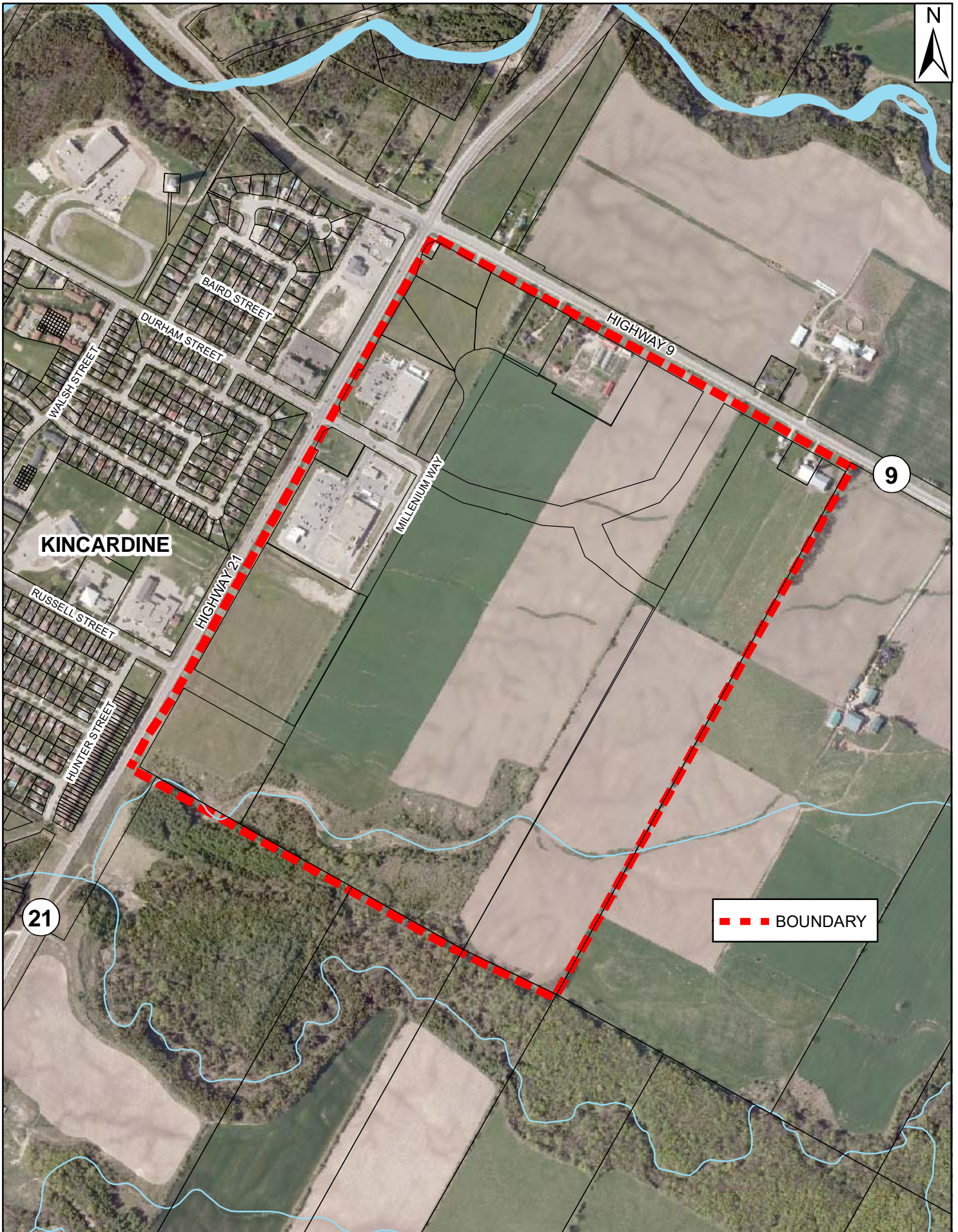
2006 – Class Environmental Assessment for the Extension of Millennium Way

- ◆ To investigate the potential impacts of the extension of Millennium Way north of Durham Street and extension of full municipal services within the planned road allowance, the Municipality completed a Class EA.
- ◆ The Class EA included Stage 1 and 2 archaeological assessments. Stage 2 investigation revealed the project area contained no material of archaeological significance.
- ◆ The EA review period concluded October 15, 2006. The extension of Millennium Way and associated municipal services was constructed subsequently.

SERVICING MASTER PLAN – KINCARDINE BUSINESS PARK

MAJOR TASKS

- ◆ Review existing sanitary and storm water drainage designs;
- ◆ Review sanitary sewage and storm water drainage catchments through topographic mapping review and field confirmation;
- ◆ Forecast future development and servicing needs based on Official Plan designations, environmental constraints, and consultations with property owners. Base development densities on County of Bruce Official Plan and density assumptions.
- ◆ Define future sewage and water flows based on MOE Guidelines;
- ◆ Review water supply and Booster Pumping needs;
- ◆ Review water supply and sewage treatment capacities and identify constraints and future needs, including facilities, pipe sizing, pipe capacity and storage, and costs;
- ◆ Evaluate the viability of current transportation network with a traffic study and define need for additional collector and secondary road construction;
- ◆ Identify any additional EA requirements;
- ◆ Conduct public consultation with property owners, municipal residents and government review agencies, including information mail-outs and a public information meeting;
- ◆ Identify potential environmental impacts and mitigating measures;
- ◆ Determine an environmentally and cost efficient strategy for providing municipal servicing;
- ◆ Preparation of a Master Plan document which identifies the preferred servicing strategy for the subject lands, identifies required facilities, provides an estimate of potential costs and cost allocation and provides an expected timeline for implementation of new works and expansion of existing facilities;
- ◆ Circulation of the Master Plan to the public and review agencies.



21

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■ ■ ■ BOUNDARY



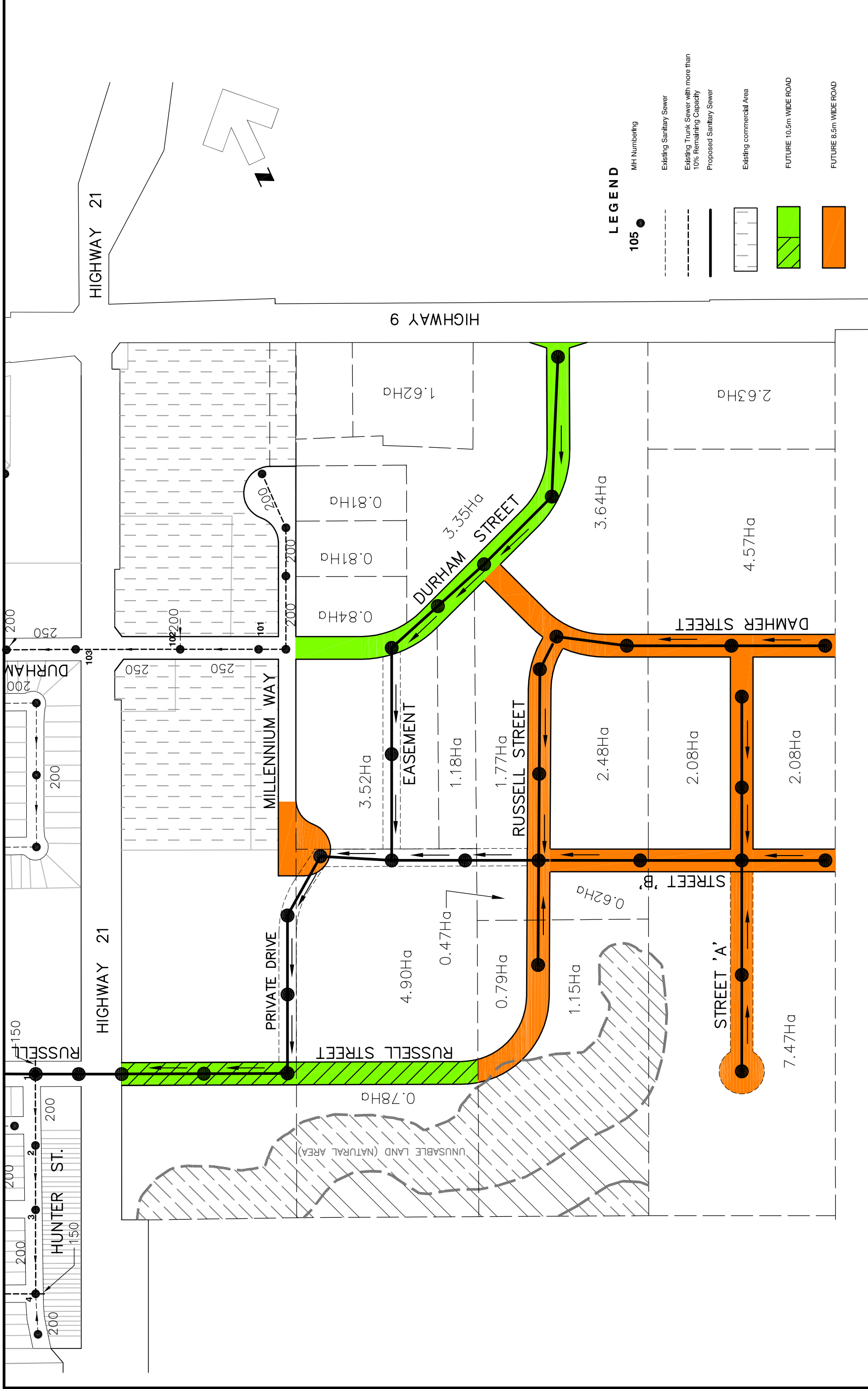
MUNICIPALITY OF KINCARDINE
 SERVICING MASTER PLAN FOR KINCARDINE BUSINSS PARK
 (COMMUNITY OF KINCARDINE)
 PROJECT STUDY AREA

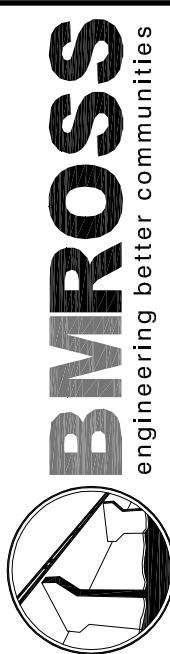
DATE
 JAN. 19, 2011

PROJECT No.
 08055

SCALE
 1: 8 000

FIGURE No.
 1



		Municipality of Kincardine Business Park Development Area Full Development Roads and Sanitary Sewer	
DATE	JAN. 19, 2011	PROJECT No.	08055
SCALE	N.T.S.	FIGURE	2

MUNICIPALITY OF KINCARDINE

**SERVICING MASTER PLAN
KINCARDINE BUSINESS PARK**

FIRST NATIONS CIRCULATION LIST

FIRST NATION	CONTACT
Indian and Northern Affairs Canada	Franklin Roy, Director General Litigation Portfolio Operations Indian and Northern Affairs Canada Eastern Litigation Directorate 10 Wellington Street Gatineau, QC K1A 0H4
	Ralph Brant, Direction General, Specific Claims Branch Indian and Northern Affairs Canada 10 Wellington Street Gatineau, QC K1A 0H4
	Lynn Bernard, Direction General, Indian and Northern Affairs Canada Negotiations - East 10 Wellington Street Gatineau, QC K1A 0H4
Ministry of Aboriginal Affairs	Pam Wheaton, Director Aboriginal and Ministry Relationships Branch Ministry of Aboriginal Affairs 160 Bloor Street East, 9 th Floor Toronto, ON M7A 2E6
Métis Nation of Ontario	Métis Nation of Ontario 500 Old St. Patrick Street, Unit D Ottawa, ON K1N 9G4
Chippewas of Saugeen	Chippewas of Saugeen RR 1 Southampton, ON N0H 2L0
Chippewas of Nawash	Chief Ralph Akiwenzie Chippewas of Nawash Unceded First Nation R.R. #5 Warton ON N0H 2T0
Grey-Bruce Peninsula Métis Council	Ray Raciot, President Grey Bruce Penninsula Metis Council 380 9 th Street East Owen Sound ON N4K 1P1
Historic Saugeen Métis	Historic Saugeen Métis 204 High Street, Box 1492 Southampton ON N0H 2L0

January 26, 2011

First Nation and Métis Community

**RE: Kincardine Business Park Servicing Master Plan
Municipality of Kincardine**

The Municipality of Kincardine is undertaking a Master Plan process to identify infrastructure requirements associated with the development of the Kincardine Business Park (refer to Figure No.1, attached) over the next 20 – 25 years. The study is being conducted in accordance with the requirements of Phases 1 and 2 of the Municipal Class Environmental Assessment (EA) process which is an approved planning process under the Environmental Assessment Act.

The Master Plan study process will include a detailed investigation of existing roads, water supply, stormwater drainage and sanitary sewage collection infrastructure present in the vicinity of the Business Park. Additionally, the study will identify future infrastructure needs required to service the remainder of the Business Park. The impacts of future development on existing services will also be assessed. The Master Plan will establish a plan to integrate the remainder of the Business Park into an expanded municipal service area, while identifying appropriate strategies to coordinate construction of roads, watermains, sanitary and storm sewer facilities within the study area with other municipal infrastructure improvement projects.

Your organization has been identified as possibly having an interest in this project and we are soliciting your input. If you have any questions or require further information on this project, please contact the undersigned at 519-524-2641 or by e-mail at lcourtney@bmross.net.

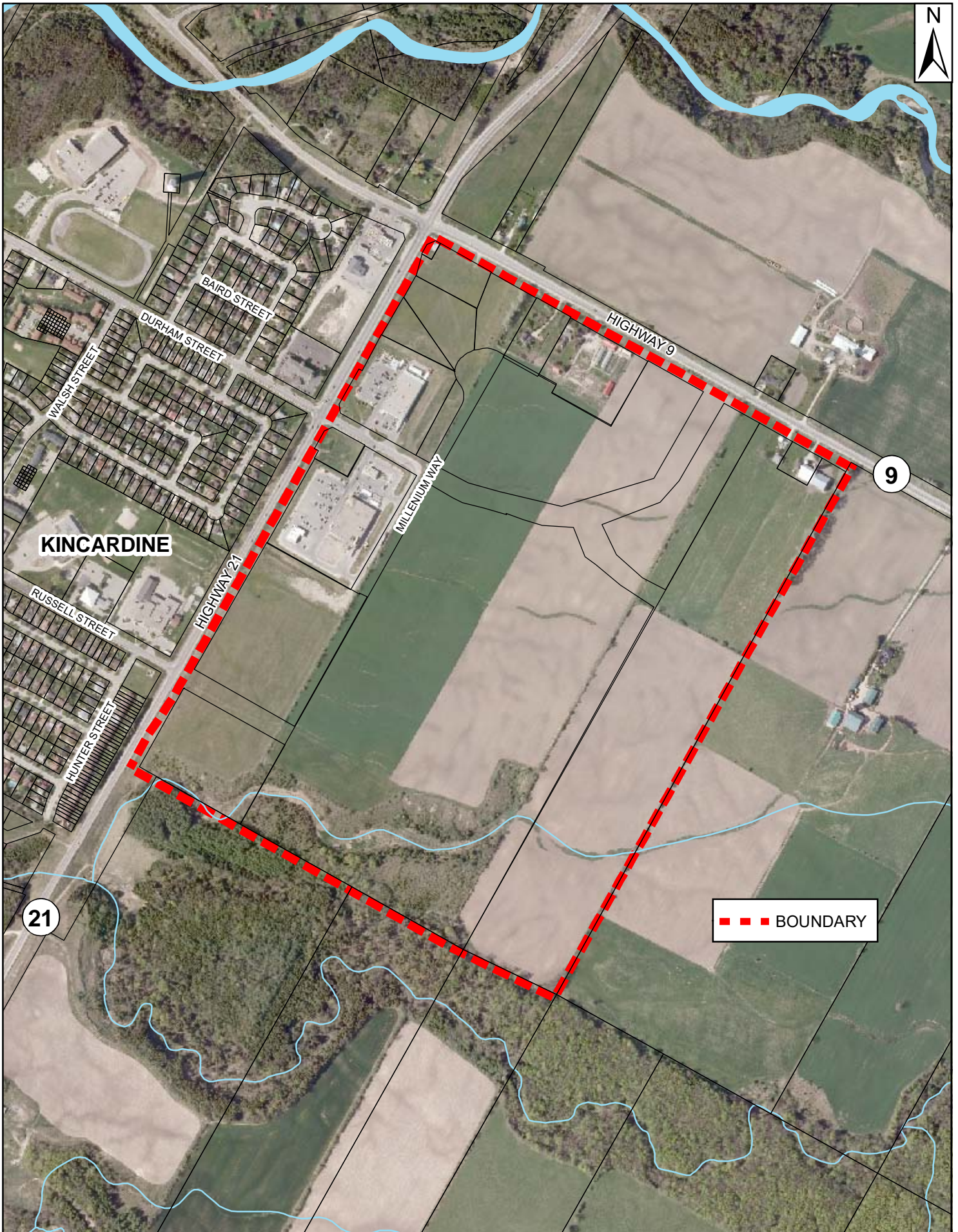
Yours very truly,

B. M. ROSS AND ASSOCIATES LIMITED

Per _____

Lisa J. Courtney, M.Sc.
Environmental Planner

LJC:es
Encl.



Ministry of the Environment

Ministère de l'Environnement

733 Exeter Road
London ON N6E 1L3
Tel: 519 873-5000
Fax: 519 873-5020

733, rue Exeter
London ON N6E 1L3
Tél.: 519 873-5000
Télééc.: 519 873-5020

**BY FAX ONLY**

February 4, 2011

Lisa J. Courtney, M.Sc
B. M. Ross & Associates
62 North Street
Goderich, Ontario
N7A 2T4

Dear Ms Courtney:

RE: Kincardine Business Park Servicing Master Plan

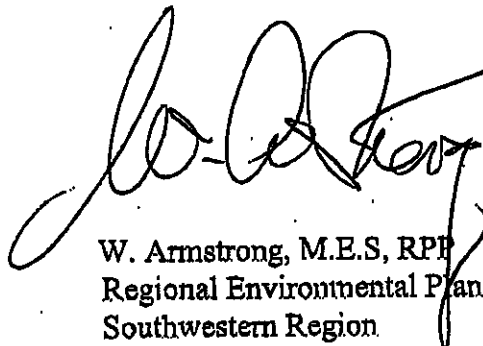
This acknowledges receipt of your notice that a master plan for servicing of the Kincardine Business Park has begun following the MBEA Municipal Class Environment Assessment and your invitation to provide input.

At this early stage in the master planning process we are unable to identify detailed issues or concerns beyond:

- expressing an interest in understanding how the proposed development may impact the watercourse which flows through the southerly portion of the property (mainly stormwater management in this context) and
- noting that present flows to the municipal sewage treatment facility are approaching 80% of its approved capacity and therefore the implications of the development of the business park upon near term available capacity and potentially the need for expansion in the near-term

If questions arise or if clarification is needed please contact the undersigned at (519) 873-5013 or via email at bill.armstrong@ontario.ca.

Yours truly,

A handwritten signature in black ink, appearing to read 'W. Armstrong', written over a printed name and title.

W. Armstrong, M.E.S, RPP
Regional Environmental Planner
Southwestern Region

cc. J. Bromley

Ministry of
Municipal Affairs
and Housing

Ministère des
Affaires municipales
et du Logement



Municipal Services Office -
Western

Bureau des services aux municipalités -
région de l'Ouest

659 Exeter Road, 2nd Floor
London ON N6E 1L3
Tel. (519) 873-4020
Toll Free 1-800-265-4736
Fax (519) 873-4018

659, rue Exeter, 2^e étage
London ON N6E 1L3
Tél. (519) 873-4020
Sans frais 1 800 265-4736
Télé (519) 873-4018

RECEIVED

FEB 28 2011

B.M. ROSS & ASSOC. LTD.

February 24, 2011

Ms. Lisa Courtney
Environmental Planner
BM Ross and Associates Limited
62 North Street
Goderich, ON N7A 2T4

Dear Ms. Courtney:

Re: **Municipal Class Environmental Assessment
Kincardine Business Park Servicing Master Plan
Municipality of Kincardine, County of Bruce**

Thank you for your recent circulation of the above-noted matter. In this regard, we offer the following comments for your consideration.

It is understood the Municipality of Kincardine is undertaking a Master Plan process to identify infrastructure requirements associated with the development of the Kincardine Business Park over the next 20-25 years. The Master Plan study process will include a detailed investigation of existing roads, water supply, stormwater drainage and sanitary sewage collection infrastructure present in the vicinity of the Business Park. Further, it is understood the study will identify future infrastructure needs required to service the remainder of the Business Park and impacts of future development on existing services will also be addressed. It is also understood the Master Plan will establish a plan to integrate the remainder of the Business Park into an expanded municipal service area, while identifying appropriate strategies to coordinate construction of roads, watermains, sanitary and storm sewer facilities within the study area with other municipal infrastructure improvement projects.

This office provides access to provincial services on municipal government, finance and administration, as well as land use planning and development issues covered under the *Planning Act*. Section 2 of the *Planning Act* speaks to matters of provincial interest. This section directs decision-making bodies (whether it is a council of a municipality, a local board, a planning board, a minister of the Crown and a ministry, board, commission or agency of the government, or the Ontario Municipal Board) to be consistent with the policy statements issued under Section 3 of the *Planning Act* in exercising any authority that affects a planning matter.

The current policy on land use planning matters for the County of Bruce is the Provincial Policy Statement, 2005 (PPS). The PPS speaks to issues such as the promotion of efficient, cost-effective development and land use patterns, and the proper consideration of the various resources of this province as well as matters dealing with public health and safety.

The requirements of the *Planning Act* apply to applications for planning approvals under this legislation; these applications include official plan amendments and zoning bylaw amendments. From our review of this particular matter, it appears no such approvals are being sought at this time. However, we recommend that you consider the Provincial Policy Statement policies in their entirety in developing the proposed Master Plan.

Environmental Assessment Studies that examine water supply, stormwater drainage and sanitary sewage collection should ensure that these systems are provided in a manner that: 1) are of an appropriate size and type to accommodate present and future requirements; 2) can be sustained by the water resources upon which these services rely; 3) are located and designed in accordance with provincial standards; 4) are financially viable and comply with all other regulatory requirements; 5) promote water conservation and water use efficiency; and 6) protects human health and the natural environment. Additionally, you should ensure that the Municipality of Kincardine and Bruce County's Official Plan policies regarding water supply, stormwater drainage and sanitary sewage collection are integrated into the Master Plan process.

Further, the portion of this Environmental Assessment Study that examines transportation systems (including existing roads), should ensure these systems are: (1) safe, energy efficient and facilitate the movement of people and goods; (2) appropriate to address projected needs; (3) use existing and planned infrastructure efficiently; (4) integrate transportation and land use considerations at all stages of the planning process; and (5) connectivity within and among transportation systems and modes is maintained. Additionally, you should ensure that the Municipality of Kincardine and Bruce County Official Plan policies regarding transportation are integrated into the Master Plan process.

Additionally, and as you are aware, the Ministry of Transportation has been discussing the proposed road network for the Kincardine Business Park with the Municipality of Kincardine and the County of Bruce since 2007. The Ministry of Transportation (MTO) has received a copy of the 'Notice' for this project and we understand MTO will be providing comments on the proposed undertaking. If you have not received comments from the Ministry of Transportation by your requested deadline date (March 23, 2011), please contact Ian Smyth, Planner, Corridor Management, Ministry of Transportation (London office) at (519) 873-4598.

Finally, our comments on this undertaking should not be considered as approval for any other related applications under the *Planning Act* or other provincial legislation that may be required, may be related to, or may result from this project.

Please keep us on your circulation list for this project. If you have any questions or comments, please telephone me at (519) 873-4695 or by email at: Dwayne.Evans@ontario.ca.

Yours truly,



Dwayne Evans, M.A., MCIP, RPP
Planner
Municipal Services Office – Western

March 21, 2011

B.M. Ross and Associates Limited
Consulting Engineers
62 North Street, Goderich, ON N7A 2T4



Dear Lisa Courtney:

**RE: Municipality of Kincardine
Kincardine Business Park Servicing Master Plan**

The Grey Bruce Health Unit is mandated by the Ontario Public Health Standards to work with Municipalities to create healthy built environments. This provincial direction allows health units to support the intentions of the Provincial Policy Statement, especially with regard to endorsement of land use planning principles that support healthy, liveable communities, protection of our natural heritage and resources, and bolstering public health and safety. The Public Health goal for creating and supporting healthy communities is also in alignment with the goals and objectives of the Bruce County Official Plan, which calls for “quality of life” and “sustainable communities.”

Within this framework, please review the following considerations for the development of the Kincardine Business Park:

1) Environment

- a) Ensure the proposed development is compatible with neighbouring uses from a community health perspective including industrial and commercial emissions, nuisance noise and odour impacts.

Rationale: The close proximity of residential neighbourhoods to the proposed development, if uses are non-compatible, could result in adverse health effects.

- Exposure to noise can introduce or aggravate stress-related health outcomes, including those on the cardiovascular system, immune system, sleep, behaviour, and mental health.
- Periods of odour nuisance often go together with headache, nausea, sleep disturbances, a loss of appetite and stress.

- b) Ensure the proposed development is designed to improve rather than diminish air and water quality for the community through the preservation of green space.
- Rationale:* The preservation of green space minimizes the effects of heat islands, which drive up cooling and refrigeration-related energy consumption and generation.

- Trees can reduce air temperature thereby reducing ozone formation and removing air pollutants.
 - Green spaces protect water quality by providing opportunity for water absorption and filtration.
 - Research suggests a positive impact on the psychological well-being of people who are able to interact with the natural environment, particularly green space.
- c) Promote sustainable green building and development approaches (e.g. LEED standards) to reduce reliance on traditional energy systems, conserve energy and protect air quality.
- Rationale:* The most significant sources of air pollution in Ontario are energy generation and transportation.
- Electricity generation produces a significant share of nitrogen oxides and sulphur dioxide emissions, which contribute to the reduction in air and water quality.
 - Numerous studies show that poor air quality contributes to premature death, cardiovascular disease, cancer, stroke, asthma and other respiratory diseases.
- d) Ensure the transportation network prioritizes active modes of transportation (e.g. walking, cycling) to decrease use of single occupancy motor vehicles and reduce motor vehicle trips.
- Rationale:* Transportation is the primary contributor to air pollution.
- Health impacts from air pollution include respiratory problems, asthma and increased risk of heart attack.

2) Physical Activity and Injury Prevention

- a) Design the transportation network in a way that ensures access for all modes of transportation, with specific attention to active transportation and pedestrian needs.
- Rationale:* Moderately intense physical activity such as walking and cycling increases health benefits and has the potential to reduce cardiovascular disease by as much as 50 percent.
- Communities and neighbourhoods that are designed with an active transportation infrastructure that prioritizes the pedestrian and cyclist while reducing automobile dependency support daily physical activity.
 - Active transportation can also lead to economic and environmental sustainability.
- b) Ensure the provision of active transportation infrastructure that is safe, accessible, barrier-free, and aesthetically pleasing, and that is connected to the street system with direct and convenient links to adjacent uses, residential, commercial, and recreational spaces.

Rationale: The more people travel by car the greater potential for motor vehicle-related injury for vehicle users and pedestrians.

- Concentrating uses, increasing density, and reducing distances between place of employment, recreation and residency reduces the need for vehicle travel and make active transportation options more viable.
- Road design affects the physical form and walkability of neighbourhoods as well as the placement, viability and safety of active transportation infrastructure. Road design influences the behaviour of all transportation users; safe road design results in lower rates of vehicle-pedestrian collisions.

3) Social Cohesion and Quality of Life

- a) Provide green spaces for people to meet and congregate

Rationale: Creating public spaces within a neighbourhood/community allows individuals to meet and congregate, providing opportunities for social interaction.

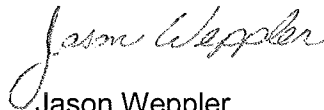
- Research shows that people with strong social networks live longer.
- Research also shows that exposure to the natural environment is associated with feelings of well-being in individuals.
- Designing neighbourhoods where people have access to green space can result in physical and mental health benefits.

The Grey Bruce Health Unit is pleased to be working in partnership with municipalities and counties in developing policies and environments to support healthy communities. Should further questions arise, do not hesitate to contact Jennifer Croft or Jason Wepler at the Owen Sound office.

Sincerely,



Jennifer Croft
Health Promoter
Grey Bruce Health Unit
519-376-9420 ext 1469



Jason Wepler
Health Promoter
Grey Bruce Health Unit
519-376-9420 ext 1408

Reference:

Simcoe Muskoka District Health Unit. (2010). Healthy communities design: Policy statements for official plans. Barrie, Ontario.



1078 Bruce Rd. 12
P.O. Box 150
Formosa, Ontario
N0G 1W0

Tel 519-367-3040
Fax 519-367-3041
www.syca.on.ca
publicinfo@svca.on.ca

RECEIVED

MAR 28 2011

B.M. ROSS & ASSOC. LTD.

BY REGULAR MAIL AND FAX: 519-524-4403

March 23rd, 2011

B.M. Ross and Associates Limited
62 North Street, Goderich
ON N7A 2T4

Attention: Lisa J. Courtney, Environmental Planner

RE: "Kincardine Business Park Servicing Master Plan"
(Your Project File No. 08055)
Geographic Town of Kincardine
Municipality of Kincardine

Thank you for the opportunity to comment on the proposed Kincardine Business Park Servicing Master Plan. The Saugeen Valley Conservation Authority (SVCA) offers the following comments based on the information package received from B.M. Ross dated January 26th, 2011.

Subject Area

The subject area is approximately 50 ha in size and includes a portion of Environmental Protection (EP) which is labeled as "Unusable Land (Natural Area)" on Figure 2. Located within the EP lands is a municipal drain known as the "Holtby Drain". The Holtby Drain is included in the Town of Kincardine Floodplain as an area which would flood under a Regulatory event (Hurricane Hazel Flood event). Mapping is available from the SVCA for the subject property.

SVCA Regulation

Please be advised that portions of the area are subject to the SVCA's Development, Interference with Wetlands and Alterations to Shorelines and Watercourses Regulation (Ontario Regulation 169/06). Regulated Area mapping is available which generally identifies those areas in which the SVCA's Regulation applies.

This Regulation requires that a person obtain the written permission of the SVCA prior to any "development" in the Regulated Area or "alteration" to a watercourse or wetland. As such, the written permission of the SVCA will be required prior to the commencement of any site alteration or development related to this proposal, within SVCA's Regulated Area.

Conservation
Through
Cooperation

A MEMBER OF



Conservation
ONTARIO
Natural Champions

As preliminary construction plans become available, they should be forwarded to the SVCA for review. The SVCA will continue to review this file with respect to Ontario Regulation 169/06 as well as on behalf of the Federal Department of Fisheries and Oceans (DFO) with regard to potential harmful alteration, disruption or destruction of fish habitat. The harmful alteration, disruption or destruction of fish is prohibited unless authorized by the DFO pursuant to Section 35(2) of the *Fisheries Act*. If the SVCA determines that fish habitat may be altered, disrupted or destroyed as a result of this project, the file will be referred to the DFO. The decision, by the SVCA, to involve the DFO will be determined as further information is submitted to this office for review.

Review of the Preliminary Servicing Network Design

Road Locations

The proposed location and extension of Russell Street appears to be adjacent the Natural Area (EP). As the current plans are still preliminary the SVCA would comment that the subject area appears to be adjacent to a natural slope for the Holtby Drain. Design and location of the road should ensure that the road is not affected by the hazard, nor does it create or aggravate an existing hazard. The SVCA may require a permit for the proposed road construction.

Street 'A' appears to bisect a portion of the Holtby Drain floodplain. Initial comments from the Conservation Authority would be that no negative effect upstream or downstream on the floodplain of the Holtby Drain be created due to the placement and instillation of the roads. The extended floodplain does not appear to have been captured in Figure 2. Further details and engineered floodplain mapping on the extent of the floodplain is available from the Conservation Authority.

Stormwater

While it is anticipated that further details on the design and routing of stormwater shall be addressed further in the study, the SVCA would comment that should an outlet to the Holtby Drain be a required a permit from the Authority will be required. Location of any future stormwater management facilities (ie. Stormwater pond) should maintain an appropriate setback from the top of the slope adjacent to the Holtby Drain to ensure that slope stability is not affected. Water quality and quantity should also be reviewed and addressed as part of future studies and reports.

Sanitary and Water Services

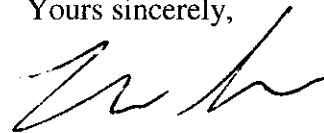
At this time SVCA staff do not foresee any concerns over the proposed routing of the sanitary services. Routing for the proposed water services has not yet be submitted; however, the SVCA staff do not foresee any concerns should the services follow the approximate location of the sanitary locations.

B.M. Ross and Associates
March 23rd, 2011
Page 3

The SVCA will continue review of this project when further information is received by this office.

We trust that the above information is helpful. If any questions arise, please contact this office.

Yours sincerely,

A handwritten signature in black ink, appearing to read "Nathan Garland", written in a cursive style.

Nathan Garland
Regulations Officer

NGI/6

cc: Ron Coristine, Director, SVCA (via e-mail)
Mike Leggett, Director, SVCA (via e-mail)

**Historic Saugeen Metis:
Lands and Resources Department**
204 High Street
P.O. Box 1492
Southampton Ontario
N0H 2L0
Phone: 519-483-4001 Fax 519-483-4002
Email: saugeenmetisadmin@bmts.com

Fax

To: B.M Ross and Associated Ltd. **From:** Historic Saugeen Metis (LRCC)
(Municipality of Kincardine)

Fax: (519)524-4403 **Pages:** 1

Phone: (519)524-2641 **Date:** 04 February 2011

Re: File#08055 **CC:**

Urgent **For Review** **Please Comment** **Please Reply** **Please Recycle**

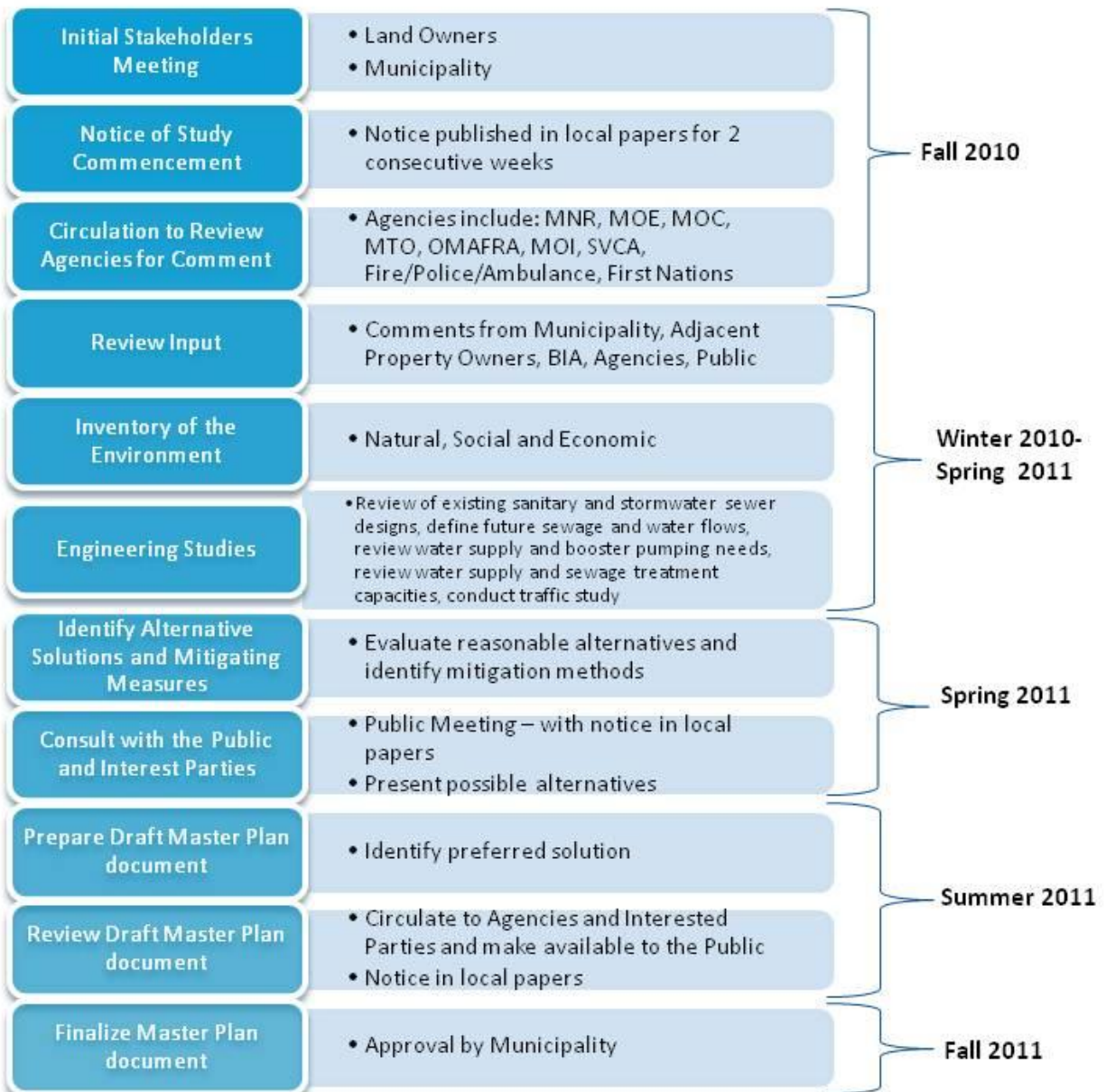
• **Comments:**

HMS Lands and Resources Dept. would like to request any copies of all archaeological studies that take place relating to the Kincardine Business Park during the various stages of the development process.

Thank you for the information already provided.

Audrey Erin Holden
Lands and Resources Consultation Coordinator
Historic Saugeen Metis
204 High Street
Southampton, Ontario, N0H 2L0
Phone: 519-483-4001

THE MASTER PLAN PROCESS





MUNICIPALITY OF KINCARDINE

KINCARDINE BUSINESS PARK MASTER PLAN

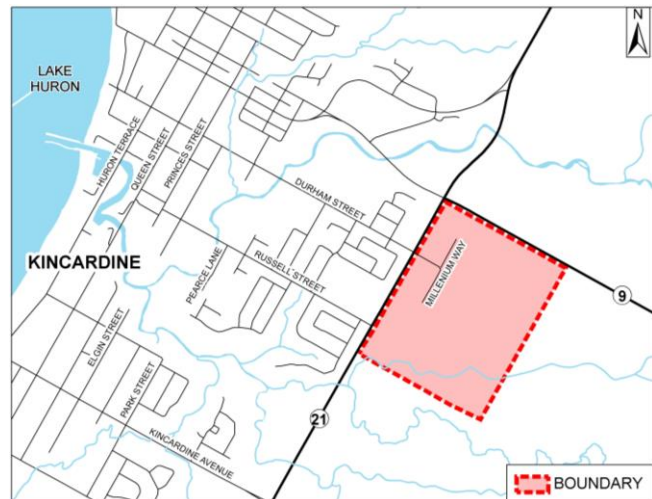
NOTICE OF PUBLIC OPEN HOUSE

PUBLIC COMMENT INVITED

THE PROJECT:

The Municipality of Kincardine is undertaking a Master Plan process to identify infrastructure requirements associated with development of the Kincardine Business Park. The study is being conducted in accordance with the requirements of Phases 1 & 2 of the Municipal Class Environmental Assessment process which is an approved planning process under the Environmental Assessment Act.

The Master Plan study process will involve a detailed investigation of the existing roads, water supply, storm drainage and sanitary sewage collection infrastructure components present in the vicinity of the Business Park and identify future infrastructure needs required to service the remainder of the Business Park footprint. Impacts to existing infrastructure will also be assessed. Upon completion, the study will establish a plan to integrate the remainder of the Business Park land base into an expanded municipal service area. The study will also identify strategies to coordinate the construction of roads, watermains, sanitary and storm sewer facilities within the study area with other municipal infrastructure improvement projects.



THE ENVIRONMENTAL ASSESSMENT PROCESS:

The investigation is being planned as a Master Plan project under the Municipal Class Environmental Assessment document, dated October 2000, as amended in 2007. Master Plan projects incorporate Phases 1 & 2 of the Class EA process and also include consultation with the general public, government review agencies and affected property owners.

PUBLIC INVOLVEMENT:

Public consultation is a key component of this study. The proposed consultation plan provides for a public open house and presentation to be held to review servicing solutions and to give interested parties an opportunity to provide input into the project. Details regarding the date and location of the Public Open House are as follows:

Date: Wednesday March 27th, 2013

Time: Open House: 7:00 – 9:00 PM, Presentation at 7:30 PM

**Location: Municipality of Kincardine Municipal Administration Centre
1475 Concession 5, R.R. 5 Kincardine, ON N2Z 2X6**

For further information on this project, or to review the Master Plan process, please contact the consulting engineers: B.M. Ross and Associates: 62 North Street, Goderich, Ontario, N7A 2T4. Telephone: (519) 524-2641. Fax: (519) 524-4403. Lisa Courtney, Environmental Planner (e-mail: lcourtney@bmross.net).

Michele Barr, Director of Building and Planning
Municipality of Kincardine

This Notice issued March 13th, 2013

Municipality of Kincardine Kincardine Business Park (KBP) Servicing Master Plan

Public Meeting and Open-House

March 27, 2013



KBP – Servicing Master Plan Agenda

- The Master Plan Process
- History of the Area
- Draft Servicing Strategy
- Next Steps
- Questions and Comments



2



KBP – Servicing Master Plan General Location



3



KBP – Servicing Master Plan Master Plan Process

- What is a Master Plan
- Official Plan Information
- Study Limits for the Business Park



4



KBP – Servicing Master Plan Master Plan Process

Initial Stakeholders Meeting	<ul style="list-style-type: none"> Land Owners Municipality
Notice of Study Commencement	<ul style="list-style-type: none"> Notice published in local papers for 2 consecutive weeks
Circulation to Review Agencies for Comment	<ul style="list-style-type: none"> Agencies include: WRA, WOE, WDC, MTO, OMAHA, WCA, SPCA, Fire/Police/Recreation, First Nations
Review Input	<ul style="list-style-type: none"> Comments from Municipality, Adjacent Property Owners, ISA, Agencies, Public
Engineering Studies	<ul style="list-style-type: none"> Review of existing sanitary and stormwater sewer design, define future sewage and water flows, make water supply and local pumping needs, review water supply and sewage treatment capacities, conduct traffic study
Inventory of the Environment	<ul style="list-style-type: none"> Natural, Social and Economic
Identify Alternative Solutions and Mitigating Measures	<ul style="list-style-type: none"> Evaluate reasonable alternatives and identify mitigation methods
Consult with the Public and Interested Parties	<ul style="list-style-type: none"> Public Meeting – with notice in local papers Present possible alternatives
Propose Draft Master Plan Document	<ul style="list-style-type: none"> Identify preferred solution
Review Draft Master Plan Document	<ul style="list-style-type: none"> Circulate to Agencies and Interested Parties and make available to the Public Notice in local papers
Finalize Master Plan Document	<ul style="list-style-type: none"> Approval by Municipality

Schedule 'A' Community of Kincairdine Land Use Plan



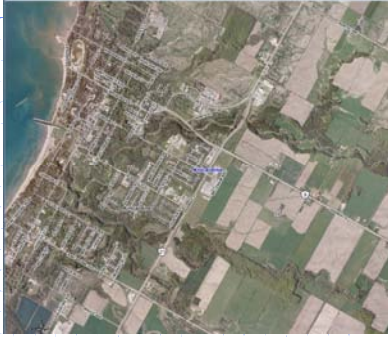
KBP – Servicing Master Plan Study Limits



KBP – Servicing Master Plan History

- Extent of Existing Servicing and Development
 - Water
 - Sanitary
 - Storm Drainage
- Access to Highway 9 and MTO

KBP – Servicing Master Plan History



KBP – Servicing Master Plan Draft Servicing Strategy

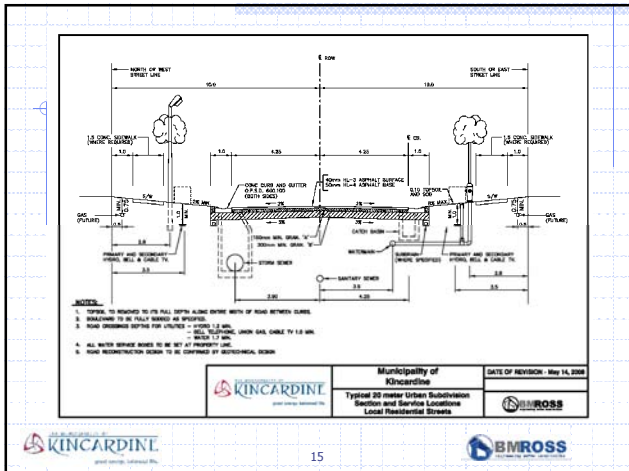
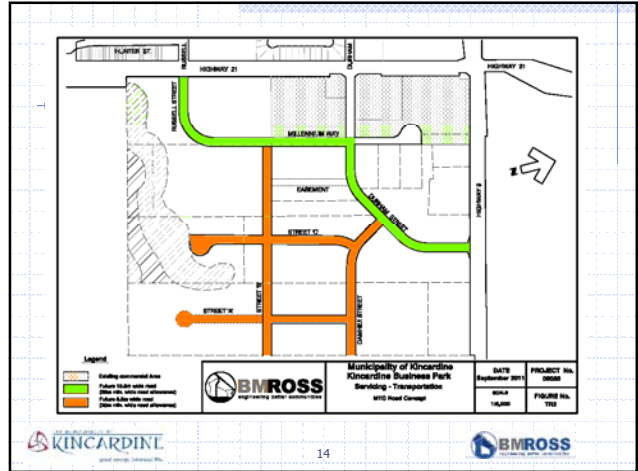
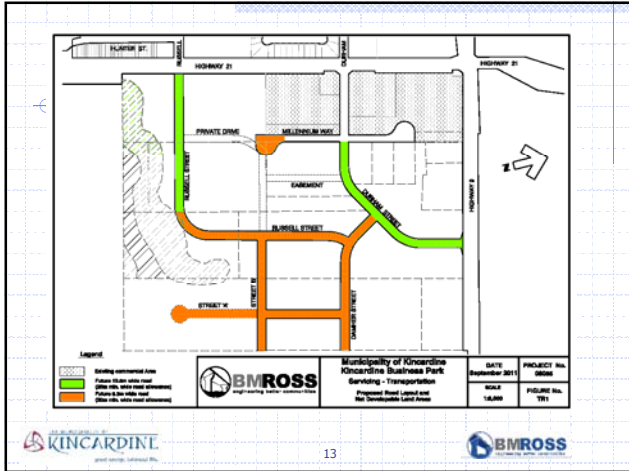
- Transportation and Roads Pattern
- Water Servicing
- Sanitary Servicing
- Storm Water Management
- Phasing
- Costs

KBP – Servicing Master Plan Transportation and Roads Pattern

- Theoretical Landuse and Road Pattern
- Typical Cross Sections
- Traffic Impact Study – Possible External Improvements

KBP – Servicing Master Plan Conceptual Land Use





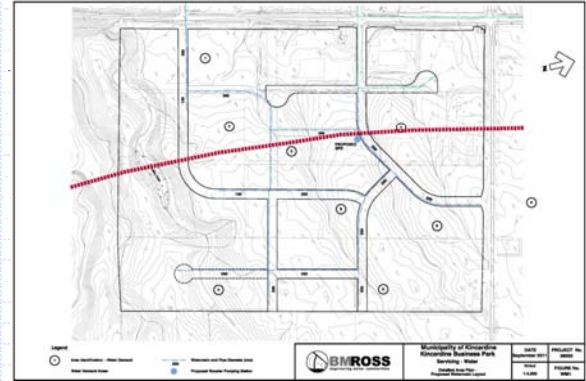
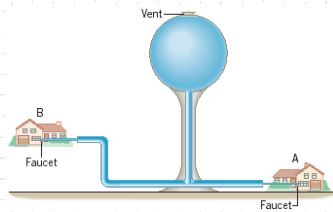
KBP – Servicing Master Plan Water Servicing

- Existing System and Constraints
- Available Outlet Locations
- Proposed Distribution
- Booster Pumping Station

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KBP – Servicing Master Plan Water Servicing

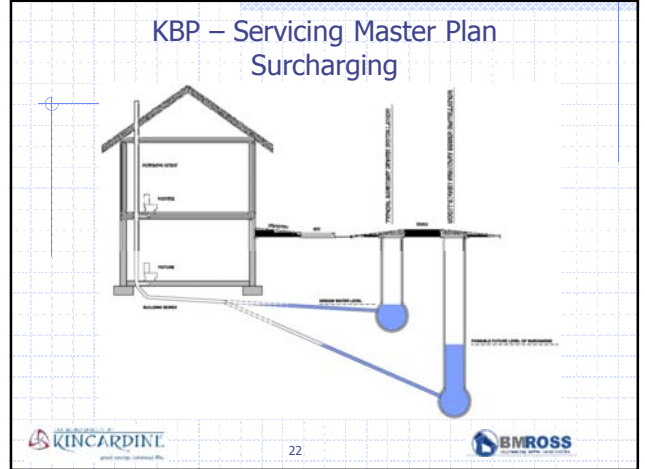
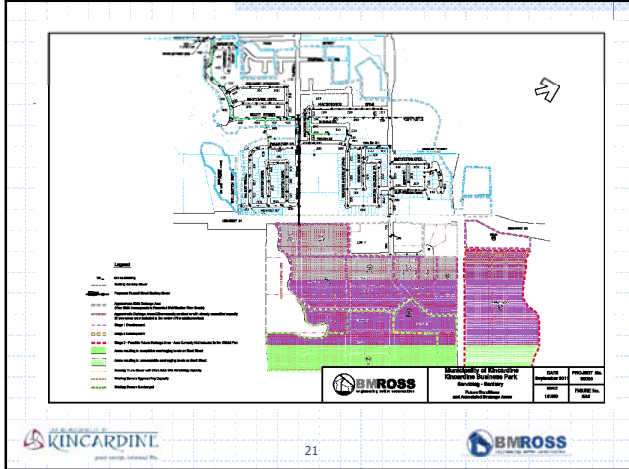
- Supply Pressure and Demand



KBP – Servicing Master Plan Sanitary Servicing

- Existing System and Constraints
- Available Connection Locations
- Proposed Sanitary System
- Park Street Pumping Station Upgrades



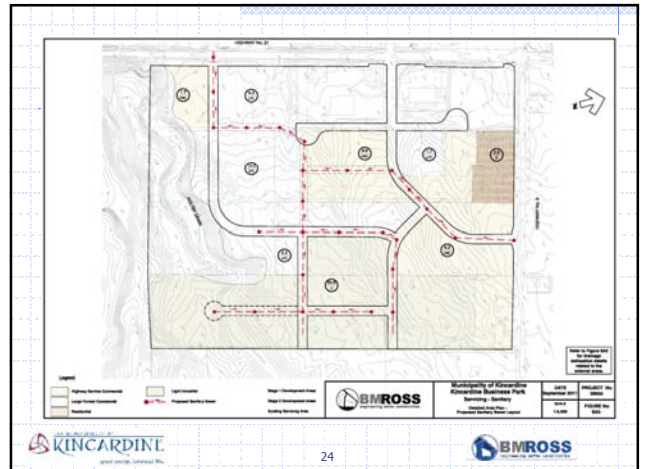


KBP – Servicing Master Plan Park Street Sewage Pumping Station

- Existing Station
- Forcemain to Lagoons
- Upgrade Possibilities

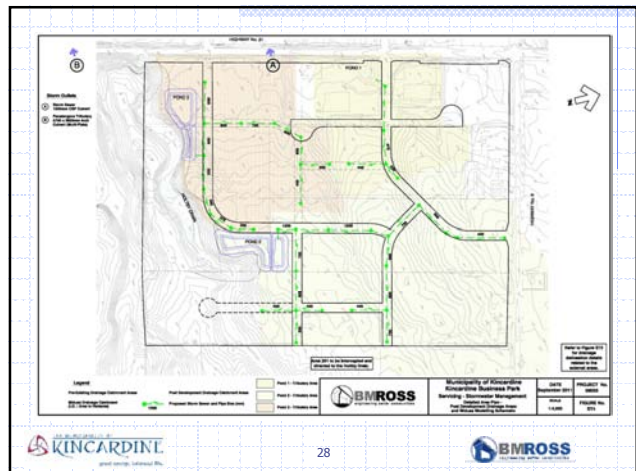
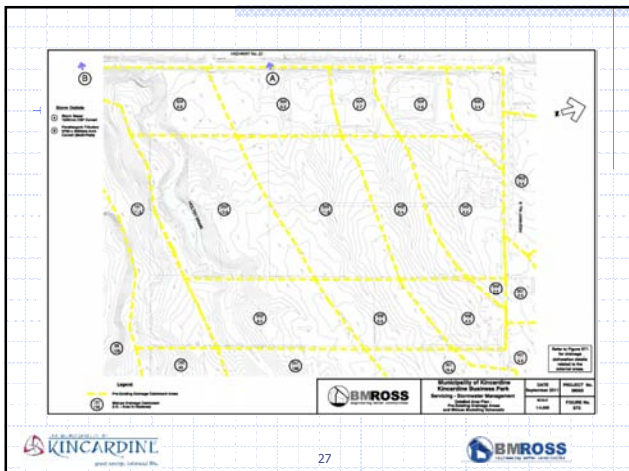
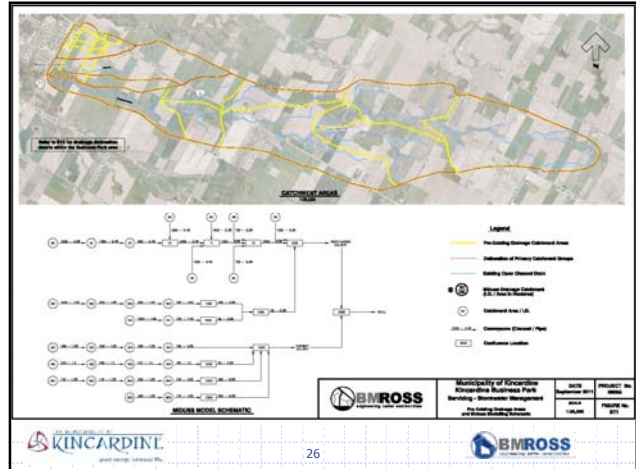



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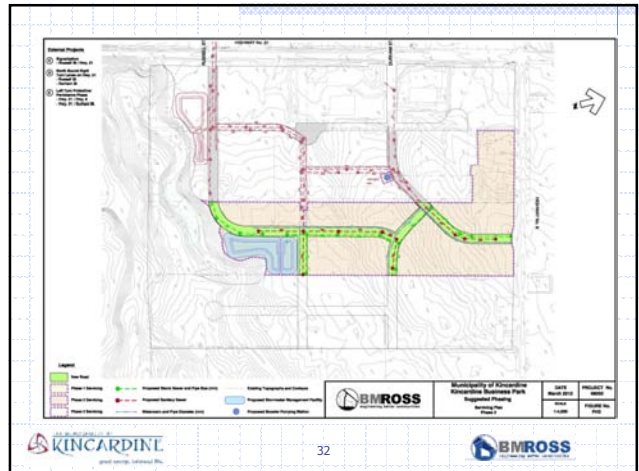
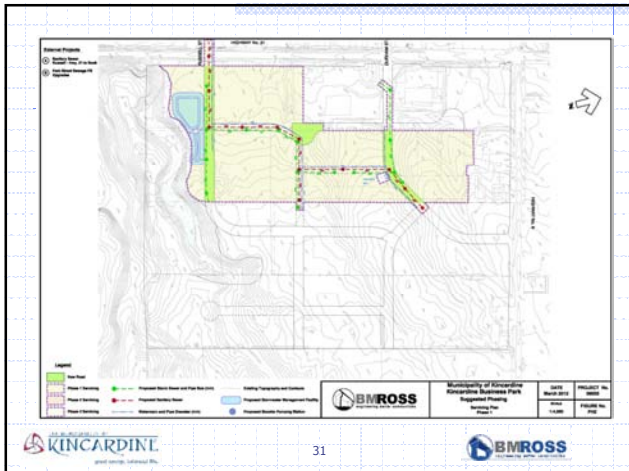
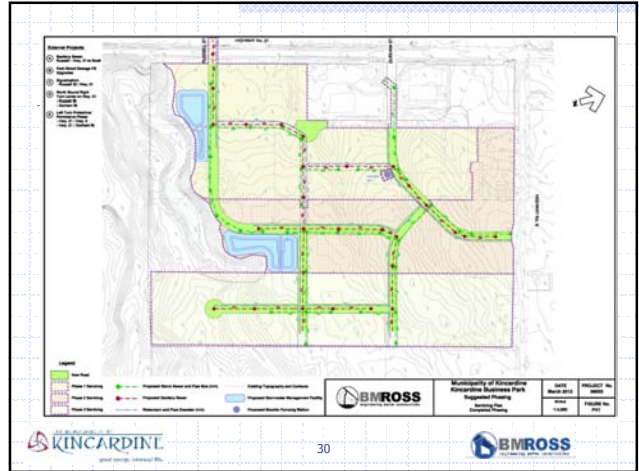
KBP – Servicing Master Plan Storm Water Management (SWM)

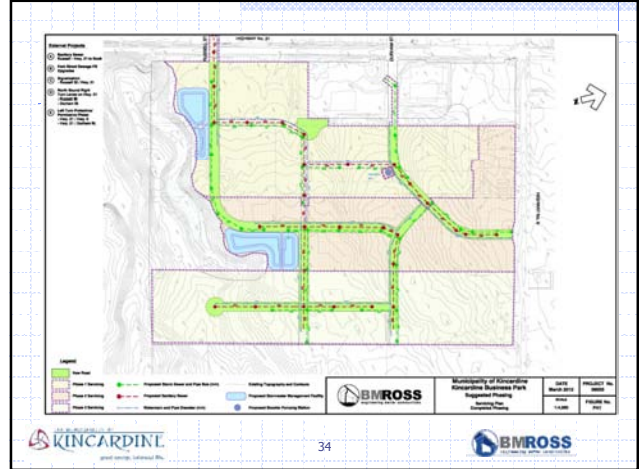
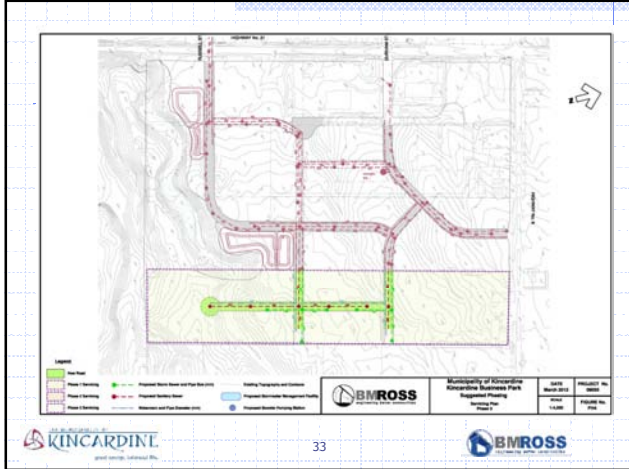
- Existing Conditions and Existing Drainage Outlets
- Proposed Storm Sewer System
- Individual Ponds vs. Communal/Regional
- Proposed SWM Facilities



KBP – Servicing Master Plan Phasing

- Possible Initial Phases
 - West to East with Extension of Services
- Development Interests





KBP – Servicing Master Plan Costs

- Total Costs
- Recovery Strategies

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<u>Work Item</u>	<u>Estimated Cost</u>
External Servicing	
Park Street Pumping Station Upgrades	850,000
Russell St. Sanitary Sewer – Hwy 21 to Scott St.	500,000
Transportation Improvements – Miscellaneous	350,000
Internal Servicing	
Sanitary Collection System	850,000
Water Distribution System	950,000
Water Booster Station	700,000
Storm Collection System	1,550,000
Stormwater Management Facilities	550,000
Road	3,700,000
TOTAL	\$10,000,000
Approx. Cost per Developable Hectare	\$200,000
(Cost per Acre)	\$80,000

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KBP – Servicing Master Plan Next Steps

- Receive and Review Comments from Public and Agencies and considered in the Master Plan
- Prepare Master Plan Report
- Review with Council
- Proceed with Environmental Assessment for Sewage Pumping Station and Water Booster Station

KBP – Servicing Master Plan

Questions and Comments

Ministry of Transportation

Engineering Office
Corridor Management Section
West Region

659 Exeter Road
London, Ontario N6E 1L3
Telephone: (519) 873-4598
Facsimile: (519) 873-4228

Ministère des Transports

Bureau du génie
Section de gestion des couloirs routiers
Région de l'Ouest

659, chemin Exeter
London (Ontario) N6E 1L3
Téléphone: (519) 873-4598
Télécopieur: (519) 873-4228



April 23, 2013

By email: derb@bmross.net

Dale Erb, P. Eng
B. M. Ross and Associates Limited
Engineers and Planners
62 North Street
Goderich, ON
N7A 1L3

RE: Applicant: Municipality of Kincardine
Submission No.: Kincardine Business Park Servicing Plan
Lots 1 & 2, Concession 1 South of Durham Road
Municipality of Kincardine, County of Bruce – Highways 21 and 9

The Ministry of Transportation has completed its review of the above noted Servicing Plan. The Servicing Plan has been considered and reviewed in accordance with the requirements of our highway access policies and criteria, and the permit requirements of the *Public Transportation and Highway Improvement Act*. The following outlines our comments and requirements.

1. Use a 2% growth rate for the purpose of this study
2. The report indicates completion of the first phase of the proposed development by 2016 and the second phase by 2021. An analysis for each major phase of development and the 5, 10 year horizons beyond full build-out of the site are required as per Ministry of Transportation Guidelines for the Preparation of Traffic Impact Studies.
3. The Durham Street distance between Highway 21 and Millennium Way is approximately 150 meters and contains three access points serving the Canadian Tire store, Sobeys and Tim Horton's. The proposed site traffic assignment along this link road may cause traffic operational problems for intersections and site access. The consultant is to identify other viable option(s) to reduce site traffic through this link.
4. The Highway 21 distance between Highway 9 and Durham Street is approximately 325 meters long. This distance is not adequate for single back-to-back left-turn lanes to serve projected left-turning traffic volumes. The consultant is to identify any required geometric improvements or other viable option(s) to accommodate future left-turning traffic volume.
5. The private drive, access point with Russel Street indicated in the site plan is in close proximity to Highway 21, and may cause traffic operational problems for the intersection

.../2

of Highway 21@Russel Street. We recommend the consultant consider relocating the access point to Russel Street of this private drive.

6. The report assessed the requirement for traffic signal installation as a result of the proposed development at the intersection of Highway 21 and Russell Street. The consultant is to include any required geometric improvements resulting from the signal installation at this intersection in the revised report.
7. The consultant should assess the geometric improvement requirements for existing signalized intersections. The consultant should calculate the required storage lanes using the Geometric Design Standards for Ontario Highways and/or Ontario Traffic Manual Book 12 (March 2012 Edition) methodologies.
8. Synchro input/output:
 - I. Existing traffic signal cycle length is approximately 90 sec. for the intersection of Highway 21 @ Highway 9 and approximately 100 sec. for the intersection of Highway 21 @ Durham Street. The need for additional advanced or protected phases will result in longer cycle lengths.
 - II. We recommend the consultant using existing signal timing splits for analysis in this study rather than Synchro optimization.
 - III. We recommend the consultant justify the requirement for protective-permissive left-turn phase using methodology described in the Ontario Traffic Manual Book 12.
 - IV. Highway 9 link speed is 80 km/hr.
9. We request that the consultant provide the electronic Synchro files for our review.
10. Provisions must be in place to protect all of the highway ditches, if necessary during construction, and at the developers expense.
11. The developer must obtain all necessary approvals including the Municipality, the Conservation Authority, Ministry of Environment, Ministry of Natural Resources and Ministry of Transportation.
12. The Ministry of Transportation requires analysis for the storm events for both the pre-development and post-development conditions showing no increase in flow towards either Highway 21 or Highway 9 drainage systems after post-development.
13. The report must demonstrate that there will be no negative impacts upstream or downstream to the Highway 21 and Highway 9 drainage systems (up to and including the 100yr storm event) because of this development or because of the failure of the proposed drainage works.
14. The Ministry of Transportation does not recognize any benefit from the attenuation of stormwater runoff using parking lot or rooftop storage where the control is achieved by orifice devices.

15. The report indicates that Business Park development may be done in phases but no indication of stormwater control during the development and if not all phases developed at the same time is there efficient stormwater management in place?
16. The owner's consultant in preparing the Traffic Impact Study should refer to the Ministry of Transportation's website for a comprehensive set of traffic related documentation requirements to assist in preparing their report:
http://www.mto.gov.on.ca/english/engineering/management/corridor/TIS_Guidelines_EN.pdf. The owner should be aware that any highway improvements identified from to the Ministry of Transportation's review and analysis of the Traffic Impact Study will be the responsibility, financial and otherwise, of the owner.
17. The owner's consultant in preparing the Stormwater Management Report should refer to the Ministry of Transportation's website for a comprehensive set of ministry drainage related documentation requirements to assist in preparing their report:
<http://www.mto.gov.on.ca/english/engineering/drainage/index.shtml>
18. Under the *Public Transportation and Highway Improvement Act*, Ministry of Transportation permits are required for all grading/construction located within 800 m of the Highway 21 and Highway 9 highway (property) limits. The Ministry of Transportation will require that all new residential structures be setback a minimum of 8.0 m from the Highway 21 and Highway 9 highway (property) limits. The Ministry of Transportation will require that all new commercial buildings and structures, both above and below ground, including stormwater management ponds/facilities, be setback a minimum of 14.0 m from the Highway 21 and Highway 9 highway (property) limits.
19. Under the *Public Transportation and Highway Improvement Act*, Ministry of Transportation permits are required for all visible signs proposed to be located within 400 m of the Highway 21 and Highway 9 highway (property) limits.
20. Under the *Public Transportation and Highway Improvement Act*, Ministry of Transportation permits are required for all access points to Highway 21 and Highway 9.
21. Under the *Public Transportation and Highway Improvement Act*, Ministry of Transportation permits are required for all encroachments proposed to be located, both above and below ground within the Highway 21 and Highway 9 highway (property) limits.

Should you have any questions, please contact our office.



Chris Dixon
Corridor Management Planner
Corridor Management Section
MTO - West Region, London

- c. Jessica Pegelo, Corridor Management Officer, Ministry of Transportation
Michelle Bar, Director of Building and Planning, Municipality of Kincardine



BMROSS
engineering better communities

B. M. ROSS AND ASSOCIATES LIMITED
Engineers and Planners
62 North Street, Goderich, ON N7A 2T4
p. (519) 524-2641 • f. (519) 524-4403
www.bmross.net

Transmittal Record

From: Lisa Courtney
lcourtney@bmross.net

<input checked="" type="checkbox"/> Regular Mail	<input type="checkbox"/> Hand
<input type="checkbox"/> Courier	<input type="checkbox"/> Delivered

To:
Audrey Holden, Historic Saugeen Métis

Re:
Kincardine Business Park – Stage 1 Archaeology
Assessment

Date: April 23, 2014

File #: 08055

We enclose:

- 1 copy of the Stage 1 Archaeological Assessment for the Kincardine Business Park Servicing Master Plan by Timmins Martelle Heritage Consultants Inc.



1078 Bruce Road 12, P.O. Box 150, Formosa ON Canada N0G 1W0
Tel 519-367-3040, Fax 519-367-3041, publicinfo@svca.on.ca, www.svca.on.ca

Sent via email and regular mail

B.M. Ross and Associates Limited
62 North Street,
Goderich, ON
N7A 2T4

October 28, 2016

ATTENTION: Dale Erb, P.Eng.

Dear Mr. Erb:

RE: Kincardine Business Park Servicing Plan
Part Lots 1-4, Concession 1 SDR
Southeast Corner of Highway 9 and Highway 21
Geographic Township of Kincardine
Municipality of Kincardine (Kincardine Business Park Expansion)

The Saugeen Valley Conservation Authority (SVCA) has reviewed this proposed servicing plan in accordance with the SVCA's mandate and policies. The proposed Kincardine Business Park Servicing Plan would facilitate the creation of a commercial development area and a new roadway network complete with servicing and stormwater management.

Details to the proposed servicing with sanitary, water, roadways, and stormwater management have been provided to the SVCA December 3, 2013 and September 6, 2016. The SVCA has reviewed the Servicing Plan dated September 19, 2011, revised June 29, 2016. The proposed development will be subject to an Environmental Assessment review process that the SVCA will have opportunity to review and comment on. The SVCA offers the following comments.

1. It appears the proposed stormwater pond in the southwest corner of the property may be located within the SVCA's Regulated Area, and potentially within the valley slope setback of the Holtby Municipal Drain. The extension east of Russel street may also intersect this area, and street 'A' may be within the floodplain of the Holtby Drain. These proposals would require permission from the SVCA in the form of an SVCA permit to Alter a Regulated Area or Watercourse.
 - i) Alterations to the valley of a watercourse may not be acceptable to SVCA staff.
 - ii) Alterations to the floodplain of a watercourse may not be acceptable to SVCA staff.
 - iii) Alterations within the slope setback of a steep slope many not be acceptable to SVCA staff.
 - iv) Please confirm access for maintenance purposes to the Holtby Drain is available with the proposed southwest pond design and roadways.

2. There has been a new stormwater pond constructed associated with new development in the area in part lot 2, concession 1 SDR associated with a new hotel. Has this pond been considered in this



Watershed Member Municipalities

Municipality of Arran-Elderslie, Municipality of Brockton, Township of Chatsworth, Municipality of Grey Highlands, Town of Hanover, Township of Howick, Municipality of Morris-Turnberry, Municipality of South Bruce, Township of Huron-Kinloss, Municipality of Kincardine, Town of Minto, Township of Wellington North, Town of Saugeen Shores, Township of Southgate, Municipality of West Grey

report?

3. The drainage characteristics of lands that the ponds will be installed upon are being altered as a part of this proposal and will need to be accounted for by the report (permeability, runoff, etc.).
4. The area, or a portion of the area, appears to have existing agricultural field tile installed. During works on site, for various phases any encountered field tiles should be appropriately outlet. Have these field tile outlets been factored into the stormwater plan, pre and post development? Phasing of development may impact these tiles if present.
5. Please clarify the allowable proposed impervious area of the proposed development areas. The SVCA is not clear how the impervious roadway surfaces, ponds, boulevards, etc. have factored into the allowable impermeable calculations for the developable lands.
6. A portion of the southwest Stormwater Management pond is not within Phase 1 servicing lands.
7. The central proposed pond is shared between two phases of the proposed development. The pond would need to be part of one phase or another the SVCA suggests (Phase 1 appropriate the SVCA recommends).
8. The SVCA is aware that in nearby stormwater ponds there has been local interest to provide habitat in these features compared with a typical dry pond design. The Municipality appears to proposed wet pond design. Could habitat enhancement components be added to the proposed ponds?
9. Additional details are needed with regards to lot grading and sediment control as the process proceeds for SVCA review.
10. Proposed roadways are indicating development lands will extend to the east in the future. No development potential has been taken into consideration upstream of lot 4. Perhaps a drainage route, or capacity for that future development, can be included in the proposed.
11. The SVCA notices there are proposed watermains to cross the valley and watercourse to the south (Holtby Drain). While not necessarily unacceptable permission will be required from the SVCA and these features would need to be designed to not impact the watercourse and be done in the appropriate time of year.

The SVCA will continue our review upon clarifications and/or revisions being provided to the SVCA. Generally this proposal is acceptable to the SVCA provided the above comments are addressed. The SVCA will be involved with the Environmental Assessment review process and will provide additional review comments when more detailed plans are provided for review.

If you have any questions on the above, please do not hesitate to contact this office.

Sincerely,



Erik Downing
Manager, Environmental Planning and Regulations
Saugeen Conservation

ED/

cc: Maureen Couture, Authority Member, SVCA, via e-mail
Andrew White, Authority Member, SVCA, via e-mail
Donna MacDougall, Clerk, Municipality of Kincardine, 1475 Con. 5 R.R#5, Kincardine, ON N2Z 2X6

Ministry of Transportation

Engineering Office
Planning and Design Section
Southwestern Region

659 Exeter Road
London, Ontario N6E 1L3
Telephone: (519) 873-4598
Facsimile: (519) 873-4228

Ministère des Transports

Bureau du génie
Section de planification et de conception
Région du Sud-Ouest

659, chemin Exeter
London (Ontario) N6E 1L3
Téléphone: (519) 873-4598
Télécopieur: (519) 873-4228



Dale Erb,

January 23, 2017

*B. M. Ross and Associates Limited
Engineers and Planners
62 North Street
Goderich, ON N7A 2T4*

RE: Kincardine Business Park – 2016 Document Review

Submission No.: 2016
Lot 2 & 3, Concession 1 SDR
County of Bruce
Municipality of Kincardine - Highway 21

Further to our meeting on December 20, 2016 regarding the subject proposed development lands, the following summarize our comments:

Documents Reviewed

- Municipality of Kincardine – Kincardine Business Park – Servicing Plan – File No. 08055 – Revised June 29, 2016.

Traffic Impact Study

- Turning movements that were conducted in 2012 and 2013, some of the development was built between the years 2008 and 2012. The 2012 turning movement counts may not have all of the new traffic from the development that was built between these years. We suggest that the consultant use more current volumes to reflect current conditions. This update can be by addendum of the TIS.

Stormwater Management Report

- The MTO requires at set back of 14m from property line with no fixed structures in that designated area (headwalls, retaining walls, berms etc.).
- The report must demonstrate that there will be no negative impacts upstream or downstream to the Highway 21 drainage system (up to and including the 100yr storm event) because of this development or because of the failure of the proposed drainage works.
- The Ministry requires analysis for a full range of storm events for both the pre-development and post development conditions showing no increase in flows for all storm events.

- Provisions must be in place to protect the highway ditch, if necessary during construction, at the developer's expense.
- The rainfall data and IDF curve information should be taken from the MTO drainage website.
- The Rational method should be used for areas under 100ha.
- The ministry does not allow the use of orifice plates as a means of control. A section of reducer pipe with an inside diameter equivalent to the inside diameter of the orifice design is acceptable.
- The indication is that the ponds (2 & 3) are going to outlet into our Highway 21 ditch and the Holtby Drain respectively how is this being accomplished, pond 2 is located in the middle of the industrial park.

Proposed Road Layout

- In regards to the configuration of the municipal road network that connects to the provincial highway network, MTO wants to ensure that there is adequate setback for entrances and municipal road intersections. The configuration shown should consider adequate spacing for future warranted turning lanes and other traffic impact mitigation measures for any entrance or intersection that is expected to intensify.
- In review of the municipal road network configurations detailed in TR1 and TR2, for the reason noted above, MTO's preference would be TR1 because this configuration would allow for more future traffic mitigation measures when the developments intensify and also to protect the highway intersection for additional future traffic mitigation measures (turning lanes/storage etc.) when warranted by increase demand from population growth and development intensification.
 - As a note regarding the private drive shown in Figure TR1, MTO provided comments in the past (April 23, 2013) recommending the reconsideration of this access point. MTO would like to reiterate this comment as any access point that is in close proximity to the intersection will limit the future traffic mitigation measures such as turning lanes.

Municipal Services

In review of Figure WM1 and Figure SA3 which show proposed utility extensions crossing Highway 21, MTO has the following comments:

- MTO will require further detail of the proposed crossing locations including construction method, Geotechnical details, depth (and location) of crossing, casing detail and impacts to highway traffic. As municipal utilities are not identified under the Public Service Works on Highways Act, MTO may require the municipality to enter into a legal agreement (with MTO) to address items such as (but not limited to) relocation responsibilities and indemnification.

Visibility Triangles

- That prior to final approval, MTO will require a review of all of the access points in the Kincardine Business Park to ensure the visibility triangles are designed to meet the minimum

dimensions in accordance with the *Geometric Design Standards Manual for Ontario Highways*. All visibility triangles shall be dedicated as public highway under the owner's certificate on the final plan. A draft of the final Plan of Subdivision must be submitted to MTO for review.

0.3m Reserve

- That prior to final approval, a 0.3 m reserve extended across the entire highway frontage including the visibility triangles (with the exception of the street opening(s)) be conveyed by deed to the MTO. All reserves by deed must be free and clear of all mortgages, liens, and encumbrances. The reserve must be illustrated as Blocks on the Plan of Subdivision. A draft of the final Plan of Subdivision must be submitted to MTO for review. A draft of the transfer of deed and certification of title conveying the Blocks to the MTO must be submitted for review and approval prior to being registered.

Please feel free to contact me for further information, clarity or discussion.

Regards,



Zsolt Katzirz
Corridor Management Planner
Corridor Management Section

- c. *Bruce Potter – B.M. Ross – email only (bpotter@bmross.net)*
Michele Barr – Municipality of Kincardine – email only (mbarr@kincardine.net)



November 7, 2008

John deRosenroll, CAO
Municipality of Kincardine
1475 Concession 5, R. R. 5
Kincardine, ON N2Z 2X6

via email

Dear Sir:

RE: Business Park Servicing

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The purpose of that presentation was to determine how the costs of servicing for road extensions and trunk sanitary sewers could be shared amongst the developers of the balance of the business park.

It was noted that 21 Russ had purchased the balance of farm lot 1, with the exception of a small portion to be set aside for a Municipal tourist information booth, and would develop that land being fully responsible for all servicing and improvements related to that development. 21 Russ has also purchased that portion of farm lot 2 immediately behind their lot 1 property and a further portion of farm lot 3. BMROSS were instructed to consider the development on lot 2 which is proposed to be continuous with the lot 1 development in a similar manner. All costs of constructing roads and servicing for the 21 Ross lands on farm lots 1 and 2 were excluded from the cost sharing as was the developer's acreage for this portion of the development.

The County of Bruce Planning Department had provided suggestions for a proposed ultimate road pattern and following comments and revisions by municipal staff, that pattern was included as Figure 1 of the April 28th document. Based upon discussions with adjacent developers it is now proposed to delete that portion of Millenium Way between the 21 Russ and Dalron sites. The attached amended road pattern is shown on Figure 1A. Whether the cul-de-sac shown is constructed in the manner illustrated will be based on the final configurations of the site plans for the adjacent developments.

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- Russell Street extension to easterly limit of lot 2
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- Trunk sanitary sewer construction on Russell Street, through the 21 Russ and Dalron lands, and along the Durham Street extension.

Attached as Figure 2A is an amended drawing showing this interim development.

It is noted that the downstream sewers in the adjacent residential subdivision have little surplus capacity and this has resulted in a proposal that a new trunk sanitary sewer be constructed from Scott Street easterly on Russell to service the balance of the business park lands. While the Municipality may allow sanitary service sewer connections either on a permanent or interim basis to the existing Durham Street sanitary sewer, it is the intent that all properties on the remaining three farm lots would participate in cost sharing for the installation of the trunk sewer. The location of the sewer shown on the attached sketch on the Dalron site is in a location compatible with the most recent draft site plans received by the Municipality. This sewer can be moved to a more appropriate location if needed.

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In a subsequent meeting with 21 Russ they asked that the Municipality look at sharing the cost based upon:

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Based upon the discussions at our meeting with staff and the planning department on August 5th, we were instructed to provide an updated cost sharing schedule in a similar format to that presented in April. Attached, as Table 2A is that schedule. This document is based upon the

slightly revised interim servicing scheme and presents possible cost estimates for the works. Included in these estimates are allowances for construction, engineering and some contingencies. No detailed design has been completed. Excluded from these costs are improvements to the Park St. Pumping Station, any communal SWM works, and the construction of a water booster pumping station. Trunk sewer costs are proposed to be shared amongst all of the development properties and the initial road costs are proposed to be shared amongst the developers that will receive the initial benefits. The costs for the completion of the balance of the servicing in the future would be expected to be shared amongst the remaining lands.

It is important that the Municipality establish the level of commitment of each of the developers and their expected timing for their development so that a detailed servicing schedule can be established.

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Yours very truly,

B. M. ROSS AND ASSOCIATES LIMITED

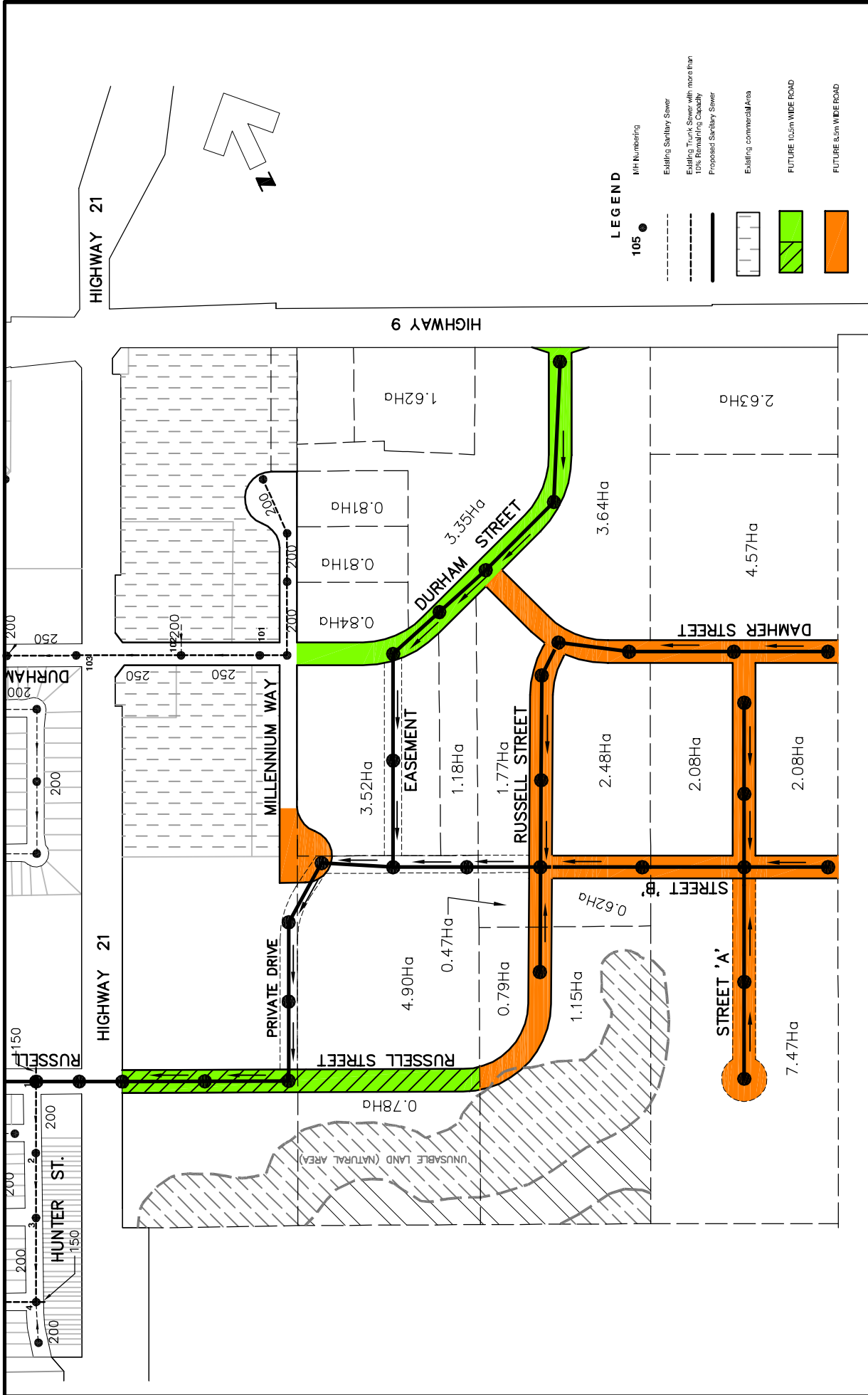
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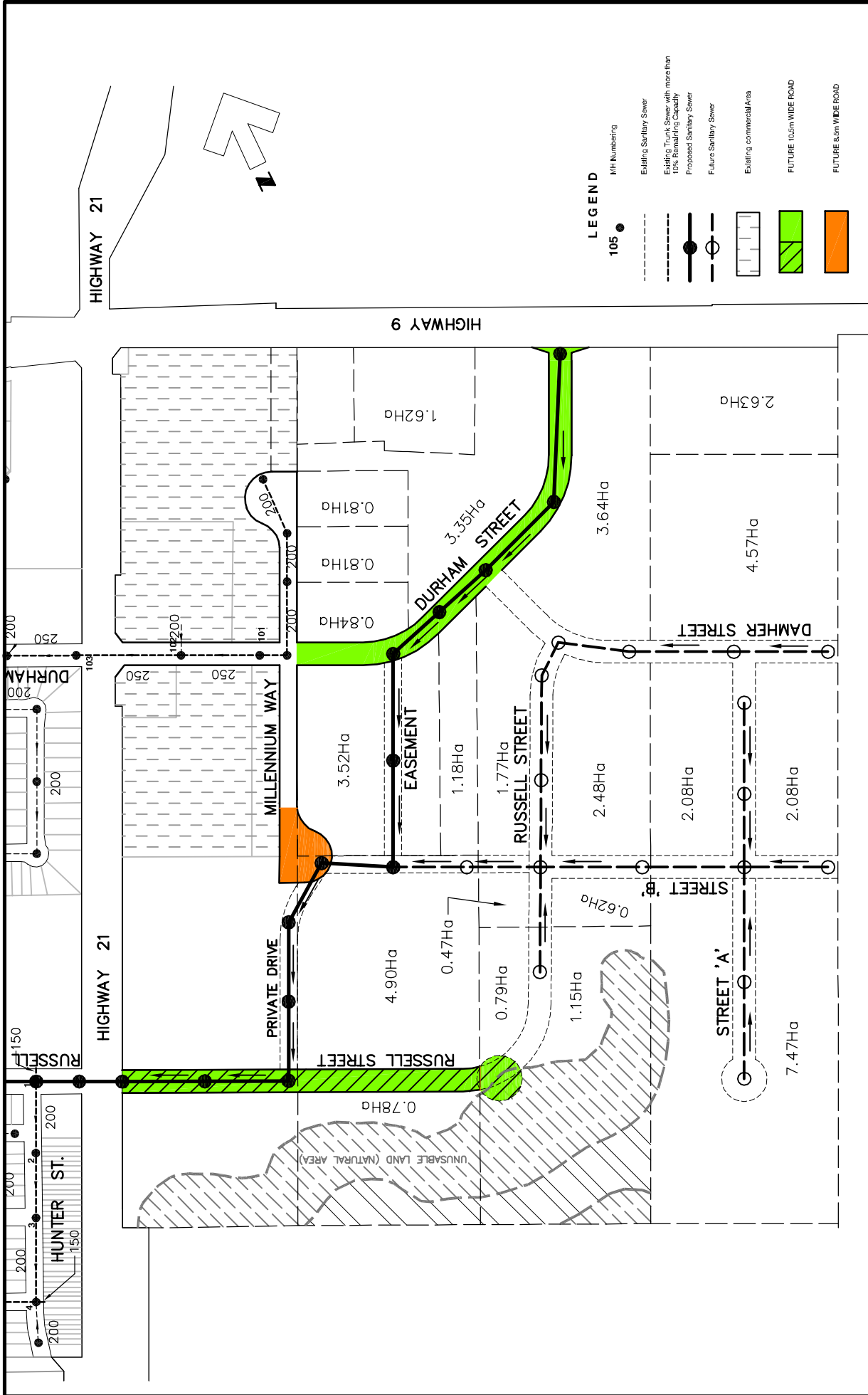
B. W. Potter, P. Eng.

BWP:es

c.c. Jim O'Rourke
Michelle Barr
Bill Hollo, County of Bruce, Planning Department



	Municipality of Kincardine Business Park Development Area Full Development Roads and Sanitary Sewer	
	DATE Nov. 7, 2008	SCALE N.T.S.
PROJECT No. 08055		FIGURE 1A



	Municipality of Kincardine Business Park Development Area Interim Development Roads and Sanitary Sewer	
	PROJECT No. 08055	FIGURE 2A
DATE Nov. 7, 2008	SCALE N.T.S.	

Table 2A

08/11/2008

Suggested Cost Sharing

Interim development:

Parcel/Owner	Approx. Developable for Trunk Sewer Area (ha.)	Cost Sharing Trunk Sewer per ha.	Approx. Developable for Roads Area (ha.)	Percent of Total	Cost Sharing Roads	Total
DHC:						
Former Quinn lands	1.62	12,811	1.62	10.31%	149,495	162,306
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Part 9	3.35	26,492	3.35	21.31%	308,995	335,487
Sub-Total	11.07	87,541	11.07	0.7042	1,021,090	1,108,631
Dalron:						
Part 4, 6	4.65	36,772	4.65	29.58%	428,910	465,682
21 Russ:						
Part 5 (21Russ)	1.94	15,342			-	15,342
Stewart:						
Part 7	5.34	42,229			-	42,229
Farrell:						
Lot 4	16.2	128,110			-	128,110
Total	39.2	309,994.00	15.72	1	1,450,000	1,759,994

Trunk Sewer Costs to be shared: \$ 310,000.00 \$ 7,908.00 per ha.

Road and sewer servicing costs to be shared: \$ 1,450,000.00

Total \$ 1,760,000.00



**MUNICIPALITY OF KINCARDINE
BUSINESS PARK
DEVELOPMENT COST SHARING**

1.0 PURPOSE

The Municipality of Kincardine wishes to determine how the costs of the road extensions and trunk sanitary sewers would be shared for the development of the balance of the Business Park. The Municipality has asked B. M. Ross and Associates to prepare this draft document to commence discussions with developers on that cost sharing.

2.0 BACKGROUND/HISTORY

Four farm lots were designated as Business Park in the Municipality's official plan.

The first lot was purchased by Kincardine. Kincardine became the developer of this parcel and for the northerly two thirds of the lot completed all services and sold parcels as serviced land.

The construction of Durham Street, Highway 9 and 21 improvements and the associated services were completed by Kincardine. This includes the Millennium Way extension to the north which has serviced the lands north of the Canadian Tire property.

The proposed sale to 21 Russ on the southerly portion of Lot 1 is contingent on that developer doing all of the servicing which includes:

- Road improvements on Highway 21.
- Construction of Russell Street extension and improvements.
- Water and sewer extensions from Hunter through their site.
- Storm water management for their site and a review of how the balance might be incorporated.
- Provisions for easements, access for traffic, site services and utilities through the site.
- Provision is to be left for the tourist information booth.

The final layout of the 21 Russ site is subject to discussions with the MTO and the outcome of their traffic study.

3.0 CURRENT DEVELOPMENT PROPOSALS

The following current development proposals are being considered or discussed:

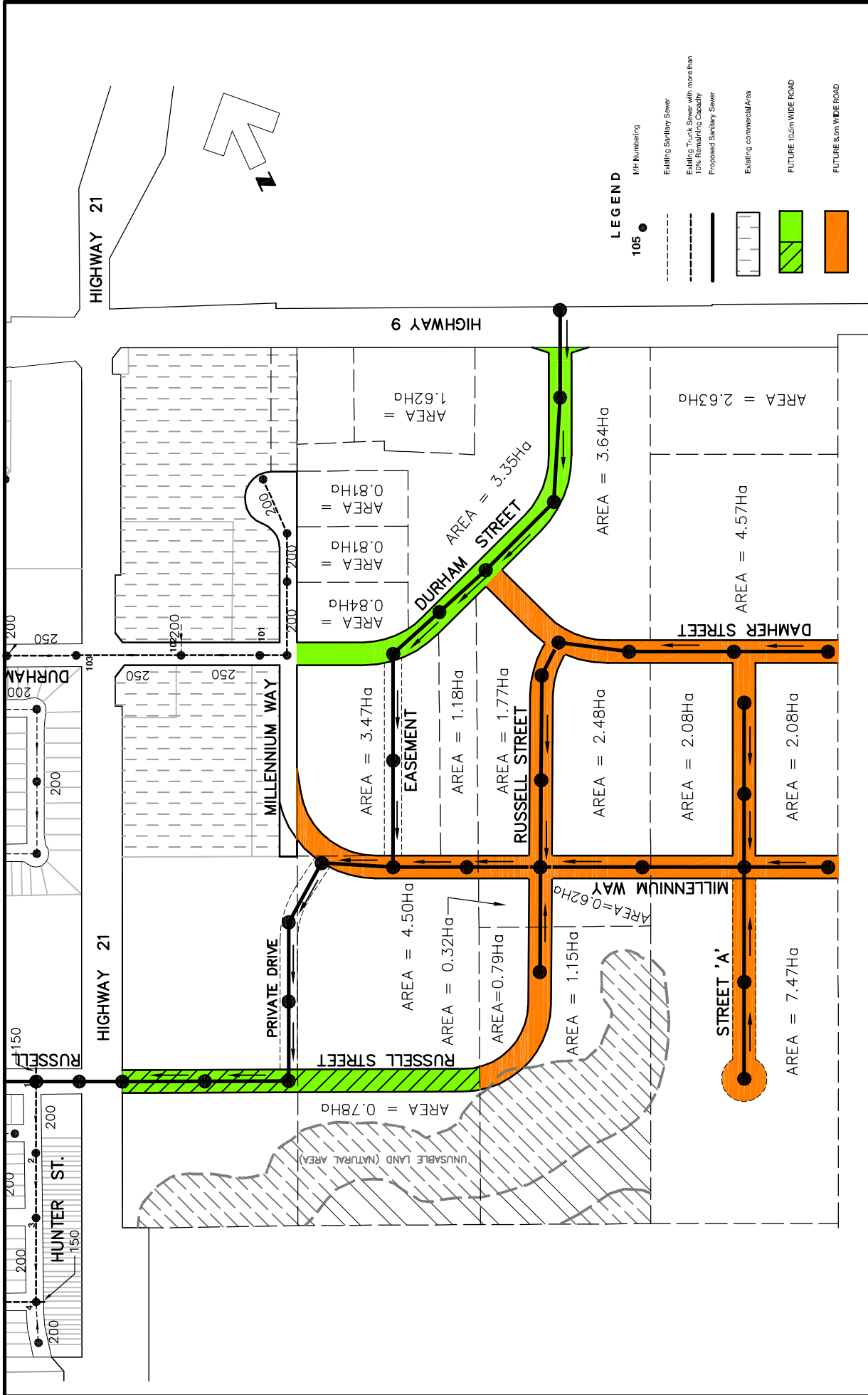
- A site plan agreement has been completed with DHC for the lands on Lot 1 at the north end of Millennium Way.
- The Canadian Tire lands on Lot 1 immediately north of the existing store are vacant.
- The developer of the carwash site on Lot 1, behind Canadian Tire would appear to be starting to proceed with his development.
- The Municipality has had preliminary discussions with respect to the proposed Bawa development.
- There have been discussions on the proposed Dalron site concerning the installation of commercial facilities.
- It is understood that a developer has purchased all of the lands north of the Durham Street extension and north of Damher Street.
- There has been a desire from some of the developers to have their sanitary sewer discharge to the existing Durham Street sewer.

4.0 SERVICING AND ROADS PATTERN

The County of Bruce Planning Department has completed a recommended pattern for development and installation of new roads through the development area. This road pattern, as slightly modified by BMROSS is shown on the attached sketch. It is anticipated these roads will be constructed as development progresses. It is also anticipated by the Municipality that the remaining development land should be assessed a share of the cost of the construction of the Russell Street trunk sewer together with a share of the cost of the various development roads.

Figure 1 shows that road pattern.

A review of anticipated ownership of the properties has been completed based upon a sketch completed by Ron Dore O.L.S. This is summarized below in Table 1.



	Municipality of Kincardine Business Park Development Area Full Development Roads and Sanitary Sewer	
	DATE April 28, 2008	SCALE N.T.S.
PROJECT No. 08055	FIGURE 1	

Table 1

Parcel/Owner	Approx. Developable Area (ha.)	Percent of Total
Former Quinn lands	1.62	4.15%
Part 1 (Bawa)	0.81	2.07%
Part 2	0.81	2.07%
Part 3	0.84	2.15%
Part 8	3.64	9.32%
Part 9	3.35	8.58%
Part 4, 6 (Dalron)	4.65	11.91%
Part 5 (21Russ)	1.94	4.97%
Part 7	5.19	13.29%
Lot 4	16.2	41.49%
Total	39.05	100%

The 21 Russ lands on lot 2 are assumed to have similar responsibilities with respect to servicing as those lands on lot 1 and the cost of services across their property and the cost of the Russell Street extension to the rear of lot 2 has been excluded. That area is excluded from the chart above.

5.0 PRELIMINARY ESTIMATED COSTS

Preliminary estimated costs of the road construction have been presented based upon recent tenders of similar works. All costs include allowances for local sanitary collection, water distribution, storm water collection, road construction complete with curb and gutter, sidewalk, engineering, contingencies and GST. No allowance for communal Storm Water Management or the construction of a water booster pumping station is included.

For the purposes of this initial proposal, two types of road have been considered and the estimated cost per metre of construction is as follows:

- Durham Street extension and Russell Street extension to rear of lot 2 (green on attached sketch) -- \$2,250
- Remaining service roads. -- \$2,000

The trunk Sanitary Sewer from Hunter through the 21 Russ lands is the responsibility of that developer. The sewer from Scott to Hunter has a preliminary estimated cost of \$290,000. It is proposed that this cost should be shared by all of the development lands.

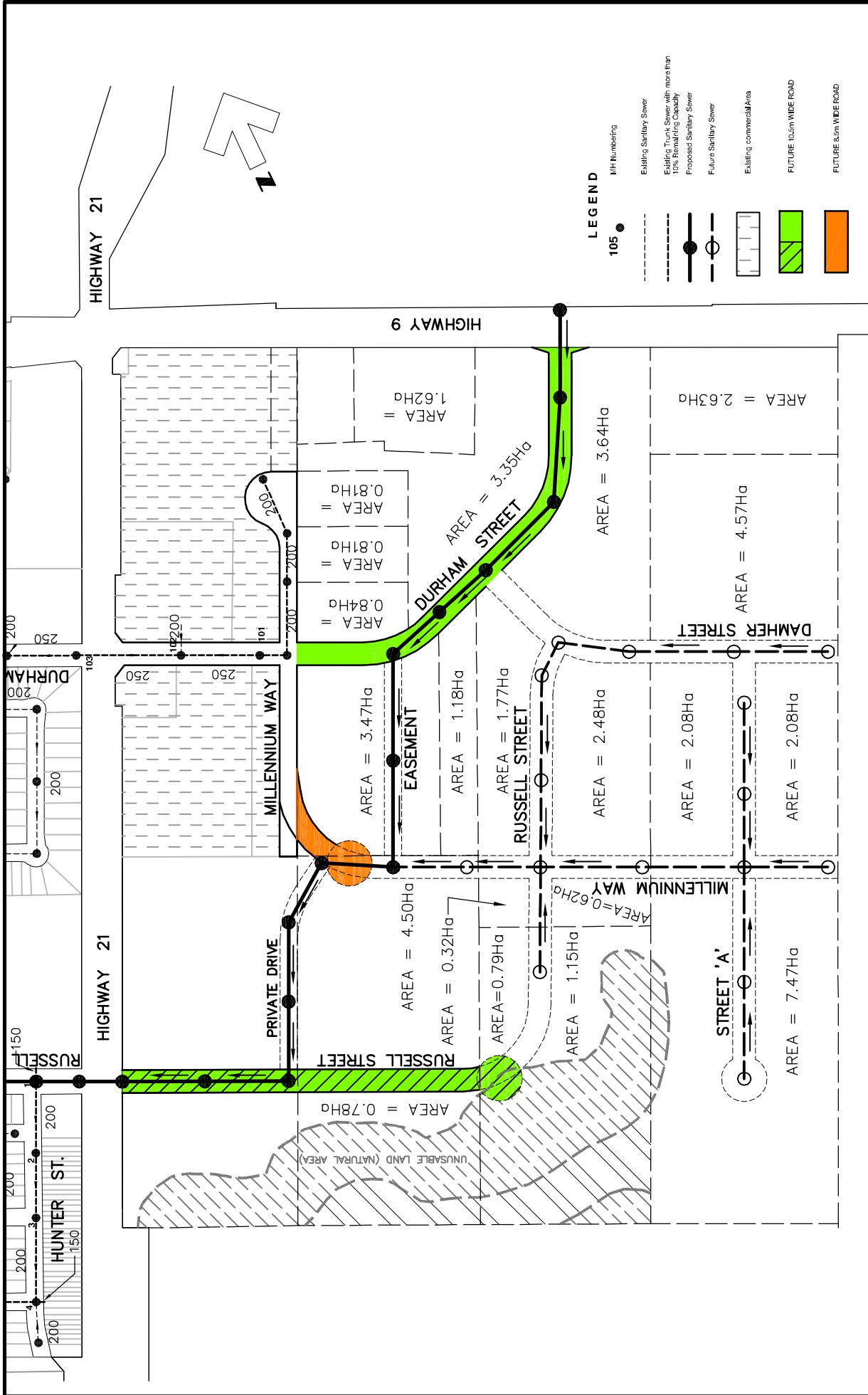
It is anticipated by the municipality that the completion of the development of the business park will take a number of years. It is assumed that initially development may be limited to the lands on the Durham St. extension and the 21 Russ lands.

The extent of this assumed interim development is shown on Figure 2. Based upon the preliminary submission for the Dalron development, a sewer easement through their property is proposed.

For that extent of development to proceed, the Durham Street extension and portions of the trunk sewer need to be constructed as shown on Figure 2. Preliminary cost sharing proposals for that extent of development are attached as Table 2.

6.0 SUMMARY

This document provides the basis for discussion for the sharing of costs for the development of the balance of the business park. The municipality and developers must reach some consensus as to how the services on the balance of the Business Park will be funded.



Municipality of Kincardine

Business Park Development Area

Interim Development Roads and Sanitary Sewer

DATE
April 25, 2008

SCALE
N.T.S.

PROJECT No.
08055

FIGURE
2

Table 2

Parcel/Owner	Approx. Developable for Trunk Sewer Area (ha.)	Cost Sharing Trunk Sewer per ha.	Approx. Developable for Roads Area (ha.)	Percent of Total	Cost Sharing Roads	Total
Former Quinn lands	1.62	12,000	1.62	10.31%	150,600	162,602
Part 1 (Bawa)	0.81	6,000	0.81	5.15%	75,200	81,201
Part 2	0.81	6,000	0.81	5.15%	75,200	81,201
Part 3	0.84	6,200	0.84	5.34%	78,000	84,201
Part 8	3.64	27,000	3.64	23.16%	338,400	365,404
Part 9	3.35	24,900	3.35	21.31%	311,300	336,204
						1,110,812
Part 4, 6 (Dalron)	4.65	34,500	4.65	29.58%	432,200	466,705
Part 5 (21Russ)	1.94	14,400			-	14,400
Part 7	5.19	38,500			-	38,500
Lot 4	16.2	120,300			-	120,300
Total	39.05	289,800	15.72	100%	1,460,900	1,750,717

Trunk Sewer Costs to be shared: \$ 290,000.00 \$ 7,426.38 /ha.

Road and sewer servicing costs to be shared:

Sewer Extension	\$ 95,000.00
Road Costs	\$ 1,366,000.00
Total	\$ 1,461,000.00

Length of 10.5 m. wide road	536	2,250	1,206,000
Length of 8.5 m wide road	80	2,000	160,000
Total	616		1,366,000

APPENDIX 4
2008 Cost Sharing Memo by BMROSS



November 7, 2008

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Municipality of Kincardine
1475 Concession 5, R. R. 5
Kincardine, ON N2Z 2X6

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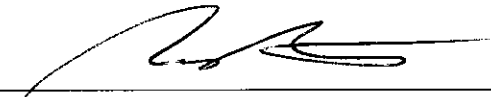
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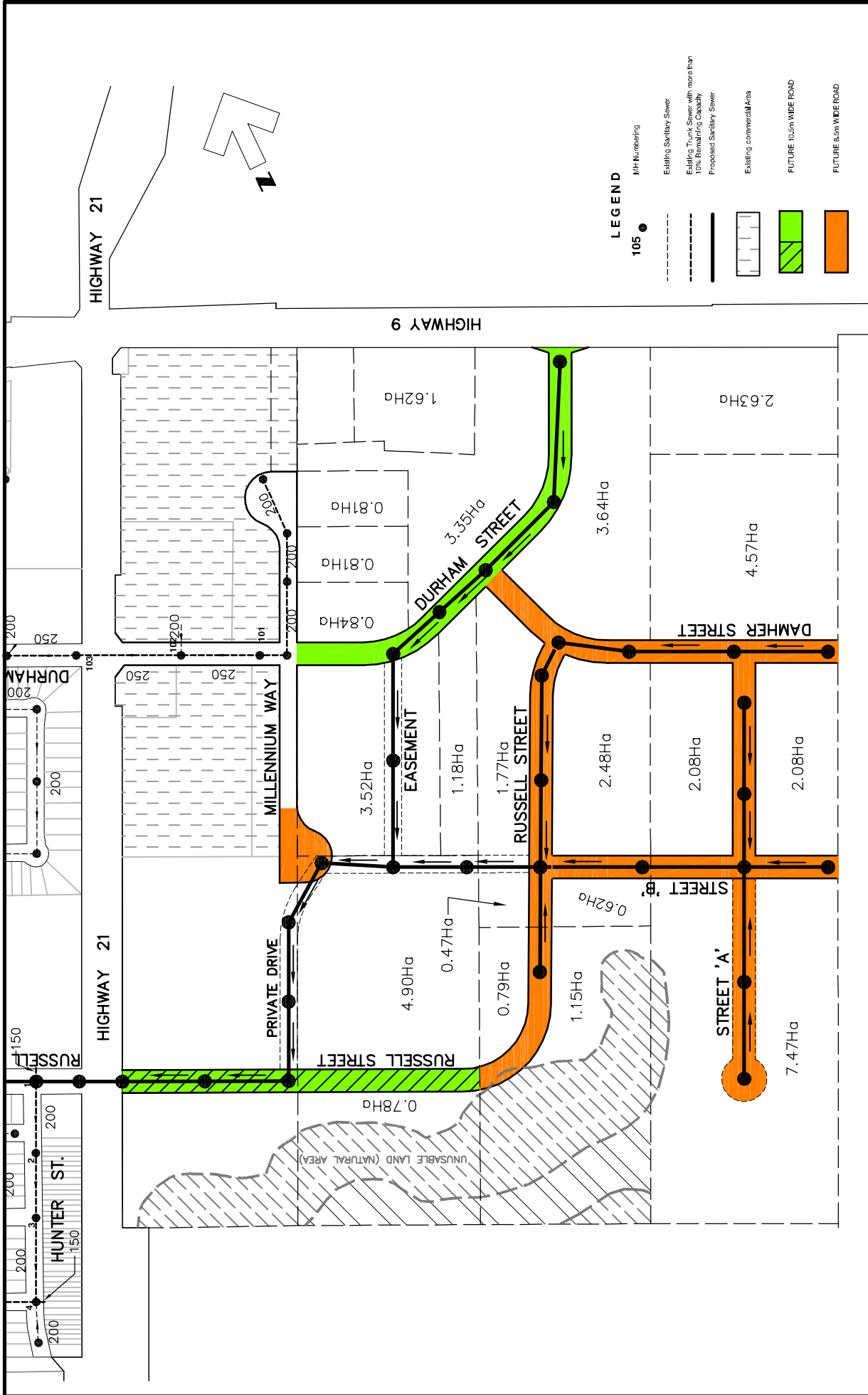
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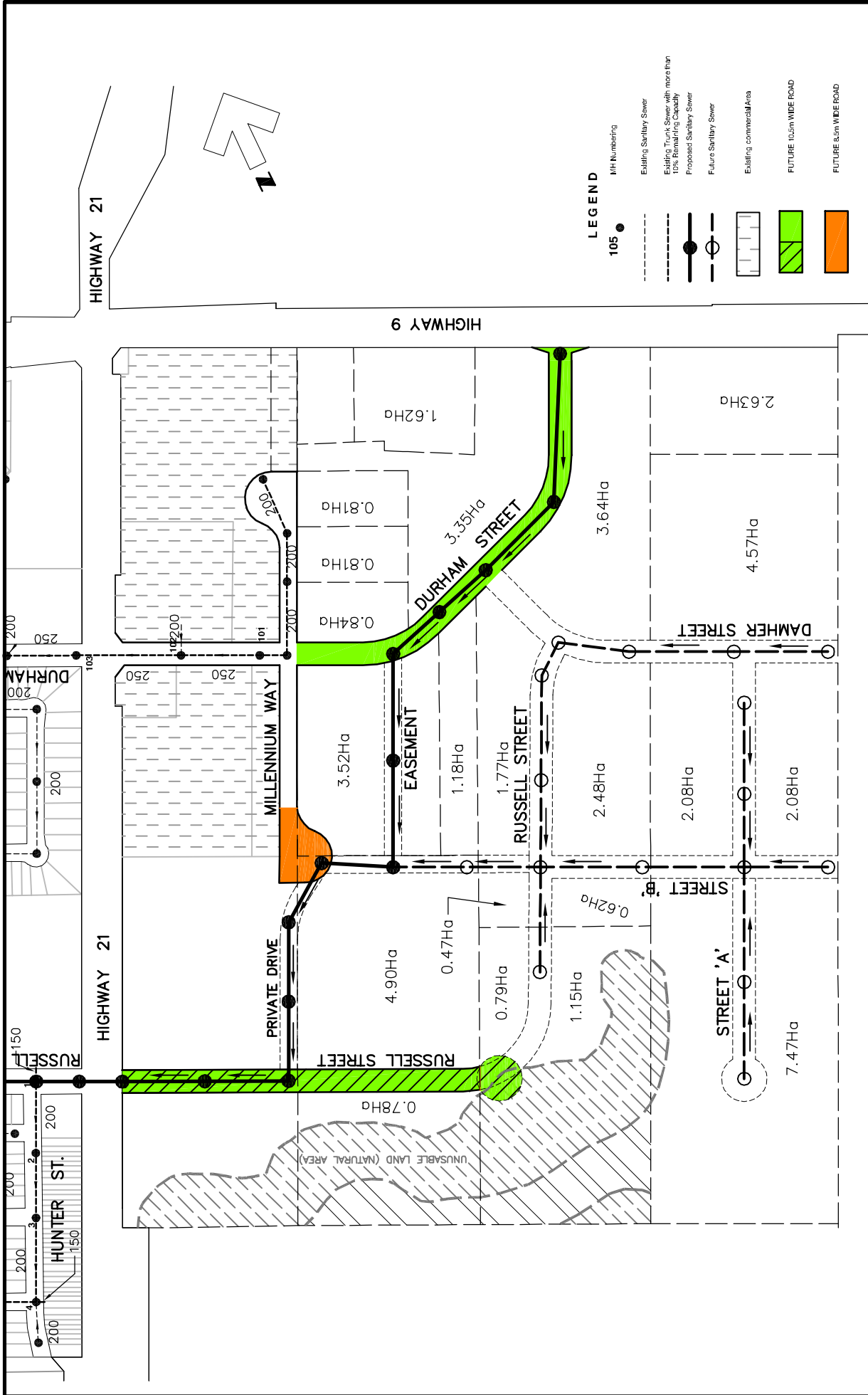
Per 
B. W. Potter, P. Eng.

BWP:es

c.c. Jim O'Rourke
Michelle Barr
Bill Hollo, County of Bruce, Planning Department



	Municipality of Kincardine Business Park Development Area Full Development Roads and Sanitary Sewer	
	DATE Nov. 7, 2008	SCALE N.T.S.
PROJECT No. 08055	FIGURE 1A	



	Municipality of Kincardine Business Park Development Area Interim Development Roads and Sanitary Sewer	
	DATE Nov. 7, 2008	SCALE N.T.S.
PROJECT No. 08055		FIGURE 2A

Table 2A

08/11/2008

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**MUNICIPALITY OF KINCARDINE
BUSINESS PARK
DEVELOPMENT COST SHARING**

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The construction of Durham Street, Highway 9 and 21 improvements and the associated services were completed by Kincardine. This includes the Millennium Way extension to the north which has serviced the lands north of the Canadian Tire property.

The proposed sale to 21 Russ on the southerly portion of Lot 1 is contingent on that developer doing all of the servicing which includes:

- Road improvements on Highway 21.
- Construction of Russell Street extension and improvements.
- Water and sewer extensions from Hunter through their site.
- Storm water management for their site and a review of how the balance might be incorporated.
- Provisions for easements, access for traffic, site services and utilities through the site.
- Provision is to be left for the tourist information booth.

The final layout of the 21 Russ site is subject to discussions with the MTO and the outcome of their traffic study.

3.0 CURRENT DEVELOPMENT PROPOSALS

The following current development proposals are being considered or discussed:

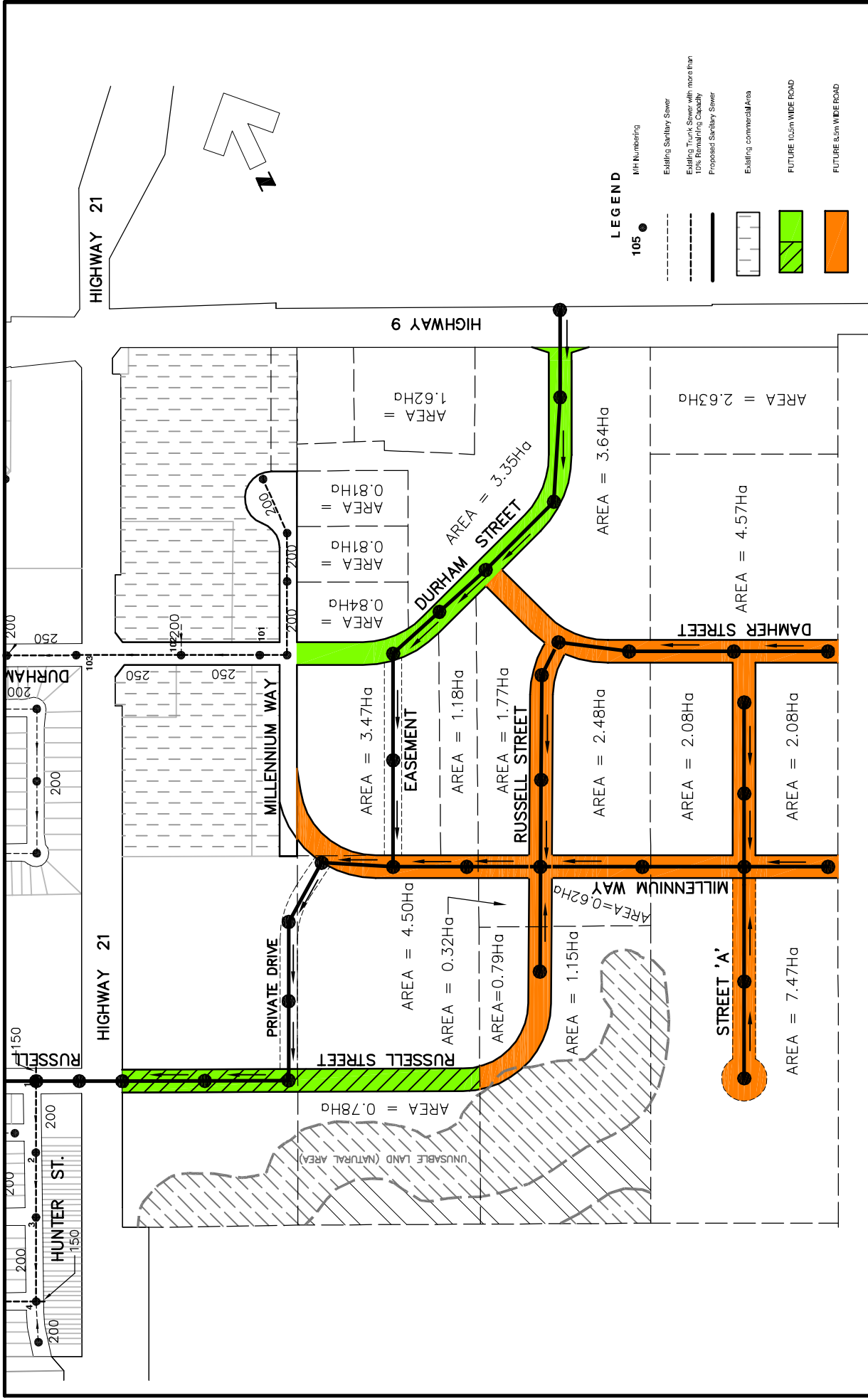
- A site plan agreement has been completed with DHC for the lands on Lot 1 at the north end of Millennium Way.
- The Canadian Tire lands on Lot 1 immediately north of the existing store are vacant.
- The developer of the carwash site on Lot 1, behind Canadian Tire would appear to be starting to proceed with his development.
- The Municipality has had preliminary discussions with respect to the proposed Bawa development.
- There have been discussions on the proposed Dalron site concerning the installation of commercial facilities.
- It is understood that a developer has purchased all of the lands north of the Durham Street extension and north of Damher Street.
- There has been a desire from some of the developers to have their sanitary sewer discharge to the existing Durham Street sewer.

4.0 SERVICING AND ROADS PATTERN

The County of Bruce Planning Department has completed a recommended pattern for development and installation of new roads through the development area. This road pattern, as slightly modified by BMROSS is shown on the attached sketch. It is anticipated these roads will be constructed as development progresses. It is also anticipated by the Municipality that the remaining development land should be assessed a share of the cost of the construction of the Russell Street trunk sewer together with a share of the cost of the various development roads.

Figure 1 shows that road pattern.

A review of anticipated ownership of the properties has been completed based upon a sketch completed by Ron Dore O.L.S. This is summarized below in Table 1.



	Municipality of Kincardine Business Park Development Area Full Development Roads and Sanitary Sewer	
	DATE April 28, 2008	SCALE N.T.S.
PROJECT No. 08055	FIGURE 1	

Table 1

Parcel/Owner	Approx. Developable Area (ha.)	Percent of Total
Former Quinn lands	1.62	4.15%
Part 1 (Bawa)	0.81	2.07%
Part 2	0.81	2.07%
Part 3	0.84	2.15%
Part 8	3.64	9.32%
Part 9	3.35	8.58%
Part 4, 6 (Dalron)	4.65	11.91%
Part 5 (21Russ)	1.94	4.97%
Part 7	5.19	13.29%
Lot 4	16.2	41.49%
Total	39.05	100%

The 21 Russ lands on lot 2 are assumed to have similar responsibilities with respect to servicing as those lands on lot 1 and the cost of services across their property and the cost of the Russell Street extension to the rear of lot 2 has been excluded. That area is excluded from the chart above.

5.0 PRELIMINARY ESTIMATED COSTS

Preliminary estimated costs of the road construction have been presented based upon recent tenders of similar works. All costs include allowances for local sanitary collection, water distribution, storm water collection, road construction complete with curb and gutter, sidewalk, engineering, contingencies and GST. No allowance for communal Storm Water Management or the construction of a water booster pumping station is included.

For the purposes of this initial proposal, two types of road have been considered and the estimated cost per metre of construction is as follows:

- Durham Street extension and Russell Street extension to rear of lot 2 (green on attached sketch) -- \$2,250
- Remaining service roads. -- \$2,000

The trunk Sanitary Sewer from Hunter through the 21 Russ lands is the responsibility of that developer. The sewer from Scott to Hunter has a preliminary estimated cost of \$290,000. It is proposed that this cost should be shared by all of the development lands.

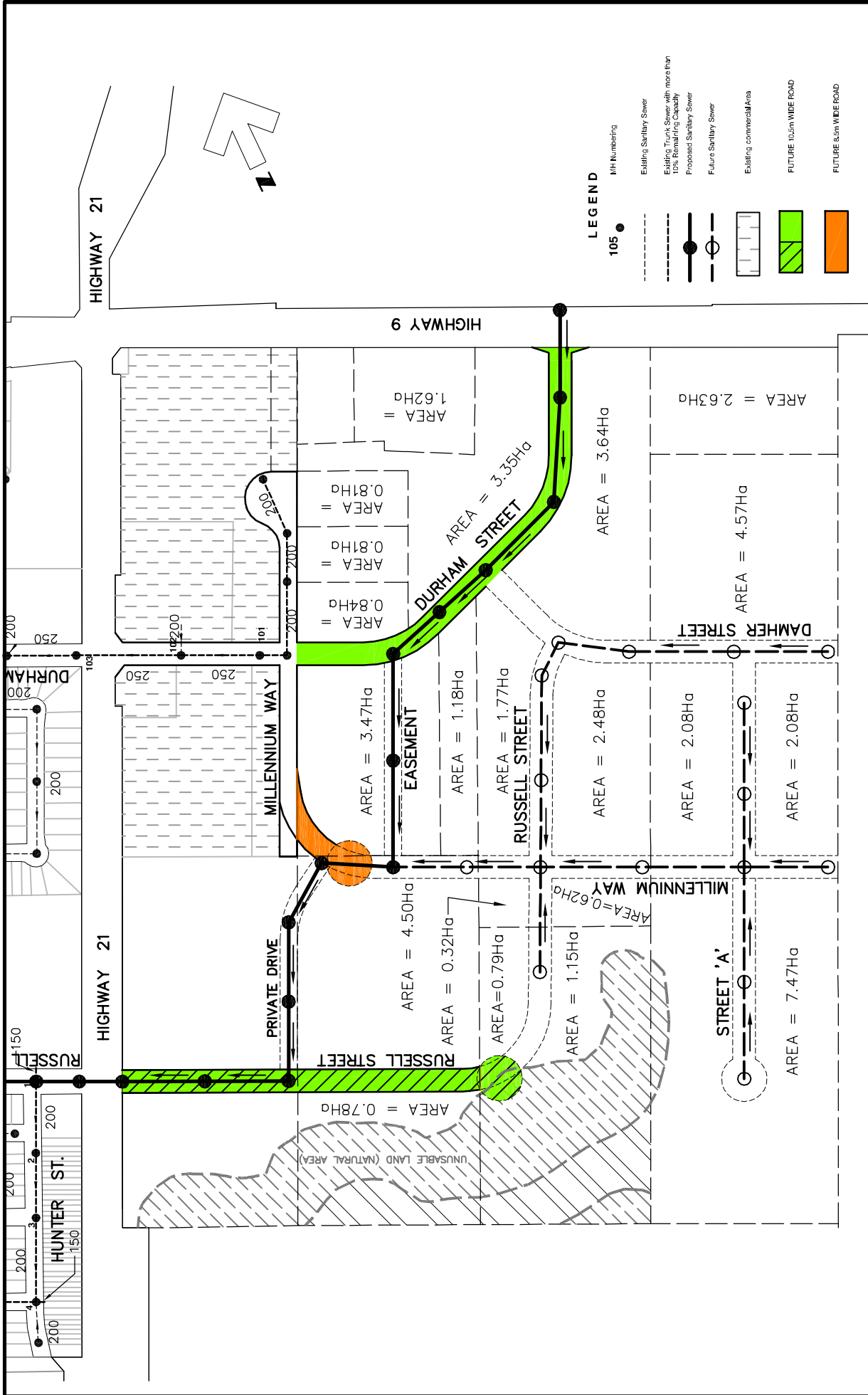
It is anticipated by the municipality that the completion of the development of the business park will take a number of years. It is assumed that initially development may be limited to the lands on the Durham St. extension and the 21 Russ lands.

The extent of this assumed interim development is shown on Figure 2. Based upon the preliminary submission for the Dalron development, a sewer easement through their property is proposed.

For that extent of development to proceed, the Durham Street extension and portions of the trunk sewer need to be constructed as shown on Figure 2. Preliminary cost sharing proposals for that extent of development are attached as Table 2.

6.0 SUMMARY

This document provides the basis for discussion for the sharing of costs for the development of the balance of the business park. The municipality and developers must reach some consensus as to how the services on the balance of the Business Park will be funded.



Municipality of Kincardine

Business Park Development Area

Interim Development Roads and Sanitary Sewer

DATE
April 25, 2008

SCALE
N.T.S.

PROJECT No.
08055

FIGURE
2

Table 2

Parcel/Owner	Approx. Developable for Trunk Sewer Area (ha.)	Cost Sharing Trunk Sewer per ha.	Approx. Developable for Roads Area (ha.)	Percent of Total	Cost Sharing Roads	Total
Former Quinn lands	1.62	12,000	1.62	10.31%	150,600	162,602
Part 1 (Bawa)	0.81	6,000	0.81	5.15%	75,200	81,201
Part 2	0.81	6,000	0.81	5.15%	75,200	81,201
Part 3	0.84	6,200	0.84	5.34%	78,000	84,201
Part 8	3.64	27,000	3.64	23.16%	338,400	365,404
Part 9	3.35	24,900	3.35	21.31%	311,300	336,204
						1,110,812
Part 4, 6 (Dalron)	4.65	34,500	4.65	29.58%	432,200	466,705
Part 5 (21Russ)	1.94	14,400			-	14,400
Part 7	5.19	38,500			-	38,500
Lot 4	16.2	120,300			-	120,300
Total	39.05	289,800	15.72	100%	1,460,900	1,750,717

Trunk Sewer Costs to be shared: \$ 290,000.00 \$ 7,426.38 /ha.

Road and sewer servicing costs to be shared:

Sewer Extension	\$ 95,000.00
Road Costs	\$ 1,366,000.00
Total	\$ 1,461,000.00

Length of 10.5 m. wide road	536	2,250	1,206,000
Length of 8.5 m wide road	80	2,000	160,000
Total	616		1,366,000